



# **Correction of Atmospheric Delay Error of Airborne and Spaceborne GNSS-R Sea Surface Altimetry**

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Yan Z, Zheng W, Wu F, Wang C, Zhu H and Xu A (2022) Correction of Atmospheric Delay Error of Airborne and Spaceborne GNSS-R Sea Surface Altimetry. Front. Earth Sci. 10:730551. doi: 10.3389/feart.2022.730551 Improving the measurement accuracy is a necessary condition for sea surface altimetry using the Global Navigation Satellite System Reflectometry (GNSS-R). The ionosphere and troposphere delay the transmission of satellite signals, which directly affect the measuring accuracy. The influence of the atmospheric environment on GNSS-R altimetry differs from different platforms. By analyzing and sorting out the altimetry data of airborne and spaceborne platforms, this paper studies the variation law of signal delay in the altimetry process from the point of view of mathematical geometry, which provides an example for improving the precision of GNSS-R altimetry measurements. Firstly, in order to facilitate data analysis, this paper constructed an altimetry model with the GNSS satellite position, specular reflection point position, receiver position as nodes, classified direct signals, and reflected signals. Secondly, calculate ionospheric puncture point coordinates , and interpolate GIM products provided by IGS using time and puncture point coordinates to obtain the VTEC value in the vertical direction of the puncture point, which was converted into the path direction STEC by projection function, the ionospheric delay of each part was obtained in this way. The tropospheric delay of each part is considered for the along-path component and the geometric component, the delay of along-path component was calculated by the UNB3m model, and the delay of geometric component was calculated by the equation provided by Nikolaidou (Nikolaidou et al., 2021). Thirdly, by comparing the sea surface height inversion results with or without atmospheric delay correction with the mean sea surface height provided by DTU15, the measurement accuracy with atmospheric delay correction is obviously improved. The study results of the influence of atmospheric delay on the altimetry experiments precision error of airborne and spaceborne platforms show that the error magnitude is consistent with the existing literature. In the airborne experiment, the influence of the ionosphere is negligible and the troposphere has sub-meter influence on altimetry results, among which the tropospheric along-path delay component occupies a high proportion. The geometric delay component has a high correlation with the satellite elevation angle and its influence on the measurement accuracy decreases with the elevation angle increase. The effect of this factor can be effectively weakened by setting a high satellite cutoff angle. In the spaceborne experiment, the effect of atmospheric delay on altimetry results fluctuates in the range of 3~5 m when the satellite elevation angle is greater than 60°. In this paper, the method of calculating signal atmospheric delay through geometric relation to improving the

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measurement accuracy can provide an example for the atmospheric delay correction of GNSS-R ocean altimetry with high precision and spatial resolution in future research.

Keywords: airborne GNSS-R, spaceborne GNSS-R, atmospheric delay, tropospheric delay, ionospheric delay, global navigation satellite system-reflectometry(GNSS-R) ocean altimetry

# INTRODUCTION

Sea surface height (SSH) is the basic data for the study of ocean dynamics, meteorology, geodesy, geophysics, geodesy, and other fields. The worldwide SSH can be used to monitor global climate change, obtain geoid, determine ocean circulation, invert the ocean gravity field, establish ocean tidal models, and conduct research on mesoscale climate models (Liu et al., 2019; Zhang et al., 2020b). It is of great significance to monitor sea level changes. At present, the SSH can be obtained from the traditional ship surveys and tidal stations to the present medium resolution spectrometer imaging, synthetic aperture radar, radar altimeter, and other methods (Liu et al., 2019; Hang et al., 2020). However, ship survey and tidal station models are limited in space, inefficient at spatial sampling, and suitable for local observation, unable to achieve global ocean coverage. Synthetic aperture radar altimeter and radar altimeter can only measure the target height of the subsatellite point and their application conditions are limited. At present, the famous Jason-2 altimeter satellite is jointly developed by CNES, NASA, EUMETSAT and NOAA, which can achieve the measurement of centimeter-level of SSH. It plays a huge role in weather forecasting and climate monitoring but its revisiting period is 9.9156 days and its coverage is concentrated in the sea, due to its lack of mesoscale spatial resolution results in that the surface water information at this scale cannot be observed steadily for a long time and cannot meet the application requirements of new ocean observation (Ren et al., 2018; Liu et al., 2019; Liu, 2020).

