



# Gradual Pre-eruptive Phase of Solar Coronal Eruptions

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Physical background of the evolution of a coronal magnetic flux rope embedded in the magnetic arcade during the gradual-rise pre-eruptive stage is studied. It is assumed that this stage represents an externally-driven evolution of the pre-eruptive structure through a series of quasi-equilibrium states, until a point when the system loses equilibrium and erupts due to unbalanced internal forces. In particular, three driving processes are considered: twisting motions of the flux-rope footpoints, emergence of new magnetic flux beneath the flux rope, and the mass leakage down the flux-rope legs. For that purpose, an analytical flux-rope model is employed, to inspect how fast the equilibrium height of the structure rises due to the increase of the poloidal-to-axial field ratio, the increase of axial electric current, and the decrease of mass. It is shown that the flux-rope twisting itself is not sufficient to reproduce the rising speeds observed during the pre-eruptive stage. Yet, it is essential for the loss-of-equilibrium process. On the other hand, the considered emerging flux and the mass loss processes reproduce well the rate at which the pre-eruptive structure rises before the main acceleration stage of the eruption sets in.

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## 1. INTRODUCTION

There is a general consensus that solar eruptions, which lead to coronal mass ejections (CMEs) and are frequently associated with solar flares, are a consequence of instability of coronal structures, most often considered to be coronal magnetic arcades embedding a helically twisted magnetic flux rope (for a review see, e.g., Schmieder et al., 2015; Green et al., 2018). Basically, there are three different scenarios that can explain the presence of the flux rope within the eruptive structure: (i) an already-formed flux rope emerged from the subphotospheric layers; (ii) rope is formed gradually by a series of reconnections within a sheared arcade; (iii) it forms during the eruption itself (e.g., Green et al., 2018, and references therein). In this paper a situation where the flux rope exists already prior to the eruption (i.e., the mentioned first two options) will be studied to get an insight into physical background of the evolution of the pre-eruptive arcade/flux-rope structure.

Most of eruptions show three basically different stages: a gradual pre-eruptive stage, main acceleration stage, and the propagation stage (e.g., Vršnak, 2001; Zhang et al., 2001, 2004; Chen, 2011; Mierla et al., 2013; D’Huys et al., 2017). The pre-eruptive stage, which is the main objective of this paper, most briefly can be described as externally-forced evolution of the pre-eruptive system through a series of equilibrium states until a stage when the system comes to the point when no equilibrium of forces is possible anymore (e.g., Priest, 1982; Vršnak, 1990; Green et al., 2018, and references therein). After that the system finds itself in an instability regime, dynamically erupting in trying to find a new equilibrium state. Such type of evolution is usually denoted as loss-of-equilibrium scenario. A critical height where the system loses equilibrium

and starts rapidly accelerating is usually comparable with the flux-rope footpoint half-separation (for the observations see, e.g., Vrřnak, 1990; Chen et al., 2006, for the theoretical aspect see, e.g., Vrřnak 1990; Chen and Krall 2003; Chen et al. 2006).

From the observational point of view, the pre-eruptive stage, often called also a gradual-rise phase, is characterized by a number of different signatures. Frequently, the new magnetic flux emergence, shearing/twisting motions, and flux cancellation are observed (e.g., Schmieder et al., 2015; Green et al., 2018, and references therein). At the same time the pre-eruptive structure slowly rises at a low almost-constant velocity, and shows signatures of swelling (e.g., Tandberg-Hanssen, 1974; Vrřnak et al., 1993; Marićić et al., 2004; Veronig et al., 2018), appearance of helical structures within the prominence (e.g., Tandberg-Hanssen, 1974; Sakurai, 1976; Vrřnak et al., 1988, 1991, 1993; Rompolt, 1990; Romano et al., 2003; Ali et al., 2007), and mass-draining down the footpoints (e.g., Tandberg-Hanssen, 1974; Rust et al., 1975; Vrřnak et al., 1987, 1993).

In this paper we analyze the influence of these processes on the evolution of the pre-eruptive system, focusing on the effects of the flux rope twisting, electric current increase, and the mass loss. The following analysis of these effects is based on the analytical semi-toroidal flux-rope model employed by Vrřnak (2008), Vrřnak (2016), and Green et al. (2018), where mainly a quantitative analysis of the acceleration stage of eruptions was considered. In contrast, this paper is focused on a quantitative study of characteristics of the pre-acceleration stage.

## 2. KINEMATICS OF THE GRADUAL-RISE PHASE

In **Figure 1** the kinematics of a limb CME that erupted on May 15, 2001 is presented (for details see, Marićić et al., 2004), to illustrate a typical example of the height–time evolution of the eruption (see, e.g., Tandberg-Hanssen, 1974, and references therein). The height–time measurements of the frontal rim, the top of the cavity, and the top of the embedded prominence are displayed in **Figure 1A**, whereas the corresponding velocity–time graph is shown in **Figure 1B**. In both graphs the gradual-rise phase and the impulsive acceleration stage are indicated.

In **Figure 2** the gradual-rise phase of the prominence is shown enlarged. The measured velocity slowly increases from 5 to 15 km s<sup>-1</sup>, within  $\Delta t \sim 2$  h, which corresponds to a very weak acceleration on the order of  $\sim 1$  m s<sup>-2</sup>. In the following, effects of the flux-rope twisting, external flux emergence, and mass loss will be considered, to find out if these processes can explain the described flux-rope behavior.

