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A multi-algorithm approach for modeling coastal wetland eco-geomorphology

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Coastal wetlands play an important role in the global water and biogeochemical cycles. Climate change makes it more difficult for these ecosystems to adapt to the fluctuation in sea levels and other environmental changes. Given the importance of eco-geomorphological processes for coastal wetland resilience, many eco-geomorphology models differing in complexity and numerical schemes have been developed in recent decades. However, their divergent estimates of the response of coastal wetlands to climate change indicate that substantial structural uncertainties exist in these models. To investigate the structural uncertainty of coastal wetland eco-geomorphology models, we developed a multi-algorithm model framework of eco-geomorphological processes, such as mineral accretion and organic matter accretion, within a single hydrodynamics model. The framework is designed to explore possible ways to represent coastal wetland eco-geomorphology in Earth system models and reduce the related uncertainties in global applications. We tested this model framework at three representative coastal wetland sites: two saltmarsh wetlands (Venice Lagoon and Plum Island Estuary) and a mangrove wetland (Hunter Estuary). Through the model-data comparison, we showed the importance of using a multi-algorithm ensemble approach for more robust predictions of the evolution of coastal wetlands. We also found that more observations of mineral and organic matter accretion at different elevations of coastal wetlands and evaluation of the coastal wetland models at different sites in diverse environments can help reduce the model uncertainty.

KEYWORDS

coastal wetland, eco-geomorphology, model uncertainty, mineral accretion, organic matter accretion

1 Introduction

Coastal wetlands, such as tidal marshes and mangroves, are valued for providing many important ecosystem services, including coastline protection, storm surge attenuation, wildlife habitat, and water quality improvement. In particular, they are observed to sequester atmospheric carbon dioxide at a rate much higher than other ecosystems, thus offering a potential nature-based solution for climate mitigation (Aburto-Oropeza et al., 2008; Temmerman et al., 2013; Teuchies et al., 2013; Macreadie et al., 2019). Despite the resilience of coastal wetlands to past fluctuations in sea level and climate over long periods of time

(Cahoon et al., 2006; Saintilan et al., 2020; Törnqvist et al., 2020), recent observations of local wetland loss raise concerns over their acclimation to intensified natural and human-induced disturbances, such as sea level rise (SLR), storm surge, sediment supply reduction, eutrophication, and drought (Blum and Roberts, 2009; Deegan et al., 2012; Kirwan and Megonigal, 2013; Crosby et al., 2016; FitzGerald et al., 2021; Törnqvist et al., 2021).

Eco-geomorphological processes, such as mineral accretion and organic matter (OM) accretion, play crucial roles in the acclimation of coastal wetlands to natural and human-induced disturbances (Craft et al., 2009; Howes et al., 2010; Kirwan et al., 2016; Leonardi et al., 2016; Schuerch et al., 2018). Mineral accretion is a process of mineral sediment accumulation on the soil bed of coastal wetlands through either plant-mediated particle settling or direct capture of sediment by plant stems (Kirwan and Mudd, 2012) and can help coastal wetlands build elevation against rising sea levels (Cahoon et al., 2021). With the accumulation of plant litter in the soil column, OM accretion can also help raise the bed elevation of coastal wetlands (Kirwan and Mudd, 2012). Due to the importance of these eco-geomorphologic processes, many eco-geomorphology models with varying complexities and parameterization methods have been developed in recent decades (D'Alpaos et al., 2011; Fagherazzi et al., 2012; Kirwan et al., 2010; Marani et al., 2007; Mcleod et al., 2010; Rodríguez et al., 2017). The applications of these models at the regional, continental, and global scales have greatly advanced our understanding of the evolution of coastal wetlands under intensified environmental changes and provided valuable insights into the management and conservation of this ecosystem (Reyes et al., 2000; Mariotti and Fagherazzi, 2010; Kirwan and Mudd, 2012; Leonardi et al., 2016).

However, substantial structural uncertainty exists in these eco-geomorphology models, as indicated by their inconsistent predictions on the fate of coastal wetlands under accelerated SLR (Craft et al., 2009; Kirwan et al., 2010; Kirwan et al., 2016; Rodríguez et al., 2017; Schuerch et al., 2018). For example, using a model ignoring the adaptation of saltmarshes to SLR, Craft et al. (2009) estimated that saltmarshes will decrease in area by 45% by 2100 under the worst SLR scenario projected by the Intergovernmental Panel on Climate Change (IPCC). However, based on a saltmarsh with complex eco-geomorphological processes, a more recent study demonstrated that marshes could survive under a wide range of future SLR scenarios by building elevations (Kirwan et al., 2016). The structural uncertainty of the eco-geomorphology models has two sources. First, ecogeomorphology models can implement different parameterization schemes for the same process. For instance, there are at least seven different mineral accretion schemes implemented in various ecogeomorphology models (D'Alpaos et al., 2007; Fagherazzi et al., 2007; French, 2006; Kirwan and Mudd, 2012; Morris et al., 2012; Temmerman et al., 2003b; van de Koppel et al., 2005). Second, as explained above, eco-geomorphology models differ in the included processes.

Our understanding of the structural uncertainty of ecogeomorphology models is still limited. A few studies have strived to understand the uncertainty of coastal wetland eco-geomorphology models through model comparison (Kirwan et al., 2010) or model review (Mcleod et al., 2010; Fagherazzi et al., 2012). However, unlike the state-of-the-art methods used to compare some other

Earth system processes (Huntzinger et al., 2013; Schellnhuber et al., 2014; Jin et al., 2016; Tan et al., 2018; Guseva et al., 2020), model comparison and review can only provide an incomplete evaluation of model uncertainty (Fisher and Koven, 2020). For model review, the related studies mostly focused on analyzing highlevel features of eco-geomorphology models, such as capability and complexity, input requirements, spatial- and temporal-scale accountability, and practical applicability, but did not consider the real performance of the eco-geomorphology models in simulating coastal wetland dynamics under diverse environmental conditions (Mcleod et al., 2010; Fagherazzi et al., 2012). For model comparison, previous studies usually compared eco-geomorphology models at the ecosystem level with a focus on the overall response of coastal wetlands to SLR, and the participant models were commonly not configured under a consistent protocol. As a result, the model uncertainty associated with individual processes cannot be isolated, and not all estimated model uncertainties can be attributed to ecogeomorphologic processes (Kirwan et al., 2010). In addition, these model comparison studies were only conducted at specific or very few sites (Kirwan et al., 2010). It is, thus, unclear how well the knowledge gained at a specific site can be transferred to other environmental conditions.

Algorithm-level model comparison approaches have shown promising skills for assessing the uncertainty of a particular process in large-scale models (Donatelli et al., 2014; Jin et al., 2016; Tan et al., 2018). Motivated by these studies, we developed an algorithm-level model comparison framework to investigate the structural uncertainty of coastal wetland ecogeomorphology models. The efficacy of the framework is evaluated at coastal wetland sites under distinct environmental conditions. Through this work, we aim to evaluate the algorithm-level uncertainties of coastal wetland eco-geomorphology modeling related to mineral and OM accretion and explore possible ways to reduce the related uncertainties in global applications.

