



WHATS-3: An Improved Flow-Through Multi-bottle Fluid Sampler for Deep-Sea Geofluid Research

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Miyazaki J, Makabe A, Matsui Y, Ebina N, Tsutsumi S, Ishibashi J, Chen C, Kaneko S, Takai K and Kawagucci S (2017) WHATS-3: An Improved Flow-Through Multi-bottle Fluid Sampler for Deep-Sea Geofluid Research. Front. Earth Sci. 5:45. doi: 10.3389/feart.2017.00045 Deep-sea geofluid systems, such as hydrothermal vents and cold seeps, are key to understanding subseafloor environments of Earth. Fluid chemistry, especially, provides crucial information toward elucidating the physical, chemical, and biological processes that occur in these ecosystems. To accurately assess fluid and gas properties of deep-sea geofluids, well-designed pressure-tight fluid samplers are indispensable and as such they are important assets of deep-sea geofluid research. Here, the development of a new flow-through, pressure-tight fluid sampler capable of four independent sampling events (two subsamples for liquid and gas analyses from each) is reported. This new sampler, named WHATS-3, is a new addition to the WHATS-series samplers and a major upgrade from the previous WHATS-2 sampler with improvements in sample number, valve operational time, physical robustness, and ease of maintenance. Routine laboratory-based pressure tests proved that it is suitable for operation up to 35 MPa pressure. Successful field tests of the new sampler were also carried out in five hydrothermal fields, two in Indian Ocean, and three in Okinawa Trough (max. depth 3,300 m). Relations of Mg and major ion species demonstrated bimodal mixing trends between a hydrothermal fluid and seawater, confirming the high quality of fluids sampled. The newly developed WHATS-3 sampler is well-balanced in sampling capability, field usability, and maintenance feasibility, and can serve as one of the best geofluid samplers available at present to conduct efficient research of deep-sea geofluid systems.

Keywords: fluid sampler, gas-tight sampler, deep-sea research, hydrothermal fluid, fluid chemistry

INTRODUCTION

The extremely important role played by the subseafloor fluid advection system in Earth's element cycle and ecosystem development has been widely recognized (e.g., Elderfield and Schultz, 1996; German and Seyfried, 2014). The total water mass below the seafloor is estimated to constitute $\sim 2\%$ of the entire seawater mass (Johnson et al., 2006; Mottl et al., 2007). Subseafloor fluid advection and

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the associated fluid-rock interaction cause elemental flux between the lithosphere and the ocean, regulating the chemical composition of the ocean. In addition, since some of the subseafloor-derived reducing species are available for chemolithoautorophic metabolism, subseafloor fluid advection, and mixing with the overlying seawater plays an important role in supporting the unique (sub)seafloor biosphere.

Geofluids discharging from sources such as hydrothermal vents and cold seeps serve as windows for looking into this dynamic system developing below the seafloor, not directly reachable without enormous efforts through scientific drilling (e.g., Fisher et al., 2003; Yanagawa et al., 2017). Properties of discharged geofluids, particularly the fluid chemistry, can be interpreted as a representation of processes occurring within the subseafloor environment across tectonic scale (e.g., magmatism and crustal recycling; Sakai et al., 1990; Lilley et al., 2003; Mottl et al., 2004), regional hydrogeological scale (e.g., hydrothermal fluid circulation; Fisher et al., 2003; Pester et al., 2011; Kawagucci et al., 2011) and field scale (e.g., chemosynthetic ecosystem; Le Bris et al., 2006; Wankel et al., 2011). Deep-diving operations utilizing submersibles and Remotely Operated Vehicles (ROVs) allow direct investigation of the geofluids by accessing the deep seafloor. In addition to in situ chemical analyses, shown to be beneficial especially for obtaining high-resolution spatial distributions of chemically and biologically unstable compounds in the seawater column (Le Bris et al., 2000; Okamura et al., 2001, 2015; Wankel et al., 2010), fluid sampling followed by on-board/on-shore chemical analyses has been and remains an important asset for revealing compositional and isotopic characteristics of the fluid in its entirety.

Obtaining high-quality fluid sample is, however, difficult—a key hindrance in fluid chemistry research. The collection of vent fluids must be completed without mixing with the surrounding seawater, and the preservation of chemical species must be ensured during recovery of the sampler onto the research vessel. The latter is a substantial issue as a few hours generally pass between collection and recovery; both pressure and temperature condition of the laboratory is also usually quite different from that of the sampled fluid. Limited opportunities for dive operation and limited time on the seafloor during a dive are also obstacles in studying fluid chemistry.

A number of deep-sea geofluid samplers have been developed so far to overcome these hindrances (**Table 1**). It is vital that the sampler actively draws the fluid concerned, because contamination from the surrounding seawater cannot be reliably avoided with passive samplers such as Niskin bottles (e.g., Connelly et al., 2012). The actively fluid drawing geofluid samplers developed so far can be further classified by the sample container style (semi-closed and flow-through) and their gas tightness (gas-tight and non-gas-tight; **Table 1**). A semi-closed sampler is defined as a fluid sampler where the sample container is open at only one end. Such semi-closed samplers have a drawback, the fluid pre-filled in the tubes and containers before the dive commences (seawater or pure water) is unavoidably incorporated partly into the collected geofluid. Although, this contamination can be calibrated based on analytical data with appropriate assumptions, some bias at the calibration stage is unavoidable. This issue can be overcome by using a flowthrough type sampler, in which the fluid container is purged and rinsed by the *in situ* geofluid prior to formal sampling. One risk concerning high-temperature hydrothermal fluid is that metals and sulfide may precipitate in flow-through tubes prior to reaching the sampling container, resulting in the underestimation of their concentrations. Gas tightness of the sampler is necessary for the accurate assessment of chemical conditions concerning subseafloor fluid-rock interactions and magmatism, gas flux from solid Earth to Ocean, and potential functioning of chemosynthetic ecosystems in consuming and producing gas species such as H₂ and CH₄ (Von Damm and Lilley, 2004; Proskurowski et al., 2008; Nakamura and Takai, 2014).

