



A Cost Estimation for CO₂ Reduction and Reuse by Methanation from Cement Industry Sources in Switzerland

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Baier J, Schneider G and Heel A (2018) A Cost Estimation for CO₂ Reduction and Reuse by Methanation from Cement Industry Sources in Switzerland. Front. Energy Res. 6:5. doi: 10.3389/fenrg.2018.00005 The Swiss government has signed the Paris Climate Agreement and various measures need to be implemented in order to reach the target of a 50% reduction in CO₂ emissions in Switzerland by 2030 compared with the value for 1990. Considering the fact that the production of cement in Switzerland accounts around 2.5 million ton for CO₂ emissions of which corresponds to roughly 7% of the country's total CO₂ emissions, the following article examines how this amount could be put to meaningful use in order to create a new value-added chain through CO₂ methanation, and thus reduce the consumption and import of fossil fuels in Switzerland. With power-to-gas technology, this CO₂, along with regenerative hydrogen from photovoltaics, can be converted into methane, which can then be fed into the existing natural-gas grid. This economic case study shows a cost prediction for conversion of all the CO₂ from the cement industry into methane by using the technologies available today in order to replacing fossil methane imports.

 $Keywords: CO_2 \ methanation, \ cement-based \ CO_2, \ power-to-gas, \ hydrogen, \ economics, \ photovoltaics, \ electrolysis, \ Switzerland$

INTRODUCTION

The Climate Background

The Climate Agreement negotiated in Paris came into force on November 4, 2016. The community laid down in this agreement that, up until 2030, there would have to be a 50% reduction in the emission of greenhouse gas compared with 1990 (Schweizerischer Bundesrat, 2016). Switzerland has signed the Paris Agreement and, through its Federal Council, has proposed ratifying it in the course of 2017 (Akademien der Wissenschaften Schweiz, 2017). The key statistics from 1990 and 2015 as well as the defined targets of Switzerland are listed in **Table 1** and shown in **Figure 1**.

For the interested reader: In 2015, Switzerland ranked 23rd in the world with a per-capita output of 4.64 ton of CO₂. In comparison, China, the world's largest carbon emitter, has a per capita output of 6.59 ton, Germany 9.6 ton, and Qatar has an output of 35.77 tons per capita (Statista, 2017a; Umweltbundesamt, 2017). In Switzerland's case, it is planned to achieve the target of a 50% reduction through 30% domestic measures and 20% foreign ones (Bundesamt für Umwelt, 2016). In addition, to showing the trend in CO₂ emissions over recent years, **Figure 1** indicates the future aims up to 2050. The shape of the curve is based on the aim of a 70% reduction, what is the most conservative assumption.

The curve points to the reduction in emissions inside Switzerland contributing to approximately 50% up to 2050. If further foreign measures were to be planned for 2030 and later, the final value inside Switzerland would be higher than 22.26 million ton. An emission target of zero inside Switzerland is thus excluded from the outset.

Origins of CO₂ Sources in Switzerland

Figure 2 gives an overview on the distribution of the various CO₂ emitters in Switzerland without gray emissions (Bundesamt für Umwelt, 2017).

Although the emission of CO_2 is highly decentralized and irregular in the sectors of transport, households, services, and agriculture, emissions in the sectors of industry and waste management occur in large quantities both centrally and continuously. Particularly in industrial processes where CO_2 emissions cannot currently be reduced through either substitution or renunciation, it would make sense to feed the emissions into Swiss power-to-gas and produce a reusable waste product. Therefore, this article deals with making use of the climate-damaging gas CO_2 for producing a renewable energy vector, i.e., methane (CH₄) by applying the

TABLE 1 | Survey of the greenhouse gas and carbon dioxide emissions of

 Switzerland, population figures, and the determination of the output per capita

 (Bundesamt für Statistik, 2016; Bundesamt für Umwelt, 2017).

	1990	2015	2020	2030	2050
Determined data				Targets	i
Greenhouse gases (10 ⁶ t/a)	53.72	48.14			
CO ₂ emissions (10 ⁶ t/a)	44.52	38.85	35.6	22.3	13.4
Inhabitants (million)	6.751	8.327			
Tonnes per capita	6.59	4.64			

well-known Sabatier reaction for a power-to-gas application (Sabatier and Senderens, 1902) and substitute fossil imports (c.f. chapter about technical considerations).