2 Materials and methods

2.1 Model description

We developed a multi-algorithm coastal wetland ecogeomorphology simulator (MACES) model framework to assess the structural uncertainty of eco-geomorphology models. The MACES framework consists of two components (Supplementary Figure S1): a one-dimensional (1D) transect-based hydrodynamic module (MACES-hydro) and an algorithm-level model comparison module that implements different eco-geomorphologic process algorithms (MACES-geomor). MACES-hydro simulates water level, tide velocity, significant wave height, bottom shear stress, suspended sediment, and other hydrodynamic conditions along a 1D coastal transect that varies from low-elevation open water at the ocean side to high-elevation upland at the land side (Figure 1). All ecogeomorphology algorithms in MACES-geomor (Table 1) use the same hydrodynamic conditions simulated by MACES-hydro to model eco-geomorphologic processes at each grid cell of the coastal transect. At the end of each year, MACES updates the transect elevation profile and land cover. A design feature of MACES is that a new coastal wetland eco-geomorphology model can be



Sketch of the coastal system and notations. L denotes the 1D transect domain of coastal landscapes, with L_f as the domain of tidal flats and L_w as the domain of coastal wetland. MSL is the mean sea level, MHT is the mean high tide water level, and WL is the water level. H, h, and η represent the water level relative to MSL, water depth, and bottom elevation relative to MSL, respectively. H_0 is the water level at the seaward boundary, and η_0 is the bottom elevation at the seaward boundary.

TABLE 1	Summary	of the M	IACES-geomor	eco-geomoi	phology	algorithms.
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Eco-geomorphology	Category	Algorithm	
	Only sediment deposition	F06 (French, 2006); T03 (Temmerman et al., 2003)	
	Both sediment deposition and vegetation trapping	KM12 (Kirwan and Mudd, 2012)	
Mineral accretion	Both sediment deposition and erosion	F07 (Fagherazzi et al., 2007); VDK05 (van de Koppel et al., 2005)	
	Sediment deposition, vegetation trapping, and erosion	DA07 (D'Alpaos et al., 2007); M12 (Morris et al., 2012)	
	No growth seasonality and static shoot:root ratio	M12 (Morris et al., 2012)	
OM accretion	Growth seasonality and static shoot:root ratio	DA07 (D'Alpaos et al., 2007); K16 (Kakeh et al., 2016)	
	Growth seasonality, dynamic shoot:root ratio, and dynamic carbon turnover	KM12 (Kirwan and Mudd, 2012)	

easily created by configuring MACES-geomor with a different combination of eco-geomorphologic algorithms. Although we focus on mineral and OM accretion, the developed framework can be extended to other eco-geomorphologic processes, such as landward migration and wave-action erosion.

The 1D transect-based coastal hydrodynamic model MACEShydro was developed mainly based on the work by Tambroni and Seminara (2012) and Carniello et al. (2005) for cross-section averaged physical variables on the coastal landscape. It simulates tide and storm surge propagation (Eqs 1, 2), wave generation and propagation (Eq. 3), and particle transport (Eq. 7). Tide and storm surge-driven water flows are governed by the 1D Saint-Venant equations (Tambroni and Seminara, 2012):

$$\frac{\partial h}{\partial t} + \frac{\partial (Uh)}{\partial x} = 0, \tag{1}$$

$$\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + g \frac{\partial H}{\partial x} + g \frac{U|U|}{C_z^2 h} = 0, \qquad (2)$$

where *h* is the water flow depth (m), *U* is the water flow velocity (m s^{-1}), *H* is the water surface elevation (m) relative to the mean sea level (MSL), *g* is the acceleration due to gravity (m^{1/2} s^{-1}), and *C_z* is Chézy's friction coefficient (m^{1/2} s^{-1}). The friction coefficient *C_z* is a function of bed roughness, vegetation stem size, and vegetation density. Wave generation and propagation in shallow waters are described by the conservation of the wave action *N*, which is defined as the ratio of wave energy *E* (J m⁻²) to the relative wave frequency σ . By using the linear wave theory, the wave action conservation equation can be simplified as follows (Carniello et al., 2005):

$$\frac{\partial N}{\partial t} + \frac{\partial (c_g N)}{\partial x} = \frac{S}{\sigma}.$$
(3)

The wave group celerity c_g is given Eq. 4 as follows (Mariotti and Fagherazzi, 2010):

$$c_g = \frac{\sigma}{2k} \left(1 + \frac{2kh}{\sinh\left(2kh\right)} \right),\tag{4}$$

where *k* is the wave number ($k = 2\pi/\lambda$, where λ is the wavelength). The wave energy source term *S* (Eq. 5) is determined by the wind wave generation S_{wg} , wind wave dissipation through bottom friction S_{bf} , white capping S_{wc} , and depth-induced breaking S_{brk} :

$$S = S_{wg} - S_{bf} - S_{wc} - S_{brk}.$$
 (5)

Both tide and storm surge-induced water flow and wind-induced waves contribute to the production of bottom shear stress τ_b , which is important for the modeling of sediment deposition and resuspension over the coastal landscape. As suggested by Soulsby (1997), the nonlinear interaction between these two forces can be evaluated using the below empirical formulation (Eq. 6):

$$\tau_b = \tau_{wave} + \tau_{curr} \left[1 + 1.2 \left(\frac{\tau_{wave}}{\tau_{curr} + \tau_{wave}} \right)^{3.2} \right],\tag{6}$$

where τ_{curr} is the bottom shear stress induced by water flow only and τ_{wave} is the bottom shear stress induced by wave only. The shear stress τ_{curr} is a function of water flow velocity U and water depth h, and the shear stress τ_{wave} is a function of significant wave height H_w , water depth h, and wave period T. The transport of the suspended sediment in the water column is governed by the advection-dispersion continuity equation (Maan et al., 2015):

$$\frac{\partial c_{ss}h}{\partial t} + \frac{\partial (Uc_{ss}h)}{\partial x} - \frac{\partial}{\partial x} \left(Kh \frac{\partial c_{ss}}{\partial x} \right) = -Q_m, \tag{7}$$

where c_{ss} is the depth-averaged suspended sediment concentration (SSC) (kg m⁻³), K is the dispersion coefficient (m² s⁻¹), and Q_m is the net sediment deposition rate (kg m⁻² s⁻¹). The net sediment deposition is defined as sediment deposition minus sediment resuspension, and the long-term average of Q_m equals to mineral accretion. For salinity and nutrients, it is assumed that their concentrations do not change during transport over the coastal landscape, and thus, the dynamics are directly controlled by inundation.