"Major" and "Bag" samplers are two widely-utilized semiclosed fluid samplers. The "Major" sampler, developed by Woods Hole Oceanographic Institution (WHOI; Von Damm et al., 1985), is essentially a titanium syringe consisting of a \sim 750 mL fluid chamber with an internal piston to draw the fluid from the inlet nozzle. The "Bag" sampler collects geofluids via an impeller pump (or a peristaltic pump) into a flexible-volume plastic container (~20 L), capable of quantifying elements and molecules present only in low concentration and also used to collect suspended particles including microbes and viruses (Huber et al., 2002; AEM; Lang et al., 2006; Yoshida-Takashima et al., 2012). The "ORI" sampler is another semi-closed sampler with the inlet nozzle connected to a manifold for multiple sampling events, each into a ~750 mL titanium or acrylic glass container (Tsunogai et al., 1994; Ishibashi et al., 1995). The recently developed "ANEMONE" sampler (Okamura et al., 2014) is a further flow-through type sampler with 40 mL-volume plastic tubes as fluid containers and is capable of collecting 128 samples during each dive. All the samplers mentioned above are, nevertheless, not gas-tight and therefore do not prevent dissolved gas components escaping from the collected fluid during recovery from the deep-sea, due to decreasing pressure and thus gas decompression.

The "vacuum" sampler is a simple and comparatively inexpensive sampler consisting of a stainless-steel (or titanium) container and a manually operated three-way valve (Sedwick et al., 1994; Kawagucci et al., 2013a). The sample chamber is evacuated prior to a dive (i.e., vacuum is maintained within) and draws the geofluid simply by opening the valve. The "gastight" (GT) sampler has a titanium cylinder body equipped with a gas-tight titanium valve actuated by hydraulic power supplied from the vehicle (Edmond et al., 1992). The "isobaric gas-tight" (IGT) sampler (Seewald et al., 2001) consists of an inlet nozzle, an electrically or hydraulically manipulated needle valve (Wu et al., 2011), and a titanium cylinder. The cylinder includes a \sim 150 mL sample container as well as the mechanics for maintaining the internal pressure of the collected fluid sample up to 450 bar prior to subsampling on-board. The IGT sampler is, to date, the only sampler capable of subsampling for both gas and liquid analyses from a single sample chamber. However, these gas-tight samplers described above are all semi-closed and without a flow-through system.

Name	Gas-tight	Fluid path	Numbers of chambers (series × parallel)	Volume (mL)	Drawing force	References
WHATS 3	Yes	Flow through	8 (2 × 4)	20 or 50	Peristalic pump (pull)	This study
WHATS 2	Yes	Flow through	4 (1 × 4)	150	Peristalic pump (pull)	Saegusa et al., 2006
Isobaric	Yes	Semi-closed	1	150	Pulling piston by internal low pressure	Seewald et al., 2001
Vacuum (GT)	Yes	Semi-closed	1	150	Internal low pressure	Edmond et al., 1992; Sedwick et al., 1994
Major	No	Semi-closed	1	750	Pulling piston by hydraulic ram	Von Damm et al., 1985
ORI	No	Semi-closed	6 (1 × 6)	750	Pulling piston by DC motor	Tsunogai et al., 1994
Bag	No	Semi-closed	1	(~20,000)	Peristalic or impeller pump (push)	Huber et al., 2002; Lang et al. 2006
ANEMONE	No	Flow through	128 (1 × 128)	40	Diaphragm pump (push)	Okamura et al., 2015
Niskin	No	Flow through	1	1,000-12,000	(passive)	

TABLE 1 | Comparison of deep-sea geofluid samplers.

The WHATS-2 sampler (Saegusa et al., 2006), modified from the first-generation WHATS sampler (Tsunogai et al., 2003), is a flow-through, gas-tight fluid sampler (Table 1) capable of multiple sampling events under hydrostatic pressure up to 40 MPa. The WHATS-2 consists of four 150 mL stainless-steel containers, a motor-driven arm to manipulate the valves on the containers, a peristaltic pump, a control unit, and a flexible tube manifold connected by a titanium inlet. The mechanism of using a single electronic motor-driven arm to manipulate all eight valves reduces efforts required in both routine maintenance and operation. However, the WHATS-2 still had several shortcomings in terms of sample numbers and physical robustness of the system. As subsampling for gas analysis consumes an entire fluid container, two of the four containers are required at each sampling location in order to reveal both liquid and gas compositions of the geofluid concerned. As a result, the WHATS-2 can practically only obtain geofluid sample from two locations during one dive. Moreover, this shortcoming brings about two further unavoidable issues. One is that two temporally different fluid samples from each sampling point may not be entirely homogeneous, which is a potential source of bias in the interpretation of fluid chemistry. The other is that relatively longer sampling time is required at each fluid discharge location in order to fill two containers. In terms of physical robustness, the complicated mechanical geometry required for valve operation in the WHATS-2 is rather troublesome. As outlined above, the WHATS-2 is a superior system, but these issues still remain to be solved in order to maximize efficiency during limited deep-sea sampling opportunities.

We here report the development of a new version of the WHATS sampler, named WHATS-3 (Figure 1). The most notable improvement from WHATS-2 is the increased number of samples, by development of a system consisting of four sampling bottles with two separate chambers in each bottle. This enables collection of two gas-tight subsamples simultaneously from each sampling location, and from four different locations during one dive. In addition, there are several improvements, including (1) reduction of area required for equipment on vehicles, (2) reduction of valve operation time (from a few minutes to a few seconds), (3) improved physical robustness by modifying geometry involved in valve-manipulation, and (4) adoption of a new cylindrical outer frame to effortlessly prepare and maintain the sampler.