The Cement Industry and CO₂ Emissions

In 2015, the industry sector itself alone emitted 7.5 million ton of carbon dioxide. After waste incineration the cement industry, with an output of 2.5 million ton CO₂ is the second largest emitter in the industrial sector (E-PRTR, 2017). The waste gas (20–35% CO₂ in variable N₂ to O₂ ratios) emitted by the cement industry is made up, firstly, of the CO₂ from the combustion process (38.5%) and, secondly, from the CaCO₃ dissociation of the feedstock (61.5%) (Locher, 2000). However, using these 2.5 million ton of mainly unavoidable CO₂ would offer a possibility to replace large amounts of natural gas and reduce fossil imports with corresponding emissions.

In Switzerland, there are six large-scale installations for the production of cement. Given its centralized structure and the continuous occurrence of CO_2 emissions, it is this industrial sector that is particularly appropriate for the downstream addition of power-to-gas plants for converting CO_2 to methane in large quantities. Second, the process intrinsic high calcination temperatures (above 1,200°C) necessary for the CaCO₃ processing are an ideal source of heat for some novel methanation reactor concepts, which are not self-sustaining at about 300°C. An additional source of heat can be avoided, what is a substantial economic benefit.

As remark to the reader, cement industry is conscious of the fact that it emits large amounts of CO_2 and has been following various strategies for many years to counter these emissions. Measures implemented up until 2010 resulted in a reduction from 3.85 to 2.9 million ton CO_2 a total cut of 25% in emissions (Eidgenössiches Departement für Umwelt, 2003; E-PRTR, 2017). Since only limited possibilities for further process optimizations





are still available and since no alternative building material is going to exist for the near future, it is going to be necessary to consider additional approaches to reducing the high levels of CO_2 emissions or to putting these to other uses. The here proposed reuse of the emitted CO_2 in terms of its conversion to CH_4 is one possible scenario to do so.

Power-to-Gas and its Role in CO₂ Reduction

Power-to-gas technology offers the possibility of using technical or electrochemical conversion processes by use of electricity from renewable sources to produce hydrogen (H_2), thereby turning the electric energy into a chemical energy carrier, such as H_2 or subsequently to methane (CH₄) that can be long-term stored for any period of time until it is needed again for use (Specht et al.,



2010). The production of pure hydrogen faces challenges in the domains of storage, transport and shortage of consumers. Given the characteristics of the equipment currently installed by the end consumers, it is neither possible nor legally permissible to add large amounts of hydrogen to the natural-gas supply (max. 2 vol% H_2), because a higher percentage of hydrogen in natural gas changes the gas feed, flame conditions and combustion properties, which strongly influences the operation of the end consumer devices.

In the case of the here presented Swiss power-to-gas model, the hydrogen produced is put to further use and reacted with carbon dioxide (CO_2) to form methane, which is simpler to handle and transport. This process, which is also known as CO_2 methanation, is already in use today in small to medium-sized installations (Zapf, 2017).

Figure 3 illustrates the process for the model subject to an economic investigation in this study. The only technologies included here, were technologies that are already technically mature today. The authors clearly want to state here, that this examination is focusing exclusively on power from photovoltaic (PV), since further PV installations are feasible in Switzerland, while, e.g., hydro and wind power has very limited potential to be further increased or installed. Furthermore, there are several alternative technologies which may be taken into account. But for the sake of a definite energy value chain, it is not further spread to other technologies. One example of this is large-scale electrolysis, which uses an alkaline electrolysis (AEL), a technology which provides since decades sufficient lifetimes and large hydrogen production rates (90,000 h with up to 750 m³/h) (Carmo et al., 2013). It might be based on polymer electrolyte membrane (PEM) technology in future at such large scales. However, it is believed that at an industrial scale, as it is evaluated here, PEM electrolysis is nowadays still not the most reliable path (Götz et al., 2016). Table 2 provides a brief comparison of AEL and PEM electrolysis with the main advantages and disadvantages for the interested reader.



TABLE 2 Comparison of AEL and PEM (Schiller, 2012; Carmo et al., 2	013;
Zapf, 2017).	