## 3. FLUX-ROPE MODEL

For the previously mentioned purpose, let us apply the semi-toroidal flux-rope model (**Figure 3**) proposed by Vrřnak (1990) and elaborated by Vrřnak (2008), Vrřnak (2016), and Green et al. (2018), to study the effects of the increase of the flux-rope twist, the increase of the flux-rope electric current, and the mass leakage through the flux-rope legs (the former two

processes are illustrated schematically in **Figure 4**). A simplified equation of motion, relevant for the processes which are essential for comprehending processes that govern the gradual-rise phase, can be expressed in the form that defines the force per unit mass (i.e., acceleration):

$$a = \frac{C_L}{\Lambda} \left[ \frac{1}{2R_t} - \frac{1}{R_t X^2} + \frac{1}{Z} \right] - \frac{C_c}{\Lambda^2 R_t}. \quad (1)$$

where  $\Lambda$ ,  $R_t$ , and  $Z$  are the length of the flux rope axis, major radius of the torus, and the height of its summit, all normalized with respect to the footpoint half-separation  $d$  [ $\Lambda = \lambda/d$ ,  $R_t = \hat{R}_t/d$ ,  $Z = z/d$ ; for symbols see **Figure 3**; see also (Vrřnak, 2008; Green et al., 2018)], whereas  $X$  represents the ratio of the poloidal and axial flux-rope field  $X \equiv B_\phi/B_\parallel$  at the flux-rope surface. The first two terms in brackets on the right-hand side of Equation (1) represent the so called “hoop force” (Chen, 1989), whereas the third term is due to the diamagnetic effect (Kuperus and Raadu, 1974). The last term represents the Lorentz force related to the background arcade magnetic field.

The expressions for the parameter  $C_L$  and  $C_c$  read:

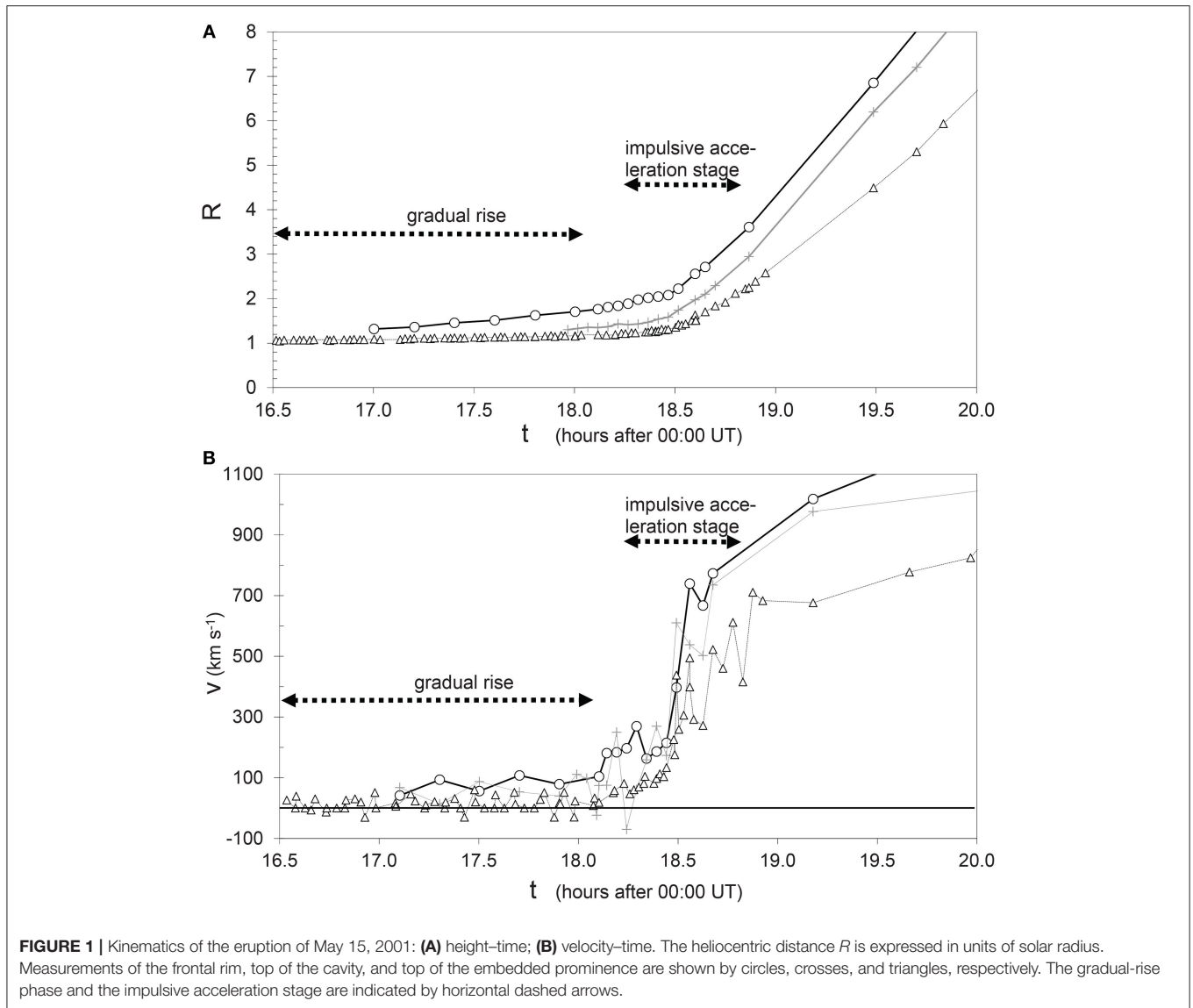
$$C_L = \frac{\mu_0 I_\parallel^2 \pi}{4M}, \quad (2)$$

$$C_c = \frac{I_\parallel B_c \pi^3 d}{M}, \quad (3)$$

respectively. Here,  $I_\parallel$  and  $M$  represent the axial electric current and total mass within the flux rope, respectively,  $B_c$  is the background arcade field and  $\mu_0$  stands for the permeability.

