



# Effect of Organic Loading Rate and Temperature on the Anaerobic Digestion of Municipal Solid Waste: Process Performance and Energy Recovery

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#### **OPEN ACCESS**

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#### Specialty section:

This article was submitted to Bioenergy and Biofuels, a section of the journal Frontiers in Energy Research

Received: 22 December 2019 Accepted: 28 April 2020 Published: 29 May 2020

#### Citation:

Jiang J, He S, Kang X, Sun Y, Yuan Z, Xing T, Guo Y and Li L (2020) Effect of Organic Loading Rate and Temperature on the Anaerobic Digestion of Municipal Solid Waste: Process Performance and Energy Recovery. Front. Energy Res. 8:89. doi: 10.3389/fenrg.2020.00089 This study investigated the effects of organic loading rates (OLRs) and temperature on the performance and stability of anaerobic digestion treating the organic fraction of municipal solid waste (OFMSW) in a semi-continuous mode. Furthermore, a preliminary energy analysis was conducted to determine the optimal application parameters for anaerobic digestion of OFMSW. Results showed that the maximum achievable OLR was 9.00 g VS/(L·d), with a volumetric biogas yield of 4.03 L/(L·d) and 4.31 L/(L·d) for mesophilic and thermophilic systems, respectively. However, the preliminary energy analysis showed higher energy conversion efficiency was achieved for the system operated at an OLR of 7.50 g VS/(L·d). The system operated at the thermophilic condition had a higher total energy due to more electricity and heat energy generated than the mesophilic one. Therefore, the recommended operating conditions for the anaerobic digestion of OFMSW is an OLR of 7.50 g VS/(L·d) and thermophilic condition. Based on the annual yield of OFMSW in China, the estimated net output energy was 69970.61 GWh per year.

Keywords: anaerobic digestion, municipal solid wastes, temperature, OLRs, biogas yield

## INTRODUCTION

With the rapid development of urbanization and industrialization, the output of municipal solid waste (MSW) has increased dramatically. For example, the total production of MSW in China was  $\sim$ 192 million tons in 2015 (Liu et al., 2017c), resulting in serious environmental and health problems. Current methods for the disposal of MSW include landfill, incineration, and biological processing. Landfill is an undesirable technology due to its requirement for land resources, and environmental issues (Mu et al., 2018). Incineration is often affected by the chemical composition of MSW. In China, typical MSW has the characteristics of high moisture content (>50%) and high organic fractions (60–70%) (Liu et al., 2017b), which lowers the energy recovery rate, and thus necessitates supplementation with auxiliary fuel. The high organic component in MSW favors

biological treatment, and anaerobic digestion can achieve better environmental performance than incineration, bio-landfills or composting (Arafat et al., 2015). Liu et al. (2017c) concluded that the "best" treatment scenario for MSW is biological treatment of the biodegradable fractions and incineration of the high calorific value components, followed by landfill of the remaining residues if the land application of digestive residue become feasibility. Therefore, for the organic fraction of MSW (OFMSW), anaerobic digestion may be an alternative treatment method.

The anaerobic digestion of MSW is receiving increasing attention, with the reported specific methane yields of MSW of 158-553 mL/g vs. (Mu et al., 2018). Temperature and OLRs are one of the most important parameters of anaerobic digestion (Wirth et al., 2015; Hu et al., 2018). Although thermophilic condition can increase the performance of anaerobic digestion, its energy requirement and energy loss accordingly increase (Siqueiros et al., 2019). On the other hand, higher organic loading rates (OLRs) could improve the processing efficiency of anaerobic digestion, while it might inhibit the biogas production (Pearse et al., 2018; Rattanapan et al., 2019). Thus, both OLRs and temperature can be considered key parameters for digestion, and their suitable application will determine the outcome in terms of energy feasibility (Barbot et al., 2016; Ganesh Saratale et al., 2018). The methane yield is considered as one of the key parameters affecting output energy (thermal energy and electricity energy) (Abad et al., 2019). However, limited literatures focused on OFMSW treatment and management with considering energy benefits (Callan and Thomas, 2001; Martinez-Sanchez et al., 2016). Therefore, an energy analysis is required to evaluate before determining optimal operating conditions.