	AEL electrolyzer	PEM electrolyzer
Electrolyte	 Liquid Electrolyte solution 20–40% KOH 	 Solid Highly porous polymer electrolyte (nafion)
Materials	Steel (frame)Nickel (catalyst)Asbestos, titanium, zirconium (separator)	 Titanium (bipolar plates) Noble metals (platinum, ruthenium, iridium)
Advantages	 Technology already proven on a large scale Low production and investment costs High long-term stability 	 Good part-load and overload capability Fast response and reaction times High current densities Compact design
Disadvantages	 Optimization needs for dynamic operation Alkaline purity and gas cleaning Corrosive liquid electrolyte 	 Membrane sensitivity and lifetime Only smaller installations tested to date High investment costs Noble metals indispensable
Investment costs	500–1,500 €/kW (as of 2014)	2,000–6,000 €/kW (as of 2014)

GENERAL TECHNICAL CONSIDERATIONS FOR THE APPLIED MODEL

The authors investigated a possible and reliable way for the production of methane with commercially available technologies from CO_2 emissions of the cement industry (**Figure 3**) (Matter et al., 2016).

In the scenario considered here, the electricity needed for operation of the alkaline electrolyzer is generated by conventional PV modules, attached to potentially appropriate roof surfaces (about 140 km² in Switzerland) or on suitable facades (50 km²) (International Energy Agency, 2002; Akademien der Wissenschaften Schweiz, 2012). The technology used for electrochemical water splitting is the abovementioned AEL with the following reactions and characteristics (Zapf, 2017):

Cathode reaction: $4H_2O + 4e^- \rightarrow 2H_2 + 4OH^-$. (1)

Anode reaction:
$$4OH^- \rightarrow O_2 + 2H_2O + 4e^-$$
. (2)

Total: $2H_2O(l) \rightarrow 2H_2(g) + O_2(g)$ with $\Delta H_R = +571.7$ kJ. (3)

Once the hydrogen has been produced, it can be converted into methane by reacting it with CO_2 in a catalytic fixed-bed reactor at atmospheric pressure according to the Sabatier reaction in Eq. 4. Atmospheric pressure is assumed here from the authors, since recent developments in catalysis showed methane yields up to 100% already at atmospheric pressure (Delmelle et al., 2016). By this, the compression energy is also significantly lower since only methane must be compressed to natural gas grid pressure instead of CO_2 and H_2 , which needs five times more compression **TABLE 3** | Typical efficiency values and chain efficiency of the overall power-togas processes by provision of solar electricity according to Stolten and Krieg (2010) and Schnurbein (2012).

Infrastructure	System efficiency (%)		
Power grid	95–100		
Alkaline electrolysis	64–80		
Catalytic methanation	80–85		
Compression	85–95		
Overall process chain	41–65		

energy and a H_2 suitable technology. The reaction of CO_2 and H_2 to form methane *via* the Sabatier reaction runs at temperatures of between 200 and 700°C and pressures from atmosphere up to 80 bar depending on the type of reactor and catalyst (Kopyscinski et al., 2010; Schaaf et al., 2014).

$CO_2(g) + 4H_2(g) \rightarrow CH_4(g) + 2H_2O(g)$ with $\Delta H_R = -165$ kJ. (4)

The supply of CO₂ comes from the process of separating the cement exhaust waste gases. While CO2 concentration in the exhaust is between 20 and 35% (Fischedick, 2015), typical separation costs arise of about 35 CHF/t CO₂ (European Cement Research Academy, 2009). Methane, produced from this purified CO₂, has a composition corresponding to natural methane and can be stored as an interim measure in the gas grid and retrieved as needed. Switzerland's gas grid is fundamentally designed to distribute natural gas rather than to store it in large quantities. In normal circumstances, a maximum of 2.7 million m³ can be accommodated in various storage devices. Thanks to good interconnections with the gas networks of neighboring countries, it is, however, possible to store considerably greater volumes of natural gas. The storage capacity of the Switzerland's next neighbors are, e.g., Germany with 19.2 billion m³ and Italy with 17.4 billion m³ (Hochschule für Technik Rapperswil, 2014).

It is further recommended that the hydrogen production and methanation plant itself be installed in the immediate vicinity of the CO_2 emitters in order to minimize the problems and costs associated with the transport of hydrogen and CO_2 . The entire design of the plant later on and the calculation of the costs associated with it are based on the fact that PV generation of electricity in Switzerland is only available for approximately 1,200 h per year (Verband Schweizer Elektrizitätsunternehmen VSE, 2015; Statista, 2017b). That means that the plant must be operated in standby mode for the rest of the 7,560 h. It is to mention here, that a plant in existence today has not been designed for on/off operation. Operating at full load for only 1,200 h a year, which is assumed for the purpose of this study, might have negative effects on the degree of efficiency, gas quality, gas production, and service life of the plant.