Note that  $a$ ,  $C_L$ , and  $C_c$  are expressed in m s<sup>-2</sup>, and that in Equation (1) the drag force and gravity are neglected. Details of derivation of Equation (1) can be found in Vrřnak (2008) and Green et al. (2018).

The geometrical quantities  $\Lambda$ ,  $R_t$ , and  $Z$  are mutually related, i.e.,  $\Lambda \equiv \Lambda(Z)$  and  $R_t \equiv R_t(Z)$ . Taking approximately that the flux-rope axis remains a part of the circle with fixed footpoint separation  $2d$ , and inspecting **Figure 3**, where the angle  $\zeta$  is introduced, one finds simple parametric relationships:  $R_t = 1/\cos\zeta$ ,  $Z = (1 + \sin\zeta)/\cos\zeta$ , and  $\Lambda = (\pi + 2\zeta)/\cos\zeta$ . Thus, at given values of  $C_L$  and  $X$ , Equation (1) in fact defines  $a$  as a function of  $Z$ ,  $a \equiv a_{C_L, X}(Z)$ . For low values of  $X$  and  $C_L$ , the structure is stable ( $da/dZ < 0$ ) and has only one equilibrium height  $Z_s$ , where  $a_{C_L, X}(Z_s) = 0$  (e.g., black curve in **Figure 5A**). As  $X$  or  $C_L$  increase, the equilibrium height rises and the shape of  $a(Z)$  transforms, which is illustrated in **Figure 5**. To distinguish what are the effects of increasing  $X$  and  $C_L$ , the graphs  $a(Z)$  are shown separately for the case when the evolution of the system is driven by increasing  $X$ , and analogously, by increasing  $C_L$ . The former option is presented in **Figures 5A, B**, where the graph in **Figure 5B** shows an enlarged part of **Figure 5A** around the stable-equilibrium. Analogous graphs are displayed in **Figures 5C, D** for the effect of increasing  $C_L$ , where the increase of  $C_L$  can be either due to the increasing current  $I_\parallel$  or decreasing mass  $M$  [see Equation (2)]. In **Figure 5D**, the stable-equilibrium heights are explicitly denoted as  $Z_1 - Z_4$ , and the height at which



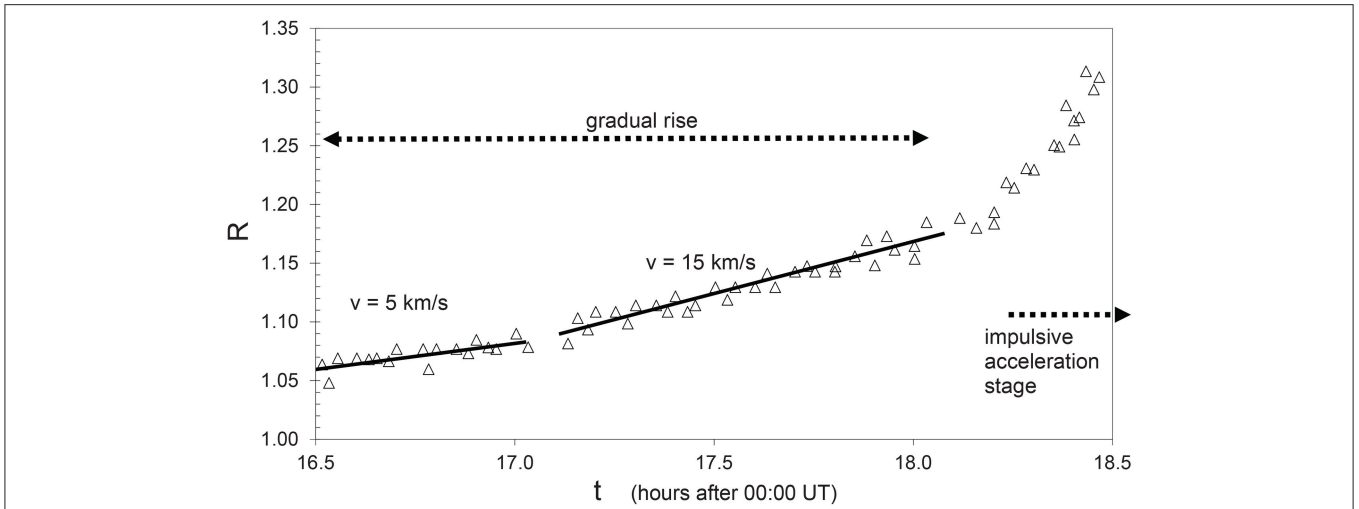
the system loses equilibrium as  $Z^*$  (red curve). In the insets of **Figures 5B,D** the change of the stable-equilibrium height  $Z_s(X)$  and  $Z_s(C_L)$  is presented, respectively, all the way to the state when the system loses equilibrium (marked by a square symbol).