The present study aims to: (1) assess the biogas production performance and stability of anaerobic digestion system feeding OFMSW at different temperatures and OLRs; (2) calculate the potential biogas production based on the annual production of OFMSW in China; (3) conduct a preliminary energy analysis to determine the optimal temperature and the maximum operating OLR for OFMSW.

## MATERIALS AND METHODS

### **Feedstock and Inoculum**

Municipal solid waste was collected four times from the Heyuan district, Guangdong, China. OFMSW was obtained by removing impurities such as plastic, foam, stone, glass and metal. The collected OFMSW was milled and stored in a refrigerator prior to further utilization and analysis. The materials from the 1st, 2nd,  $3^{rd}$ , and 4th batches were used for the OLRs of 0.75–1.00 g VS/(L·d), 1.25–2.00 g VS/(L·d), 2.50–3.50 g VS/(L·d), and 4.00–11.00 g VS/(L·d), respectively.

The inoculum was taken from existing CSTR reactors in the lab, which were fed an artificially prepared substrate composed of peptone, yeast powder, xylose, cellulose, starch, and glucose. The characteristics of the feedstock and inoculum were listed in **Table 1**.

## **Experimental Setup and Procedure**

Two CSTR-type reactors (2 L) were operated semi-continuously at a temperature of  $35 \pm 1^{\circ}$ C for mesophilic conditions, and  $55 \pm 1^{\circ}$ C for thermophilic conditions. The biogas produced was collected in a gas sampling bag (5 L, Dalian Hede Technologies Co., Ltd.).

Each reactor was filled with 1800 mL of inoculum, and fed material at different weights to achieve the required OLRs, which ranged from 0.75 g VS/(L·d) to 11.00 g VS/(L·d). A 30-day hydraulic retention time was used for OLRs of 0.75-6.50 g VS/(L·d), coupled with a wet weight of 4.45-59.98 g/d. For OLRs of 7.50, 9.00, and 11.00 g VS/(L·d), the average weights were 69.21, 82.96 and 101.50 g/d, respectively, and the hydraulic retention times were 26, 22 and 18 days, respectively. Each OLR was run for 22–40 d except for the OLR of 11.00 g VS/(L·d). The experimental lasted for 402-410 days.

## Analytical Methods

The values of total solids (TS) content, violate solids (VS) content, pH, total ammonia nitrogen (TAN), partial alkalinity (PA), intermediate alkalinity (IA), volatile fatty acids (VFAs), and methane content (CH<sub>4</sub>) were measured according to previously described methods (Li et al., 2012, 2018a). Elemental carbon (C), nitrogen (N), and hydrogen (H) were measured using a Vario EL element analyzer (Elementar Analysensysteme GmbH, Hanau, Germany). Oxygen (O) content was calculated by subtracting the C, H and N content from 100%.

## **Calculation Methods**

Following Buswell and Boruff (1932), theoretical biogas potential (TBP) was calculated based on the elemental contents (Equation 1).

$$C_n H_a O_b N_c + \left(n - \frac{a}{4} - \frac{b}{2} + \frac{3c}{4}\right) H_2 O$$
  

$$\rightarrow \left(\frac{n}{2} + \frac{a}{8} - \frac{b}{4} - \frac{3c}{8}\right) CH_4$$
  

$$+ \left(\frac{n}{2} - \frac{a}{8} + \frac{b}{4} + \frac{3c}{8}\right) CO_2 + c \cdot NH_3 \quad (1)$$

## **Statistical Analysis**

The physical and chemical properties of OFMSW were statistically analyzed using IBM SPSS Statistics 25 software with one-way analysis of variance (ANOVA) at a probability level of 0.05.

