



Characteristics of Shale Pores and Surfaces and Their Potential Effects on the Fluid Flow From Shale Formation to Fractures

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Li X, Cai J, Gao B, Long S, Feng D, Peng Z and Guo B (2021) Characteristics of Shale Pores and Surfaces and Their Potential Effects on the Fluid Flow From Shale Formation to Fractures. Front. Earth Sci. 9:751543. doi: 10.3389/feart.2021.751543 Fluid flow is critical for the efficient exploitation of shale resources and can be split into two stages: the flow in the artificial fractures and, more importantly, the flow from shale formations to the artificial fractures. In this study, X-ray diffraction, N₂ adsorption, mercury intrusion, and ethylene glycol monoethyl ether adsorption were conducted on the shales collected from Es_3^{middle} , Es_3^{lower} , and Es_4^{upper} sub-members in the Dongying Sag to reveal the potential effects of the characteristics and properties of pores and surfaces on the fluid flow in shale formations. The results are indicated as follows: 1) The shales from Es3^{middle} and Es₃lower contain more I/S and detrital minerals but less illite and carbonate minerals than those of Es_4^{upper} . 2) The shales from Es_3^{middle} and Es_3^{lower} are mainly composed of smaller pores present in larger surface areas and lead to the steeper slope between the BrunauerEmmettTeller specific surface area (BET-SSA) and pore volumes. 3) Clay minerals mainly contribute to pore development, and carbonate minerals inhibit pore development. All kinds of surface areas (especially the inner surface area) are sourced by clay minerals, while I/S and illite present opposite effects. 4) Pore size and surface properties affect significantly the fluid flow in shale formations. The shales from Es_4^{upper} are the favorable interval for shale oil accumulation and flow, especially for the shales with depth ranges of 3360~3410 m, which possess high carbonates, illite and total organic carbon content, low clay mineral content, large pore volume, high large pore content, and small surface areas. Additionally, fluid composition needs to be paid more concern in the future.

Keywords: pore characteristics, surface characteristics, mineral composition, interfacial interaction, fluid flow

INTRODUCTION

Hydraulic fracturing is one of the most important technologies for the successful exploitation of unconventional oil and gas resources with ultra-low porosity and permeability, especially for shale resources (Osiptsov, 2017; Wang and Sheng, 2017; Lu et al., 2018; Aadnøy and Looyeh, 2019; Yang and Guo, 2019; Lu et al., 2020; Shi et al., 2020; Xie et al., 2020; Wang et al., 2022). One of the key concerns of the exploitation of shale resources is the evaluation of the production performance after fracturing (Jarvie et al., 2007; Wang and Gale, 2009; Jin et al., 2014; Tang et al., 2019; Wei et al., 2020). Previous studies have observed that the fracturing fluids interact significantly with minerals and

change their properties such as wettability, morphology, composition, water-bearing properties, and cation exchange capacity (CEC) (Chen et al., 2016; Chen et al., 2018a; Chen et al., 2018b; Lu et al., 2018; Sari et al., 2019; Zeng et al., 2019), leading to problems such as low flowback recovery of fracturing fluids, environment hazard, hydration, expansion, and rheology of clay minerals (O'Brien and Chenevert, 1973; Makhanov et al., 2014; Al-Ameri et al., 2018; Sui et al., 2018; Aadnøy and Looyeh, 2019; Zeng et al., 2019) and will impact seriously on the production progress. Therefore, to better understand the mechanisms of these problems and their potential effect on production performance, a detailed analysis of the characteristics of shale pores and surface structures and their potential interactions with the fracturing fluids and the confined fluids in shale formations is of great significance.

The fluid flow after hydraulic fracturing in the shales can be divided into two stages: the flow from shale formations to the fractures and the flow in the fractures. Because the ultimate and the most important purpose of hydraulic fracturing is to release oil and gas occluded in pores or adsorbed on surfaces as much as possible, the former stage is more important and is affected more significantly by pore and surface attributes. The international union of pure and applied chemistry (IUPAC) classified the pores into micropore (<2 nm), mesopore (2~50 nm), and macropore (>50 nm) according to the pore size, adsorption properties, and capillary condensation (Sing, 1985). Shale presents pores with a wide diameter range, and the capillary pressure that relates closely to fluid flow differs according to the pore size if the properties of pore walls are the same. More importantly, the fluid flow in nanopores and the space close to surfaces do not follow Darcy's law because of the strong interactions between fluids and pore walls (Zeng et al., 2011; Wang et al., 2015; Wang Z. et al., 2016; Wang and Sheng, 2017; Yu et al., 2017; Song et al., 2018; Cheng et al., 2019). Pore walls are constructed by minerals or organic matter (OM) that presents significant divergences in their physical and chemical properties. Differences in the origin of the pores result in the differences in the morphology, size, and attributes of pore walls (surfaces). For example, the pores formed by plate-like clay minerals tend to be slit-like (Curtis et al., 2012; Kuila and Prasad, 2013; Mathia et al., 2016); micropores and small mesopores are mainly related to clay minerals and organic matter (Chalmers and Bustin, 2008; Klaver et al., 2012; Zhang et al., 2012; Kuila and Prasad, 2013; Kuila et al., 2014). Therefore, the distribution of confined fluids differs greatly according to the shale pore structure and surface properties, which are closely related to the shale mineral composition and burial evolution. For example, nanopores with higher elastic buckling pressure increase with increasing depth (Curtis et al., 2012; Kuila and Prasad, 2013); mineral composition changes significantly due to diagenesis including illitization, dolomitization, recrystallization (Li W. et al., 2016; Wilson et al., 2016a; Mathia et al., 2016; Bai et al., 2018; Cai et al., 2018; Liang et al., 2018; Du et al., 2019; Wang and Guo, 2019), leading to the changes of pore and surface properties (Klaver et al., 2012; Li W. et al., 2016; Wilson et al., 2016b; Wang and Guo, 2019). In summary, shale pores and surfaces are complex, and their characteristics and properties change significantly according to the mineral composition and

burial evolution. These complexities control the interactions between pore walls and confined fluids, and they must affect the shale oil mobility and production performance.