INSTRUMENT DESIGN

Overview of the System

The WHATS-3 system consists of five components, including (1) a fluid inlet (so-called "pistol"), (2) four sets of dual-chambered sampling bottles, (3) a valve-manipulating system (Figure 1B), (4) an impeller pump unit, and (5) an electric control unit to operate the valve-manipulating digits and the impeller pump. The main body (including the sampling bottles and the manipulating system) is a titanium frame, semi-cylindrical in shape, with a dimension (H \times W \times D) of 700 \times 375 \times 395 (mm) (Figure 1A). A rectangular face 700×375 (mm) in size is required for tight attachment onto submersible vehicles; WHATS-2 had a larger attachment face of 595 \times 560 (mm) (Saegusa et al., 2006). So far, the WHATS-3 has been attached on the payload space behind the right manipulator of the ROV Hyper-Dolphin, the rear payload space of ROV Kaiko (vehicle Mk-IV), and between the two manipulators of the Human Occupied Vehicle (HOV) Shinkai 6500 (Figure 2). Unlike most other fluid samplers including the WHATS-2, the pistol, the impeller pump unit, and the control unit are isolated from the main body. This is beneficial as it reduces the space required in the main payload space, usually in the front of submersible vehicles.

The pistol consists of a T-shaped titanium tube (O.D. 10 mm, I.D. 9 mm) and a thermometer (Pt 100 Ω) blanketed with a steel shell. The thermometer, inserted from right side of the T tube through to the fluid inlet on the left and sealed with double silicon O-rings at the insertion end, is responsible for real-time monitoring of the fluid temperature during sampling, with a precision of $\pm 1^{\circ}$ C. Incoming fluid from the inlet on the left side flows to bottom end of the T tube, completely flushing any possible residues at the right side. For sampling of diffusive fluids, a funnel (>300 mL) is mounted on the inlet end as a reservoir of the geofluid to avoid mixing and contamination by ambient seawater. The impeller pump unit contains, in addition

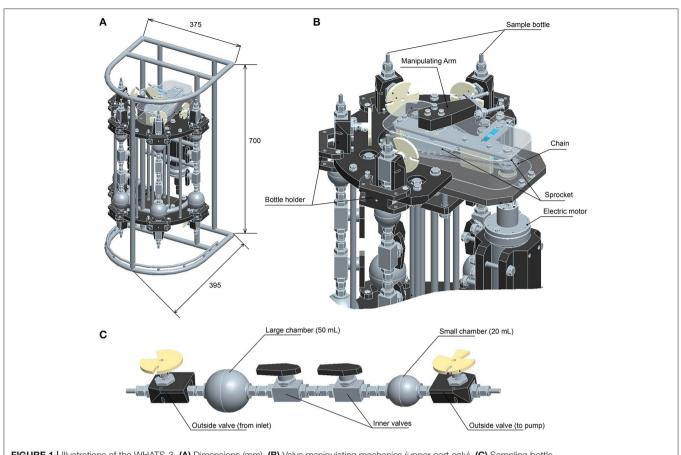


FIGURE 1 | Illustrations of the WHATS-3. (A) Dimensions (mm). (B) Valve manipulating mechanics (upper part only). (C) Sampling bottle.

to the pump, an electronic motor contained within a pressureresistance chamber sealed against a maximum pressure of 40 MPa. The pumping speed can be adjusted at three steps: \sim 400, \sim 200, and \sim 100 mL/min. In general, a slower pumping speed better avoids contamination of ambient seawater.

Fluid flow pathways of the pistol, the sampling bottles, and the impeller pump unit are connected in this order using polypropylene tubes (PP-PS-M, AS ONE, Osaka, Japan) and Tshaped connections (PP-PT-M, AS ONE, Osaka, Japan). These can also be made with Teflon, if necessary. The length of the plastic tube depends on attachment locations of each component, but is typically \sim 5 m. The inner volume of a 5 mlong tube is \sim 100 mL. The impeller pump unit is located at the most downstream part of the fluid pathway in order to avoid contamination from potential exfoliation of the tube in the pump.

Sampling Bottle

Each sampling bottle consists of two ball valves (SS-4SKPS4, Swagelok, Ohio, US) mounted on the two ends of the bottle, two spherical fluid chambers, and two ball valves (SS-4SKPS4) located between the chambers in a series (see Figure 1C). The SS-4SKPS4 valve has a gas-tight capacity for pressure difference up to 41.3 MPa (guaranteed by Swagelok), the same valve has been used without problem in the former WHATS-series samplers. The bottle is of a stainless-steel construct, the surface is treated with a SilicoNert coating (Silcotek Corporation, Bellefonte,

Pennsylvania, USA) to avoid corrosion and metal contamination (particularly Fe, Cr, and Ni). Blank of H2 from the stainless-steel bottle has been examined and confirmed to be as low as 0.03 μM (Kawagucci et al., 2010). As in the WHATS-2, specific gingkoleaf-shaped discs are mounted as handles of the outside valves (see Saegusa et al., 2006 for a detailed description; Figure 1C). The two spherical fluid chambers differ in volumes (20 and 50 mL) but they may be attached in either order. When sampling, the two fluid chambers are connected and function as a single fluid container. When the WHATS-3 is recovered on-board, the two chambers are manually isolated using inner valves. This dualchamber system allows separation of a single fluid sample into two discrete subsamples, each to be used for chemical analyses of gas or liquid.

Construction of Electric Motor-Driven Valve Manipulation

The construction of the valve manipulation system is newly designed for rapid and smooth operation, as well as increasing the robustness of the system (Figure 1B). As a common feature of the WHATS-series samplers, the handles mounted outside ball valves of the sampling bottles are operated by valve-manipulating digits. Specifically, the digits move horizontally at a right angle against the valves, rotating the valve handles for opening and/or closing them (see Saegusa et al., 2006 for detailed description).



FIGURE 2 | Photograph showing the WHATS-3 being installed directly below the center window of the HOV *Shinkai* 6500.