Inspecting **Figure 5**, one finds that by increasing  $C_L$  and/or  $X$ , first the  $a(Z)$  curve evolves into a shape where another equilibrium point occurs  $Z_u$ . However, this one is unstable (green, yellow, and blue curves in **Figures 5A,C**), since  $da/dZ > 0$ . Thus, in this stage the structure is metastable, since if pushed from a stable equilibrium height  $Z_s$  to a height above the unstable-equilibrium height  $Z_u$ , it will erupt, because beyond this height the acceleration becomes  $a(Z) > 0$  for any  $Z > Z_u$ .

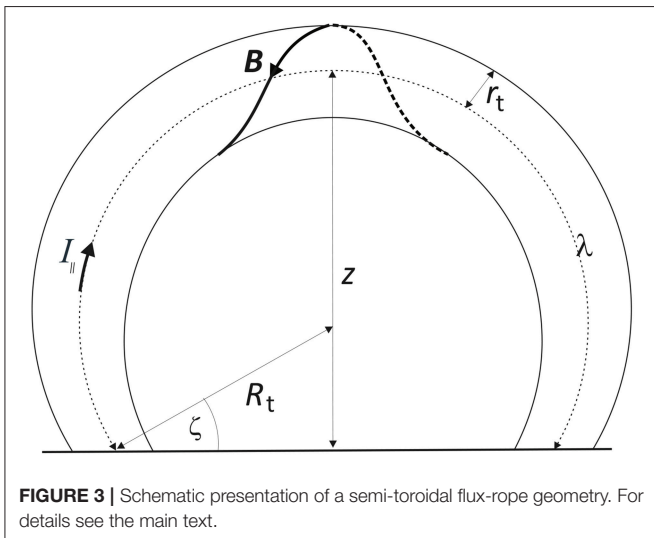
In other words, **Figure 5** shows that the increase of  $C_L$  or  $X$  implies rising of  $Z_s$ , and in the following this will be considered as a cause of the gradual rise of the pre-eruptive structure. Furthermore, one finds out that the unstable equilibrium height  $Z_u$  descends, so the distance between  $Z_s$  and  $Z_u$  decreases,

implying that the structure becomes more and more unstable, since weaker and weaker push is required to move the structure from the stable to the unstable equilibrium point. Eventually, at a given critical combination of  $C_L$  and  $X$ , the stable and unstable heights merge,  $Z_u = Z_s$ , meaning that there is no equilibrium existing any more, i.e., equilibrium state is lost and the structure erupts ( $a(Z) > 0$  for any  $Z$ ; see red curve in **Figures 5A–D**).

In the following, Equation (1) will be employed to inspect the effects of the increasing  $C_L$  and  $X$ , as generally illustrated in **Figure 5**, by specifically considering the two processes depicted in **Figure 4**. These are twisting motions at the flux-rope footpoints (e.g., Török et al., 2013, and references therein) and emerging-flux process (e.g., Schmieder et al., 2015, and references therein). The former process leads to the increase of  $X$ , whereas the latter one directly induces an increase of the current  $I_{\parallel}$ , i.e., increases the value of the parameter  $C_L$ . It should be noted that the change of  $X$  causes also a change of  $I_{\parallel}$ , whereas the change of



**FIGURE 2** | Detailed kinematics of the gradual-rise phase of the eruptive prominence shown in **Figure 1A**.



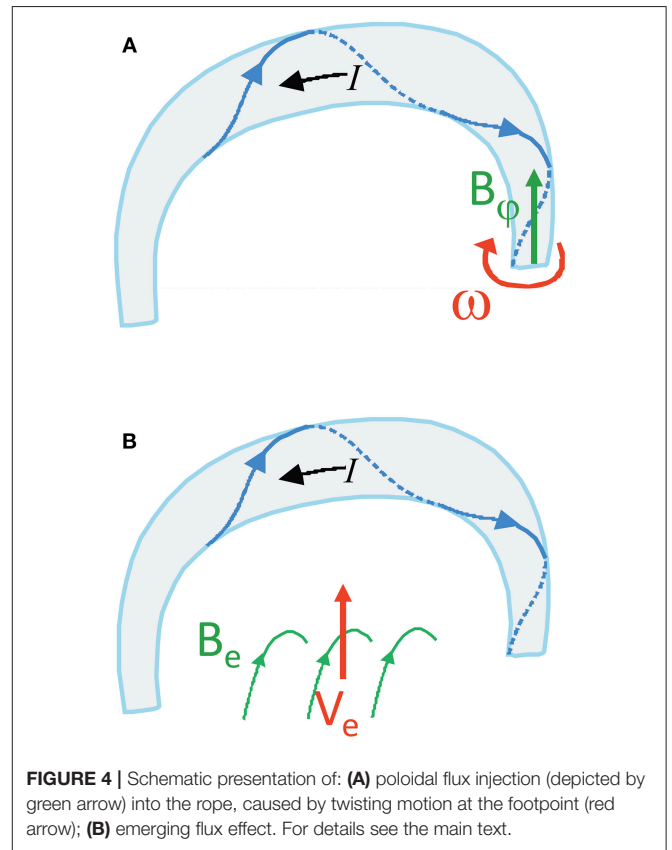
**FIGURE 3** | Schematic presentation of a semi-toroidal flux-rope geometry. For details see the main text.

