



# Economic Evaluation of Combined Heat and Power Integrated With Food Waste-Based Ethanol Production

Noor Intan Shafinas Muhammad<sup>1,2</sup> and Kurt A. Rosentrater<sup>1</sup>\*

<sup>1</sup>Agricultural and Biosystems Engineering Department, Iowa State University, Ames, IA, United States, <sup>2</sup>Faculty of Civil Engineering Technology, Universiti Malaysia Pahang, Kuantan, Malaysia

The concern of food waste (FW) impact on the environment, societies, and economies, has triggered many researchers to find alternative ways to utilize these materials. FW can be high in glucose and other sugars (depending upon the food used) and has the potential to be converted into value-added products such as ethanol. Ethanol is an organic material that has a high demand from different industries for products such as fuel, beverages, pharmaceuticals, and other industrial applications. FW fermentation to produce ethanol may be a promising method, and might results in positive impacts on economies. However, it is a challenge for the product price to compete with that of corn ethanol due to low yield and the inconsistency of FW composition. Thus, to increase the profitability, a conventional fermentation plant integrated with a combined heat and power (CHP) system might be a great combination, and was analyzed in this study. Solid waste stream from the process can be converted into energy and could reduce the utility cost. Therefore, the main focus of this study is to evaluate the economic impact of this integrated system by estimating the minimum selling price (MSP) using techno-economic analysis (TEA) and compare to conventional plants without CHP. Results from this analysis showed that the MSE value for this integrated system was \$1.88 per gallon (\$0.50 per liter). This study suggests that an integrated system with CHP was found to be more economical and attractive to be implemented on a commercial scale.

Keywords: food waste, ethanol, CHP (combined heat and power), techno-economic analysis, biofuel, industrial fermentation

# INTRODUCTION

Every year, the world generates about 1.3 billion tons of food waste (FW) through supply food chain stages including at the consumer level. In addition to that, this waste is expected to increase due to several factors such as managerial and technical limitation, global population, modernization, and living style (Gustavsson et al., 2011; Aschemann-Witzel et al., 2015). In the United States, 76.1% of the FW will be sent to the landfills as a final destination (EPA 2018). Furthermore, FW could lead to various problems such as to the environment, society, the ecosystem, and the economy (Papargyropoulou et al., 2014).

Prevention is the best option in the FW management hierarchy, followed by recycling, energy recovery, and disposal. Thus, by considering the amount of valuable nutrients in the FW, recycling using the biological platform in producing other value-added products would be a great approach. This method is expected to have a good impact on the economy and the environment compared to the thermochemical technology.

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> \*Correspondence: Kurt A. Rosentrater Karosent@iastate.edu

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Anaerobic digestion (AD) and fermentation are relatively a matured technology that could produce energy such as biogas and ethanol respectively. However, according to Pham et al., 2015, an AD method will add a negative impact on the environment and be more costly.

In a study performed by Shafinas and Rosentrater, ethanol conversion from FW fermentation without enzymes was shown to have good potential from an economic perspective. Even though the distillation column was identified as an energy-intensive process, the minimum selling price (MSP) value was the lowest compared to the membrane separation process. From the economic analysis, the MSE for FW fermentation without enzymes and 2-step distillation system was found to be \$2.41/gal (Muhammad and Rosentrater 2020a). This value is in between corn ethanol price and cellulosic ethanol. However, the ethanol price from FW fermentation is expected to be more economical if the production process could integrate with the combined heat process (CHP) by producing insite energy to minimizing the utility cost.

CHP is an integrated system that could produce electric power and steam on site. The advantages of embedded on site the plant are to avoid losses in distribution and transportation from the electrical power grid. The CHP is not considered as technology, but a method in applying technologies. Therefore, the implementation of this system could increase energy efficiency, minimize the emission, reduce utility cost, and promote sustainable development. Various studies have been suggested to use the integrated system in the ethanol fermentation plant due to advantages as mentioned above (Daianova et al., 2012; Raj, Iniyan, and Goic 2011; Eriksson and Kjellström 2010; Dias, Lima, and Mariano 2018).

The concept of CHP is direct combustion of the solid waste stream that will convert chemical energy into heat energy. The consistent of the heat source from the boiler will turn water into high-pressure steam. By using the Rankine cycle principle, the steam turbine can produce electricity. The backpressure steam turbine is commonly used in the industrial plant because of the low capital cost, simple configuration, and high efficiency (DOE 2016). The steam exhausts from the system will be recovered and used directly to a process and steam distribution. The biomass moisture content of biomass should be in the range of 15–55% before it can be directly burnt in the combustion system (Pirouti et al., 2010). Details of the overall process are shown in the schematic diagram in **Figure 1**.



In this study, FW fermentation without enzymes integrated with the CHP process is modeled. The process model and conditions are similar to a study done by Muhammad and Rosentrater but with an additional energy cogeneration model (Muhammad and Rosentrater 2020b). The primary target of this study is to evaluate and compare the economic performance between with and without the integrated system. The technoeconomic analysis will be performed to estimate the minimum selling price (\$/gal) and compared with previous studies. The sensitivity analysis will be performed to identify the impact of the processing parameter on economic feasibility.