## **Preliminary Energy Analysis**

A preliminary energy analysis was conducted to compare the energy revenue under different conditions. The designed anaerobic reactor was set to 3000 m<sup>3</sup>, a typical volume of largescale commercial reactors (Milledge and Heaven, 2017). When the height is equal to the diameter, the reactor has minimal heat loss (Taricska et al., 2011). The number of anaerobic reactors used to treat OFMSW produced in China was calculated according to Equation (2):

Sample	TS (%)	VS (%)	C (%)	N (%)	C/N	H (%)
OFMSW	$29.42 \pm 0.19^{a}$	$20.21\pm0.06^{a}$	$35.97 \pm 0.36^{\rm b}$	$1.25\pm0.19^{\rm b}$	$29.57 \pm 4.36^{\rm b}$	$5.37\pm0.14^{\rm b}$
	$28.11 \pm 1.03^{a}$	$20.55\pm0.85^{\rm a}$	$32.84\pm0.82^{a}$	$1.46 \pm 0.01^{\circ}$	$22.49\pm0.72^{a}$	$4.88\pm0.15^{\rm a}$
	$32.62\pm0.59^{\rm b}$	$24.02\pm0.22^{a}$	$35.27\pm0.36^{\text{b}}$	$1.75\pm0.03^{\rm d}$	$20.16\pm0.55^{\rm a}$	$5.33\pm0.02^{\rm b}$
	$26.82\pm0.03^{\text{a}}$	$19.51 \pm 1.70^{a}$	$37.13 \pm 0.73^{\circ}$	$0.92\pm0.09^{\rm a}$	$41.01 \pm 4.61^{\circ}$	$5.53\pm0.07^{\rm b}$
Inoculum	$0.97\pm0.002$	$0.44\pm0.003$	-	-	-	-

TABLE 1 | Characteristics of the organic fraction of municipal solid wastes and inoculum.

"-" no analysis.

<sup>abcd</sup>Mean with different superscripts in row (P < 0.05).

$$N = \frac{M^* VS}{V_R * K * OLR}$$
(2)

Where N = number of anaerobic reactors; M = OFMSW produced in China per day, 144,123 kilotons, which was calculated in section 4.2; VS = volatile solid content of OFMSW, 21.07% which was the average of VS of material in this study;  $V_R$  = volume of reactor for OFMSW digestion, 3000 m<sup>3</sup>; K = the utilization rate of  $V_R$ , 80%; OLR = organic loading rate.

For anaerobic digestion of OFMSW at mesophilic and thermophilic conditions, the input energy includes energy for feedstock transportation, feedstock separation, feedstock heating  $(Q_{heating})$ , pumping  $(Q_{pumping})$ , mixing  $(Q_{mixing})$ , and heat loss of reactors  $(Q_{heatloss})$  (Milledge and Heaven, 2017; Mu et al., 2018). The output energy (biogas) from anaerobic digestion can be transferred into thermal  $(Q_{thermal energy})$  and electricity  $(Q_{electricity energy})$  energy through a combined heat and power unit (CHP) (Zema, 2017; Li et al., 2019).

Related calculations involved in the preliminary energy analysis are shown in Figure 1, where C = specific heat of influent, which approximated to water, 4.18 KJ/(kg °C);  $V_I =$ the flow volume fed to the digester per day;  $\phi$  = the electricity energy used for pumping, 0.5 KWh/m<sup>3</sup> (Lu et al., 2008; Mu et al., 2018);  $\omega$  = the electricity energy used for stirring, 0.08 KWh/ $(m^3 \cdot d)$  (Lu et al., 2008; Mu et al., 2018); The material used for the designed reactor was 300 mm thick insulated concrete wall, U = heat transfer coefficient, 1.99 W/(m<sup>2</sup>·°C) (Liu et al., 2017a); A = superficial area of reactor, which was calculated according to the calculation formula, 1152 m<sup>2</sup>;  $T_1$ = ambient temperature, which is close the average annual temperature in China, 10.3°C;  $T_2$  = reactor temperature, 35°C for mesophilic condition or 55°C for thermophilic condition; The efficiency of the CHP in converting biogas into thermal and electricity energy were 33 and 50%, respectively (Feiz et al., 2019; Valentino et al., 2019),  $H_M$  = calorific value of methane, 35.8 kJ/L (Chen et al., 2019), and  $V_M$  = volume of methane produced.