To further illustrate the potential impacts of the complexity of the characteristics and properties of pores and surfaces on the fluid flow from shale formation to fractures, the interactions between fluids and pores or surfaces in different fracturing stages were summarized. During the pumping stage, fracturing fluids are pumped into shale formation and forming fractures. Then, fracturing fluids gradually intrude into shale rocks under high fluid pressure. After pumping, the well will be shut. Shut-in is commonly used and is important for the formation of stable fractures and provides time for the water blockage removal (Al-Ameri et al., 2018; Wijaya and Sheng, 2019). During this stage, fracturing fluids imbibe into the formation spontaneously. It is important to note that spontaneous imbibition also happens during the fluid pumping, the flowback, and the long-term production stage (Al-Ameri et al., 2018; Zeng et al., 2019). The strength of the imbibition is greatly affected by the wettability, the pore structure, and the pore connectivity of the rock (Dehghanpour et al., 2012; Xu and Dehghanpour, 2014; Wilson et al., 2016b; Zolfaghari et al., 2016; Sun et al., 2017; Yu et al., 2017; Yang et al., 2018). In addition, the wettability of some surfaces can be changed from oil wetting to water wetting due to imbibition (Chen et al., 2016; Roshan et al., 2016; Chen et al., 2018a; Chen et al., 2018b; Zeng et al., 2019), and the pore structure can also be changed by fracturing fluids and surfactant (Xu and Dehghanpour, 2014; Lu et al., 2019), which will further change the flow characteristics conversely. During the flowback stage, part of the fracturing fluids is adsorbed by the minerals (especially the clay minerals) or trapped into the pores with narrow throat, leading to low flowback recovery of the fracturing fluids (Xu and Dehghanpour, 2014; Al-Ameri et al., 2018; Wijaya and Sheng, 2019). Meanwhile, the chemical properties of the flowback fluids change obviously due to the mass exchange between the fracturing fluids and the pore fluids or the mineral components (Haluszczak et al., 2013; Engle and Rowan, 2014; Zolfaghari et al., 2016). Additionally, the strength of the impacts differs according to mineral types because of the divergences in their physical and chemical properties (Zolfaghari et al., 2016). For example, smectite and I/S impact more on the flowback water chemical properties than illite (Zolfaghari et al., 2016). In summary, characteristics and properties of pores and surfaces will impact the absolute permeability of shale and, more importantly, the relative permeability of oil. Thus, the analysis of the characteristics and properties of shale pores and surfaces is important for the evaluation of shale oil potential, but they are seldomly considered previously.

In this study, shale samples with different mineral compositions and degrees of evolution were collected from different shale formations in the Dongying Sag, Jiyang Depression. The complete shale pore's size distribution and surfaces with different properties were analyzed by N_2 adsorption, mercury intrusion porosimetry, and EGME adsorption methods. Then, the mineral composition, pore, and surface characteristics and properties were compared among the shales at different intervals. Based on all these detections and



comparisons, the fluids flow from shale formation to the hydraulic fractures was evaluated, and the favorable interval for shale oil storage and flow was obtained on the profile from the perspective of potential fluid flow properties. This study can benefit the selection of fracturing fluids, the implementation of fracturing, and the accurate evaluation of shale oil production performance.

MATERIALS AND METHODS

Materials

The Dongying Sag locates in the southeastern of Bohai Bay Basin, northern China. Previous exploration has confirmed the great shale oil potential in the third and fourth members of Shahejie Formation (Li Z. et al., 2016; Li et al., 2020). In order to characterize the influence of pore structure on the fracturing of the shales with different compositions, thirty-four argillaceous source rocks were selected for detection, which were taken from well NY1, N38, and N872 at depths of 3000~3500 m in the middle and lower section of the third member (Es3^{middle} and Es3^{lower}) and upper section of the fourth member (Es4^{upper}) of Shahejie Formation (Figure 1; Table 1) in the Dongying Sag. All the bulk samples were detected by X-ray diffraction (XRD), Rock-Eval VI pyrolysis, N₂ adsorption, mercury injection porosimetry (MIP), and ethylene glycol monoethyl ether (EGME) adsorption methods. The clay fraction of each sample was detected by XRD to obtain the clay mineral composition. For the separation of the clay-sized fractions, the bulk rocks were ground to less than 1 mm and were then soaked in deionized water within a 2000-ml beaker at room temperature via natural sedimentation.

Methods X-Ray Diffraction (XRD)

An X'pert-MPD diffraction instrument (Philips Corp) was employed for XRD measurements. The samples were crushed to a particle size of 320 mesh. The test conditions include a copper butt, pipe pressure of 30 kV, conduit flow of 40 mA, and scanning speed of 2° (2 θ)/min. The bulk mineral composition was detected by a natural thin section of bulk rock. The clay mineral composition detection was conducted on natural ethylene glycol saturated and 550 C heated orientation sheet of clay fractions. The ethylene glycol-saturated orientation sheet was made by exposing the naturally oriented sheet in ethylene glycol vapor at 60°C for 8 h, and 550°C heated orientation sheet was made by heating at 550°C for 2 h.