In the WHATS-2, the four sampling bottles were aligned on a plane, and the narrow and elongate valve manipulating arm (with one and two digits on each end) was mounted on a small block moving linearly by means of a rotating screw pole powered by an electronic motor. The delicate shape of the arm was vulnerable to external forces. Indeed, it was sometimes bent due to accidents during routine maintenance on-board, resulting in errors manipulating the valves in situ. The force transformation to linear movement was time-consuming with more than 1 min being required to manipulate the valves of a bottle. In addition, the sampling bottles were attached on the main body using stainless-steel tubes that also functioned as a fluid path. These tubes were sometimes bent or broken due to the sheer weight of the bottles when they were attached or detached. To resolve these issues, the WHATS-3 adopted a new semi-circular alignment with the sampling bottles set in 60° intervals (see Figure 1B). The valve-manipulating digits are mounted directly on blocks and rotate on a fixed axis via a roller-chain powered by an electronic motor. The sampling bottles are held on the built-in ports of the main frame, independent from tubes that make up the fluid path. The sturdy construction and the simplified geometry of valve manipulation in the WHATS-3 reduce potentials of inadvertent failures during operation, and the time required for manipulating the valves of a bottle is reduced to just a few seconds.

Construction of the Electronics

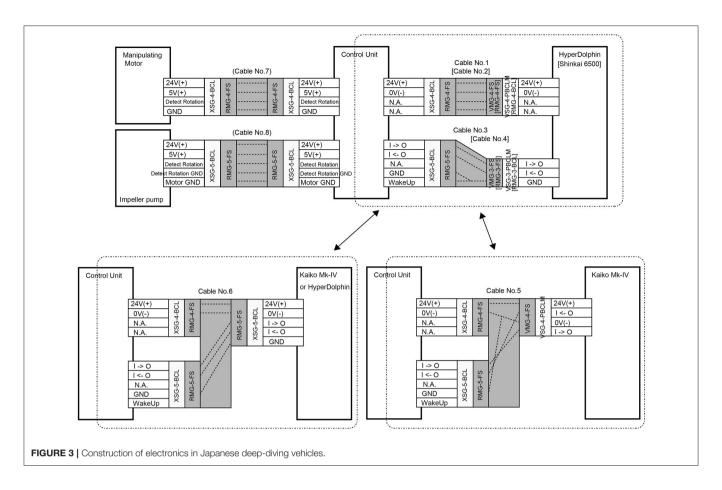
A power supply of DC24V is independently required for: (1) main electric system for valve manipulation, fluid pumping, and signal communication with the submersible vehicle (**Figure 3**) and (2) the thermometer. Cables and connectors used are made by SEACON (El Cajon, CA, US) and/or IMPULSE (San Diego, CA, US). The operating software for the main system and the thermometer was developed for Microsoft Windows operating systems and has been confirmed to function normally and successfully on Windows XP and Windows 7. The main functions of the software are: (1) to switch pumping ON/OFF, (2) to change the speed of pumping, (3) to operate the manipulator for opening/closing of the valves, and (4) to display and record the fluid temperature.

ON-SHORE TESTS

Pressure Resistance

The WHATS-3 system is designed to resist a pressure of 35 MPa, corresponding to 3,500 m water depth, with a safety coefficient of 1.7. It has been successfully operated under 33 MPa in deepsea field testing. The 35 MPa resistance covers \sim 50% of the global seafloor, including most of Mid-Ocean Ridges, Arc, and Back Arc where hydrothermal activity is expected (German and Seyfried, 2014; Beaulieu et al., 2015; Ishibashi et al., 2015). The three sealed chambers (the pump unit, valve-manipulating motor, and electronic unit) are designed to resist an external pressure of 40 MPa while the sampling bottles withstand 30 MPa. The actual external high-pressure resistance of the whole system was examined in a laboratory pressure bath and confirmed to match the designed levels. Successful operations of the valves and manipulator were confirmed under 32 MPa external pressure in the laboratory.

For the sampling bottles, in reality, resistance against external high pressure is not important because all sampling bottles are open to ambient seawater during the descent to the seafloor (see Saegusa et al., 2006 for detailed description). Rather, resistance against internal high pressure post-sampling is more crucial for successful gas-tight fluid sampling because the pressure sealed sampling bottles, containing sampled fluids with dissolved gases, must be recovered intact from the deep-sea. The actual internalhigh pressure resistance was examined by connecting a hydraulic pump (TP-500, Syn Corporation, Kyo-tanabe, Japan) and a digital pressure gage (VSMC series, VALCOM, Osaka, Japan) to the two ends of a sampling bottle. When pure water was filled at 40 MPa and stored for 22 h at room temperature, the sampling bottle did not show any visible leakage. Furthermore, when the sampling bottle was filled with pure water at 35 MPa and 2°C (mimicking the deep-sea environment), closed, and heated up to 20°C, as expected at the sea surface and during the recovery, the internal pressure increased to 38 MPa but there was again no visible leakage. These examinations demonstrate that the newly designed sampling bottle is suitable for use under deep-sea condition at a depth of 3,500 m.