Global Navigation Satellite System Reflectometry (GNSS-R) Remote Sensing Technology is a new generation of altimetry technology which uses the reflection of GNSS signals on the sea surface to achieve altimetry (Hu et al., 2020a; Zhang et al., 2020b). In GNSS navigation and positioning, the reflected signals as multi-path interference are generally considered harmful when receiving direct signals and need to be suppressed and eliminated. However, from the point of view of electromagnetic wave propagation theory, the reflected signals carry the physical characteristics information of the reflecting surface, which can be obtained by the parameters change of reflected signals such as waveform, polarization characteristics, amplitude, phase, and frequency (Yang and Zhang, 2011). Therefore, it is possible to estimate and invert the physical properties of the reflecting surface by accurately receiving and estimating the reflected signals. Based on this theory, in 1993, ESA scientist Martin-Neira first proposed and described the concept of PARIS (passive reflectometry and interferometry system) using sea surface reflected signals (Martin-Neira, 1993). The main idea is to use the GPS sea surface reflected wave as the ranging signal to measure the ocean altimetry. In 1994, French scientist Auber accidentally found that the receiver could receive GPS sea surface

reflected signals through flight tests (Auber et al., 1994). The Langley Research Center of NASA in the United States concluded, through the series of experiments, that the GPS reflected signals need a special receiver (Liu et al., 2007). Martin-Neira designed bridgel, bridgelland bridge III tests of PARIS altimeter in Holland in September 1997, June 2001, and February 2003 respectively, and verified the possibility of GNSS-R altimetry by using the methods of C/A code phase delay and carrier phase measurement (Martin-Neira et al., 2001; Caparrini et al., 2003; Rivas and Martin-Neira, 2006; Liu et al., 2007). In 2003, the GNSS-R equipment carried by the UK-DMC satellite successfully obtained surface physical coefficients such as sea surface roughness. In 2014, the first GNSS-R satellite (TDS-1) was launched (Jin et al., 2017). These achievements have stimulated the interest of many researchers in GPS reflected signals and prompted countries, world-wide, to begin the exploration and research of GNSS-R technology, and thus, GNSS-R technology has been developed rapidly.

GNSS-R Remote Sensing Technology is a new and effective dual-base radar passive remote sensing technology, compared with the traditional remote sensing technology, and it has the advantage of rich signal sources, low cost, wide-coverage, low power consumption, all-weather, high spatio-temporal resolution, and other advantages. At present, GNSS-R has been widely used in ocean wind measurement, ocean altimetry, sea ice detection, ocean salinity detection, soil moisture detection, moving target detection, and other fields. GNSS-R ocean altimetry technology mainly includes five methods, which are code delay altimetry, carrier phase altimetry, carrier frequency variation altimetry, interference altimetry, delay-doppler map (DDM) altimetry, and signal-tonoise ratio (SNR) altimetry (Hu et al., 2020a).

The realization of GNSS-R ocean altimetry depends on the transmission of GNSS electromagnetic wave signals in space. Signal propagation in space will be affected by the ionosphere, troposphere, multipath, and more. These factors, as error terms, will affect the accuracy of GNSS sea surface measurement, so it is necessary to eliminate the influence of these errors as much as possible (Camps et al., 2014; Zhang et al., 2020b). Literature (Katzberg and Garrison, 2001) pointed out that the ionosphere on the satellite altimeter uses the high frequency signal of dozens of centimeters of distance error, single frequency altimeter is useful in a low electron concentration areas with the scientific research needed, high-precision ionospheric correction is inevitable, and double-frequency altimeters on the spacecraft will produce cost and problem complexity. The GNSS-R technique is proposed by the author to determine the ionospheric electron density near the satellite and analyze the possibility of this technique. The literature (Ruffini et al., 2001) also studied the feasibility of using spaceborne GNSS-R technology to study the ionosphere.

Through simulation experiments, the results showed that GNSS dual-frequency or multi-frequency signals could be used to estimate the ionospheric delay by GNSS-R technology and the dual-frequency pseudo-distance measurement and model prediction could be used to obtain the result that the measurement accuracy of 2 m could be improved after 1s integration. In terms of ionospheric detection, Chen Biyan proposed an improved ionization layer chromatography method which used the observation data of the ground GPS receiver to establish the regional ionospheric model and interpolated it to obtain sufficient TEC, and overcome the shortcomings of the empirical ionospheric model affected by spatial environment and distortion (Chen, 2012). Literature (Yan and Huang, 2016) proposed a method of using DDM to inversion the total electron content in the ionosphere over the ocean. The results are in good agreement with the IRI-2012 model. Based on the data of GPS, GLONASS, BDS and Galileo combined with MGEX network and IGS network, Ren Xiaodong established the ionospheric model based on the multisystem GNSS observation data and analyzed the accuracy of the model, and the results showed that the accuracy was similar to that of IGS products. At the same time, the un-difference ambiguity fixing technique is proposed to extract TEC. Compared with the traditional carrier phase smoothing pseudo distance, the accuracy of ionospheric TEC extracted by this method is significantly improved, which is of great value for the future extraction of TEC from short-period low-orbit satellite data (Ren, 2017). In other studies of GNSS-R application, researchers used models to correct atmospheric delay errors, which were divided into single-frequency navigation receivers using the global ionospheric model for correction, such as the Klobuchar model, and dual-frequency navigation receivers using a linear combination of carrier phase and pseudo-range code to eliminate ionospheric errors (Adriano et al., 2016). There is no systematic study on the variation law of atmospheric delay. In the study of the airborne GNSS-R reflected signal altimetry model, Zhang Yun only excluded the influence of the ionosphere on the experimental results theoretically but did not give the actual results in depth (Zhang et al., 2020b).