Pore Characteristics Determination

N_2 Adsorption

Pore size distribution (PSD) of pores with diameters ranging from approximately 1-50 nm was conducted with the lowtemperature (77 K) N2 adsorption methods on the JW-BK adsorption instrument (Beijing JWGB SCI & Tech Corp). Approximately 2~4 g of sample was crushed to a particle size smaller than 3 mm and degassed by heating at 80°C for more than 6 h under vacuum (10 µm Hg) to remove adsorbed moisture and volatile matter prior to the analysis. Measurements in adsorption mode were performed over the relative pressure (P/P0) range of 0.1 ~ 0.95 to obtain the adsorption isotherm. The PSD was obtained by inverting the adsorption branch of the isotherm using BarrettJoynerHalenda (BJH) method (Barrett et al., 1951).

TABLE 1	Sample information and mineral composition.	

Sample no.	Well	Depth	Member	Bull	k mineral comp	osition/%	Clay mineral composition/%				
		м		Clay	Detrital	Carbonate	I/S	Illite	Kaolinite	Chlorite	
1	NY1	3334.36	Es4 ^{upper}	37	21	39	61	36	2	1	
2	NY1	3355.61	Es4 ^{upper}	22	26	49	67	33	0	0	
3	NY1	3372.01	Es_4^{upper}	8	24	66	0	100	0	0	
4	NY1	3378.36	Es4 ^{upper}	9	25	64	30	70	0	0	
5	NY1	3380.21	Es_4^{upper}	15	21	62	28	72	0	0	
6	NY1	3382.16	Es4 ^{upper}	48	33	16	35	65	0	0	
7	NY1	3385.76	Es4 ^{upper}	22	19	56	12	88	0	0	
8	NY1	3390.45	Es4 ^{upper}	13	24	62	0	100	0	0	
9	NY1	3398.90	Es4 ^{upper}	6	19	74	0	100	0	0	
10	NY1	3408.00	Es4 ^{upper}	24	21	53	0	100	0	0	
11	NY1	3468.63	Es4 ^{upper}	44	39	14	50	50	0	0	
12	NY1	3479.73	Es4 ^{upper}	5	12	83	0	100	0	0	
13	NY1	3494.45	Es4 ^{upper}	9	10	38	0	100	0	0	
14	NY1	3497.90	Es4 ^{upper}	15	15	31	3	97	0	0	
15	N38	3022.00	Es ₃ ^{middle}	42	50	4	74	14	7	5	
16	N38	3025.00	Es ₃ ^{middle}	31	46	20	76	13	6	5	
17	N38	3034.81	Es ₃ ^{middle}	27	38	32	69	15	9	7	
18	N38	3089.52	Es ₃ ^{middle}	47	42	11	68	22	6	4	
19	N38	3137.61	Es ^{2^{middle}}	42	35	21	81	15	2	2	
20	N38	3140.91	Esa ^{middle}	45	39	14	74	19	4	3	
21	N38	3143.41	Es ₃ ^{middle}	45	50	5	68	20	7	5	
22	N38	3147.41	Es ₃ ^{middle}	51	41	6	73	20	4	3	
23	N38	3336.60	Es ₃ ^{lower}	43	44	13	65	30	3	2	
24	N38	3342.60	Es ₃ lower	41	34	22	59	41	0	0	
25	N872	3050.80	Es ₃ ^{middle}	30	33	31	72	20	4	4	
26	N872	3049.70	Es ₃ ^{middle}	34	28	32	71	17	7	5	
27	N872	3053.50	Es ₃ ^{middle}	37	40	21	71	25	2	2	
28	N872	3072.30	Es ₃ ^{middle}	32	50	16	73	22	3	2	
29	N872	3074.30	Es ₃ ^{middle}	26	53	20	73	22	3	2	
30	N872	3201.00	Es ₃ ^{lower}	25	35	35	52	40	4	4	
31	N872	3203.00	Es ₃ ^{lower}	29	27	39	69	27	2	2	
32	N872	3208.70	Es ₃ ^{lower}	18	29	49	57	36	4	3	
33	N872	3327.30	Es ₄ ^{upper}	19	36	43	5	95	0	0	
34	N872	3329.40	Es ₄ ^{upper}	38	35	24	49	51	0	0	

Mercury Intrusion Porosimetry

The PSD of pores with diameters ranging from approximately $3.2 \text{ nm}-40 \mu \text{m}$ was determined using the mercury intrusion method on a Micromeritics Autopore IV 9500 series apparatus. Samples (2~4 g) were crushed to a particle size smaller than 3 mm and were oven-dried (80°C) and evacuated under vacuum (30 μ m Hg) for 30 min prior to mercury intrusion. The measured pressure ranged from 0.5 to 60,000 psia, and the PSD was calculated by the Washburn equation (Schmitt et al., 2013). In our calculations, the interfacial tension of Hg was 485 mN/m, the wetting angle was 140°, and the density of Hg was 13.5335 g/ml.

Combination of N_2 Adsorption and MIP and Calculation of Pore Characteristics Parameters

Previous researchers have established several methods to combine N_2 adsorption method and MIP for obtaining the complete PSD of shales (Spitzer et al., 1976; Echeverria et al., 1999; Schmitt et al., 2013; Kenvin et al., 2015). In this study, we obtained the complete PSD referring to the method proposed by Schmitt et al. (2013) and Li et al. (2020). The junction point of

each sample is listed in **Table 2**. After achieving the complete PSD, the total pore volume (Vt) was calculated.

Surface Areas Measurement

N_2 Adsorption

The determination procedure is the same as the *Surface Areas Measurement section*. After obtaining the adsorption isotherms, the outer surface area (BET-SSA) for each sample was determined by inversion of the adsorption branch of the isotherm using the BrunauerEmmettTeller (BET) analysis procedure (Brunauer et al., 1938), with a relative pressure range of 0.05 ~ 0.3. The molecular sectional area of N₂ was 0.162 nm².

