

Supplementary Material

Continue from Eq. 90. Integrating by parts for (ρu) and (ρv) results in:

$$\begin{aligned} \int_0^h \frac{\partial \rho}{\partial t} dz + h \left[\frac{\partial(\rho U)_2}{\partial x} + \frac{\partial(\rho V)_2}{\partial y} \right] - \frac{\partial}{\partial x} \int_0^h z \left(\rho \frac{\partial u}{\partial z} + u \frac{\partial \rho}{\partial z} \right) dz \\ - \frac{\partial}{\partial y} \int_0^h z \left(\rho \frac{\partial v}{\partial z} + v \frac{\partial \rho}{\partial z} \right) dz + (\rho w)_0^h = 0 \end{aligned} \quad (S1)$$

The expressions of velocity gradients and velocities are:

$$\begin{aligned} \frac{\partial u}{\partial z} = \left(\frac{z}{\eta_{EM}(\gamma, T)} - \frac{f_5(h)}{\eta_{EM}(\gamma, T) f_{10}(h)} \right) \frac{\partial p}{\partial x} \\ + \frac{U_2 - U_1 - f_6(h) - f_8(h)}{\eta_{EM}(\gamma, T) f_{10}(h)} + f_1(z) + f_3(z) \end{aligned} \quad (S2)$$

$$\begin{aligned} \frac{\partial v}{\partial z} = \left(\frac{z}{\eta_{EM}(\gamma, T)} - \frac{f_5(h)}{\eta_{EM}(\gamma, T) f_{10}(h)} \right) \frac{\partial p}{\partial y} \\ + \frac{V_2 - V_1 - f_7(h) - f_9(h)}{\eta_{EM}(\gamma, T) f_{10}(h)} + f_2(z) + f_4(z) \end{aligned} \quad (S3)$$

$$\begin{aligned} u = f_{11}(z) \frac{\partial p}{\partial x} + \frac{U_2 - U_1 - f_6(h) - f_8(h)}{f_{10}(h)} f_{10}(z) \\ + f_6(z) + f_8(z) + U_1 \end{aligned} \quad (S4)$$

$$\begin{aligned} v = f_{11}(z) \frac{\partial p}{\partial y} + \frac{V_2 - V_1 - f_7(h) - f_9(h)}{f_{10}(h)} f_{10}(z) \\ + f_7(z) + f_9(z) + V_1 \end{aligned} \quad (S5)$$

Substitute Eq. (S2)~(S5) into Eq. (S1), one could get:

$$\begin{aligned} - \frac{\partial}{\partial x} \int_0^h z \left(\rho \frac{\partial u}{\partial z} + u \frac{\partial \rho}{\partial z} \right) dz \\ = - \frac{\partial}{\partial x} \left(\frac{\partial p}{\partial x} \int_0^h z \rho \left(\frac{z}{\eta_{EM}(\gamma, T)} - \frac{f_5(h)}{\eta_{EM}(\gamma, T) f_{10}(h)} \right) dz \right. \\ \left. + \frac{U_2 - U_1 - f_6(h) - f_8(h)}{f_{10}(h)} \int_0^h \frac{z \rho}{\eta_{EM}(\gamma, T)} dz + \int_0^h z \rho f_1(z) dz + \int_0^h z \rho f_3(z) dz \right) \\ - \frac{\partial}{\partial x} \left(\frac{\partial p}{\partial x} \int_0^h z \frac{\partial \rho}{\partial z} f_{11}(z) dz + \frac{U_2 - U_1 - f_6(h) - f_8(h)}{f_{10}(h)} \int_0^h z \frac{\partial \rho}{\partial z} f_{10}(z) dz \right. \\ \left. + \int_0^h z \frac{\partial \rho}{\partial z} f_6(z) dz + \int_0^h z \frac{\partial \rho}{\partial z} f_8(z) dz + U_1 \int_0^h z \frac{\partial \rho}{\partial z} dz \right) \end{aligned} \quad (S6)$$

$$\begin{aligned}
& -\frac{\partial}{\partial y} \int_0^h z \left(\rho \frac{\partial v}{\partial z} + v \frac{\partial \rho}{\partial z} \right) dz \\
& = -\frac{\partial}{\partial y} \left(\frac{\partial p}{\partial y} \int_0^h z \rho \left(\frac{z}{\eta_{EM}(\gamma, T)} - \frac{f_5(h)}{\eta_{EM}(\gamma, T) f_{10}(h)} \right) dz \right. \\
& \quad \left. + \frac{V_2 - V_1 - f_7(h) - f_9(h)}{f_{10}(h)} \int_0^h \frac{z \rho}{\eta_{EM}(\gamma, T)} dz + \int_0^h z \rho f_2(z) dz + \int_0^h z \rho f_4(z) dz \right) \\
& \quad - \frac{\partial}{\partial y} \left(\frac{\partial p}{\partial y} \int_0^h z \frac{\partial \rho}{\partial z} f_{11}(z) dz + \frac{V_2 - V_1 - f_7(h) - f_9(h)}{f_{10}(h)} \int_0^h z \frac{\partial \rho}{\partial z} f_{10}(z) dz \right. \\
& \quad \left. + \int_0^h z \frac{\partial \rho}{\partial z} f_7(z) dz + \int_0^h z \frac{\partial \rho}{\partial z} f_9(z) dz + V_1 \int_0^h z \frac{\partial \rho}{\partial z} dz \right)
\end{aligned} \tag{S7}$$