The troposphere is a non-dispersive medium. The delayed effect of the troposphere is only related to atmospheric refraction for electromagnetic wave signals and the delay effect is manifested as the propagation path increases and the propagation speed decreases. At present, the existing tropospheric delay correction models include the Saastamoinen model, the UNB3m model, the Hopfield model, and so on. In the application of GNSS-R, some scholars have noticed the influence of tropospheric delay and corrected it, but no specific algorithm or research has been presented. Nikolaidou explained the influence of the troposphere on experimental results for groundbased GNSS-R measurements in detail and showed the change of tropospheric delay from two components of the geometric and the along-path, which accounted for 50% each at low elevation angles, and with the increase of elevation angle, the proportion of the geometric component decreased and the proportion of the alongpath component increased. Based on the variation of altimetry platform height and elevation angle, the atmospheric correction is

Unlike previous research, this article is from the math geometric point of view, to subdivide the signal path from the receiver, GPS satellite, and specular reflection point actual spatial changes to study the ionosphere and troposphere effect for the GNSS-R sea surface altimetry, and explore the relationship between the satellite elevation angle with atmosphere delay, based on an airborne experiment, and extend the study to the spaceborne platform to provide a possibility to improve the precision of the spaceborne GNSS-R altimetry.

# MATERIALS AND METHODS

# **GNSS-R** Ocean Altimetry Model

According to the geometric path of signal propagation, the geometric path delay model of GNSS-R altimetry can be established as shown in **Figure 1**.

Path delay refers to the distance that the reflected signal experiences more than the direct signal. As shown in **Figure 1**, the total path delay is: (Katzberg and Garrison, 1997; Yang and Zhang, 2011):

$$\Delta \rho = \rho_E = \rho_r - \rho_i \tag{1}$$

According to the geometric relationship, it can be concluded that: (Yang and Zhang, 2011; Wang et al., 2021):

$$2h = \frac{\Delta \rho}{\cos\left(\frac{\pi}{2} - \theta\right)} \tag{2}$$

$$h = \frac{\Delta \rho}{2\sin\theta} \tag{3}$$

Where, *h* represents the height from the receiving platform to the reflecting surface, and  $\theta$  represents the satellite elevation angle at the mirror reflection point.

GNSS signals propagate through the ionosphere and troposphere in space, resulting in the atmospheric delay. Therefore, the distance relationship between the observed pseudo distance and the actual distance is:

$$\rho_e = \rho_p + \rho_{ion} + \rho_{tro} - c \cdot \delta t_i + c \cdot \delta t^j + \varepsilon$$
(4)

Among them,  $\rho_p$  represents the actual distance,  $\rho_{ion}$  represents the ionospheric delay,  $\rho_{tro}$  represents the tropospheric delay,  $\varepsilon$  represents other error terms,  $\delta t_i$  represents the receiver clock difference,  $\delta t^j$  represents the satellite clock difference, and c represents the speed of light. The path delay between the GNSS direct signal and the reflected signal is:

$$\begin{aligned} \Delta \rho &= \rho_e^r - \rho_e^d \\ &= \rho_p^r + \rho_{iono}^r + \rho_{tro}^r - c \cdot \delta t_i^r + c \cdot \delta t^{rj} + \varepsilon^r \\ &- \rho_p^d - \rho_{iono}^d - \rho_{tro}^d + c \cdot \delta t_i^d - c \cdot \delta t^{dj} - \varepsilon^d \\ &= \Delta \rho_p + \Delta \rho_{iono} + \Delta \rho_{tro} - c \cdot \Delta \delta t_i + c \cdot \Delta \delta t^j + \Delta \varepsilon \end{aligned}$$
(5)

Among them,  $\Delta \rho_{ion}$  represents the difference of the ionospheric delay between reflected signals and direct signals,  $\Delta \rho_{tro}$  represents



the difference of the tropospheric delay between reflected signals and direct signals. Substitute **Eq. 5** into **Eq. 3** while only considering the atmospheric delay, and it can be expressed as:

$$h = \frac{\Delta \rho_p + \Delta \rho_{ion} + \Delta \rho_{tro}}{2sin\theta} \tag{6}$$