EGME Adsorption

For the EGME procedure, a vacuum pump (with a vacuum pressure of 609 mmHg) and an electronic analytical balance (with an accuracy of 0.0001 g) were employed. Approximately 1 g of sample was weighed and put in the oven at 80°C for more than 6 h. Then, the sample was taken out and put in the aluminum tare (with a diameter of 5 cm and a height of 8 mm), and 3 ml EGME solution (analytical grade) was quickly

Sample no	Junction point nm	Vt cm ³ /g	V1 cm ³ /g	V2 cm ³ /g	V3 cm ³ /g	V1%	V2%	V3 %	TSA m²/g	ISA m²/g	BET-SSA
2	18.32	0.003750	0.000341	0.001806	0.001604	9.08	48.16	42.76	78.91	78.76	0.15
3	14.08	0.011062	0.000187	0.001401	0.009474	1.69	12.67	85.64	34.14	33.85	0.29
4	13.52	0.007807	0.000553	0.003219	0.004035	7.09	41.23	51.69	34.92	34.07	0.85
5	6.75	0.003593	0.003106	0.000163	0.000324	86.44	4.53	9.03	70.74	67.70	3.05
6	36.79	0.088121	0.000608	0.007541	0.079972	0.69	8.56	90.75	129.65	128.31	1.34
7	17.66	0.027352	0.009051	0.006746	0.011555	33.09	24.66	42.24	65.80	60.06	5.74
8	26.33	0.005770	0.000029	0.001438	0.004303	0.50	24.92	74.58	32.00	30.07	1.93
9	18.73	0.004906	0.000048	0.000763	0.004095	0.98	15.56	83.46	22.16	21.51	0.65
10	25.52	0.021793	0.003493	0.007661	0.010639	16.03	35.15	48.82	51.58	49.04	2.54
11	13.74	0.087995	0.036221	0.036579	0.015195	41.16	41.57	17.27	128.88	98.35	30.53
12	25.33	0.005556	0.000308	0.002110	0.003138	5.55	37.97	56.48	20.91	19.74	1.17
13	31.85	0.006996	0.001080	0.005282	0.000634	15.43	75.50	9.06	23.20	22.37	0.83
14	15.92	0.014206	0.002730	0.010687	0.000789	19.22	75.23	5.56	40.15	38.43	1.72
15	12.67	0.009972	0.005662	0.003765	0.000545	56.78	37.75	5.47	107.98	102.15	5.83
16	15.42	0.013532	0.005506	0.006636	0.001391	40.69	49.03	10.28	117.03	109.31	7.72
17	13.31	0.005320	0.002438	0.002114	0.000768	45.83	39.73	14.44	109.86	107.72	2.14
18	17.47	0.027000	0.016127	0.010290	0.000583	59.73	38.11	2.16	160.87	131.25	29.62
19	14.26	0.027401	0.012389	0.012697	0.002316	45.21	46.34	8.45	151.98	131.77	20.21
20	14.75	0.020501	0.011490	0.007354	0.001657	56.05	35.87	8.08	155.70	140.25	15.45
21	23.39	0.028910	0.013045	0.012291	0.003575	45.12	42.51	12.37	115.33	91.45	23.88
22	19.71	0.030813	0.016797	0.012868	0.001148	54.51	41.76	3.73	162.53	132.96	29.57
23	17.56	0.026642	0.014331	0.011117	0.001195	53.79	41.73	4.48	122.70	104.95	17.74
24	21.06	0.018754	0.004835	0.005779	0.008139	25.78	30.82	43.40	147.47	144.01	3.46
25	24.95	0.006979	0.000583	0.003136	0.003260	8.35	44.94	46.71	125.03	123.97	1.05
26	13.47	0.006426	0.002081	0.003374	0.000971	32.39	52.51	15.11	134.92	132.97	1.95
27	12.13	0.015185	0.009051	0.004849	0.001286	59.60	31.93	8.47	151.86	141.16	10.70
28	14.69	0.020578	0.012020	0.006391	0.002167	58.41	31.06	10.53	138.95	124.26	14.69
29	18.94	0.018109	0.008317	0.009056	0.000736	45.93	50.01	4.06	116.64	106.58	10.06
30	14.26	0.007901	0.000140	0.004101	0.003660	1.77	51.90	46.33	113.77	113.16	0.61
31	27.63	0.004121	0.000020	0.002119	0.001982	0.49	51.42	48.09	153.49	151.88	1.61
32	27.63	0.005280	0.000067	0.002008	0.003205	1.27	38.03	60.71	93.85	91.93	1.92
33	15.70	0.009027	0.001751	0.003340	0.003936	19.40	37.00	43.61	62.81	60.96	1.85
34	24.59	0.088952	0.006882	0.024590	0.057480	7.74	27.64	64.62	124.09	119.36	4.73

TABLE 2 | Junction points, pore volumes and contents, surface areas.

added to the sample with a pipette and swirled gently until the sample was soaked. Afterward, the aluminum tares with mixture were placed in a sealed desiccator with EGME solution, calcium chloride (CaCl₂), and phosphorus pentoxide (P₂O₅). The desiccator was evacuated for approximately 1 hour to remove water vapor. More than 8 h later, the tares were weighed after the desiccator was evacuated again. The process of evacuation was repeated, and they were weighed until a constant weight was attained (the mass difference between the two measurements was less than 0.001 g). Finally, the total surface area (TSA) of the sample was calculated based on the absorbed quantity of EGME molecules (the conversion factor is 2.86×10^{-4} g/m²), and the inner surface area (ISA) was the differences between TSA and BET-SSA.