Energy Losses and Efficiencies

Each energy conversion step represents a technical process that is subject to a loss of efficiency. **Table 3** shows the bandwidth between the best and worst case for the entire facility, both with and without the PVs. The technologies available today result, in dependency of the applied process chain, in an overall efficiency of between 41 and 65% as worst case and best case scenario (Stolten and Krieg, 2010; Schnurbein, 2012).

It might be possible to achieve further optimization of overall efficiency by using energy and mass flows between the individual process steps, for instance by using the waste heat from methanation for electrolysis. The interested reader may get further details from current research projects such as the Swiss "High Efficiency Power-to-Gas Plant" and EU project "Pentagon" (Institut für Energietechnik—HSR, 2017; Pentagon, 2017), integrating high temperature solid oxide electrolyzer cells into a demonstration plant.

Mass Flow Consideration

To calculate the annual masses of the reactants of CO₂ $(M_{CO2} = 44.01 \text{ g/mol}), H_2 (M_{H2} = 2.02 \text{ g/mol})$ as well as of the products CH_4 ($M_{CH4} = 16.05$ g/mol) and H_2O ($MH_{H2O} = 18.02$ g/ mol) (Wächter, 2012), one can simply scale up the stoichiometric reaction from Eqs. 1-4 to the addressed 2.5 million ton of CO₂ from cement industry. The resulting mass flows in terms of per reaction and per cement plant and year are shown in Table 4. The methanation of these annual 2.5 million ton CO_2 from the year 2015 requires 0.46 million ton of H₂ (5.08 billion m³/a), which have to be produced through electrolysis. The reaction products are 0.9 million ton (1.26 billion m³/a) of CH₄ and 2.04 million ton of H₂O. This amount of methane produced corresponds to roughly 33% of the annual consumption of natural gas in Switzerland, which is as high as 119,420 TJ (3.821 billion m³/a) (Fachagentur Nachwachsende Rohstoffe e.V.—FNR, 2016; Verband der Schweizerischen Gasindustrie - VSG, 2017). By comparison with that, in 2015 Germany produced 3.8 million m^{3}/a of CH₄ by chemical methanation (Zapf, 2017).

For the needed 0.46 million ton of H_2 , the electrolyzer consumes 4.1 million ton of fresh and deionized water and produces another 3.6 million ton of oxygen (O₂) according to Eq. 3 and **Table 5**. Further use and economic aspects of the oxygen as well as a possible water circulation from the methanation to the electrolyzer to compensate the water consumption were not considered in this study. If a suitable consumer for the oxygen would be available, e.g., ozone-based purification of waste water in sewage-treatment facilities, it might have a positive impact on the economic perspective. But the water purification process itself will have a negative economic impact.

Energetic Consideration for H₂ Production by AEL and its Conversion to CH₄

The reaction in the electrolyzer as mentioned above is strongly endothermic and requires a great deal of energy to split water into

 $\ensuremath{\mathsf{TABLE}}\xspace 4$ | Overview of mass flows in methanation reaction on a molar and industry level.

	Input		Output	
		H₂	H ₂ O	CH₄
Stoichiometry	1	4	2	1
Molar weight (g/mol)	44.01	2.02	18.02	16.05
Industry level (million ton)	2.5	0.46	2.04	0.9

 H_2 and O_2 . The specific energy consumption of an alkaline electrolyzer is given as 4.2 kWh/m³ and 4.7 kWh/m³ of H_2 including the power electronics, respectively (Noack et al., 2015). For the production of a total mass of 0.46 million ton of H_2 , corresponding to 5.1 billion m³ (ρ_{H2} = 0.0899 kg/m³), the necessary annual energy input is 23,900 GWh. Expressed in terms of the lower heating value or net calorific value (NCV) of H_2 (H_i = 3.00 kWh/m³), the output amounts to 15,255 GWh, with an average electrolyzer efficiency of about 64%.