$I_{\parallel}$  causes also the change of  $X$ , i.e., the behaviors of  $X$  and  $C_L$  are tightly physically related. Finally, note that from the point of view of Equation (1), the mass loss related to the material draining down the prominence legs is equivalent to the increase of axial electric current  $I_{\parallel}$  related to emerging flux and/or twisting processes, since the mass loss also increases the value of  $C_L$  [see Equation (2)].

## 4. RESULTS

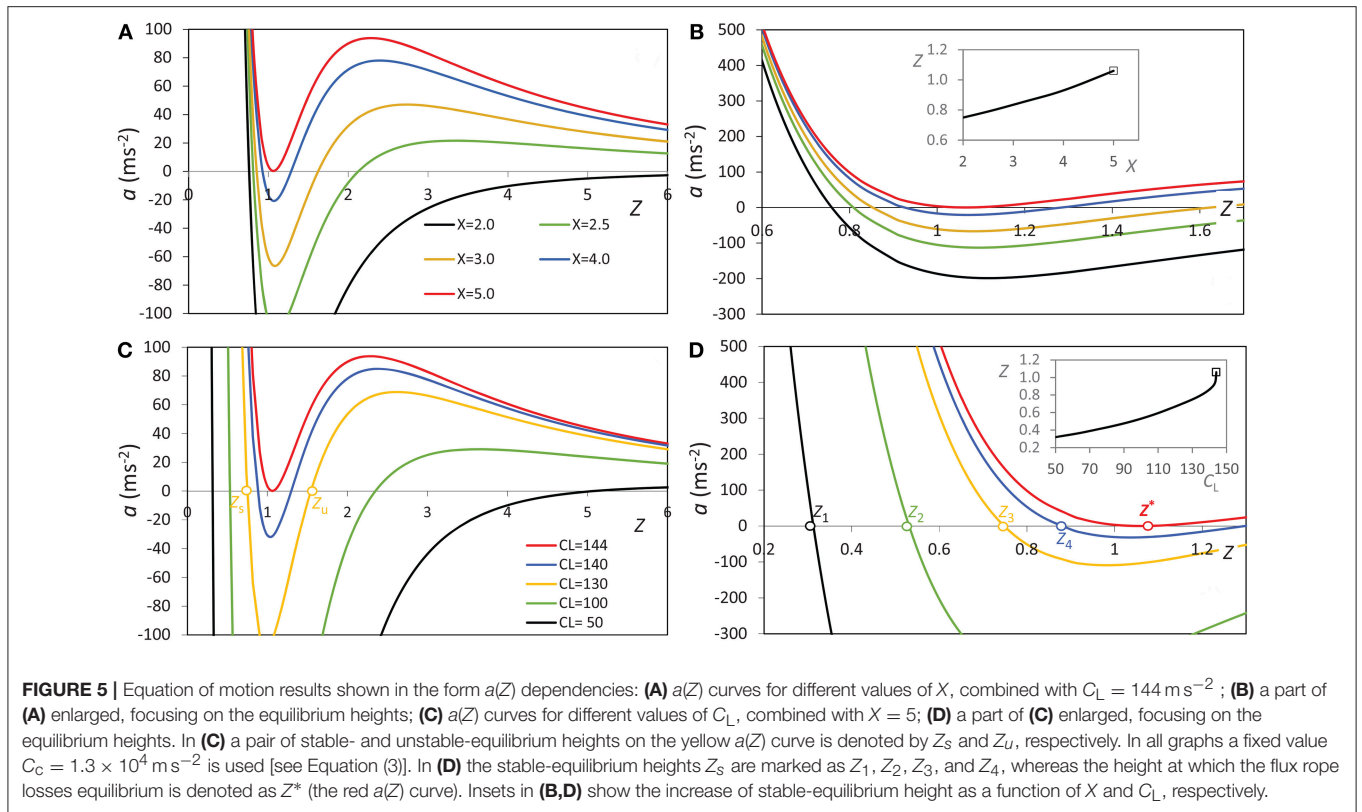
### 4.1. Poloidal Flux Injection

In **Figure 6** the effect of increasing poloidal flux caused by twisting motion at one of the flux-rope footpoints is illustrated for two initial  $C_L$  values, 145 and 150  $\text{m s}^{-2}$ , respectively, combined with two values of the normalized flux-rope initial minor radius,  $r/d = 0.1$  and 0.2, where in all combinations the



**FIGURE 4** | Schematic presentation of: **(A)** poloidal flux injection (depicted by green arrow) into the rope, caused by twisting motion at the footpoint (red arrow); **(B)** emerging flux effect. For details see the main text.

flux-rope footpoint half-separation is taken as  $d = 50$  Mm and the axial field as  $B_{\parallel} = 100$  G. The presented cases correspond to the longitudinal magnetic flux of  $\Psi_{\parallel} \approx 0.8 \times 10^{20}$  Mx (red curve) and  $\Psi_{\parallel} \approx 3 \times 10^{20}$  Mx (gray and blue curve), as listed in 7th column of **Table 1**.