RESULTS

Mineral Composition Bulk Mineral Composition

It is found from the XRD curves of typical bulk rocks (**Figure 2A**) that although clay, quartz, calcite are the main mineral types of all

the shales, the relative contents of different types of minerals vary greatly among the shales from different sections. For example, the shales from $\text{Es}_4^{\text{upper}}$ contain more dolomite, especially for the deeper burial samples. Comparison of bulk mineral composition of the shales from different sections (**Figure 2B**) shows that the shales from $\text{Es}_3^{\text{middle}}$ contain the most amount of clay (37.62%) and detrital (41.92%) minerals and the least amount of carbonate (17.92%) minerals; the shales from $\text{Es}_4^{\text{upper}}$ are composed of much more calcite (31.94%) and dolomite (15.31%) than those of $\text{Es}_3^{\text{middle}}$ and $\text{Es}_3^{\text{lower}}$; the shales from $\text{Es}_3^{\text{lower}}$ contain moderate content of almost all types of minerals.

Clay Mineral Composition

From the analysis of the composition of clay minerals (**Table 1**; **Figure 2C**), the average contents of mixed-layer illite/smectite (I/S) (46.62%) and illite (49.26%) of all the shales were found to be high, while there are also great differences among the shales from different sections. The shales from Es_3^{middle} contain the most amount of I/S (72.54%) and the least amount of illite (18.77%); the shales from Es_4^{upper} are composed of much more illite (78.56%) than those of Es_3^{middle} and Es_3^{lower} ; the shales from



 $\text{Es}_3^{\rm lower}$ contain moderate content of I/S (60.40%) and illite (34.80%).

Pore and Surface Characteristics Surface Characteristics

From the results of the N₂ adsorption measurement (**Tables 2**; **Figure 3A**), the shales from Es_3^{middle} have the largest average BET-SSA (13.30 m²/g), which ranges from 1.05 to 29.62 m²/g; the BET-SSA of the shales from Es_3^{lower} ranges from 0.61 to 17.74 m²/ g with an average of 5.07 m²/g; the shales from Es_4^{upper} possess BET-SSA ranges from 0.15 to 30.53 m²/g, with 3.70 m²/g on average. According to the EGME measurement (**Table 2**; **Figure 3C**), the shales from Es_3^{middle} possess the largest average TSA (134.51 m²/g), which ranges from 107.98 to 162.53 m²/g; the TSA of the shales from Es_3^{lower} ranges from 93.85 to 153.49 m²/g with an average of 126.26 m²/g; the shales from Es_4^{upper} present minimal TSA ranges from 20.91 to 129.65 m²/g, with 65.17 m²/g on average. Based on N₂ adsorption and EGME measurements (**Table 2**; **Figure 3B**), the ISA can be calculated. The results show that the shales from ${\rm Es_3}^{\rm middle}$ and ${\rm Es_3}^{\rm lower}$ also present larger ISA (with 121.21 m²/g and 121.19 m²/g on average, respectively), while the shales from ${\rm Es_4}^{\rm upper}$ have much smaller ISA (61.47 m²/g).

Pore Characteristics

According to the complete pore size distribution (PSD) curves of the shales from different sections (**Figure 4**), most of the shales are mainly composed of the large mesopore (10~50 nm) and small macropore (50~100 nm), while most of the shales from Es_4^{upper} contain a significant amount of pores with diameter >100 nm (**Figures 4A–D**). In addition, the PSD of the shales from different sections shows great differences. Qualitatively, the shales from Es_4^{upper} contain more pores with larger diameter than the shales from Es_3^{middle} and Es_3^{lower} , while the shales from Es_3^{middle} present a very low amount of larger pores. Considering the characteristics of the PSD curves, the volumes of the pores with diameter <10 nm (V1), 10~100 nm (V2), and >100 nm (V3) were further calculated by interpolation (**Table 2**).

Based on these findings, Vt, V1, V2, and V3 and their relative contents of the shales from different sections were further

С

180

В



160

120

80-

Α

average; the Vt of the shales from Es_4^{upper} ranges from 0.003593 to $0.088952 \text{ cm}^3/\text{g}$, with an average of $0.024668 \text{ cm}^3/\text{g}$ (Table 2; Figure 3D). Further comparing the pore volumes of the pores with different diameter ranges (**Figures 5A–C**), it can be found that the shales from $\text{Es}_3^{\text{middle}}$ have the largest V1 (0.008885 cm³/ g) and V2 (0.007294 cm³/g) and minimal V3 (0.001569 cm³/g); the shales from $\text{Es}_3^{\text{lower}}$ possess minimal V1 (0.003879 cm³/g) and V2 ($0.005025 \text{ cm}^3/\text{g}$) and moderate V3 ($0.003636 \text{ cm}^3/\text{g}$), while the shales from Es_4^{upper} have maximal V3 (0.013135 cm³/g) and moderate V1 (0.004350 cm³/g) and V2 (0.007183 cm³/g). Viewing from the contents of V1, V2, and V3 (Figures 5D-F), the shales from Es3^{middle} contain the most amount of V1 (46.81%) and the least amount of V3 (11.53%), the shales from Es₃^{lower} possess minimal V1 (16.62%) and maximal V2 (42.78%), the shales from Es4^{upper} present maximal V3 (47.74%) and minimal V2 (33.18%).