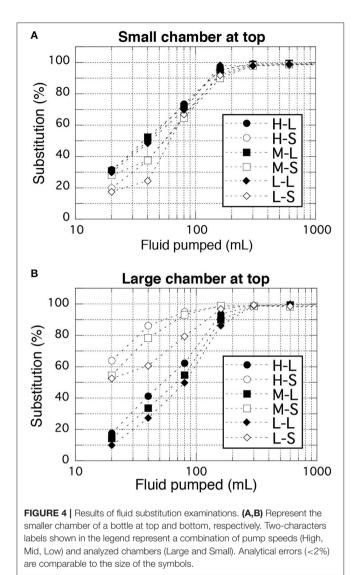
Fluid Substitution

Sufficient substitution of the pre-filled fluid in the bottle (usually pure water) with the target geofluid was examined because unlike the simple rod-shaped sampling bottles in the WHATS-2, the relatively complex dual spherical chamber design of the sampling bottles in the WHATS-3 may make smooth and complete substitution difficult. In the WHATS-series samplers, the sampling bottles are positioned vertically (Figure 1) while the more dense seawater is introduced from the bottom for efficient substitution. During testing, pure water and seawater were used as the pre-filled fluid and the target fluid, respectively (Figure 4). Chloride concentrations of the fluid in the bottle were determined by ion chromatography (IC) (Dionex ICS-2100, Thermo Fisher Scientific) after 2,500 times dilution, within analytical errors of 2%. Substitution, represented by relative Cl concentration against seawater, was analyzed in relation to the amount of fluid pumping. The analyses were conducted in all three pumping speeds and both possible attachment orders of the two spherical chambers (large-small chamber and vice versa). The examination results proved that >98% substitution was achieved with 300 mL pumping under all settings of the pumping speed and both chamber attachment orders (Figure 4). Here, more than 98% substitution practically indicates complete substitution, when the 2% analytical errors is taken into consideration. In actual field usage, more than 600 mL of fluid is generally pumped to provide extra assurance of a complete substitution. The required time for pumping 600 mL was only 1.5, 3, and 6 min at high, mid, and slow speed pumping, respectively.

ONBOARD APPLICATION

Procedure for Sampling at the Seafloor

At the beginning of a cruise, the main body, the pump unit, and the control unit of the WHATS-3 are mounted on the submersible vehicle to confirm electronic power supply and communication. Just before the actual dive, the four sets of sampling bottles and plastic tubes are connected and filled by water, as any internal air bubbles may cause disastrous crushing of the bottles and tubes during descent. At the same time, tubes and connections are carefully checked for any fluid leakage. As the vehicle approaches the seafloor, the first sampling bottle is opened, and fluid pumping is started to sufficiently flush and substitute the pre-filled water in the fluid pathway with ambient seawater (Figure 5A). In the case of high-temperature hydrothermal fluid sampling, fluid temperature monitored in real-time gives an indication of the relative position of the pistol inlet with regards to fluid effluent. Fluid collection is undertaken at the highest possible temperature in order to collect as close to pure geofluid as possible. After successfully collecting geofluids into the last (fourth) sampling bottle, all external valves are closed to avoid fluid leakage from sampling bottles. When the vehicle



is recovered on-board, all sample bottles are detached from the main body, and then all the internal valves are closed manually to separate the two chambers of a bottle (**Figure 5B**). The bottles are stored in a refrigerator prior to subsequent subsampling, as heating of the bottles increase the internal pressure and therefore risks leakage and explosion. After subsampling (see below), each of the fluid-path tubes (usually remains on the vehicle) and sampling bottles are sufficiently flushed with tap water to remove any remaining fluids and particles, and then rinsed with pure water prior to the subsequent dive.

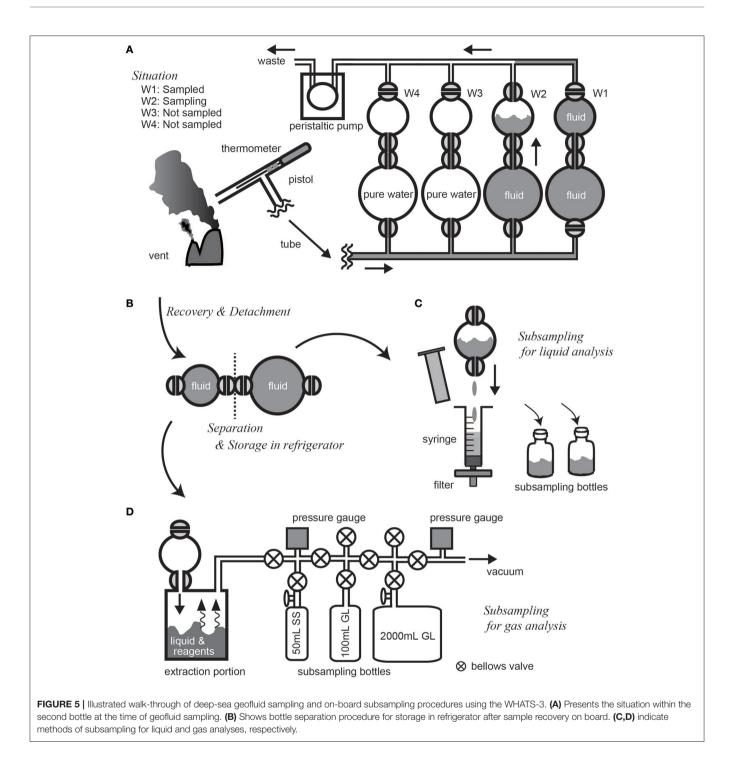
The two chambers in a sampling bottle serves as subsamples for liquid and gas analyses. Subsampling procedure for the WHATS-3 is the same as the WHATS-2, as presented elsewhere (e.g., Kawagucci et al., 2016). Although the current sampling chamber volumes of 20 and 50 mL in the WHATS-3 is less than the previous versions of WHATS (150 mL), these are already sufficient for subsequent analyses, described as follows.

For liquid subsampling (Figure 5C), a ${\sim}5\,mL$ aliquot of the fluid sample is used without filtration for on-board analyses of