The subsequent conversion of this H₂ with CO₂ is assumed to take place at ambient pressure and 300°C, since these conditions are technically feasible to reach 100% CO₂ conversion with stateof-the-art for common nickel catalysts (Delmelle et al., 2016). The authors furthermore assumed for this case study that compression of one unit of CH₄ is more efficient and more economic than compressing 5 units of reactant gasses under stoichiometric conditions, i.e., 4 units H₂ and one unit of CO₂ and therefore, compression on gas grid conditions takes place after methanation. Despite that, an additional electrical energy of 0.4 kWh/m³ synthetic natural gas (Zapf, 2017) is calculated to heat the CO₂ and H₂ mixture (1:4) up to 300°C for the catalytic reaction. In best case, this energy can be saved, if exhaust heat from the cement kiln can be recuperated and used for this heating purpose.

COSTS ESTIMATION FOR THE POWER-TO-GAS MODEL

As a general remark prior to the detailed cost analyses, is has to be mentioned that the cost calculation is based on the net present value method (Staehelin et al., 2007). The interest rate was set at 3.5% and the investment period has been fixed at 30 years.

Photovoltaics

According to the considerations made in 2.3 the annual energy needed for producing hydrogen *via* PV amounts to 24,403 GWh/a, from which 23,900 GWh are for electrolysis to receive H₂ and 503 GWh for the conversion to CH₄. Losses of about 5% occur in the inverter system, therefore, the system must be designed for 25,095 GWh/a. The following calculations that are summarized in **Table 6**, assume a PV module efficiency of 16%, but a loss of about 20% of the output in the course of a service life of 30 years has to be considered (Meyer Burger, 2017). For this reason, the plant was oversized by a further 10% to balance these losses off, and finally the whole system needs to be dimensioned for 27,604 GWh/a. With an operation of 1,200 full load hours per year a necessary system performance of 23 GW results. While the peak output per unit area of present-day modules is about 0.23 kW/m² (Meyer

TABLE 5 | Overview of mass flows in electrolysis on a molar level and industry level for 2.5 million ton of CO_2 .

	Input	Output		
	H₂O	H ₂	O ₂	
Stoichiometry	2	2	1	
Molar weight (g/mol)	36.04	2.02	32	
Industry level (million ton)	4.1	0.46	3.6	

TABLE 6 | Breakdown of the costs for the photovoltaic plant for a total installed plant power of 23 GW.

Investment costs	23,003 million CHF
10% saving through quantity of installation	-2,300 million CHF
Investment costs	20,703 million CHF
Investment costs/power	900 CHF/kW
OpEx (operational expenses)	
Depreciation and interest	697 million CHF/a
Replace inverter (1.5 Rp/kwh)	428 million CHF/a
Roof rental (1 Rp/kwh)	286 million CHF/a
Administration, insurance, repair (2 Rp/kwh)	571 million CHF/a
Total	1,982 million CHF/a

Burger, 2017) an overall surface area of 100 km² is required for the installation of these modules. One should know, that the roof area that can sensibly used for PVs in Switzerland is indicated as 100–150 km² (Akademien der Wissenschaften Schweiz, 2012).

To calculate the investment costs, the first step is to estimate 1,000 CHF/kW of installed capacity (Mayer, 2015; Arnold et al., 2016). Considering the quantity of the installations involved and the resulting effective economies of scale, a 10% reduction is a commonly applicable reduction for the investment costs (Noack et al., 2015). The investment costs or capital expenditures (CapEx) for all the PV installations therefore amount to 20,703 million CHF.

The operating costs or operating expenditures (OpEx) consist of the cost depreciation and interest (697 million CHF/a), replacing the inverters twice during the total running time (428 million CHF/a), the roof rent (286 million CHF/a), as well as other costs such as administration, insurance, repair, cleaning and control (571 million CHF/a) (Baumgartner et al., 2015). Together, OpEx costs are 1,982 million CHF/a and for an annual production of 25,095 GWh/a mean operating costs are assumed to 0.09 CHF/ kWh (c.f. **Table 6**).

Alkaline Electrolysis

The economic appraisal for the AEL design is based on data of the German Aerospace Center (DLR) in its study into planning a demonstration plant for the production of hydrogen (Noack et al., 2015). The DLR study is evaluating plants designed for two different sizes, 5 and 100 MW, respectively. The cost estimation presented in this study is based on the data for a 100 MW plant, with an amortization time of 30 years. With a hydrogen production rate of 20,000 m3/h, which is typical for plant of this size and with the plant operating time of 1,200 h/a, the annual H₂ production rate is 24 million m³. For production of the annual amount of 5.1 billion m3 of hydrogen calculated above, 212 installations like this are needed to reach a power of 21,188 MW. The DLR report indicates the investment costs for a 100 MW plant as being 52.1 million EUR or 56.5 million CHF (exchange rate used for the calculation: 1 EUR = 1.084 CHF from May 2017). The total investment sum for all 212 plants is 14,968 million CHF. Under consideration of a 10% cost reduction attributable to economies of scale, the necessary investments for the alkaline

TABLE 7 | Breakdown of the costs for AEL for total plant power of 21,188 MW.