DISCUSSIONS

Relationships Between Pores and Surfaces

Pores and outer surfaces are the places where shale oil occurs. Their relationships depend on the relative contribution of free oil and adsorbed oil. Therefore, the relationships between pore volumes and the BET-SSA were analyzed firstly. It can be found that Vt of the shales from $\text{Es}_3^{\text{middle}}$ and $\text{Es}_3^{\text{lower}}$ presents a better relationship with BET-SSA (especially for $\text{Es}_3^{\text{middle}}$) than that of Es_4^{upper} (Figure 6A). Viewing from the pores with different diameter ranges (Figures 6B,C), the correlation coefficients of the relationships between V1 of the shales from each section with BET-SSA are high (>0.95), while the correlation coefficients of the relationships between V2 of the shales from each section are smaller, especially for the shales from Es₄^{upper}; there are no relationships between V3 and BET-SSA (the data were not shown in Figure 6). These observations coincide well with previous researches; that is, the pores with small size contribute primarily to the outer surface area, while the pores with larger size mainly contribute to the pore volume (Beliveau, 1993; Chalmers et al., 2012; Curtis et al., 2012; Wang and Guo, 2019). Further comparison of the shales from different sections suggests that (Figure 6) the slopes of the shales from Es_3^{middle} and Es₃^{lower} are steeper than those of Es₄^{upper}, especially for V2 and Vt, indicating the differences in their pore size and in the ratio between pore volume and outer surface area. It has been confirmed previously that pores with different sizes have different ratios between pore volume and outer surface area, leading to the difference in the proportion of oil with different occurrence states (Chalmers et al., 2012; Curtis et al., 2012; Wang and Guo, 2019). MDSs and spontaneous imbibition experiments also showed that the intensity of the interfacial interaction of the pores with different pore volume/surface area ratios (or pore diameter) differs significantly (Xu and Dehghanpour, 2014; Yu et al., 2017). The pores with smaller pore volume and larger surface area possess stronger interfacial interaction intensity and larger capillary force, leading to larger adsorption potential to wetting phase fluids and stronger inhibition to non-wetting phase fluids (Wang et al., 2015; Wang S. et al., 2016; Yu et al., 2017; Zeng et al., 2019). Therefore, the shales from Es₄^{upper} which present larger pore volume and smaller surface area are more conducive to fluid flow without considering the properties of the pore walls.

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However, shales are composed of varieties of minerals which present divergence attributes. Thus, to analyze the properties of pore walls and their influence on fluid mobility of the shales from different sections, the relationships between minerals and pores/ surfaces were further analyzed.

Contributions of Mineral Components to Pores and Surfaces

Pores

Clay minerals (I/S, illite), detrital minerals (quartz, feldspar), and carbonate minerals (calcite, dolomite) are the main bulk mineral components in shale rocks (**Table 1**; **Figure 2**). According to the relationships between bulk mineral compositions with Vt (**Figure 7**), it is found that Vt positively correlates with clay and detrital mineral content but negatively correlates with carbonate mineral content for the shales from all sections and generally presents a high correlation coefficient. These correlations indicate that inorganic pores are the main pore

type of the studied area, while clay and detrital minerals contribute to the shale pores and carbonate minerals generally inhibit the development of pores. These findings are similar to previous studies on the shales from similar locations (Zhang et al., 2016; Zhu et al., 2019; Zhang et al., 2019; Liu et al., 2019). Previous studies have confirmed the chemical instability of carbonate minerals, and they probably destroy or block the pores by digenesis such as dissolution, precipitation, and recrystallization (Chalmers et al., 2012; Gaines et al., 2012; Loucks et al., 2012; Liu et al., 2019). In addition, the correlations between Vt and clay and carbonate mineral are usually better than those of detrital minerals, indicating the stronger control of clay and carbonate minerals in shale pores.

Comparison of the correlations of the shales from different sections shows that the slopes of the shales from Es_4^{upper} are much larger than those of the other two sections (**Figure** 7), suggesting the greater role of mineral components in the development of pores, especially for the relatively larger pores. The conclusion can be certificated by the previous studies





indicating that clay minerals mainly relate to micropores and small mesopores while carbonate minerals generally correlate well with pores with larger diameter (Chalmers et al., 2012; Klaver et al., 2012; Kuila and Prasad, 2013; Mathia et al., 2016; Liu et al., 2019; Zhang et al., 2020) and the relatively high carbonate mineral content of the shales from Es_4^{upper} . Moreover, based on the relationships between clay mineral content and pore volumes of pores with different diameter range (**Figure 8**), it can be found that V3 of the shales from Es_4^{upper} correlates well with clay mineral content while present no obvious relationships for the shales from Es_3^{middle} and Es_3^{lower} . On the contrary, the correlation coefficients between V1 and clay mineral contents for the shales from Es_3^{middle} and Es_3^{lower} are much higher than that of Es_4^{upper} (**Figure 8**). The results indicate that although clay minerals mainly benefit the development of pores, the relative contributions of clay minerals to pores with different diameters for the shales from different sections differ significantly. Previous studies indicated that illitization, dolomitization, and dissolution benefit the shale reservoir properties and create more macropores for oil accumulation and flow (Chalmers et al., 2012; Li W. et al., 2016; Mathia et al., 2016; Bai et al., 2018; Liang et al., 2018; Wang and Guo, 2019). Thus, considering differences in mineral composition of different sections (**Figure 2**), we attribute these divergences to the clay mineral composition of the shales from different sections. In summary, the shales from Es₄^{upper} contain more carbonate minerals and undergone a higher degree of illitization and dolomitization than those of Es₃^{middle} and Es₃^{lower}, thus leading to more pores with larger diameter





(**Table 2**; **Figures 3–5**). Therefore, the shales from Es_4^{upper} present a higher potential for oil accumulation and flow from shale formations to fractures.

Surfaces

Clay minerals correlate with smaller pores with large correlation coefficients (**Figure 8**) (Kuila and Prasad, 2013) and possess larger outer surface area than detrital and carbonate minerals (Beliveau, 1993; Chalmers and Bustin, 2008; Chalmers et al., 2012; Kuila and Prasad, 2013; Zhu et al., 2015; Saidian et al., 2016). Additionally, clay minerals such as smectite and I/S have inner surface areas between clay sheets, and ISA is usually one or two orders of magnitude larger than the outer surface area (Macht et al., 2011; Zhu et al., 2015). Thus, we only analyze the contributions of clay minerals to surface areas. Comparison of the clay mineral composition of the shales from different sections (**Table 1**) indicates that I/S and illite contents of the shales from Es₃^{middle} and Es₃^{lower} only distribute in a narrow range ($\approx 20 \sim 30\%$), which is much smaller than that of Es₄^{upper}. Therefore, it is more appropriate to put all the shales from different sections together when analyzing the relationships between clay