pH, alkalinity, H₂S, and NH₃ concentration. The remaining fluid in the bottle (either 15 or 45 mL) is filtered through a 0.2 µm pore sized filter and used for major cation and anion analyses with Inductively Coupled Plasma Atomic Emission Spectroscopy (ICP-AES) and IC. Both ICP-AES and IC analyses generally consume \sim 0.1 mL of the sample because the sample is subjected to >1,000 times dilution with pure water prior to the analyses. The Cl concentration is sometimes quantified by the Mohr titration method without dilution (as it is more precise than IC) which consumes $\sim 1 \text{ mL}$ of the filtered subsample. For gas subsampling (Figure 5D), a chamber is connected to a vacuum line typically consisting of a glass-constructed gas extraction portion, subsampling bottles, pressure gauges, and a vacuum pump. Entire body of fluid in a chamber is introduced into the extraction portion and mixed with solid reagents, sulfamic acid (H₃NSO₃) and cadmium acetate [Cd(CH₃COO)₂, respectively, to extract inorganic carbon as CO₂ and precipitate H₂S as sulfide mineral. Subsampling bottles are optional, although 100 mL glass ampule, 50 mL stainless-steel bottle, and 2 L glass canister are usually used for general, He, and ¹⁴C analyses, respectively. The total gas content of a fluid sample is determined barometrically in the vacuum line. The volume of the vacuum line is adjusted to maintain an internal pressure not exceeding atmospheric pressure (0.1 MPa), because internal high pressure may cause gas leakage or explosion of the line. For example, a fluid sample collected in the larger chamber (containing 50 mL fluid) and expected to have a total gas content of 200 mM (likely for example in the hydrothermal fluids from the Okinawa Trough vents (Kawagucci, 2015)] requires a volume more than 250 mL in the vacuum line. For safety reasons, when processing the first sample from a new geofluid site where the total gas content is unknown, a 2 L glass canister is applied to the line to ensure sufficient volume is achieved. Although the small chamber of WHATS-3 is only one-tenth in volume compared to many other gas-tight samplers (Seewald et al., 2001; Saegusa et al., 2006), the amount of recovered major gases (CO2, CH4, H2, etc.) are usually sufficient to quantify their concentrations and isotope compositions using commercially available detectors via gas chromatography (e.g., Helium Ionization Detector; VICI, Houston) and continuousflow isotope-ratio mass spectrometry (e.g., Proskurowski et al., 2006; Reeves et al., 2011).

Examples of Results from *In situ* Sampling at Deep-Sea Hydrothermal Fields

Pressure resistance and field operational feasibility of the WHATS-3 system were tested and confirmed at Kairei (2,450 m) and Edmond (3,300 m) hydrothermal fields in the Indian Ocean (Gamo et al., 2001; Van Dover et al., 2001). The whole system operated under a maximum external pressure of 33 MPa and experienced no operational or visible damage when inspected closely after recovery. Fluids collected from black smoker vents in each field were completely depleted in Mg (**Table 2**), suggesting successful samplings of "pure" hydrothermal fluids (Von Damm et al., 1985). Their fluid chemistry, including gas composition, showed good agreement with previously reported values (Kumagai et al., 2008; Kawagucci et al., 2016), despite limited sample numbers.



Furthermore, the WHTAS-3 was applied together with previous versions of the WHATS-series samplers [WHATS-2 and Cheap-WHATS (Kawagucci et al., 2016)], to determine the fluid chemistry of three recently discovered deep-sea hydrothermal sites in the mid-Okinawa Trough. These include Aki site in the Iheya North field (Kasaya et al., 2015) and Hitoshi and pseudo-Noho (pNoho) sites in the Sakai field (Nakamura et al., 2015).

The "Mg diagram" (Von Damm et al., 1985) for major ion species in each site demonstrated bimodal mixing trends between a hydrothermal fluid and seawater, regardless of the samplers used (**Table 2**). Gas concentrations show scattering on the Mg diagram, similar to observations from other Okinawa Trough hydrothermal sites reported in previous studies (Konno et al., 2006; Kawagucci et al., 2013a; Toki et al., 2016). This is because the Mg concentration is

MatterMatte	Site	Sample sampler ID		MaxT pH (°C)	Mg (mM)	Na (mM)	K (mM)	(mM)	Ca (mM)	Sr (mM) (T	Si (mM) (T	B (mM) (m	Fe Mr (mM) (ml	Mn Cl (mM) (mM)	SO4 (mM)	Br (mM)	NH₄ (µ.M)	H ₂ S (µM)	Н ² (F M)	CH4 (µM)	(F W)	CO ₂ (mM)	с C ₂ H ₆ 1) (µM)	6 8 ¹³ C- (%) CH4		8D-CH4 8D-H2 (%) (%)	H ₂ 8 ¹³ C- CO ₂ (%)	- 8 ¹⁸ 0- (%)	0- 8D-H2O (%)
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Weighting	Aki	0#1859		7.51	53.0	445											N.D.	N.D.											
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Manuality of the set of the	Aki	#1616	305																23	537		56	0 >			Q	-8.97	26	
The sector of the sector	Aki	#1617	316			468			22.4	12	4.7	0.				0.91	1930	1930										1.10	-1.78
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Housing Not Total Bit Not No	pNoho	#1860	4.2	5.33	47.3	436											784		59	814	<0.£		<0.1			8374	74 -4.09	g	
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HPD#1800 No Total	pNoho	#1857		7.54	52.0	443											N.D.												
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	pNoho		53.6		44.2	462		0.44	15.0	ci	.21	õ						430	Q	628	0		0.0			_			

(Continued)