Among them, the latter two atmospheric delays are the terms that affect the height accuracy of inversion:

$$\Delta h = \frac{\Delta \rho_{ion} + \Delta \rho_{tro}}{2\sin\theta} \tag{7}$$

#### **Ionospheric Delay Correction**

The ionosphere is a dispersive medium in which electromagnetic waves of different frequencies have different propagation paths and velocities. This effect is called ionospheric delay. For GNSS signals, the distance difference of the electromagnetic wave propagation path caused by ionospheric refraction can reach a maximum of 50 m in the vertical gradient direction and 150 m in the horizontal gradient direction (Wang, 2008). According to the A-H (Appleton-Hartree) equation, without considering the higher-order terms, the refraction index of the ionosphere is: (Yuan, 2002; Dong et al., 2018):

$$n = 1 - \frac{k}{f^2}, k = 40.3N_e \left(Hz^2m^3\right)$$
(8)

Among them,  $N_e$  represents the electron density along the path of the signal. Carrier phase signal and code signal go through

phase path and group path, respectively, in the ionospheric region and the corresponding delay is called phase lead and code delay. The phase refraction index is used respectively,  $n_p$ , group refraction index  $n_g$  combined with the mathematical equation, the TEC (Total Electron Content) indicates the total amount of electrons contained in the column per unit area of ionosphere, and it is generally representative  $10^{16}$ ~ $10^{17}$  electronic per square (Yuan, 2002; Camps et al., 2017; Taoufiq et al., 2018; Liu, 2020).

$$n_p = 1 - 40.3 \frac{TEC_{f_i}}{f_i^2}, n_g = 1 + 40.3 \frac{TEC_{f_i}}{f_i^2}$$
(9)

The phase lead caused by the ionospheric phase path is: (Yuan, 2002):

$$I = \int_{l_1}^{l_2} \left( n_p - 1 \right) dl = -\frac{40.3}{f_i^2} TEC_{f_i}$$
(10)

The code delay caused by the ionospheric group path is: (Yuan, 2002):

$$I = \int_{l_1}^{l_2} (n_g - 1) dl = \frac{40.3}{f_i^2} TEC_{f_i}$$
(11)

The ionosphere contains the most electrons at a distance of 130–500 km from the ground. For the convenience of research, the ionosphere is regarded as a compressed layer 450 km from the ground, which is called the ionospheric single layer model. The intersection point where the GPS signal passes through the model



is called the puncture point and the coordinates of this point can be obtained by the following equation: (Liu, 2020):

$$\gamma = \frac{\pi}{2} - \theta - \arcsin\left(\frac{R_e * \cos\theta}{R_e + h}\right)$$
$$\varphi_m = \arcsin\left(\sin\phi_n\cos\gamma + \cos\phi_n\sin\gamma + \cos A\right) \qquad (12)$$
$$\lambda_m = \lambda_n + \arcsin\left(\frac{\sin\lambda\sin A}{\cos\varphi_m}\right)$$

Among them,  $\varphi_m$ ,  $\lambda_m$  represents the longitude and latitude of the puncture point,  $\varphi_n$ ,  $\lambda_n$  represents the latitude and longitude of the receiver,  $\theta$  represents satellite elevation angle, A represents the azimuth of the satellite,  $\Upsilon$  represents the angle of the center of the earth,  $R_e$  is the radius of the earth, *h* represents the ionospheric monolayer height.

In this work, the GIM (Grid Ionospheric Model) products published by IGS (International GNSS Services) are used to obtain the electron concentration information. The ionospheric grid model divides the space into several grids according to a certain longitude and latitude and the intersection point of each grid is called the ionospheric grid point. At present, IGS divides the world into 5,183 grids according to the longitude from -180°-180° with an interval of 5° and latitude from -87.5°-87.5° with an interval of 2.5°. By interpolating the coordinate values of ionospheric grid points, VTEC at any position can be obtained. Compared with other ionospheric models, GIM can provide a wide range of ionospheric data and is not limited by the environment of the base station. The ionospheric products of the CODE analysis center have high accuracy (Li et al., 2017; Hu et al., 2020b; Liu, 2020), so the ionospheric products provided by CODE is selected for this research. Figure 2 shows the global ionospheric VTEC distribution map obtained from the GIM product provided by CODE at 10:00 on December 3, 2015.

In this work, the IDW (inverse distance weighting) method is used to interpolate the GIM to obtain the ionospheric VTEC value at the puncture point and then the STEC value in the signal path direction is calculated through the geometric relationship to obtain the ionospheric delay in the signal path direction.