mineral composition and surface areas. The results show that all kinds of surface areas correlate with clay mineral content, in which BET-SSA mainly trend correlates with clay mineral contents, while ISA and TSA present excellent correlations with clay mineral (Figures 9A-C). Further comparison of the contents relationships between surfaces areas and specific clay mineral types indicates that all types of surface areas positively correlate with I/S content while negatively correlate with illite content (Figures 9D-I). Also, BET-SSA only shows trend relations with I/S and illite contents, while ISA and TSA present an excellent correlation with I/S and illite contents. These findings indicate that surfaces are mainly constructed by clay minerals, especially for ISA, while I/S and illite present the opposite effect. Therefore, the lower clay mineral content and higher illite content of the shales from Es_4^{upper} lead to its smaller surface areas (Figures 2, 3).

According to **Figure 9**, the correlation coefficients for BET-SSA are much worse than those of ISA. To understand these differences, it must be noted that the measured surface areas are the surface areas after the release of hydrocarbon or other confined fluid during coring and subsequent sample preservation (Jiang et al.,



2016; Li et al., 2020; Wang et al., 2022). It has been demonstrated that free and physically adsorbed hydrocarbons or OM is mainly occurred on the outer surface, and they vaporize much easier and faster than chemically adsorbed hydrocarbons or OM which mainly occur on the inner surface (Jiang et al., 2016; Zhu et al., 2016). Therefore, the outer surface area is affected by hydrocarbons or OM that is confined in the shale pores more remarkably, and leading to relatively poor relationships between BET-SSA and mineral compositions.

To summarize, pores and surfaces are all greatly affected by mineral components, especially clay minerals. Previous studies have indicated that the physical and chemical properties differ significantly according to mineral types and clay minerals are more active. For example, clay minerals mainly correlate with smaller pores; smectite and I/S are easier to hydrate and swell than illite and kaolinite (Zolfaghari et al., 2016; Al-Ameri et al., 2018; Sui et al., 2018), and their higher CEC will lead to stronger impacts on the chemical properties of flowback water (Greenland, 1971; Han et al., 2016; Saidian et al., 2016; Zolfaghari et al., 2016); along with burial evolution, smectite with large ISA will transfer to illite with no ISA by illitization, leading to the decreasing of ISA (Zhu et al., 2015; Wilson et al., 2016b; Singh et al., 2016) and the change of pore structure and BET-SSA (Wu et al., 2015; Wang and Guo, 2019). These differences will result in divergences in the interactions between pore walls and fluids and then affect the fluid flow significantly.

Effects of Pore and Surface Characteristics and Properties on Fluid Flow

Based on the discussions above, a hypothesis model was established to illustrate the effects of the characteristics and properties of pores and surfaces on the fluid flow from shale formation to hydraulic fractures (**Figure 10**). It has been confirmed that the affinity to fluids of different minerals follows the order: I/S > illite > carbonate minerals \approx detrital minerals (Zhang et al., 2012; Singh et al., 2016; Zolfaghari et al., 2016; Al-Ameri et al., 2018; Saikia et al., 2018). Therefore, if the pore size and fluid condition are assumed to be the same: for the pores constructed by I/S, more fluids will be adsorbed onto the



pore walls, and the mobility pore diameter is much smaller than the real pore diameter (**Figure 10A**); for the pores related to illite, the thickness and distribution range of residual fluids are smaller than those of the I/S (**Figure 10B**); for the pores related to carbonate and detrital minerals, the thickness of the residual fluids reduces further and the distribution is localized (**Figure 10C**).

Combined with the features and the differences in the mineral composition and pore and surface characteristics of the shales from different sections (Figures 2-9), the fluid distribution and flow pattern were established to illustrate the differences in the production potential of the shales from different sections (Figures 10D,E). Comparison of the fluid flow characteristics between the same mineral types of the shales from different sections indicates that because the interfacial interaction strength of pores with a smaller diameter is much larger than that of larger pores (Wang S. et al., 2016; Yu et al., 2017), more oil is retained in shale formation (Figures 10D,E) for the shales from Es₃^{middle} and Es_3^{lower} than that of Es_4^{upper} (Figures 4, 5). In addition, fracturing fluids that intruded into the shales may also be trapped more seriously in the shales with smaller pores and leading to more oil blocked in shale formation if the trapped fracturing fluids block the pores or pore throat (Figures 10D,E). Further comparison of the fluid flow characteristics between different mineral types

shows that (**Figures 10D,E**) more oil and intruded fracturing fluids are trapped in shale formations due to the generally smaller pore size of the pores correlate to clay minerals than those of carbonate and detrital minerals (Klaver et al., 2012; Kuila and Prasad, 2013; Malik and Lu, 2015; Li W. et al., 2016; Mathia et al., 2016) and the larger affinity to fluids of clay minerals, especially for I/S (Zhang et al., 2012; Singh et al., 2016; Zolfaghari et al., 2016; Al-Ameri et al., 2018; Saikia et al., 2018). In summary, the fluid flow in shale formation is controlled both by the pore size and by the properties of pore walls (surfaces). Due to the larger Vt, V2, V3, and smaller surface areas, as well as the high carbonate and illite content, the shales from Es_4^{upper} possess better production potential (**Figures 10D,E**).