Matrix Matrix<		Sample sampler ID		MaxT pH (°C)	Mg (MM)	Na (mM	Na K (mM) (mM)	(mM	Li Ca Sr (mM) (mM) (mM)	Sr (mM)	Si (mM)	B (mM)	Fe (mM)	Mn (mM)	(mM)	SO4 (mM)	Br (mM)	NH4 (µM)	H ₂ S (µ.М)	Н ² (н. М)	СН ₄ (µ.M)	(F W)	CO ₂ (mM)	С ₂ Н ₆ (µ M)	⁶¹³ C- CH4	8 D-CH4 (%)	8 D-H 2 (%)	° ¹³ C-	8 ¹⁸ 0- H ₂ 0	8 D-H2 O (%)
301 301 <th>HPD#1</th> <th>772 vC</th> <th>3.8</th> <th>7.21</th> <th></th> <th></th> <th></th> <th>0.0</th> <th></th> <th></th> <th>0.17</th> <th></th> <th>000</th> <th></th> <th></th> <th>27.4</th> <th></th> <th></th> <th>6</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>(00%)</th> <th></th> <th></th> <th>(00%)</th> <th>(00%)</th> <th></th>	HPD#1	772 vC	3.8	7.21				0.0			0.17		000			27.4			6						(00%)			(00%)	(00%)	
2 3837 31	CW W	hite																												
1 1	HPD#1 W1		335.	4																304	2784	0.71	116	< 0.5	-28.8	-112	-360	-4.72		
177 2 3163 41 4	HPD# W2		338				94.8				13.9		0.23			0.5			692											
2 313 41 1 31 </td <td>HPD#1 W3</td> <td></td> <td>318.</td> <td>Q</td> <td></td> <td>408</td> <td>3615</td> <td>1.98</td> <td>117</td> <td>< 0.5</td> <td>-27.3</td> <td>-116</td> <td>-378</td> <td>-4.66</td> <td></td> <td></td>	HPD#1 W3		318.	Q																408	3615	1.98	117	< 0.5	-27.3	-116	-378	-4.66		
1 1	HPD# ⁻ W4	1772 v2	318.	5 4.62		515					14.3		0.75	0.94		0.4			561											
1 1	YK#14 W1																													
22 3 3 3 1 1 3	YK#14 W2				51.9				7.9	0.088	0.28	0.47	0.03			27.6														
22 10 510 100 500 101 120 051	YK#1 [,] W3																													
138 14 10 47 134 104 104 104 107 104 105 146	YK#1 [,] W4				1.0	518		4	26.8		12.4	4.30	0.57	0.97		0.2														
188 10 314 310 104 014 104 014 104 014 104 014 105 34 11	HPD# W1	1858 v3	145	5.6(0.083	0.85	0.77	0.07			25.2		473	205	Ø	1070	<0.5	14.6	v	-33.2	-115				
188 1	HPD# W2	1858 v3	278	5.16			28.2			0.081	3.17	1.81	0.06			20.2		2276		с	2011	<0.5	S	v	-32.2	-111	-511	-2.46		
188 264 53 0.6 4.5 4.4 19.1 0.06 1.6 0.6 <td>HPD# W3</td> <td>1858 v3</td> <td>4.9</td> <td>5.9{</td> <td></td> <td></td> <td>10.7</td> <td></td> <td></td> <td>0.086</td> <td>0.36</td> <td>0.57</td> <td>0.04</td> <td>0.01</td> <td></td> <td>26.5</td> <td></td> <td>116</td> <td>116</td> <td>10</td> <td>402</td> <td><0.5</td> <td>5.5</td> <td>v</td> <td>-32.6</td> <td>-116</td> <td></td> <td></td> <td></td> <td></td>	HPD# W3	1858 v3	4.9	5.9{			10.7			0.086	0.36	0.57	0.04	0.01		26.5		116	116	10	402	<0.5	5.5	v	-32.6	-116				
1770 C2 2855 6.30 6.45 1.34 1.36 1.31 2.32 4.0 1.370 C1 7.30 2.31 7.30 C1 7.30 C1 7.30 7.30 C1 7.30 C1 7.30	HPD# W4		264	5.3(455	82.5			0.068	11.8	5.61	0.04	0.86		0.6		7676		27	3000	<0.5	87	v	29.8	-112	-496	-2.78		
1770 vC 245 65 145 463 248 10 106 01 016 01 01 01 01 01 104 188 N 756 529 43 101 74 028 03	HPD# CWR	1770 vC	285.	5 5.3(455	81.7				12.9		0.09			0.3			228	40	13700	<0.1	278	1.04	-33.1	-114	-428			
ISB N 7.9 2.9 4.3 10.1 7.4 0.086 0.4 0.5 0.00 0.5 0.7 ND. ISB N 7.67 5.30 41 9.3 0.09 6.7 0.00 53 27.6 ND. 47 V 7.67 5.30 41 9.9 0.09 6.7 0.00 53 27.6 ND. 47 V 7.67 530 41 0.0 53 0.0 53 27.6 ND. 40 V 530 42 0.0 53 0.1 0.0 53 27.6 ND. 40 V 53 49 V 53 28 7.6 ND. 41 V 53 54 28 27.7 54 28 27.6 10.7 42 V 54 0.0 53 28 28 28 28 28 28 28 28 28 28 <td>HPD# CWW</td> <td>022</td> <td>245.</td> <td>9 5.5(</td> <td></td> <td></td> <td>68.9</td> <td></td> <td></td> <td></td> <td>10.6</td> <td></td> <td>0.15</td> <td></td> <td></td> <td>5.3</td> <td></td> <td></td> <td>184</td> <td>41</td> <td>7350</td> <td><0.1 1</td> <td>207</td> <td>1.04</td> <td>-32.1</td> <td>-112</td> <td>-448</td> <td></td> <td></td> <td></td>	HPD# CWW	022	245.	9 5.5(68.9				10.6		0.15			5.3			184	41	7350	<0.1 1	207	1.04	-32.1	-112	-448			
185 N 7.67 5.0 41 9. 0.08 0.15 0.01 0.00 53 27.6 ND. 47 V X 50 450 95 99 552 28.2 7 552 28.2 49 V3 361 363 562 58.2 56.2 5530 128 553	HPD# NG	1858 N		7.95					7.4	0.086	0.04	0.59	0.03			27.7		N.D.												
47 \sigma\$ 500 450 550 552 28.2 49 \sigma\$ 344 0.0 531 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.4 30.5 15.5 15.4 30.5 15.4 30.5 15.4 30.4 0.77 8.8 57 35 35.5 35.5 15.5 15.5 15.4 0.77 8.8 15.5 15.4 0.77 8.8	HPD# NR	1858 N		7.67			9.9	0.09		0.088	0.16	0.53	0.01			27.6		N.D.												
47 v3 500 450 9.5 9.9 552 28.2 49 v3 361 3.4 0.0 531 15.4 30.5 6.46 0.9 57 v3 375 3.65 0.0 680 39.8 56.2 90.5 1.8 7 181 374 0.77 8.8	EAN																													
v3 361 3.44 0.0 531 15.4 30.5 646 0.9 5530 128 0.58 7.5 v3 375 3.65 0.0 630 39.8 66.2 905 1.8 7 181 374 0.77 8.8	6K#1 ² W1	47			50.0				9.9							28.2														
v3 375 3.65 0.0 680 39.8 56.2 905 1.8 7 1.81 374 0.77 8.8	6K#1 ² W1		361	3.4		531	15.4		30.5							0.9				5530	128	0.58	7.5	< 0.2						
	6K#1 W1		375			680			56.2							1.8		7		181	374	0.77	8.8	< 0.2						