MACES-geomor implements seven widely used algorithms for mineral accretion (D'Alpaos et al., 2007; Fagherazzi et al., 2007; French, 2006; Kirwan and Mudd, 2012; Morris et al., 2012; Temmerman et al., 2003b; van de Koppel et al., 2005) and four algorithms for OM accretion (D'Alpaos et al., 2007; Kakeh et al., 2016; Kirwan and Mudd, 2012; Morris et al., 2012) (Table 1). Correspondingly, the change in transect elevation η (m) is calculated using the Exner equation (Eq. 8):

$$(1-\lambda)\frac{d(\rho_s\eta)}{dt} = Q_m + Q_{om},\tag{8}$$

where λ is the sediment porosity, ρ_s is the sediment wet bulk density (kg m⁻³), and Q_{om} is the OM accretion rate (kg m⁻² s⁻¹). The detailed descriptions of these eco-geomorphologic algorithms are given in Supplementary Material. It should be noted that for OM accretion, we included one more algorithm corresponding to the null hypothesis that OM accretion is negligible for the transect elevation change. Here, the algorithms of mineral and OM accretion were selected based on three criteria through a literature review. First, the selected algorithms must have been successfully applied in multiple studies (ideally for coastal wetlands under different environmental conditions). Second, the selected algorithms are substantially different from each other in mathematical formulations

and conceptual understanding. Third, the selected algorithms can be implemented using 1D hydrodynamics. Table 1 provides all the MACES-geomor algorithms and their characteristics. The free parameters of the mineral and OM accretion algorithms are given in Supplementary Tables S1, S2, respectively.

2.2 Numerical methods

We used a 1D Godunov-type central-upwind scheme (Kurganov and Levy, 2002) to discretize the spatial domain of the Saint-Venant equations, which include source terms due to bottom topography, the wave equation, and the particle transport equation. This finite volume scheme introduces a linear piecewise approximation to each grid cell with the superbee slope limiter (Roe, 1986) to achieve the solutions of both second-order accuracy in space and diminishing total variation. Because this scheme is very effective in suppressing spurious oscillation of the simulated water level in periodically flooded areas, it has been widely used as a numerical solver for coastal hydrodynamics (Liang and Marche, 2009). After spatial discretization, we used a fourth-order adaptive Runge-Kutta-Fehlberg method to discretize the hydrodynamic equations in the time domain to achieve second-order accuracy in time (Burden et al., 1978). In addition, to avoid negative particle concentrations, we incorporated a scheme described by Tan et al. (2015) into the Runge-Kutta-Fehlberg method to recursively curtail the running time step when large negative concentrations occur until the negative values are small enough to be assigned safely as zero.

One prominent feature of MACES is the use of a hybrid FORTRAN and Python programming approach to balance computational efficiency and software usability. The computationalintensive hydrodynamic module was written in FORTRAN and then converted to a Python package using f2py (Python Software Foundation, Fredericksburg, VA, United States). All the other modules, including eco-geomorphology, I/O, and settings, were written in Python 3 directly. As such, new algorithms for ecogeomorphology can be easily integrated into MACES in the future. Model input and output files are written in the NetCDF and Excel formats, and model settings are written in the user-friendly Extensible Markup Language (XML) format.

Model calibration of different MACES-geomor algorithms is conducted using the Python-version Parameter ESTimation tool (PyPEST). The PyPEST tool was developed by Liao et al. (2019) based on the model-independent parameter estimation code PEST (Doherty et al., 1994). PyPEST carries out the calibration process iteratively with six steps (parameter generation, model configuration, input data generation, model run in parallel, output extraction, and output post-processing) until the user-defined cost function threshold criteria are met (Supplementary Figure S1). It should be mentioned that only the parameters of MACESgeomor (Supplementary Tables S1, S2) are calibrated. For the parameters related to flow and waves (e.g., the reference Chézy's friction coefficient and the dispersion coefficient), default values are used at all the sites. Depending on data availability at different sites, different combinations of observed datasets are used to calibrate different geomorphology module algorithms with the consideration of module dependency. For example, the observed long-term mineral accretion rate and SSC are used to calibrate the mineral accretion algorithms. The observed long-term OM accretion rates and aboveground biomass are used to calibrate the OM accretion algorithms.

2.3 Model input and evaluation

MACES-hydro is validated against the observed or benchmark water level, significant wave height, and/or bottom shear stress without calibration. In the experiments to validate MACES-hydro, we configured the model with null mineral and OM accretion algorithms and chose the method proposed by Morris et al. (2012) to calculate the aboveground biomass. In the experiments to validate the simulated suspended sediment, we only compared mineral accretion algorithms and used only one OM accretion algorithm at each site that simulated the most realistic aboveground biomass. Because the related observations and benchmark estimates usually cover only a few days, the related validation is only run for a few weeks. For MACES-geomor, our analysis focuses on analyzing the uncertainty of mineral and OM accretion algorithms across the 1D wetland transects, which is important for explaining their divergent predictions in coastal wetland evolution under SLR (Tambroni and Seminara, 2012).

We evaluate the model at three representative coastal wetland sites, with two located in midlatitude and one located in the subtropics: Venice Lagoon, Plum Island Estuary, and Hunter Estuary (Table 2). Venice Lagoon is a microtidal wetland with a large central waterbody and extensive intertidal saltmarshes. The dominant saltmarsh species include Limonium serotinum, Puccinellia palustris, Arthrocnemum fruticosum, and Spartina maritima. The long-term mineral and OM accretion rates of the saltmarsh are 3.5 mm yr^{-1} and $132 \text{ gC m}^{-2} \text{ yr}^{-1}$, respectively (Bellucci et al., 2007; Roner et al., 2016). Plum Island Estuary is a macrotidal wetland with extensive areas of productive tidal marshes. The dominant saltmarsh species include Spartina alterniflora at lower elevations and Spartina patens at higher elevations. The longterm mineral accretion rate can be as high as $6.9 \pm 0.9 \text{ mm yr}^{-1}$ (Wilson et al., 2014), and the long-term OM accretion rate is $69.9 \pm 9.4 \text{ gC m}^{-2} \text{ yr}^{-1}$ (Wang et al., 2019). Hunter Estuary is a microtidal wetland with gray mangrove (Avicennia marina) at lower elevations and a Sporobolus virginicus-Sarcocornia quinquefloramixed saltmarsh at higher elevations. The mineral accretion rates of mangroves and saltmarsh are 3.66 mm yr^{-1} and 3.37 mm yr^{-1} , respectively (Howe et al., 2009). The OM accretion rates of mangroves and saltmarsh are 105 gC m⁻² yr⁻¹ and 137 gC m⁻² yr⁻¹, respectively (Howe et al., 2009).