### RESULTS

#### **Chemical Composition of the Material**

The TS content of OFMSW ranged from 26.82 to 32.62%, and the VS/TS ratio was 68.69–73.64%, suggesting that the major part of the feedstock was biodegradable. The C, N, and H contents were in the range of 32.84–37.13%, 0.92–1.75%, and 5.33–5.53%,

respectively. Correspondingly, the C/N ratios were in the range of 20.16-41.01. In general, a C/N ratio of 15-35 is suitable for anaerobic digestion (Silvestre et al., 2015; Capson-Tojo et al., 2016; Li et al., 2018b). While, the material with C/N ratio of 2.3-152 was used for anaerobic digestion (Xu et al., 2018), indicating that the effect of C/N ratio on the performance of anaerobic digestion influenced by other factors, such as carbon type (Choi et al., 2020). No obvious difference was observed for the TS and VS contents, while elemental composition significantly changed. The chemical composition of MSW is site- and season-specific (Breitenmoser et al., 2018), which affects the performance and stability of anaerobic digestion. The specific biogas yields for the component of MSW, such as fruit, vegetable and yard wastes from different seasons, were between 360 and 620 mL/g VS for mono- or co-digested systems (Korai et al., 2018). The reported specific methane yields for meat/fish and paper waste were 293  $\pm$ 3 mL/g VS and  $217 \pm 5 \text{ mL/g VS}$ , respectively (Nielfa et al., 2015).

## Performance of Anaerobic Digestion of OFMSW in Semi-Continuous Mode The Performance at Mesophilic Condition

For the system operated at mesophilic condition, the volumetric biogas yields increased from  $0.17 \pm 0.03$  to  $4.03 \pm 0.42$  L/(L·d) with the OLRs increased from 0.75 to 9.00 g VS/(L·d) (Figure S1 and Table 2). Meanwhile, the specific biogas and methane yields varied from 335–495 to 196–278 mL/g VS, respectively, with the methane contents of 55.23–59.97%. During the process, the pH maintained at a range of 6.49–7.73 (Figure 2A), and the concentrations of TAN, acetic acid and propionic acid were <860, 596, and 340 mg/L, respectively (Figures 2A,B), below the reported inhibition values (Zhang et al., 2014; Meng et al., 2018). In addition, the values of stability indicator, IA/PA ratio, was within the range of 0.03–0.51 (Figure 3), suggesting that the system well-performed at an OLR of 0.75–9.00 g VS/(L·d). An IA/PA ratio of <0.9 indicated that the system is in a stable condition (Ferrer et al., 2010).

Increasing the OLR to 11.00 g VS/(L·d), the volumetric biogas yield decreased to  $3.80 \pm 0.42$  L/(L·d), and correspondingly the specific biogas yield decreased to  $346 \pm 38$  mL/g VS. At the OLR, the system became hard to operate due to overloading. Rincón et al. (2008) revealed that OFMSW anaerobic digestion failed at an OLR of 11.00 g COD/L due to the sudden drop in alkalinity and TVFA accumulation. Under a high OLR, the system has a