The IDW method is based on the distance between the point to be solved and the surrounding known points, to determine the correlation degree between the point to be solved and the known points, to determine the weight coefficient, and to obtain the attribute value of the point to be solved (Wu et al., 2018). The closer the point to be solved is to the known point, the greater the weight. Using the IDW method, the expression of the zenith direction VTEC at the ionospheric puncture point is as follows: (Wu et al., 2018):

$$VTEC_{ion}^{j} = \begin{cases} \left(\sum_{i=1}^{n} \frac{VTEC_{ion}^{j}}{d_{ij}}\right) / \left(\sum_{i=1}^{n} \frac{1}{d_{ij}}\right), |d_{ij} < DR \\ VTEC_{ion}^{l}, |d_{ij} = 0 \end{cases}$$
(13)

Among them,  $VTEC_{ion}^{j}$  represent the VTEC value of j at the ionospheric puncture point to be solved,  $VTEC_{ion}^{i}$  represent the VTEC value at the ionospheric grid point i within the range of the ionospheric puncture point,  $d_{ij}$  represent the distance between the ionospheric puncture point j and the ionospheric grid point i, DR represent the distance threshold (Wu et al., 2018).

The value obtained through the above interpolate is the TEC in the zenith direction at the ionospheric puncture point, denoted as VTEC. In the calculation, the TEC along the propagation path of the signal is required, denoted as STEC. Usually, a projection function is used to convert STEC to VTEC. In this experiment, a single-layer projection function is used to convert VTEC to STEC. The projection function is as follows (Liu, 2020):

$$m(\xi) = \frac{1}{\cos \xi} = \frac{STEC}{VTEC}$$

$$\xi = \arcsin\left(\frac{R_e \times \cos \theta}{R_e + h}\right)$$
(14)

Among them,  $\xi$  represent the angle between VTEC and STEC at the ionospheric puncture point and the other values are consistent with the above.

In this work, we studied the process of the GNSS-R SSH measurement of atmospheric delay influence on measuring precision, and the VTEC at the ionospheric puncture point is obtained by interpolating the GIM production which is provided from IGS, which is then converted into the path direction STEC through the projection function. Finally, the corresponding ionospheric delay is obtained through **Eq. 15** (Yuan, 2002).

$$\rho_{iono} = \frac{40.3}{f^2} \times STEC \tag{15}$$

#### **Tropospheric Delay Correction**

From the ground to an altitude of about 60 km is the earth's atmosphere, of which about 8 km above the ground is the troposphere. When electromagnetic waves pass through the atmosphere, the signal propagation is delayed due to the change of medium density. About 80% of the atmospheric delay occurs in the troposphere, which is called the tropospheric delay. Nikolaidou has pointed out that delay caused by the troposphere is represented by signal velocity delay (linear refraction) and direction bending (angular refraction) (Nikolaidou et al., 2021). In the existing literature, the tropospheric delay for the direct and reflected paths above the receiving platform is offset. Nikolaidou believes this method has certain error defects and ignores the angular refraction delay of signal in space, and this delay will cause an additional atmospheric delay of geometric nature. Nikolaidou creatively analyzed the delay effect caused by signal angular refraction and pointed out that the along-path component and the geometric component must both, be considered in the calculation of tropospheric delay. The equation for the geometric component is as follows: (Nikolaidou et al., 2020a; Nikolaidou et al., 2020b; Nikolaidou, 2020c):

$$\rho_{tro}^g = 2H\delta\theta\cos\theta \tag{16}$$

The equation for the along-path component is as follows: (Nikolaidou et al., 2020a; Nikolaidou et al., 2020b; Nikolaidou, 2020c):

$$\rho_{tro}^a = 2HN_l \csc \theta' \tag{17}$$

Among them,  $\theta$  represent the satellite elevation angle in the vacuum,  $\theta'$  represent the satellite elevation angle in the presence of the atmosphere, *H* represent the height of the receiver (m),  $\delta\theta$  represent the difference between the elevation angle in the presence of the atmosphere and the elevation angle in the vacuum;

The equation of the geometric delay component for atmospheric altimetry correction is also given in the literature (Nikolaidou et al., 2021):

$$\Delta H_q = H \delta \theta \cot \theta \tag{18}$$

This experiment adopted the UNB3m model from the University of New Brunswick to calculate tropospheric delay for along-path component. This model is composed of the Saastamoinen model, Niel mapping function, and annual mean and amplitude table of meteorological parameters. The advantage is that no measured meteorological parameters are needed. The tropospheric delay can be calculated only from the information of altitude, latitude, and annual date.