For Venice Lagoon, we use the observed water level, SSC, and significant wave height and benchmark bottom shear stress estimates from a 2D hydrodynamic model called the wind wave tidal model (WWTM) (Carniello et al., 2011) at two tidal flat stations (1BF, 1.1 masl; 2BF, 2.1 masl) for model evaluation. For Plum Island Estuary, we use the observed water level at the channel (-0.73 masl) and marsh edge (1.25 masl) of Nelson Island, observed SSC at the channel (-1.45 masl) and marsh interior (1.69 masl) of Law's Point, observed mineral accretion at three saltmarsh stations (LAC: a *S. alterniflora*-dominated high saltmarsh with an elevation of

1.4 masl; and MRS: a *S. alterniflora*-dominated high saltmarsh with an elevation of 0.89 masl), and observed aboveground biomass at LAC and MRS for model evaluation. For Hunter Estuary, we use the benchmark estimates of water level and SSC at four stations (channel: 0.22 mAHD; mangrove edge: 0.05 mAHD; mangrove interior: 0.38 mAHD; and saltmarsh edge: 0.65 mAHD) of the wetland for model evaluation. For a specific site, when validating our model over a station, we always choose the grid cell with the closest elevation to the station for comparison.

To simulate the hydrodynamics and eco-geomorphology of coastal wetlands, MACES is driven by the seaward-side water level, SSC, and averaged wind speed and air temperature over the coastal transect (Tan, 2023). We extracted the water level and wind conditions from high-frequency (10-min or 15-min) measurements for the three sites. The seaward boundary SSC was set based on the high-frequency (15-min) analytical estimates for Hunter Estuary and fixed values extracted from the global coastal Database for Impact and Vulnerability Analysis (DIVA) to sea level rise (Vafeidis et al., 2008; Schuerch et al., 2018) for the other two sites. The daily air temperature was extracted from measurements for Venice Lagoon and Plum Island Estuary and the European Center for Medium-Range Weather Forecasts (ECMWF) Interim Reanalysis (ERA-Interim) (Dee and Uppala, 2009) for Hunter Estuary.

For each site, we constructed its 1D transect from a highresolution digital elevation model (DEM) and land cover maps (Hawker et al, 2022; Hopkinson and Valentine, 2005; Tambroni and Seminara, 2012; Ye and Pontius, 2016; Rodríguez et al., 2017) by 1) dividing all grid cells into 17 elevation groups spanning from -12.5 m to 16.5 m (some elevation groups can be empty); 2) calculating the average slope and land cover fractions of each elevation group; and 3) calculating the transect length of each elevation group based on its slope and elevation range. For the first step, the elevation range of the 17 groups is the largest (i.e., 4 m) near the land and sea edges and the smallest (i.e., 0.5 m) near the sea level. For the third step, the slope of a grid cell is calculated by dividing its elevation by its distance to the nearest channel network. The constructed 1D transects of the three sites are shown in Figure 2.

3 Results

3.1 Simulated hydrodynamics

The MACES model can reproduce the observed hydrodynamics at the three coastal wetland sites. The simulated hydrodynamics at Venice Lagoon were validated into two periods of very different tide and wind conditions: 12/10/2002-12/11/2002 and 4/2/2003-4/4/2003 (Figure 3). Specifically, the spring period in 2003 had a high tide of 64 cm asl and a maximum wind speed of 17.3 m s⁻¹ (Supplementary Figure S3). In contrast, the winter period in 2002 had a much smaller high tide and maximum wind speed of only 38 cm asl and 11.6 m s⁻¹, respectively (Supplementary Figure S3). The 1D MACES-hydro performs reasonably well in capturing the observed tide and wave dynamics in both periods (Figure 3), with low root mean square errors (RMSEs) of simulated water depth and significant wave height at the 1BF and 2BF stations. During the low-wind and tide period when observations are available

Site name	Location	Tidal range (m)	Wetland	Evaluation data	Data source
Venice Lagoon	45°33′N/12°27′E	0.84	Salt marshes	Water level, significant wave height, suspended sediment, bottom shear stress, long-term mineral accretion, and long-term OM accretion	Bellucci et al. (2007), Carniello et al. (2011), Carniello et al. (2012), and Roner et al. (2016)
Plum Island Estuary	42°49′N/70°49′W	4.45	Saltmarshes	Water level, suspended sediment, aboveground biomass, long-term mineral accretion, and long-term OM accretion	Coleman and Kirwan (2020), Giblin (2018), Giblin (2019), Morris and Sundberg (2006), Morris and Sundberg (2020), Vallino (2018), Wang et al. (2019), and Wilson et al. (2014)
Hunter Estuary	32°55′S/151°48′E	1.11	Mangroves and saltmarshes	Water level, suspended sediment, long-term mineral accretion, and long-term OM accretion	Howe et al. (2009), Sandi et al. (2018), and Rodríguez et al. (2017)

TABLE 2 Characteristics and observational data of the three coastal wetland sites.



(Figures 3A–D), the RMSEs of the simulated water depth at 1BF and 2BF are 5.8 cm and 4.2 cm, respectively, which correspond to only 5% and 2% of the observed mean water depth, and the RMSEs of the simulated significant wave height at 1BF and 2BF are 4.7 cm

and 4.6 cm, respectively, which correspond to 35% and 19% of the observed mean significant wave height. The error in simulating the significant wave height at 1BF is higher than that at 2BF. Particularly, the MACES-hydro substantially overestimates the significant wave

height at 1BF on 10 December 2002. This is probably because 1BF is a shallower and more inland station with denser vegetation covers, and our model has large uncertainties in representing the effect of vegetation on wave damping. Despite the larger error, given the reduced wave energy at 1BF, the error of simulating the bottom shear stress did not increase significantly. As shown in Figures 3K,L, the model captures the temporal variability of the bottom shear stress benchmark at 1BF and 2BF during the high-tide and wind periods, with RMSE values of 0.13 Pa and 0.15 Pa, respectively. However, it should be mentioned that as the simulated bottom shear stress is compared to the WWTM benchmark instead of observations, the evaluation could be marked by substantial uncertainty.

For both periods, the simulated significant wave height mainly followed the wind dynamics (Figure 3). The wind-induced bottom shear stress is also the dominant component of the total bottom shear stress (Figure 4). On the morning of 12/10/2002, when wind speed exceeded 11 m s⁻¹, the simulated significant wave height reached its peak value at the two stations: 22.6 cm and 39.4 cm, respectively. Correspondingly, the simulated bottom shear stress also reached its peak value at the two stations, i.e., 0.19 and 0.31 Pa, respectively. On 3 April 2003, when wind speed frequently exceeded 15 m s⁻¹, the simulated significant wave height reached its peak value at the two stations, i.e., 31.4 and 52.4 cm, respectively. The contribution of the current-induced bottom shear stress to the total bottom shear stress never exceeded 10% in both periods (Figures 3E,F, I-K), showing that wind action dominates the generation of bottom shear stress. Both the observations and simulations show that 2BF has larger, more significant wave height values than 1BF. This difference could be explained by the attenuation of wave energy by friction when the wave moves toward land as 2BF is deeper and closer to the seaward boundary than 1BF.