Introducing F and G functions (same as Eq. 92), then Eqs. (S6) and (S7) can be written as:

$$\begin{aligned}
& -\frac{\partial}{\partial x} \int_0^h z \left(\rho \frac{\partial u}{\partial z} + u \frac{\partial \rho}{\partial z} \right) dz \\
& = -\frac{\partial}{\partial x} \left([F_2 + G_1] \frac{\partial p}{\partial x} \right) - \frac{\partial}{\partial x} \left(\frac{(U_2 - U_1)(F_3 + G_2)}{F_0} + U_1 G_3 \right)
\end{aligned} \tag{S8}$$

$$\begin{aligned}
& -\frac{\partial}{\partial x} (F_4 + F_5) - \frac{\partial}{\partial x} (G_4 + G_5) \\
& -\frac{\partial}{\partial y} \int_0^h z \left(\rho \frac{\partial v}{\partial z} + v \frac{\partial \rho}{\partial z} \right) dz \\
& = -\frac{\partial}{\partial y} \left([F_2 + G_1] \frac{\partial p}{\partial y} \right) - \frac{\partial}{\partial y} \left(\frac{(V_2 - V_1)(F_3 + G_2)}{F_0} + V_1 G_3 \right) \\
& -\frac{\partial}{\partial y} (F_6 + F_7) - \frac{\partial}{\partial y} (G_6 + G_7)
\end{aligned} \tag{S9}$$

Substitute Eq. (S8) and Eq. (S9) into Eq. (S1) results in generalized MEMT-field Reynolds equation, Eq. 91, which is repeated here:

$$\begin{aligned}
& \frac{\partial}{\partial x} \left([F_2 + G_1] \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left([F_2 + G_1] \frac{\partial p}{\partial y} \right) = h \left[\frac{\partial(\rho U)_2}{\partial x} + \frac{\partial(\rho V)_2}{\partial y} \right] \\
& -\frac{\partial}{\partial x} \left(\frac{(U_2 - U_1)(F_3 + G_2)}{F_0} + U_1 G_3 \right) - \frac{\partial}{\partial y} \left(\frac{(V_2 - V_1)(F_3 + G_2)}{F_0} + V_1 G_3 \right) \\
& -\frac{\partial}{\partial x} (F_4 + G_4) - \frac{\partial}{\partial y} (F_6 + G_6) - \frac{\partial}{\partial x} (F_5 + G_5) - \frac{\partial}{\partial y} (F_7 + G_7) \\
& + \int_0^h \frac{\partial \rho}{\partial t} dz + (\rho W)_2 - (\rho W)_1
\end{aligned} \tag{S10}$$

In most engineering applications, the boundary surface velocities in the x and y directions are constants, which leads to:

$$\frac{\partial(U_2 - U_1)}{\partial x} = \frac{\partial(V_2 - V_1)}{\partial y} = 0 \quad (\text{S11})$$

In the z direction, when setting $W_1 = 0$, the following is accepted:

$$\frac{\partial h}{\partial t} \approx W_2 - W_1 - U_2 \frac{\partial h}{\partial x} - V_2 \frac{\partial h}{\partial y} \quad (\text{S12})$$

As a result, Eq. (S10) can be written as:

$$\begin{aligned} & \frac{\partial}{\partial x} \left([F_2 + G_1] \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left([F_2 + G_1] \frac{\partial p}{\partial y} \right) = U_2 \frac{\partial(\rho h)}{\partial x} + V_2 \frac{\partial(\rho h)}{\partial y} \\ & - (U_2 - U_1) \frac{\partial}{\partial x} \left(\frac{F_3 + G_2}{F_0} \right) - U_1 \frac{\partial G_3}{\partial x} - (V_2 - V_1) \frac{\partial}{\partial y} \left(\frac{F_3 + G_2}{F_0} \right) - V_1 \frac{\partial G_3}{\partial y} \\ & - \frac{\partial}{\partial x} (F_4 + G_4) - \frac{\partial}{\partial y} (F_6 + G_6) - \frac{\partial}{\partial x} (F_5 + G_5) - \frac{\partial}{\partial y} (F_7 + G_7) \\ & + \int_0^h \frac{\partial \rho}{\partial t} dz + \rho \frac{\partial h}{\partial t} \end{aligned} \quad (\text{S13})$$

For liquid lubricant, density variation across the film can be neglected, i.e. $\partial \rho / \partial z = 0$. Thus, all G functions are zero, hence generalized MEMT-field Reynolds equation can be reduced to Eq. 93, which is repeated here:

$$\begin{aligned} & \frac{\partial}{\partial x} \left(F_2 \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(F_2 \frac{\partial p}{\partial y} \right) = U_2 \frac{\partial(\rho h)}{\partial x} + V_2 \frac{\partial(\rho h)}{\partial y} \\ & - (U_2 - U_1) \frac{\partial}{\partial x} \left(\frac{F_3}{F_0} \right) - (V_2 - V_1) \frac{\partial}{\partial y} \left(\frac{F_3}{F_0} \right) \\ & - \frac{\partial}{\partial x} F_4 - \frac{\partial}{\partial y} F_6 - \frac{\partial}{\partial x} F_5 - \frac{\partial}{\partial y} F_7 + \frac{\partial(\rho h)}{\partial t} \end{aligned} \quad (\text{S14})$$