Note that the values of the parameter  $C_L$  and  $r/d$  are not kept fixed, but they evolve due to change of the poloidal flux. The evolution of  $C_L$  is followed by taking into account that the poloidal flux and the axial current scale as  $\Psi_\phi \propto B_\phi r \lambda$  and  $I_\parallel \propto B_\phi r$ , respectively, where  $B_\phi$  is the poloidal field at the flux-rope boundary. From this one finds  $\Psi_\phi \propto I_\parallel \lambda$ , i.e.,  $I_\parallel \propto \Psi_\phi / \lambda \propto \Psi_\phi / \Lambda$ . Substitution of this relation to Equations (2, 3) defines the evolution of  $C_L$ . Setting  $a = 0$  in Equation (1) and taking into account the expressions for  $C_L(\Psi_\phi, \Lambda)$  and  $C_L(\Psi_\phi, \Lambda)$ , Equation (1) becomes an implicit relation that defines the equilibrium value of the angle  $\zeta$  as a function of prescribed values of  $X$ , i.e.,  $\Psi_\phi$ . The solution of this equation, giving the equilibrium  $\zeta$ , then provides also the equilibrium values of  $R_t$ ,  $z$ , and  $\lambda$ , as well as the equilibrium value of  $I_\parallel$ . In a similar manner, the evolution of the torus minor radius  $r$  can be traced. From the poloidal-to-axial flux ratio  $\Psi_\phi / \Psi_\parallel \propto (B_\phi r \lambda) / (B_\parallel r^2)$  one finds  $r \propto X \lambda \Psi_\parallel / \Psi_\phi$ . Since the rotational motions at the footpoints do not affect  $\Psi_\parallel$  and thus it stays constant, the value of  $r$  scales as  $r \propto X \lambda / \Psi_\phi$ , where the evolution of  $X$  and  $\Psi_\phi$  is prescribed as the input.

For the twisting motion, i.e., rotational motion at one of footpoints (illustrated in **Figure 4A**), a typical value of  $\omega = 100 \text{ deg/day}$  (e.g., Török et al., 2013, and references therein) is applied to the flux rope characterized by the initial value  $X_1 = 3.5$  (blue curve in **Figure 6**) and 4.5 (red and gray curves in **Figure 6**). The twisting motion increases the poloidal flux, and consequently changes the value of  $X$ . The change of the parameter  $X$  can be expressed as  $dX/dt = \omega r / \lambda$ , where  $\lambda$  represents the

length of the flux-rope axis. Since the poloidal and axial flux are related as  $\Psi_\phi = \Psi_\parallel \lambda X / 2r\pi$ , the rate at which the poloidal flux increases,  $d\Psi_\phi/dt$  can be calculated (the corresponding values are shown in Column 9 of **Table 1A**). Other relevant informations related to the graphs displayed in **Figure 6** are presented in the upper part of **Table 1**, where the first column identifies the curves in **Figure 6**. The duration of the pre-eruption interval,  $\Delta t$  over which the changes are followed is shown in Column 2. The height and speed of the flux-rope axis at the beginning of the interval ( $z_1$  and  $v_1$ ) are presented in Columns 3 and 5, respectively, whereas the height and speed at the onset of the eruption ( $z_2$  and  $v_2$ ) are given in Columns 4 and 6, respectively. The values of the axial and the initial poloidal flux are presented in the Columns 7 and 8. The rate by which the poloidal flux is changing due to the twisting motion at the flux-rope footpoint is displayed in Column 9, its total change over the interval  $\Delta t$  is presented in Column 10, and the relative change, expressed in percentages, is given in Column 11. The last two columns show the corresponding relative change of the parameter  $C_L$  and the flux-rope minor radius  $r$ , both presented in percentages.

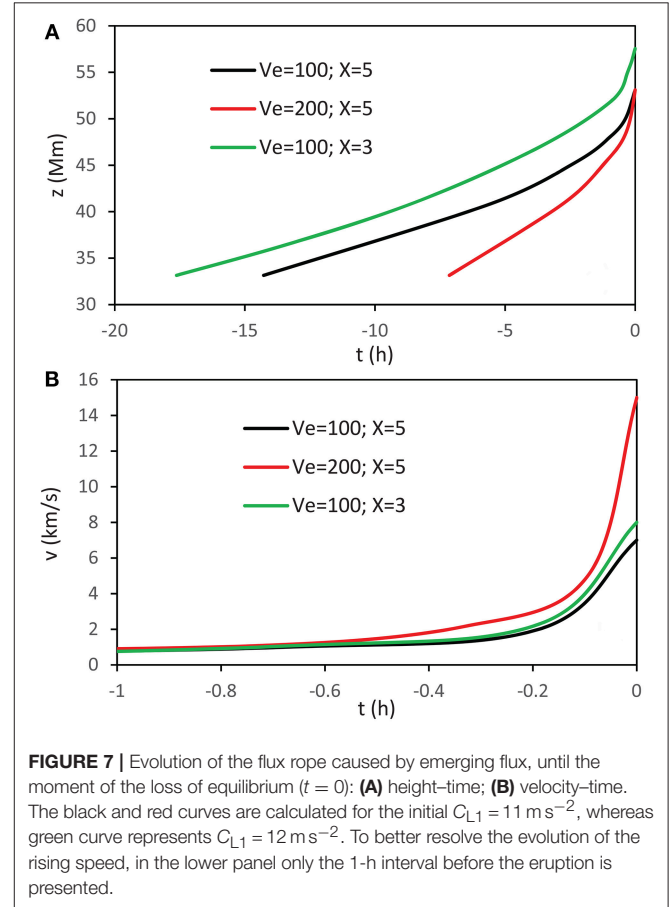
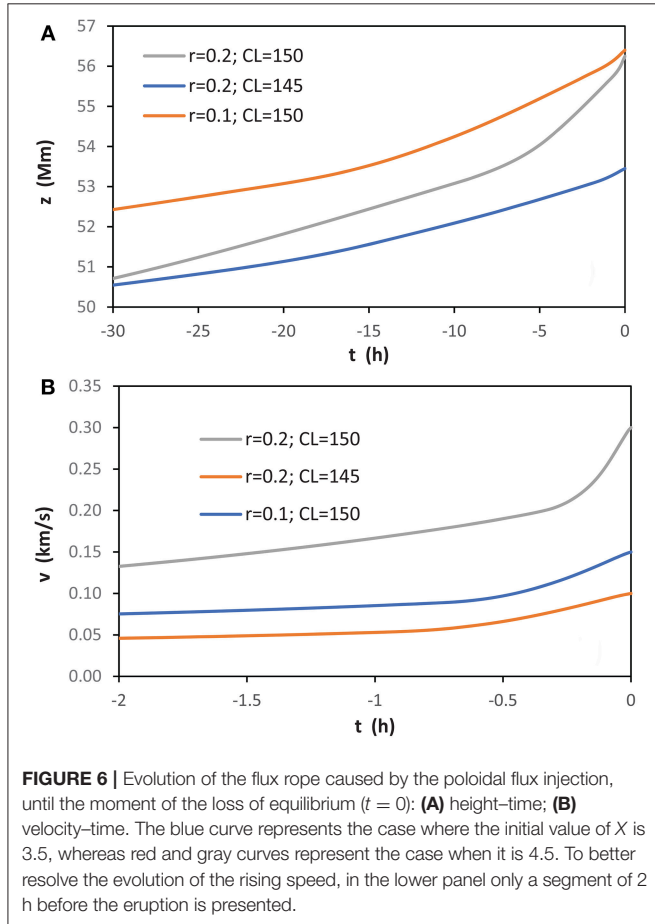
The graph of the gradual-rise velocity presented in **Figure 6B** shows that the twisting motion itself cannot explain the characteristics of the gradual-rise pre-eruptive phase, since the obtained velocities are for at least an order of magnitude too low. Yet, note that the increase of  $X$  is important in reaching the critical loss-of-equilibrium state (see **Figures 5A,B**).