CapEx (capital expenditures)	
Investment costs for plant	14,968 million CHF
10% saving through quantity of installation	–1,497 million CHF
Investment costs	13,471 million CHF
Investment costs/power	636 CHF/kW
OpEx (operational expenses)	
Depreciation and interest	454 million CHF/a
Materials, repairs, personnel, etc. (7% capex)	943 million CHF/a
Total	1,397 million CHF/a

electrolyzers are 13,471 million CHF. With an overall system output of 21,188 MW, the result is 636 CHF/kW. In addition to the costs for depreciation and interests (454 million CHF/a), another 7% of the investment costs are estimated for the OpEx costs. The major part of these costs is the exchange of components in the electrolyzer at an interval of 8 years. In addition, there are costs for cleaning, evaluation and administration, summing up to 943 million CHF/a. The mean operating costs are assumed to 1,397 million CHF/a or 0.11 CHF/kWh (listed in **Table 7**).

Methanation

The cost estimation of the methanation process is based on today's plants with a power consumption of up to 5 MW. These plants are generally composed of electrolyzers and methanation collectors. Based on this configuration, the cost of the methanation part is estimated to be between 208 and 440 CHF/kW (Zapf, 2017). Given the expected scale effects due to the enormous project size, the most optimistic value of 208 CHF/kW is used for further calculations and the resulting investment is 4,405 million CHF.

The costs for depreciation and interests are 148 million CHF/a. Due to a lack of experience, especially over long periods of time, there is currently little usable data available. However, various plant builders estimate a range of 1–3% of investment costs. A safety margin of 5% is additionally used and sum up to a total of 220 million CHF, required for the operation of the plants. These costs include the replacement of the catalysts, the cooling media and the handling of the necessary water. Another 88 million CHF/a are included the separation of CO₂ from the exhaust gases of the cement industry (32.6 \notin /t CO₂; Hermann et al., 2014; Schaaf et al., 2014). In summary, operating costs for the methanation plant add up to a total of 457 million CHF/a or 0.04 CHF/kWh (**Table 8**).

Is has to be mentioned explicitly that neither the waste heat of the methanation process at 300°C affects the cost estimation, since the methanation is expected to be heated from the exhaust heat of a cement kiln. Nor is the water produced catalytically during the methanation processes taken into account. In the best case, this relatively pure water can be recirculated to the electrolysis and used a water source. From an engineering point of view, a heat and mass flow exchange between two complex systems increases the system complexity even more. Therefore, the extent to which heat and water can be used as input into the electrolysis and how great the resulting benefit is, need to be clarified elsewhere. Decoupling TABLE 8 | The costs of methanation at an installed capacity of 419 MW.

Investment costs	4,405 million CHF
Investment costs/power	208 CHF/kW
OpEx (operational expenses)	
Depreciation and interest	148 million CHF/a
Material, repairs, personnel, etc. (5% capex)	220 million CHF/a
CO ₂ separation	88 million CHF/a
Total	457 million CHF/a
Costs/energy consumed	0.04 CHF/kWh

TABLE 9 | Costs of the power-to-gas concept for the twofold use of CO_2 from Swiss cement works, process chain: photovoltaics, alkaline electrolysis, and methanation.

	Photovoltaics	Alkaline electrolysis ^a	Methanation ^a	Total
CapEx (million CHF)	20,703	13,471	4,405	38,579
CapEx/power (CHF/ kW)	900	636	208	
OpEx (million CHF/a)	1,982	1,397	457	3,836
OpEx (CHF/kWh)	0.09	0.11	0.04	0.24

^aElectric power costs for alkaline electrolysis and methanation have been included in the investment calculation for the photovoltaics and separation costs of CO₂ have been included in the methanation.

the methanation processes from the electrolysis through the possible interim storage of the H_2 may be a possible solution for better use of the electricity and for coping with the problems of modulating operation, but this additional infrastructure was not included in this activity.