The simulated hydrodynamics at Plum Island Estuary were validated in the summer and fall periods of 2017 (7/19–7/22 and 10/7–10/10, respectively) when tide and wind conditions were different (Figure 4). In the summer period, the tide level varied substantially, while the wind speed never exceeded 6 m s⁻¹ (Supplementary Figure S4). In contrast, in the fall period, the wind speed sometimes exceeded 8 m s⁻¹, while the tide level varied moderately (Supplementary Figure S4). For both periods, MACES-hydro captures the observed dynamics of the water depth at a river channel station (–0.73 masl) and a saltmarsh station (1.25 masl) reasonably well (Figure 4). The RMSE values of the simulated water depth at the river channel station were 9.1 cm and 7.5 cm for the summer and fall periods, respectively. The RMSE values of the simulated water depth at the saltmarsh station were 2.2 and 1.5 cm for the summer and fall periods, respectively.

The simulated hydrodynamics at Hunter Estuary were validated in the period of 9/28/2004–9/30/2004 for both low-elevation locations where mangrove species reside and high-elevation locations where saltmarsh species reside (Figure 5). MACEShydro well reproduced the water depth benchmark at four representative locations: the river channel station (Figure 5A), the mangrove-dominated station (Figure 5B), the mangrovedominated interior station (Figure 5C), and the saltmarshdominated station (Figure 5D). The RMSE values of the simulated water depth at the four stations were 4.6 cm, 5.4 cm, 2.7 cm, and 0.4 cm, respectively. Importantly, as shown by our simulations, the water level across a coastal wetland transect is far from being spatially uniform if the seaward boundary is not extremely close to the shoreline. For instance, at Venice Lagoon and Plum Island Estuary, where the distance from the seaward boundary to the shoreline is more than 18 km and 0.7 km, respectively, the water level peaks in the wetland interiors clearly lagged those at the boundary (Figures 3, 4), showing the effect of bed roughness on water flow. In contrast, at Hunter Estuary, where the seaward boundary is very close to the shoreline (only 20 m in distance), the difference between the simulated water level and the boundary condition is negligible (Figure 5).

3.2 Simulated suspended sediment dynamics

The MACES model can capture the dynamics of the suspended sediment at the three coastal wetland sites when appropriate mineral accretion algorithms are selected. For Venice Lagoon, the observed SSC at 1BF during the low-wind and tide period ranged from 7.3 to 92.0 mg L⁻¹ (Figure 6), with one larger peak value occurring on the windy morning of 12/10/2002 and one smaller peak value occurring on the morning of 12/11/2002 (Figure 3). Three out of the seven mineral accretion algorithms, including M12, F07, and DA07, can reproduce the observed two SSC peaks (Figure 6). Among the algorithms, the F07 algorithm has the lowest RMSE of 12.0 mg l⁻¹ and the lowest normalized RMSE (NRMSE) of 0.45. However, even the three best-performing algorithms overestimated the SSC at mid-day on 12/10/2002. A possible reason is that the model does not reproduce the rapid decrease in wave energy after the windy morning on 12/10/2002. The simulated SSC by F06, T03, and KM12 is almost constant because these algorithms do not represent sediment resuspension (Supplementary Material S1), and there is limited sediment deposition at 1BF. As a result, the SSC is almost entirely determined by the seaward boundary (9.4 mg L⁻¹), which was extracted from DIVA. It should be noted that the dynamics of the suspended sediment in the coast are notoriously difficult to model (Temmerman et al., 2003; Le Hir et al., 2007). Thus, the performance achieved by our 1D model is satisfactory.

For Plum Island Estuary, the MACES model reproduces the temporal variability in the SSC at the river channel station and the decrease in SSC from the river channel to the saltmarsh station in the summer period of 2017 reasonably well (Figure 7). Because the river channel station is close to the model boundary (Figure 2), its suspended sediment dynamics are strongly regulated by the SSC boundary condition (Supplementary Figure S4), and the difference between different algorithms is mainly caused by the simulated sediment deposition rather than the simulated sediment resuspension. Among the algorithms, the M12 algorithm has the lowest RMSE of 7.4 mg l⁻¹ and the lowest NRMSE of 0.57 at the river channel station. There are several SSC peaks at the river channel that our model fails to capture (Figure 7), which could be attributed to the uncertainty in the boundary condition. For the saltmarsh station, the performance of different algorithms is similar, implying that all the algorithms predicted reasonable sediment deposition over the saltmarsh platform.

The MACES model also captures the temporal variability in the SSC along the elevation gradient of Hunter Estuary,



Dynamics of the simulated (black solid line) and observed or benchmark (red solid line with dots) water level, significant wave height, and bottom shear stress at the two stations (1BF and 2BF) of Venice Lagoon during two time periods: 12/10/2002-12/11/2002 and 4/2/2003-4/4/2003. Black dashed lines in (A), (B), (G), and (H) represent the estimated water depth at the two stations by assuming that the water level is spatially uniform across the transect. Blue dashed lines in (C), (D), (I), and (J) represent the measured wind speed. Black dashed lines in (E), (F), (K), and (L) represent the simulated current-induced bottom shear stress.



Comparison of the simulated (black solid line) and observed (red dashed line) water depth at the channel station at an elevation of -1.45 masl (A,B) and the *Spartina*-dominated saltmarsh station at an elevation of 1.69 masl (C,D) in Plum Island Estuary during two time periods: 7/19/2017-7/22/2017 and 10/7/2017-10/10/2017. Black dashed lines represent the estimated water depth at the two stations by assuming that the water level is spatially uniform across the transect.

spanning from the river channel, through the mangrove edge and interior, to the saltmarsh edge (Figure 8). Because the river channel station, in this case, is even closer to the model boundary than in Plum Island Estuary (Figure 2), the dynamics of the suspended sediment are strongly regulated by the boundary condition (Supplementary Figure S5) before being fully deposited at the saltmarsh edge. The four more complex algorithms, namely, M12, F07, VDK05, and DA07, outperform the three simpler algorithms (i.e., F06, T03, and KM12). Overall, the M12 algorithm has the best performance at the four stations: an RMSE of 1.6 mg L⁻¹ at the river channel, 0.9 mg L^{-1} at the mangrove edge, 2.8 mg L^{-1} at the mangrove interior, and 0.4 mg L⁻¹ at the saltmarsh edge (we removed data points in the comparison when the simulated water depth was zero). These algorithms seem to underestimate the sediment deposition in the mangrove wetland area. Possibly, the mineral accretion algorithms we incorporated in the model were mostly developed for saltmarshes; thus, they are less applicable to mangrove wetlands.