The calculation equation is as follows, ZHD and ZWD, respectively, represent dry and wet delay of troposphere zenith,  $m_d$  and  $m_h$ , respectively, represent mapping functions of dry delay and wet delay:

$$\rho_{tro}^{a} = ZHD \times m_{d}(\theta) + ZWD \times m_{w}(\theta)$$
<sup>(19)</sup>

$$ZHD = \frac{10^{-6}k_1 R_d P_0}{g_m} \left[ 1 - \frac{\beta H}{T_0} \right]^{\frac{1}{R_d \beta}}$$
(20)

$$ZWD = \frac{10^{-6} \left(T_m k'_2 + k_3\right) R_d}{g_m \lambda' - \beta R} \times \frac{e_0}{T_0} \times \left[1 - \frac{\beta H}{T_0}\right]_{k=0}^{\frac{d^2}{R_d \beta} - 1}$$
(21)

Among them, g represent the acceleration of gravity,  $g_m$  represent the gravitational acceleration of the cylinder atmosphere, H represent the height of the station, R represent the dry air gas constant,  $T_m$  represent the average temperature of water vapor(K),  $k_1, k_2, k_3$  represent the refraction coefficient,  $\theta$  represent the elevation angle of satellite, meteorological parameter such as  $T_0$ ,  $P_0$ ,  $e_0$ ,  $\beta$ ,  $\lambda$  are calculated by the annual mean value table and amplitude table of meteorological parameter, as shown in (Leandro et al., 2006), which will not be discussed in this work.

Therefore, the total tropospheric delay is: (Nikolaidou et al., 2021):

$$\rho_{tro} = \rho_{tro}^a + \rho_{tro}^g \tag{22}$$

When substituting **Eq. 22** into **Eq. 7**, the influence of atmospheric delay on altimetry results can be expressed as:

$$\Delta h = \frac{\Delta \rho_{iono}}{2\sin\theta} + \frac{\Delta \rho_{tro}^a}{2\sin\theta} + \frac{\Delta \rho_{tro}^g}{2\sin\theta}$$
(23)
$$= \frac{\Delta \rho_{iono}}{2\sin\theta} + \frac{\Delta \rho_{tro}^a}{2\sin\theta} + H\delta\theta\cot\theta$$

The last item is the influence value of the geometric component of tropospheric delay on altimetry results, which is consistent with the literature (Nikolaidou, 2020c).

# **EXPERIMENTAL DATA**

# Airborne GNSS-R Ocean Altimetry Experimental Data

The data were collected from an airborne experiment over the Baltic Sea of Finland by IEEE of Spain on December 3, 2015. During the experiment, the aircraft flew at an altitude of about 3 km and a flight speed of about 50 m/s (Li et al., 2018). The antenna collecting direct signals (RHCP, circularly polarized right hand) pointed to the zenith and the antenna collecting reflected



signals (LHCP, circularly polarized left hand) pointed to the ground. The direct signals and reflected signals were obtained by an antenna array of eight components, respectively. The signal is converted down through the RF module to the 35 MHz IF signal and then quantized and stored at a rate of 80 MHz at 1bit, and through the direct signal and reflected signal cross-correlation output one-dimensional delay waveform. The instrument control and data recording system consists of an industrial computer running Linux. The original data recording is turned off when the aircraft turns, and the spectrum analysis of the signals collected during the interval cannot be performed (Ribó et al., 2017).

The airborne experimental data of GPS time was 384702–386364s, and to avoid the impact of the plane turned, the plane turned period of 385121–385542s was removed so only the data of straight flight of the aircraft was selected as the experimental analysis data. The flight trajectory of the aircraft is shown in **Figure 3**, and PRN1 was selected as the signal source. The elevation angle of the satellite varies from 62.62°–72.30° in this time interval.

### Spaceborne GNSS-R Ocean Altimetry Data

The spaceborne data were derived from the products provided by the spaceborne GNSS-R satellite on June 27, 2019, and the satellite orbital altitude was 580 km. The data of different spaceboard platforms in different periods of the day were selected for analysis. The selected data creation time was 3: 33 and 20: 48 UTC on June 27, 2019 of spaceborne A platform and 3: 48 and 21: 03 UTC on June 27, 2019 of spaceborne B platform.

#### Validated Model

In this work, we adopted the method of DER tracking to obtain the delay of the reflected signal relative to the direct signal, so as to obtain the height h of the receiver platform relative to the reflected surface. After the height H of the platform relative to the reference ellipsoid is known, the SSH was obtained by the following equation:

$$h_{\rm SSH} = H - h \tag{24}$$



Due to the lack of measured data, the accuracy of SSH inversion was determined by comparing the inversion with the validation model. In this work, the global mean sea surface model (DTU15 model) explored by the University of Denmark Technical was used as the validation model and compare the SSH inversion of considering the atmospheric delay or not, and to observe the results of atmospheric delay correction.

# **RESULTS AND DISCUSSION**

#### Modified Results of Airborne Experiments

In the experiment of airborne GNSS-R sea surface altimetry, the spatial process of the signal can be divided into three parts.



The first part is the path between the GPS satellite and the airborne receiver, which is the direct signal transmission path. During the transmission, the signal through the ionosphere and troposphere suffers from the ionospheric delay and tropospheric delay. The second part is the path between the GPS satellite and the specular reflection point. The signal through the ionosphere and troposphere. The third part is the path of the signal between the airborne receiver and the specular reflection point. As the altitude of the aircraft is only about 3km, the ionospheric delay and tropospheric delay are not considered at this stage.