Significances and Prospects

The breakability of shale is one of the key characteristics that depend on the fracturing and extraction of oil and gas occluded within shale play (Aadnøy and Looyeh, 2019). Brittle mineral content is the main concern when evaluating breakability. Jarvie et al. (2007) viewed quartz as the main brittle mineral in the Barnett Shale and used its relative content for stimulation evaluation (Jarvie et al., 2007). In addition to quartz, Wang and Gale (2009) also regarded dolomite as a brittle mineral (Wang and Gale, 2009). Based on the study of the mechanical



properties of minerals, Jin et al. (2014) further classified feldspar, calcite, and mica as brittle minerals (Jin et al., 2014). In summary, it is widely accepted that breakability relates closely to mineral composition. The rocks with relatively high detrital minerals and carbonate minerals and low amount of clay mineral content present better breakability (Aadnøy and Looyeh, 2019). However, to efficiently exploit shale resources, brittle mineral content is not the only concerning factor, characteristics and properties of pores and surfaces should also be paid attention to because of their significant effects on fluid flow in shale formation (Figure 10). On the one hand, pores with different diameters present divergence capillary force and specific surface area, leading to differences in the adsorption potential and flow profile. On the other hand, the physical and chemical properties of minerals and their relationships with pores and surfaces differ significantly according to mineral types, leading to divergences in the interfacial interactions between the pore walls and the confined fluids. These divergences will change the distribution, occlusion, and flow of fracturing fluid and oil. Furthermore, water is the main component in fracturing fluids, and it will interact with clay minerals (especially I/S) significantly during the pumping, flowback, and production stages (O'Brien and Chenevert, 1973; Makhanov et al., 2014; Xu and Dehghanpour, 2014; Sui et al., 2018; Shi et al., 2020) and might lead to the low flowback recovery, the changes of pore and surface properties, and the reduction of oil relative permeability. Therefore, characteristics and properties of pores and surfaces are the indispensable factors that need to be taken into the evaluation of shale oil potential. Take the research area as an instance, based

on the burial evolution profile of TOC, pore volume, surface areas, mineral composition, and composition of pores, the deep burial shales from Es_4^{upper} are the favorable interval for shale oil accumulation and flow, especially for the shales with depth ranges of 3360~3410 m (**Figure 11**), which present high carbonate minerals, illite and TOC content, low clay mineral content, large total pore volume, more pores with a larger diameter and small surface areas.

Remarkable changes of mineral composition and pore structure along with burial evolution are some of the most important characteristics of shale resources. For example, diagenesis such as compaction, recrystallization, and cementation increases the brittleness of rocks and result in the increase of breakability of rocks; diagenesis such as illitization, dissolution, and dolomitization improves reservoir properties by forming more large pores and reducing surface areas (Chalmers et al., 2012; Li W. et al., 2016; Mathia et al., 2016; Zhang et al., 2016; Bai et al., 2018; Liang et al., 2018; Wang and Guo, 2019); I/S that contains interlayer space decreases by illitization and forms illite that without interlayer space (Wilson et al., 2016a; Wilson et al., 2016b; Saidian et al., 2016), thus leading to the decreases in the clay mineral swelling, the retention of fracturing fluids, and the effects on flowback water chemical properties (Zolfaghari et al., 2016; Al-Ameri et al., 2018). Furthermore, the flow properties are greatly affected by the fluid composition due to the divergences in the physical and chemical properties of different components and the interfacial interactions of different components with pore walls (Xu and Dehghanpour, 2014; Wang S. et al., 2016; Chen et al., 2016). Additionally, the

fluid composition also changes along with the maturation of OM and the generation of lighter hydrocarbons, leading to the increase of the mobility of shale oil (Wang et al., 2022). Ion is the other chemical additive that is important for the efficient production of shale resources. Previous studies have confirmed that the wettability of mineral surfaces or bulk rocks is significantly affected by brine (Chen et al., 2018a; Chen et al., 2018b; Zeng et al., 2019). In summary, evaluation of the hydraulic fracturing and production performance of shale resources need to consider not only the brittleness of minerals but also the characteristics and properties of pores and surfaces. In addition, diagenesis, shale oil composition, and chemical composition of fracturing and flooding fluids are also important factors that need to be paid more attention in the future.

CONCLUSION

In this study, shales samples were collected from different sections and were detected by XRD, N_2 adsorption, EGME adsorption, and mercury intrusion methods to analyze the characteristics of pores and surfaces and their potential effects on fluid flow from shale formation to hydraulic fractures. The main conclusions were listed as below:

- 1) The shales from Es_3^{middle} and Es_3^{lower} contain more clay minerals (especially I/S) and less carbonate minerals than those of Es_4^{upper} . Clay minerals mainly contribute to pore development, and carbonate minerals inhibit pore development. More importantly, the contributions of clay minerals to pores with different diameter ranges differ according to sections, and we attribute these divergences to clay mineral composition. All kinds of surface areas are mainly sourced by clay minerals, while I/S correlates positively to surface areas and illite correlates negatively to surfaces areas, especially for ISA.
- 2) Pores with smaller diameters present larger outer surface area while large pores contribute minor to surface area. The shales

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from $\text{Es}_3^{\text{middle}}$ and $\text{Es}_3^{\text{lower}}$ are mainly composed of smaller pores, leading to the larger surface areas and steeper slope between pore volume and surface area.

3) Mineral composition, fluid composition, pore structure, and surface properties are the factors that need to be considered for the evaluation of fluid flow in shale formation. The shales with high carbonate and illite content, larger total pore volume, larger pores, and smaller surface areas present better shale oil accumulation and fluid flow conditions. To better evaluate shale oil flow and production potential, fluid compositions of both the fracturing fluids and shale oil need more concern in the future.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, and further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

XL: conceptualization, methodology, investigation, data curation, formal analysis, writing—original draft preparation, writing—review and editing. JC: conceptualization, resources, supervision, project administration, methodology. BG: methodology, data curation, writing—review and editing. SL: resources, funding acquisition. DF: funding acquisition, project administration. ZP: resources. BG: data curation. All authors contributed to the article and approved the submitted version.

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Conflict of Interest: XL, BG, SL, DF, and ZP were employed by SINOPEC.

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