3.3 Simulated mineral and OM accretion

By calibration, most of the MACES mineral and OM accretion algorithms can reproduce the observed long-term mineral and OM accretion rates at the three coastal wetland sites, especially when the accretion rates are only measured at single locations. However, different algorithms demonstrate remarkable variations in the simulated mineral and OM accretion along the elevation gradient. Moreover, our ensemble simulations show that the variations in the simulated mineral and OM accretion along the elevation gradient differ substantially among the coastal wetland sites.

For Venice Lagoon, all seven mineral accretion and four OM accretion algorithms can predict the observed long-term mineral accretion rate of 3.54 mm yr⁻¹ and the observed long-term OM accretion rate of 132 gC m⁻² yr⁻¹ at the observation station that is approximately 0.2 km from the marsh shore edge (Figure 9). Good model performance does not depend on which OM or mineral accretion algorithm is combined. For example, the F06 mineral accretion algorithm, when combined with the M12 OM accretion algorithm, performs comparably to that combined with the DA07 OM accretion algorithm. Despite the convergence of different algorithms at the observation station, the simulated summer aboveground biomass, OM accretion, and mineral accretion along the elevation gradient differ substantially among the algorithms (Figure 9). For the summer aboveground biomass at the saltmarsh, the M12 algorithm predicts an increasing trend with elevation, while the other three algorithms predict slight decreases (Figure 9A). Furthermore, the marsh aboveground biomass simulated by M12



Comparison of the simulated (black solid line) and benchmark (red dashed line) water depth at the channel station at an elevation of -0.22 mAHD (A), the mangrove edge station at an elevation of 0.05 mAHD (B), the mangrove interior station at an elevation of 0.38 mAHD (C), and the saltmarsh edge station at an elevation of 0.65 mAHD (D) of Hunter Estuary during 9/28/2004–9/30/2004. Black dashed lines represent the estimated water depth at these stations by assuming that the water level is spatially uniform across the transect.



is much higher than that simulated by the other algorithms (Figure 9A), even though the estimates are all within the reported range of $1-3 \text{ kg m}^{-2}$ (Tambroni and Seminara, 2012). Driven by

the change in aboveground biomass, the M12 algorithm predicts an increase in OM accretion with elevation, while the DA07 and K16 algorithms predict a decrease (Figure 9B). However, KM12 predicts an increase in OM accretion with elevation despite the decrease in simulated aboveground biomass. It is because KM12 simulates a much larger increase in the root:shoot quotient along the elevation gradient. For mineral accretion, the F06 and KM12 algorithms predict a moderate increase with elevation, the F07 and VDK05 algorithms predict a moderate decrease, and the other algorithms predict a rapid decrease (Figure 9C). As a result, the simulated mineral accretion differs remarkably at both the marsh shore edge and the marsh-upland interface. For example, at the saltmarsh edge, the estimate by T03 is over 6 mm yr⁻¹, but that by F06 is less than 4 mm yr⁻¹. In contrast, at 1.5 km to the edge, the estimate by T03 falls close to zero, but that by F06 is over 4 mm yr⁻¹. Importantly, our model can provide a multi-algorithm ensemble estimate of mineral and OM accretion over the saltmarsh, which shows that the total accretion gradually decreases along the elevation gradient with the importance of OM accretion moderately increasing (Figure 9D). However, mineral accretion is almost always the dominant source over the saltmarsh platform, which is a more robust signal detected by our multialgorithm approach.



For Plum Island Estuary, compared with more spatiotemporally resolved validation data, some mineral and OM accretion algorithms show better performance than others. For instance, while all the OM accretion algorithms provide satisfactory simulations of the summer aboveground biomass distribution along the elevation gradient, M12 seems to capture the higher saltmarsh biomass at the edge more reasonably (Figure 10A). In addition, the DA07 and KM12 algorithms can simulate the seasonality of the saltmarsh biomass at the high-marsh station LAC (1.1 masl), while the M12 and K16 algorithms cannot simulate any seasonality (Figure 10C). All the OM accretion algorithms successfully predict the observed longterm OM accretion rate $(69.9 \pm 9.4 \text{ gC m}^{-2} \text{ yr}^{-1})$ within the elevation range of 0-1.5 masl (Supplementary Figure S4). Furthermore, we find that all the mineral accretion algorithms except F06 and KM12 can reproduce the observed long-term mineral accretion rates at the S. alterniflora-dominated low marsh station MRS $(6.9 \pm 0.9 \text{ mm yr}^{-1})$, the *S. alterniflora*-dominated high-saltmarsh station LAC (5.3 \pm 0.1 mm yr⁻¹), and the S. patens-dominated highsaltmarsh station LPC $(2.3 \pm 0.1 \text{ mm yr}^{-1})$ (Figure 11D), which shows the decrease in mineral accretion along the elevation gradient. It implies that the use of F06 and KM12 at Plum Island Estuary may lead to biased predictions of the resilience of the saltmarsh to SLR. As in Venice Lagoon, the multi-algorithm ensemble estimate indicates that the total accretion gradually decreases along the elevation gradient with the importance of OM accretion increasing (Figure 10E). However, different from Venice Lagoon, OM accretion can dominate the total accretion in some high-marsh areas of Plum Island Estuary. This is possibly because the platform of Plum Island Estuary has a much larger elevation gradient than that of Venice Lagoon (Figure 2), which impairs the landward transport of suspended sediment.

For Hunter Estuary, different mineral and OM accretion algorithms can also reproduce the observed long-term mineral accretion rate $(3.66 \text{ mm yr}^{-1})$ and OM accretion rate $(105 \text{ gC m}^{-2} \text{ yr}^{-1})$ at the mangrove-dominated station (0.56 mAHD)

after calibration (Figure 11). All four OM accretion algorithms predict the decrease in aboveground biomass along the elevation gradient and from the mangrove-dominated area at low elevations to the saltmarsh-dominated area at high elevations (Figure 11A). The simulated aboveground biomass is consistent with the reported values of 1,000 and 900 g m⁻² for mangrove and saltmarsh, respectively (Rodríguez et al., 2017). Driven by aboveground biomass, the simulated OM accretion by M12, DA07, and K16 decreases along the elevation gradient (Figure 11B). The simulated OM accretion by KM12 increases with elevation despite the negative relationship between aboveground biomass and elevation. As discussed for Venice Lagoon, it is caused by a much larger increase in the root:shoot quotient along the elevation gradient parameterized in KM12. The discontinuity of the simulated OM accretion at the mangrove-saltmarsh boundary by DA07 is because the root:shoot quotient of saltmarsh species in the DA07 is set to be higher than that of mangrove species (Kakeh et al., 2016), but these quotient ratios may also vary depending on the hydrodynamic conditions and salinity gradient (Sandi et al., 2021). In Hunter Estuary, the simulated mineral accretion on the platform shows two spatial patterns: the nearly constant rate by the F06, T03, and KM12 algorithms and the decreasing rate by other algorithms (Figure 11C). Notably, in the latter group, the simulated mineral accretion rate at the wetland shore edge is well above 10 mm yr⁻¹, which is much higher than that at Venice Lagoon and Plum Island Estuary, but the variation in accretion across the section follows a similar general pattern as observed in other recent eco-geomorphic simulations in Hunter Estuary, which used a simplified 2D domain (Breda et al., 2021). The multi-algorithm ensemble estimates show that mineral accretion dominates the total accretion in all areas of the platform except the area close to the wetland-upland boundary (Figure 11D). As explained for Plum Island Estuary, it is mainly because the large platform slope at Hunter Estuary impairs the landward transport of the suspended sediment (Figure 2).