In this work, the ionospheric delay of each part is calculated by the Klobuchar model and **Eq. 15**, the tropospheric delay geometric component of each part is calculated by **Eq. 16**, the tropospheric delay along-path component of each part is calculated by the UNB3m model, we then take the difference between the first part and the second part, and the result is the atmospheric delay experienced during the experiment, which is substituted into **Eq. 23** to obtain the influence of atmospheric delay on altimetry results.

Figure 4 shows the atmospheric delay obtained by PRN1 satellite as signal sources. The blue line represents the tropospheric delay, the red line represents the ionospheric delay calculated by the Klobuchar model, and the black line represents the ionospheric delay calculated by the GIM product. Figure 5 shows the atmospheric delay as a function of satellite elevation angle (left) and the relative contribution of the two components to the total delay (right), the red line represents the delay component of along-path, and the black line represents the delay component of the geometric. Figure 6 shows the SSH inversion results of PRN1, the black line represents the SSH provided by the DTU15 model, the red line represents the SSH inversion without considering atmospheric delay, and the blue line represents the SSH inversion which is considering atmospheric delay.



# Modification Results of Spaceborne Experiments

In the spaceborne GNSSS-R altimetry experiment, the transmission path of electromagnetic wave signals is the same as that in the airborne experiment. The difference is that in the spaceborne experiment, since the receiver is carried on a satellite running at a height of 580 km, the direct signals travel only through the ionosphere and are not affected by the troposphere. The reflected signals travel not only through the ionosphere but also through the troposphere. **Figure 7** shows the relation between the atmospheric delay by different satellites and the satellite elevation angle at the specular reflection point in the experiments in each period above. The horizontal axis represents SOW (Second of the week), while the vertical axis represents



ionospheric delay, tropospheric delay, and satellite elevation angle from top to bottom.

# DISCUSSION

By analyzing **Figure 4** to **Figure 6**, it is obvious that in the airborne platform GNSS-R altimetry experiment, the influence of the ionosphere on the altimetry is negligible, while the troposphere has a meter-level delay effect on the signal. At  $69.5^{\circ}$  elevation angles, the geometric delay component is almost 0.59 m which accounts for 41% of the total delay, the along-path delay component is almost 0.85 m which accounts for 59% of the total delay. At 71.5° elevation angles, the geometric

delay component is almost 0.48 m which accounts for 36% of the total delay, the along-path delay component is almost 0.84 m which accounts for 64% of the total delay. And with the increase of the elevation angle, the proportion of the along-path component is increased and the proportion of the geometric component is decreased. The comparison with the DTU15 model shows that the accuracy of SSH inversion is higher after eliminating atmospheric delay error. In this work, mean absolute error (MAE) and Standard Deviations (STD) were taken as the evaluation criteria of the experiment. Meanwhile, **Eq. 25** was used to calculate the average value of the influence of tropospheric delay on the altimetry results in this period, which was represented by Mean, the calculation equation is as follows: (Zhang et al., 2021):

TABLE 1 | Results of airborne altimetry experimental data.

| MAE/m  | Along-path component | 0.005 |  |
|--------|----------------------|-------|--|
|        | Geometric component  | 0.041 |  |
| STD/m  | Along-path component | 0.004 |  |
|        | Geometric component  | 0.026 |  |
| MEAN/m | Along-path component | 0.466 |  |
|        | Geometric component  | 0.264 |  |
|        |                      |       |  |

TABLE 2 | The average statistical results of the influence of atmospheric delay.

|        | Elevation (°) | 28–40 | 40–50 | 50–60 | 60–70 | 70–80 | 80–90 |
|--------|---------------|-------|-------|-------|-------|-------|-------|
| A-0333 | lono_mean/m   | 2.261 | 2.070 | 1.452 | 1.289 | 1.062 | 0.591 |
|        | Tro_mean/m    | 7.236 | 5.390 | 3.961 | 2.844 | 2.271 | 2.505 |
| A-2048 | lono_mean/m   | 1.861 | 1.621 | 1.201 | 0.957 | 0.866 | 0.732 |
|        | Tro_mean/m    | 7.552 | 5.332 | 3.734 | 3.054 | 2.647 | 2.552 |
| B-0348 | lono_mean/m   | 1.972 | 1.733 | 1.358 | 0.896 | 0.660 | 0.570 |
|        | Tro_mean/m    | 7.101 | 5.311 | 3.634 | 3.165 | 2.631 | 2.544 |
| B-2103 | lono_mean/m   | 1.727 | 1.396 | 0.834 | 0.619 | 0.583 | 0.497 |
|        | Tro_mean/m    | 7.521 | 5.043 | 3.793 | 3.030 | 2.666 | 2.562 |

$$MAE = \frac{1}{n} \sum_{a=1}^{n} (|\tilde{x}_a - x_a|)$$
  

$$STD = \sqrt{\frac{1}{n} \sum_{a=1}^{n} (|\tilde{x}_a - x_a| - MAE)^2}$$
  

$$MEAN = \frac{1}{n} \sum_{a=1}^{n} \frac{\tilde{x}_a}{2\sin\theta}$$
(25)

Among them,  $\tilde{x}_a$  represent the tropospheric delay value,  $x_a$  represent average tropospheric delay,  $\theta$  represent the elevation angle at the specular reflection point. **Table 1** shows data statistics of airborne experimental results.