## 4.2. Increase of $C_L$ (Emerging Flux Process or Mass Loss)

In **Figure 7** the evolution caused by increasing value of  $C_L$ , which can either be due to the increasing electric current in the flux

rope, or the mass draining down the flux-rope legs, is illustrated. Particulary, in the following the increase of current is attributed to the emerging flux along the magnetic inversion line beneath the flux rope (**Figure 4B**). The change of the magnetic flux  $\Psi_e$  encircled by the flux-rope current channel causes the increase



**TABLE 1** | Comparison of the footpoint-twisting process and the emerging-flux process.

<b>(A) POLOIDAL-FLUX INJECTION (FOOTPOINT TWISTING)</b>												
Curve in Figure 6	$\Delta t$ (h)	$z_1$ (Mm)	$z_2$ (Mm)	$v_1$ (km/s)	$v_2$ (km/s)	$\Psi_{  }$ (Mx)	$\Psi_{\phi 1}$ (Mx)	$d\Psi_{\phi}/dt$ (Mx/s)	$\Delta\Psi_{\phi}$ (Mx)	$\Delta\Psi_{\phi}$ %	$\Delta C_L$ %	$\Delta r$ %
Red	20	53.1	56.4	0.016	0.10	$7.9 \times 10^{19}$	$2.6 \times 10^{21}$	$1.8 \times 10^{15}$	$1.3 \times 10^{20}$	5.0	1.4	< 1
Gray	20	53.2	56.3	0.030	0.30	$3.1 \times 10^{20}$	$5.2 \times 10^{21}$	$3.6 \times 10^{15}$	$2.6 \times 10^{20}$	5.0	1.4	< 1
Blue	20	52.0	53.5	0.027	0.15	$3.1 \times 10^{20}$	$6.7 \times 10^{21}$	$2.1 \times 10^{15}$	$1.5 \times 10^{20}$	2.2	1.1	< 1
<b>(B) EMERGING FLUX</b>												
Curve in Figure 7	$\Delta t$ (h)	$z_1$ (Mm)	$z_2$ (Mm)	$v_1$ (km/s)	$v_2$ (km/s)	$\Psi_{  }$ (Mx)	$\Psi_{e1}$ (Mx)	$d\Psi_e/dt$ (Mx/s)	$\Delta\Psi_e$ (Mx)	$\Delta\Psi_{\phi}$ %	$\Delta C_L$ %	$\Delta r$ %
Red	10	31.2	53.2	0.35	15.1	$7.9 \times 10^{19}$	$5.0 \times 10^{21}$	$2.0 \times 10^{16}$	$5.7 \times 10^{21}$	54.4	57.2	86.7
Black	10	37.1	53.1	0.27	7.1	$7.9 \times 10^{19}$	$5.0 \times 10^{21}$	$1.0 \times 10^{16}$	$5.4 \times 10^{21}$	26.4	53.6	92.4
Green	10	39.2	57.6	0.26	7.9	$7.9 \times 10^{19}$	$5.0 \times 10^{21}$	$1.0 \times 10^{16}$	$5.4 \times 10^{21}$	33.7	53.6	92.4

In the first column the identification of the curves displayed in **Figures 6, 7** is defined.  $\Delta t$  represents the time interval prior to the eruption over which the changes of the parameters presented in the rest of the table are followed. Subscript “1” denotes the values at the beginning of the interval, whereas the subscript “2” represents the values at the onset of the eruption. For details see the main text.

of the flux-rope current, due to the relation  $d\Psi_e/dt = \mu_0 dI_{\parallel}/dt$  (see e.g., Batygin and Toptygin, 1962; Jackson, 1998), implying also the change of  $I$ , i.e.,  $C_L$ . Note that the change of  $I$  leads also to change of  $\Psi_{\phi}$ ,  $X$ , and  $r$ , which can be followed employing a procedure analogous to that presented in section 4.1 for the evolution of  $I$  and  $r$ , where the change of  $\Psi_{\phi}$  was used as the input.