OLR (g Opera VS/(L·d)) time	Operation time (d)	<ul> <li>Specific biogas yield (mL/g VS)</li> </ul>			Specific methane yield (mL/g VS)		Volumetric biogas yield (L/(L⋅d))			Methane content (%)		Biogas conversion rate (%)		
		Mesophilic	Thermophilic	Increase rate (%)	Mesophilic	Thermophilic	Increase rate (%)	Mesophilic	Thermophilic	Increase rate (%)	Mesophilic	Thermophilic	Mesophilic	Thermophilic
0.75	22	$381 \pm 54$	$377 \pm 44$	-1.05	$229 \pm 28$	$216 \pm 28$	-5.68	0.29 ± 0.04	$0.28 \pm 0.03$	-3.45	59.58	57.72	56.74	56.15
1.00	32	$379\pm43$	$370\pm47$	-2.37	$216\pm26$	$214 \pm 28$	-0.93	$0.38\pm0.04$	$0.37\pm0.05$	-2.63	57.28	57.81	56.45	55.11
1.25	23	$383\pm55$	$378\pm64$	-1.31	$219\pm37$	$216 \pm 42$	-1.37	$0.65\pm0.09$	$0.64\pm0.11$	-1.54	55.98	55.83	57.04	56.30
2.00	37	$470\pm43$	$514 \pm 41$	9.36	$274\pm28$	$294 \pm 24$	7.30	$0.96\pm0.09$	$1.05\pm0.08$	9.38	58.38	57.29	75.82	82.91
2.50	30	$412\pm49$	$429\pm36$	4.13	$225\pm27$	$227\pm20$	0.89	$1.03\pm0.12$	$1.07\pm0.09$	3.88	53.75	51.81	66.46	69.20
3.00	27	$372\pm43$	$434\pm48$	16.67	$212\pm24$	$246\pm30$	16.04	$1.12\pm0.13$	$1.30\pm0.14$	16.07	56.31	57.38	56.50	65.92
3.50	32	$393\pm55$	$458\pm39$	16.54	$235\pm41$	$268 \pm 26$	14.04	$1.38\pm0.19$	$1.60\pm0.13$	15.94	59.97	59.12	59.69	69.57
4.00	27	$463\pm45$	$553\pm42$	19.44	$260 \pm 27$	$318\pm25$	22.31	$1.85\pm0.18$	$2.21\pm0.17$	19.46	55.59	57.45	70.33	84.00
4.50	29	$432\pm46$	$518\pm58$	19.91	$243\pm28$	$300\pm33$	23.46	$1.94\pm0.21$	$2.33\pm0.26$	20.10	58.21	58.14	62.33	74.74
5.50	28	$453\pm44$	$478\pm43$	5.52	$261 \pm 25$	$276\pm26$	5.75	$2.49\pm0.24$	$2.63\pm0.24$	5.62	57.48	57.37	65.36	68.97
6.50	28	$474\pm54$	$523\pm58$	10.34	$269\pm30$	$297\pm32$	10.41	$3.08\pm0.35$	$3.40\pm0.38$	10.39	57.12	56.89	68.39	75.46
7.50	27	$495\pm56$	$544\pm55$	9.90	$278\pm36$	$302 \pm 42$	8.63	$3.71\pm0.42$	$4.08\pm0.42$	9.97	55.23	55.04	71.42	78.49
9.00	25	$448\pm47$	$479\pm48$	6.92	$250\pm27$	$273\pm29$	9.20	$4.03\pm0.42$	$4.31\pm0.43$	6.95	56.54	57.56	64.64	69.11
11.00	2	$346 \pm 38$	$377 \pm 47$	8.96	ND	$221 \pm 25$	ND	$3.80 \pm 0.42$	$4.15 \pm 0.52$	9.21	ND	61.90	49.92	54.39

"ND" meaning no data available.

Increase rate = (value of thermophilic condition-value of mesophilic condition)/value of mesophilic condition. Biogas conversion rate = specific biogas yield/theoretical biogas yield.









high solid content and a low moisture content, which hinder the conversion of VFAs (Veeken and Hamelers, 1999).

### The Performance at Thermophilic Condition

For the system operated at thermophilic condition, the volumetric biogas yields ranged from  $0.19 \pm 0.02$  to  $4.31 \pm 0.43$  L/(L·d) within the OLRs of 0.50-9.00 g VS/(L·d). Meanwhile the specific biogas and methane yields ranged in 370–553 and 214–302 mL/g VS, respectively, with a methane content of 51.81–60.09%. With respect to the parameters of the process, the pH was 6.84–7.99, and the concentrations of acetic acid and propionic

acid were <493 and 923 mg/L, respectively (**Figures 2A,B**). The TAN concentrations ranged between 180 and 2040 mg/L. The IA/PA ratio ranged in 0.11–0.42. These results indicated stable operation was achieved for the system operated at the OLRs of 0.75–9.00 g VS/(L·d).