For the results of the spaceborne experiment, the elevation angle of the specular reflection point is divided into  $10^{\circ}$  intervals in this work, and the average value of atmospheric delay on altimetry measurement influence is statistically calculated. The mean value of ionospheric influence is Iono-mean and the mean value of tropospheric influence is Tro-mean. The statistical results are shown in **Table 2**, and the naming rules are shown as above.

Zhang Qiuyang analyzed the corresponding ionospheric delay measurement values in eight different regions of the world in the spaceborne GNSS-R experiment (Zhang et al., 2020a), and the results showed a meter-level accuracy. Among them, the ionospheric delay at a place close to this experimental site shows a fluctuation of about 6 m. In the experiment, Zhang Yun used the international reference ionospheric model to conduct ionospheric correction on the spaceborne GNSS-R altimetry experiment and the delay error was about 15 m (Zhang et al., 2021). In the experiment data, it was found that the spaceborne GNSS-R altimetry is greatly affected by the ionosphere and the troposphere, and the order of magnitude results are the same as those in the above literature, which is an error term that must be considered to improve the measurement accuracy. Same as in the airborne experiment, the larger the elevation angle, the smaller the ionospheric delay and the tropospheric delay. As shown in **Figure 7**, when the elevation angle increases, the error effect caused by the ionosphere and troposphere decreases, the tropospheric delay mainly varies within the range of 4-10 m, and the ionospheric delay is generally less than 6 m. By choosing the suitable elevation angle and correcting the atmospheric delay error, the accuracy of GNSS-R ocean altimetry can be improved by  $3\sim 5$  m.

# CONCLUSION

As a new remote sensing measurement technology, GNSS-R has gradually attracted the attention of scholars at home and abroad. Land-based and space-based research and experiments have also achieved remarkable success. However, the research on the spaceborne platform is limited by hardware conditions and there is little research on it at home and abroad. It is not difficult to predict the development prospect of the GNSS-R application on a spaceborne platform. High precision measurement results are the key to the popularization of GNSS-R technology. Electromagnetic waves, as a signal transmission medium, are bound to be affected by the space environment. Therefore, it is necessary to deeply conduct study and exploration on atmospheric delay correction in the signal transmission process.

In this work, the influence of ionosphere and troposphere on the results of GNSS-R altimetry was analyzed by studying the variation of atmospheric delay. Research shows that:

- 1) In the airborne altimetry experiment, the accuracy of GNSS-R sea surface altimetry measurement can be improved effectively by atmospheric delay correction. Because the airborne platform is too low relative to the ionosphere, the influence of the ionosphere on altimetry can be ignored. The troposphere has a meter-level delay effect on the signal, at 69.5° elevation, the geometric delay component account for 41% of the total delay, the along-path delay component account for 59% of the total delay, at 71.5° elevation, the geometric delay component account for 36% of the total delay, the along-path delay. With the decrease of the elevation angle, this effect also decreases. Compared with the DTU15 model, it can be seen that the accuracy of SSH inversion is significantly improved by about 0.7 m after eliminating atmospheric delay.
- 2) In the spaceborne altimetry experiments, the ionospheric delay and tropospheric delay are both error terms that must be corrected to improve the measurement accuracy. The direct signal is only through the ionosphere above the GNSS-R orbit, not through the troposphere. The reflected signal passes through the entire ionosphere once and the ionosphere below the GNSS-R orbit once, and passes through the troposphere twice. Through calculation, the atmospheric delay error in the spaceborne GNSS-R altimetry fluctuates within the range of 5–16 m and the influence on the altimetry precision is in the range of 3~5 m.

3) The SSH is a function of elevation angle and the path delay, and the atmospheric delay function is also associated with the elevation angle. Both airborne and spaceborne experiments also show that the atmospheric delay at a high elevation angle is less than that at low elevation angle. Therefore, increasing the altitude cutoff angle of the satellite can effectively improve the data quality in experimental collection.

# DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding authors.

# **AUTHOR CONTRIBUTIONS**

ZY scientific analysis and manuscript writing. WZ and FW experiment design, program management, review, and editing. All authors contributed to the article and approved the submitted version.

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