Let us consider a situation where the magnetic field of  $B_e = 100$  G emerges (see the sketch in **Figure 4B**) at the speed of  $V_e = 100$   $\text{m s}^{-1}$  (black and green curves in **Figure 7**) and  $V_e = 200$   $\text{m s}^{-1}$  (red curve in **Figure 7**), which implies that the external unit-length magnetic flux increases at the rate  $d\Psi_e/dt = B_e V_e = 1$  and  $2 \times 10^6$   $\text{Mx s}^{-1} \text{cm}^{-1}$ , respectively. Assuming that the flux emerges over the distance of  $2d = 100$  Mm, one finds that the rate at which the magnetic flux encircled by the flux-rope,  $\Psi_e$ , increases as listed in Column 9 of **Table 1B** ( $d\Psi_e/dt$ ). The total increase of  $\Psi_e$  over the time of  $\Delta t = 10$  h is shown in Column 10. Taking for the initial flux encircled by the flux rope the value of  $\Psi_{e1} = 10^{12}$   $\text{Mx cm}^{-1}$  (Column 8 in **Table 1B**), and the initial value  $C_{L1} = 11$   $\text{m s}^{-2}$  (black and red curves in **Figure 7**) and  $12$   $\text{m s}^{-2}$  (green curve in **Figure 7**), one gets the relative change of  $\Psi_{\phi}$ ,  $C_L$ , and  $r$ , as displayed in the last three columns of **Table 1B** (all expressed in percentages).

**Figure 7B** shows that at the stage when the system approaches the loss-of-equilibrium point, the rise caused by increasing  $C_L$  results in rise-velocities on the order of  $10$   $\text{km s}^{-1}$ , which is compatible with observations (**Figure 2**). Comparing **Figure 7B** with **Figure 6B** one finds that the rise related to the emerging flux process is more than an order of magnitude faster than that related to the poloidal flux injection.

## 5. DISCUSSION AND CONCLUSION

In the presented analysis three processes relevant for the evolution of the pre-eruptive structure during the gradual-rise phase are considered. In particular, we focused on the height-time and velocity-time evolution, to compare it with typical behavior usually observed during the gradual-rise stage.

The first process is twisting motion at the flux-rope footpoint, which leads to the increase of the flux-rope twist, indirectly enhancing also the axial electric current and minor radius of the flux rope at its summit, causing the rise of the pre-eruptive structure. All of these signatures drive the pre-eruptive system toward a point where the structure loses its equilibrium and erupts. However, the considered twisting process is not effective enough to cause a sufficiently fast rise of the pre-eruptive structure, i.e., its rise is for at least an order of magnitude slower than observed. Note that the three examples presented in **Figure 6** cover typical values coming from observations, and even increasing the parameter-values related the poloidal flux injection (including much too-high values) could not result in sufficiently high pre-eruptive rising speeds.

The second process is related to the emergence of a new magnetic flux beneath the flux rope. This causes an increase of the magnetic flux encircled by the flux rope, which induces an increase of the electric current flowing along the rope. The increase of the current causes also the increase of the flux-rope twist and its minor radius. The analysis has demonstrated that this process results in the rise of the pre-eruptive structure that is faster than in the case of twisting for almost two orders of magnitude, and is compatible with observations. This process is more effective than the footpoint twisting, since the emerging flux occurs on the spatial scale comparable with the flux-rope length, whereas the footpoint twisting is restricted to the footpoint radius, and that is generally an order of magnitude smaller than the flux-rope length. This results in an order of magnitude larger change of poloidal flux caused by the emerging flux (see **Table 1**). Note also that the processes like flux cancellation and other various forms of reconnection beneath the flux rope, as well as the converging motions of the arcade footpoints, can result in the same effects as described emerging flux process.

The third process, the mass leakage down the flux-rope legs, results in the pre-eruptive rise similar to that caused by the emerging flux process, except that the mass loss does not cause the increase of the flux-rope twist. Although the draining of the cold plasma from the embedded prominence is most prominent during the acceleration stage of the eruption, it is frequently observed already during the gradual-rise phase. This is caused by stretching of the flux rope as it rises, which makes the magnetic dips containing dense prominence plasma successively shallower, i.e., certain fraction of the prominence material is no longer supported against the gravity. Thus, the rise of the pre-eruptive structure caused by emerging flux is likely to be additionally enhanced by the mass-loss effect, making the pre-eruptive rise even faster than shown in **Figure 7**.

To conclude, the enhancement of the flux-rope electric current, the increase of the twist, and the mass loss, are tightly related phenomena, expected to occur during the gradual pre-eruptive phase of an eruption. Combination of these three processes is sufficiently effective to explain the nature of the gradual rise of the pre-eruptive structure and its evolution to the loss-of-equilibrium point.

## AUTHOR CONTRIBUTIONS

The author confirms being the sole contributor of this work and has approved it for publication.

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**Conflict of Interest Statement:** The author declares that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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