Compared with the volumetric biogas yield obtained at the OLR of 9.00 g VS/(L·d), a slight decrease was observed at an OLR of 11.00 g VS/(L·d), coupled with a decrease of 21.29 and 19.05% in specific biogas and methane yields, respectively. In addition, higher concentrations in propionic acid (1921 mg/L) was observed, suggesting that an accumulation in VFAs had occurred due to overloading.

## DISCUSSION

# The Variation in Biogas Yield at Different OLRs and Temperature Conditions

One of the critical operational parameters of anaerobic digestion is OLR, which is determined by the material characteristics and operation conditions. Generally, improved biogas yields appeared with the OLRs increased. An optimum OLR is beneficial in reducing the capital cost of the plants, improving the biogas yield, and ensuring stability in operation (Tan et al., 2018). For both reactors operating at mesophilic or thermophilic conditions, the volumetric biogas yields increased with the OLRs, and obtained their maximum values at OLRs of 9.00 g VS/(L·d) (**Figure 4**); the performance then decreased due to overloading. The results indicated that the biogas yield increased with the OLRs within the appropriate range (Li et al., 2015; Shen et al., 2018).

Temperature is another key parameter which influences the biochemical conversion pathway, reaction rate, and input energy.



TABLE 3 | Comparison of total output energy between OLR of 7.5 and 9.0 g VS/(L-d) at mesophilic and thermophilic condition.

Items		OLR of 7	.5 g VS/(L·d)	OLR of 9.0 g VS/(L·d)			
		Mesophilic condition	Thermophilic condition	Mesophilic condition	Thermophilic condition		
Specific biogas yie	eld (mL/g VS)	495	544	448	479		
Me	ethane content (%)	55.23	55.04	56.54	57.56		
Superficial area of	reactor (m <sup>2</sup> )	1,151	1,151	1,151	1,151		
Number of reactors		4,622	4,622	3,852	3,852		
	Reactor heat loss (GWh/day)	6.28	11.36	5.23	9.47		
Specific biogas yiel Me Superficial area of t Number of reactors Input energy Output energy Total output energy Total output energy	Pumping (GWh/day)	$0.21 \times 10^{-3}$	$0.21 \times 10^{-3}$	$0.21 \times 10^{-3}$	$0.21 \times 10^{-3}$		
	Mixing (GWh/day)	$0.89 \times 10^{-3}$	$0.89 \times 10^{-3}$	$0.74 \times 10^{-3}$	0. 74 $\times$ 10 <sup>-3</sup>		
	Heating (GWh/day)	2.39	4.32	2.39	4.32		
Output energy	Thermal energy (GWh/day)	115.00	124.93	103.42	112.93		
	Electricity energy (GWh/day)	75.90	82.45	68.26	74.54		
Total output energy (GWh/day)		182.24	191.70	164.05	173.68		
Total output energy (GWh/year)		66515.94	69970.61	59879.92	63393.21		

The data is calculated according to section Preliminary Energy Analysis.

Generally, the optimum temperature is mesophilic  $(30-40^{\circ}C)$  or thermophilic  $(50-60^{\circ}C)$  (Hupfauf et al., 2018; Pearse et al., 2018). In this study, difference analysis showed that when the OLRs were 0.75-1.25 g VS/(L·d), the difference in specific biogas yields at mesophilic and thermophilic condition was not significant. When the OLRs were at 2.00-9.00 g VS/(L·d), the thermophilic reactor obtained higher specific biogas yields, with

the specific biogas yields increased by 4.13–19.91% compared to that of the mesophilic reactor. The biogas conversion rate showed similar results, which were 49.92–75.82% and 54.39–84.00% for mesophilic and thermophilic conditions, respectively. This might be related to metabolic activities of microorganisms which increased with the temperature increased (Lu et al., 2008; Ganesh Saratale et al., 2018).