TABLE 2 | Continued

Field	Iheya North	Iheya North	Iheya North	Sakai	Sakai	Sakai
Site	Aki	Natsu	Original	pNoho	Hitoshi	CLAM
Depth (m)	1,101	1,071	980	1,600	1,300	1,390
MaxT (°C)	316	305	309	331	286	220
рН	4.45	4.81	4.65	4.7	5.3	5.3
CI (mM)	594	593	599	678	595	550
Na (mM)	451	461	451	509	458	
K (mM)	81.6	83.3	73	99	83	(50–60)
Ca (mM)	22.3	22.8	21.1	27.0	19.7	(~20)
Li (mM)	1.44	1.40	1.32	3.7	4.1	(3–4)
Si (mM)	14.1	14.1	11.9	13.7	12.7	(~10)
B (mM)	2.09		1.97	4.4	5.7	(5-6)
Sr (mM)	0.086		0.077	0.111	0.068	
Fe (mM)	<0.3	0.05	0.12	0.51	<0.15	
Mn (mM)	0.76	1.02	0.69	1.01	0.88	(0.4–0.5)
Br (mM)		0.94	0.95			(1.0-1.5)
NH ₄ (mM)	1.97	1.73	2.1	7.6	7.8	(8-12)
H ₂ S (mM)	1.9	1.5	3.6	0.6	0.2	
CH ₄ (mM)	0.4-0.9	0.46	2.5	3.2	3.2	
δ ¹³ C-CH ₄ (‰)	-48.4	-52.8	-54.1	-27.8	-32.2	
δD-CH ₄ (‰)	-112	-114	-124	-111	-113	
H ₂ (μM)	22–34	22.4	100	350	26.7	
δD-H ₂ (‰)	-373	-398	-394	-359	-428	
CO (µM)	<0.5			<3	<0.5	
CO ₂ (mM)	43–63	62	63	116	89	(160–200)
δ ¹³ C-CO ₂	-9.0	-10	-9.6	-4.7	-2.8	-4.4
C ₂ H ₆ (μM)	<0.5	<0.2	<1	<0.5	1	
δ ¹⁸ O-H ₂ O	1.3	1.3	1.2			
δD-H ₂ O	-1.4	-1.4	-1			
References	This study	Kawagucci, unpub.	Kawagucci et al., 2013b	This study	This study	Gamo, 1995

For ion species, endmember composition is estimated as intercepts of the mixing line on the Mg diagram. For gas species, the observed values in Mg-depleted samples are regarded as the endmember composition.

an indicator for bimodal mixing between high-temperature fluid and seawater, but subcritical phase separation of CO2-enriched fluids results in the formation of bubbles and CO2 droplets (Sakai et al., 1990; Konno et al., 2006), serving as a third endmember in the samples collected. Erroneously high and variable gas concentrations, even in high-Mg samples, point to the incorporation of bubbles together with vent fluid and seawater because ambient seawater contains only ~ 2 mM of CO₂ and negligible amounts of CH₄ and H₂ (see Discussion in Kawagucci et al., 2013a). Iron concentrations also show scattering on the Mg diagram. Similarly high Fe level in samples from both WHATS samplers and Niskin bottles indicate possible Fe contamination occurring during on-board or on-shore sample processing, although the stainless steel used in the WHATS-3 and the deepdiving vehicles cannot be entirely excluded as potential sources of contamination.

The estimated endmember fluid composition of the Aki site is generally identical to those of the Original and Natsu sites, the other two sites located within the Iheya North field (**Table 3**). The identical major fluid chemistry implies that the three sites are connected through a subseafloor fluid reservoir, despite the three sites being separated at \sim 1 km horizontal

intervals in the North-South direction. This possible connection among the three sites will be examined by future seafloor drilling operations; previous drilling operations around the Original site has already revealed a subseafloor high-temperature fluid reservoir extending ~500 m in the East-West direction (Takai et al., 2012; Kawagucci et al., 2013b). On the other hand, CH₄ concentrations and carbon isotope ratios are notably different among the three sites. This can be explained by a higher contribution of ¹³C-depleted biogenic CH₄ incorporation into the venting fluid at the Original site.

The fluid chemistry of the pNoho and Hitoshi sites are distinct from each other (**Table 3**). The uniformly higher major ion concentrations in the pNoho site, compared to Hitoshi and CLAM sites also in the Sakai field (Gamo, 1995), are likely caused by the greater extent of vapor-lost phase formed through subseafloor fluid boiling. Such intra-field variation of fluid chemistry has also been confirmed in the Izena Hole and Daiyon-Yonaguni fields, Okinawa Trough (Suzuki et al., 2008; Ishibashi et al., 2014) and is considered to be a result of preferable emanation of the more mobile vapor-rich phase. Both maximum fluid temperature and endmember Cl concentration were highest at the pNoho site, suggesting that this is the center of activity in the Sakai field. Possible subseafloor connections among the three sites within the Sakai field will also be examined by a future drilling project.

AUTHOR CONTRIBUTIONS

JM, SKan, and KT designed and constructed the WHATS-3 system. Testing and evaluation of functionality were carried out by JM, AM, NE, ST, JI, CC, and KT. Fluid chemistry was analyzed by AM, YM, NE, ST, JI, and SKaw. The manuscript was drafted by JM, CC, SKan, KT, and SKaw. All authors gave final approval for submission and publication.

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Conflict of Interest Statement: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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