OVERALL COSTS

Everything considered, the investment volume required for the power-to-gas process in terms of an annual 2.5 million ton of CO_2 conversion to methane amounts to CHF 38,579 million CHF. The annual operating costs are highest at 1,982 million CHF for PVs. Next come the operating costs for AEL at 1,397 million CHF, while methanation accounts for a further 457 million CHF per annum, including 88 million CHF/a for CO_2 separation from the cement kiln exhaust gas. Additional annual operating costs for the whole plant have to be considered and amount to a total of 3,836 million CHF per annum. The overall economic calculations of the individual processes are aggregated in **Table 9**.

For an annual processing of 2.5 million ton of CO_2 from cement industry, the resulting costs per tonne of CO_2 are about 1,500 CHF. 1.26 billion m³ of renewable methane are produced during the processing of the carbon dioxide. This results in methane costs of 3 CHF/m³ and 0.30 CHF/kWh, respectively. Costs related to the transport and storage of hydrogen as well as the feed-in costs of methane into the natural gas network were not included in this calculation. The energy price published for natural gas for 2016 was 0.084 CHF/kWh. Without including the conversion factor and taking the NCV of methane of 9.97 kWh/ m³, the costs are calculated to be 0.84 CHF/m³. Consuming 1.26 billion m³ of methane from the natural-gas grid therefore costs 1.059 billion CHF a year. Synthetically produced methane from the power-to-gas process thus costs 3.6 times more than fossil methane costs.

These costs do vary with the economic assumptions, especially on such as electricity prices or PV operation hours per year for the H_2 production. However, overall costs of 0.30 CHF/kWh for synthetic methane from cement based CO₂ under the specific Swiss conditions, still is in the range of 0.07–0.42 CHF/kWh reported elsewhere (Brunner and Thomas, 2014; E and E Consultant, 2014; Graf et al., 2014; Ausfelder et al., 2015; Hannula, 2015; Vandewalle et al., 2015). These values strongly depend on the plant scale and technology maturity.

CONCLUSION

Within the current energy turnaround activities in Switzerland a huge momentum for a similar reduction of CO_2 emissions and replacement of fossil fuels is given, if locally available CO_2 -rich sources like the 2.5 million ton of CO_2 per year from the Swiss cement kiln plants are converted into transportable and storable methane under the use of renewable H₂. This study examined the costs of applying the current state-of-the-art technologies for a large-scale CO_2 methanation process. Since the CO_2 emissions from Swiss cement industry are classified to a large amount as unavoidable geogenous CO_2 and are emitted by only six large plants, these centralized sources of CO_2 are favored in this study.

Using the technology chain of PV, AEL, and catalytic methanation for the investigated CO_2 valorization path, it is possible to produce 0.9 million ton or 1.26 billion m³ of synthetic CH₄ per year by applying the CO₂ from the exhaust gases of all cement plants. Not less than 32.9% of the annually required 3.82 billion m³ of natural gas imports could be compensated by the produced CH₄, thus reducing the CO₂ emission from natural gas by the same amount of 32.9%.

The investment costs of the whole power-to-methane infrastructure amount to a total of 38,579 million CHF. This comprises installation costs of 20,703 million CHF for electricity generation by PVs, 13,471 million CHF for AEL and another 4,405 million CHF are required for the installation of the methanation plants itself.

Besides these installation costs annual running expenses have to be considered. Separation and conversion of the annually emitted 2.5 million ton of CO_2 to 0.9 million ton CH_4 are estimated at 3,836 million CHF per annum. The highest individual costs are 1,982 million CHF per year for the production of the electricity by PVs (51.7%), followed by 1,397 million CHF/a for AEL (36.4%) and 457 million CHF/a for the methanation (11.9%).

It is believed that the calculated investment volume of 38,579 million CHF and additional annual maintenance and operation costs of 3,836 million CHF can be judged as feasible for an energy economy such as in Switzerland. However, the economic appraisal shows that the costs estimation is about 1,500 CHF per ton of CO₂. Compared with that, a tonne of CO₂ is currently sold for only 5.43 CHF in international CO₂ trade (as per March 2017). In the light of this economic fact in combination with the unclear regulative situation and taxing system such as bonus and malus on renewable fuels and CO₂ certificates, a governmental

reassessment of the economic conditions is recommended for a successful energy transition strategy.

AUTHOR CONTRIBUTIONS

The corresponding author (AH) confirms that all listed authors (AH, GS, and JB) were involved in data acquisition, writing, proof reading and processing of this research article.

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