# Preliminary Energy Analysis of OFMSW in China

According to the China Statistical Yearbook (State Statistical Bureau, 2015), total MSW generation was about 215,209 kilotons in 2017. From the view of total yield of MSW, the districts of Guangdong, Jiangsu, Shandong, and Zhejiang produces more than 10,000 kilotons per year (Figure 5A). From a perspective of density, that is yields per area, the district of Shanghai obtains the highest value of 1.18 kilotons/km<sup>2</sup>. While, the densities of Guangdong, Jiangsu, Shandong, and Zhejiang provinces were lower Shanghai, which were 0.15, 0.17, 0.10 and 0.14 kilotons/ km<sup>2</sup>, respectively. To obtain the organic fraction of MSW, several separation technologies have been established, such as water-assisted sorting treatment, and extrusion treatment. The extrusion treatment could potentially recover about 67% (w/w) of the organic fraction from the raw MSW (Mu et al., 2018). Accordingly, the mass available for anaerobic digestion would be  $\sim$ 144,123 kilotons.

Accordingly to the yields of OFMSW in China, the energy revenues at different temperatures and OLRs were analyzed (Table 3). The results showed that the maximum total output energy of 191.70 GWh/day was obtained at the OLR of 7.50 g VS/(L·d) and thermophilic condition. At the condition, the required number of reactors for digested OFMSW was 4,622, which was 20.99% more than that of OLR of 9.00 g VS/(L·d). The increase in number of reactors led to the increase of energy consumption in mixing and heat loss of reactors. However, the higher output energy of this condition makes up for this shortcoming. Compared to other scenarios, an OLR of 7.50 g VS/(L·d) and thermophilic condition generated more thermal energy (124.93 GWh/day) and electricity energy (82.45 GWh/day), which allows it to maintain the best total output energy under high energy consumption conditions. Therefore, the condition of an OLR of 7.50 g VS/(L·d) and thermophilic condition was recommended for the anaerobic digestion of OFMSW.

Based on the specific biogas yield at the OLR of 7.50 g VS/(L·d) and thermophilic condition of this study, the MSW produced in China every year could produce 16.52 billion m<sup>3</sup> of biogas. The thermal energy and electricity energy converted from biogas were 45599.00 GWh and 30095.34 GWh, respectively. The net total output energy is ~69970.61 GWh. Accodingly, the output energy varied with the yield of MSW (**Figure 5B**). Among them, the province of Guangdong had the largest energy production

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potential of 9305.69 GWh, with the output thermal and electricity energy of 5605.84 and 3699.85 GWh, respectively. Meanwhile, the districts of Jiangsu, Zhejiang and Shandong had the energy production potential of 6104.21, 5118.57, and 5599.60 GWh, respectively. Whereas, the potential in output energy of Hainan, Tibet, Gansu, Qinghai, and Ningxia was <1000.00 GWh.

# CONCLUSIONS

The semi-continuous experiments, under mesophilic and thermophilic conditions, showed that the anaerobic digestion of OFMSW was stable at OLRs of 0.75–9.00 g VS/(L·d). The volumetric biogas production increased with OLR during stable operation. At an OLR of 7.5 g VS/(L·d), the system exhibited the maximum specific biogas yield, recorded at 495  $\pm$  56 and 544  $\pm$  55 mL/g VS for mesophilic, and thermophilic conditions, respectively. Based on the annual quantity of OFMSW of 144,123 kilotons produced in China, the potential for biogas production is about 16.52 billion m<sup>3</sup>, corresponding to a net total output energy of 69970.61 GWh.

## DATA AVAILABILITY STATEMENT

The data used to support the findings of this study are available from the corresponding author upon request.

## **AUTHOR CONTRIBUTIONS**

JJ, SH, TX, and XK performed the experiments and analyzed the data. LL, YG, YS, and ZY designed the experiment, prepared and revised the manuscript.

## FUNDING

This work was supported financially by the Strategic Priority Research Program of the Chinese Academy of Sciences [Grand No. XDA21050400]; the Science and Technology Planning Project of Guangdong Province [Grant No. 2017A050501049].

## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: https://www.frontiersin.org/articles/10.3389/fenrg. 2020.00089/full#supplementary-material

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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