Comparison of the benchmark column-integrated suspended sediment concentration (black) with the suspended sediment concentration simulated by seven mineral accretion algorithms at the channel station at an elevation of -0.22 mAHD (**A**), the mangrove edge station at an elevation of 0.05 mAHD (**B**), the mangrove interior station at an elevation of 0.38 mAHD (**C**), and the saltmarsh edge station at an elevation of 0.65 mAHD (**D**) in Hunter Estuary during 9/28/2004–9/30/2004.

4 Discussion

4.1 Algorithm-level uncertainties in modeling coastal wetland eco-geomorphology

It is not surprising that significant algorithm-level uncertainties exist in the modeled eco-geomorphology at the three coastal wetland sites. However, our study shows that a multi-algorithm ensemble simulation approach may provide more robust signals about the evolution of coastal wetlands in different environments and, thus, help reduce the prediction uncertainty. For example, the multialgorithm ensembles reveal that it is critical to represent OM accretion in the coastal wetland eco-geomorphology models to realistically predict coastal wetland resilience under future SLR. This is because while OM accretion may only account for 10% of the total accretion at low-elevation saltmarshes or mangroves, its contribution to the higher-elevation areas is much larger and even surpasses the contribution of mineral accretion. As a result, ignoring OM accretion would cause a significant underestimation of coastal wetland survival (Lorenzo-Trueba et al., 2012; Morris et al., 2016; Mariotti et al., 2020; Keogh et al., 2021).

To reduce the algorithm-level uncertainty in the simulation of coastal wetland evolution, it is also important to constrain mineral and OM accretion algorithms using observations from at least two locations at different elevations of a coastal wetland site. For example, if mineral accretion was only observed at the *S. patens*-dominated high-saltmarsh station LPC and the F06 or KM12 algorithm was chosen for modeling, the prediction of the resilience of coastal wetlands to SLR would be severely biased. Thus, new observations should be prioritized to capture the elevation and vegetation gradients of mineral and OM accretion. Although we focus on the model structural uncertainty and, thus, carefully calibrate the model parameters for each algorithm in this study, the use of multi-location observations at different elevations can also help reduce the parameter uncertainty of eco-geomorphology



modeling. For instance, for Plum Island Estuary, if only the LPC station is benchmarked, even those good algorithms (i.e., T03, M12, F07, VDK05, and DA07), albeit reproducing the decrease in mineral accretion with elevation, would produce widespread estimates of mineral accretion at the low-marsh station MRS.

Although the existence of substantial algorithm-level uncertainties in coastal wetland eco-geomorphology models is expected, due to the variations in coastal wetland characteristics, such as tidal range, SSC, topography, and vegetation species, they cannot be fully learned by analyzing the mathematical formulations alone. Instead, these uncertainties must be carefully evaluated using a multi-algorithm approach like MACES. For example, as the mineral accretion algorithms F06 and KM12 use spatially constant SSC to derive sediment deposition, it would be expected that the estimated mineral accretion by these two algorithms is uniform over coastal wetland platforms. However, as simulated bottom shear stress decreases with water depth along the elevation gradient, the simulated force to resuspend the sediment decreases in higher-elevation wetlands, and correspondingly, sediment deposition is simulated to increase along the elevation gradient. Furthermore, this effect varies among the coastal wetland sites due to the differences in tidal range, topography, and vegetation species (Figures 9–11). Similarly, while it is expected that the simulated mineral accretion by M12, F07, VDK05, and DA07 would decrease with elevation because the modeled SSC in the interior areas decreases due to deposition, and sediment resuspension is weak over the vegetated platform, it is still difficult to discern which algorithm simulates the strongest decreasing effect without testing the algorithms in a united hydrodynamics model.

4.2 Modeling coastal wetland eco-geomorphology in diverse environments

Coastal wetlands are an important type of ecosystem spanning broad geographic regions, from tropical and subtropical mangroves and mid-latitude saltmarshes to arctic coastal tundra (Keddy, 2000). Through the application of a multi-algorithm model framework developed in this study, we show that the uncertainties in coastal wetland eco-geomorphology models should be evaluated for coastal



Comparison of the simulated aboveground biomass in July 2018 at three elevation zones by four MACES algorithms (A), comparison of the simulated long-term OM accretion by four MACES algorithms (B), comparison of the simulated monthly mean aboveground biomass during 2017–2018 at the LAC station by four MACES algorithms (C), comparison of the simulated long-term mineral accretion by seven MACES algorithms (D), and the mean (solid line) and standard deviation (shared area) of the simulated long-term total accretion and the contribution of OM accretion to total accretion (E) over the Plum Island wetland. Gray bars in (A), (C), and (D) represent the mean and standard deviation of the observed summer aboveground biomass, monthly mean aboveground biomass, and long-term mineral accretion, respectively.



accretion by four MACES algorithms (B), comparison of the simulated long-term mineral accretion by seven MACES algorithms (C), and the mean (solid line) and standard deviation (shared area) of the simulated long-term total accretion and the contribution of OM accretion to the total accretion (D) over the Hunter Estuary wetland. Black stars in (B) and (C) represent the observed long-term OM and mineral accretion at the mangrove-dominated station with an elevation of 0.56 mAHD, respectively.

wetlands in diverse environments. Previous studies that rely on the knowledge of a single type of coastal wetlands for the prediction of large-scale coastal wetland responses to SLR may lead to unreliable conclusions. For example, while Venice Lagoon and Plum Island Estuary are both saltmarshes, due to the difference in environments, substantial distinctions exist between the simulated mineral and OM accretion at the two sites, including the much more important role of OM accretion in the rise of the saltmarsh bed against SLR at Plum Island Estuary. Correspondingly, a multi-algorithm approach that includes diverse eco-geomorphology algorithms can be more capable of predicting large-scale coastal wetland evolution. As demonstrated in the study, MACES includes the mineral and OM accretion algorithms that can be applied to the most common plant species of coastal wetlands (Day Jr et al., 1999; Morris et al., 2002; Temmerman et al., 2003b; Mudd et al., 2004; Kirwan and Mudd, 2012; Crase et al., 2013; Liu et al., 2020): S. alterniflora, S. patens, P. palustris, S. maritima, and A. marina. Particularly, very few ecogeomorphology modeling studies have included both saltmarsh and mangrove. These algorithms can also be applied to different tidal ranges (microtidal and macrotidal) and climates (Mediterranean climate, humid continental climate, and humid subtropical climate).

As the algorithm-level uncertainties in eco-geomorphology models are site-dependent, this multi-algorithm model framework can also be used to select appropriate eco-geomorphology algorithms for specific coastal wetland environment. For example, our simulation indicates that it is better to avoid the use of F06 and KM12 to predict the evolution of coastal wetlands in an environment like Plum Island Estuary, but these two mineral accretion algorithms can still be useful for coastal wetlands like Venice Lagoon. To extend this algorithm selection strategy to the global scale, it would need related observations across diverse environments. Currently, many published datasets of mineral and OM accretion from coastal wetlands across broad regions exist (Chmura et al., 2003; Breithaupt et al., 2012; Lovelock et al., 2015; Crosby et al., 2016; Parkinson et al., 2017). The next step would be to identify and survey geographic and ecological factors that are crucial for the classification of coastal wetlands. Nevertheless, the development of this multi-algorithm coastal wetland eco-geomorphology model will facilitate the reduction of algorithm-level uncertainties in global applications.

4.3 Limitations

We chose to model coastal wetland eco-geomorphology on a simplified 1D coastal transect for several reasons: 1) higher computational efficiency; 2) consistency with large-scale land surface models; and 3) the easy representation of suspended sediment dynamics (Ward et al., 2020; Feng et al., 2022; Tan et al., 2022). However, this simplification implies that the MACES model cannot resolve the detailed spatial heterogeneity of coastal wetland dynamics that are needed for decision-making and damage mitigation. For instance, while the model can assess the overall wetland vulnerability under SLR, it cannot be used to locate specific areas for remedy as other more sophisticated models did (Deltares, 2022). Additionally, because the simulated variables are not linked to specific locations, the impact of SLR and other climate extremes on the ecosystem services of coastal wetlands cannot be reasonably evaluated using the current MACES framework. A possible solution is to use the emerging machine learning techniques to downscale low-fidelity, high-efficiency hydrodynamics models to emulate the high-fidelity, low-efficiency hydrodynamics models (Feng et al., 2023; Fraehr et al., 2023). For example, Fraehr et al. (2023) developed a hybrid low-fidelity, spatial analysis, and Gaussian process learning model to preserve the physics of 2D hydrodynamic equations, and the convolutional long short-term memory model (Tran et al., 2021) has been widely used to reduce the downscaling bias for data that vary both spatially and temporally. It is thus possible to map the 1D hydrodynamics simulated by MACES to the 2D high-fidelity hydrodynamics simulated by an advanced hydrodynamics model, such as Delft3D (Deltares, 2022), by combining the two techniques.

Although we intend to drive all the mineral and OM accretion algorithms under the same hydrodynamic conditions, particularly water level and SSC, due to the impact of vegetation on the transect surface roughness, the simulated hydrodynamics would be changed by the choice of mineral and OM accretion algorithms. As a result, the simulated differences between mineral and OM accretion may not be fully caused by the algorithm-level uncertainties. Furthermore, it should be noted that coastal wetland vegetation does not always serve as a sediment trap and, in some cases, can modify hydrodynamics to the extent that a dense plant cover repels overbank flow and sediment delivery (Olliver et al., 2020; Xu et al., 2022; Beltrán-Burgos et al., 2023). These nonlinear processes have not been represented in our model.

Another limitation of the model is the simplified representation of the biological and biogeochemical processes in MACES, which could limit the prediction accuracy of OM accretion. Despite the importance of macroclimatic drivers (particularly air temperature) to the evolution of coastal wetlands under climate change (Osland et al., 2016), the related effects are either neglected or only simply parameterized in the MACES algorithms (D'Alpaos et al., 2007; Kakeh et al., 2016; Kirwan and Mudd, 2012; Morris et al., 2012), which would cause biased estimates of sediment deposition, OM deposition, and coastal wetlands resilience (Schoutens et al., 2019). It is thus necessary to adopt some advanced developments in vegetation dynamics and biogeochemistry from more complex land surface models (Oleson et al., 2013).

Additionally, many other factors that can drive the ecogeomorphology of coastal wetlands have not been represented in the MACES model. These include land subsidence (Hasan et al., 2023), wave-driven coastal erosion (Leonardi et al., 2016), and wetland landward migration (Schuerch et al., 2018). For instance, the modeling of land subsidence needs to resolve the effects of both natural (e.g., site history) and anthropogenic disturbances (e.g., groundwater extraction). The modeling of wave-driven coastal erosion needs to account for the change in wind regimes. For wetland landward migration, both natural (e.g., steep slopes) and human barriers (e.g., cities) must be considered. These nonlinear factors will be included in future model development and tested under different scenarios to evaluate their impact on coastal wetlands.

5 Conclusion

We developed a multi-algorithm model framework, MACES, to evaluate the algorithm-level uncertainties in mineral and OM accretion modeling based on consistent hydrodynamic conditions. The MACES model can reproduce the observed dynamics of water depth, wave, and bottom shear stress, as well as the observed long-term mineral and OM accretion at three representative sites of coastal wetlands in diverse environments. As expected, our approach reveals significant algorithm-level uncertainties in coastal wetland eco-geomorphology modeling, which can lead to divergent estimates of the vulnerability of coastal wetlands to SLR. Importantly, we demonstrate that multi-algorithm ensemble estimates can provide more robust signals on the evolution of coastal wetlands. Thus, the approach should be more broadly explored in the future. Our study also indicates that the model uncertainty can be reduced by 1) including multiple observations of mineral and OM accretion along the elevation gradient of coastal wetlands and 2) evaluating the eco-geomorphology models at different sites in diverse environments. The MACES framework is a useful tool to test and compare different algorithms for modeling coastal wetlands and predict the fate of coastal wetlands under climate change at large scales.

Data availability statement

The datasets presented in this study can be found in online repositories. The names of the repository/repositories and accession number(s) can be found below. The MACES source code can be freely downloaded from Tan (2023) and will be routinely updated at https://github.com/tanzeli1982/MACES. The data used in this study are publicly available at Tan et al. (2023).

Author contributions

ZT: conceptualization, formal analysis, funding acquisition, investigation, methodology, project administration, resources, software, validation, visualization, and writing-original draft. LL: conceptualization, funding acquisition, supervision, and writing-review and editing. CL: software and writing-review and editing. LC: data curation, resources, and writing-review and editing. JR: data curation, resources, and writing-review and editing. PS: data curation, resources, and writing-review and editing. SS: data curation, resources, and writing-review and editing.

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Supplementary material

The Supplementary Material for this article can be found online at: https://www.frontiersin.org/articles/10.3389/feart.2024. 1421265/full#supplementary-material

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