# **METHODOLOGY**

# **Process Modeling**

**Figure 2** shows the FW composition used in this study. This information was based upon data collected in our laboratory. The fermentation process was modeled using anaerobic conditions without any hydrolysis enzymes added, and ethanol yield was set to 2.2% (w/w) (based on laboratory results). The yield is considered higher compared to the previous study (Suwannarat and Ritchie 2015).

SuperPro Designer V9.0 software was used to simulate the integrated conceptual fermentation plant and evaluate the performance on a commercial scale. The daily plant feedstock is supposed to be 2000 Mg, and assuming no cost.

A 2-step distillation process was used to separate the ethanol from the fermentation broth followed by a purification process through a molecular sieve. The waste stream from this process was considered as a co-product that can be utilized as liquid fertilizer and bio-compost. Previous study found that by selling these co-products to other industries it could maximize the profit. (Muhammad and Rosentrater 2020a). However, in this study, bio compost was being utilized to generate heat and power by using the CHP system. The moisture content of bio compost was maintained at 40% by weight before being combusted in the burner. The chemical energy will be converted into heat energy to generate steam in the boiler. High-pressure steam turns the steam turbine which satisfies the thermodynamic cycle that changes heat to mechanical works. The turbine drives the generator and finally generates electric power and then will be used back in the facilities. In this study, assume that no surplus electricity can be sold to the grid.



**TABLE 1** Detailed investment of CHP integrated with FW fermentation plant.

Assumption of investment	Peters et al.	(2003); Brown	and Brown (2014)

TPEC (Total Purchased Equipment)	Value estimate by SuperPro Simulation (2018 dollars)		
Purchased equipment	39% of TPEC		
installation			
Instrument and control	26% of TPEC		
Piping	31% of TPEC		
Electrical system	10% of TPEC		
Building (including services)	29% of TPEC		
Yard improvements	12% of TPEC		
Services facilities	55% of TPEC		
TIEC (Total Installed Equipment	202%		
Cost)			
Indirect cost			
Engineering	32% of TPEC		
Construction	24% of TPEC		
Legal and contractors' fees	23% of TPEC		
TIC (Total Indirect Cost)			
Project Contingency	20% of TIC + TIEC		
FCI (Fixed Capital Investment)	TIC + TIEC + Contingency		
Non-depreciated Direct Cost			
Working Capital	15% of FCI		
Land	6% of TPEC		
TPI (Total Project Investment)	FCI + WC + Land		
Lang Factor	5.46		

Furthermore, the exhaust steam from the steam turbine will be captured and used for the heating system. The process diagram flow is illustrated in **Figure 3**.

The size and quantity of equipment, utilities and energy consumptions, transportation cost, labor, and raw material needed were determined by mass and energy balance from the simulation. The plant had 7,900 operating hours per year.

# **Techno-Economic Assumptions**

Techno-economic analysis (TEA) is used to evaluate the economic viability of the CHP plant integrated with the FW based ethanol production plant. Equipment purchased cost was

#### TABLE 2 | Utility prices (EIA 2017).

Utility component	Prices
Electricity (¢/kW-h)	5.5
Water (¢/gal) (¢/L)	0.350 (0.09)
Steam (\$/Mg)	12.00
Cooling water (\$/Mg)	0.05
Chilled water (\$/Mg)	0.40

taken from the SuperPro Designer V9.0 software and indexed to 2018 dollars. The methodology to calculate the project investment expenditure was adopted from Peters et al., 2003. In addition to that, 3.02 installation factor was used as it is a common assumption factor for a biorenewable facilities plant. Discounted cash flow analysis spreadsheet was performed to estimate the MSE price (\$/gal) with predetermined internal rate of return to generate a net present value (NPV) of zero (Brown and Brown 2014). The IRR value was set to 10% to allow the ethanol product cost to have a competitive price in the market Most of the financial assumptions have been adapted from National Renewable Energy Laboratory Reports (NREL) (Wright et al., 2010; Tao et al., 2014). The main assumptions made in this study are listed below.

- Plant capacity: 2000 Mg/day (t/day)
- Plant feedstock: FW with 78% moisture content
- Plant distance: 12 mi (19.3 km) radius (Poliafico and Murphy 2007)
- Plant life: 20 y
- Equity financed: 100%
- The internal rate of return (IRR): 10% (Short, Packey, and Holt 1995)
- General plant depreciation: 7 y with 200% double declining balance (DDB)
- CHP plant depreciation: 20 y with 150% double declining balance (DDB)

**TABLE 3** Assumptions for operator requirements for various types of process equipment (Brown and Brown 2014).

Equipment type	Operators per unit per shift		
Boilers	1.0		
Electric generating plants	3.0		
Crushers, mills, grinders	1.0		
Evaporators	0.2		
Furnace	0.5		
Heat exchangers	0.1		
Reactors/bioreactors	0.5		
Clarifiers and thickeners	0.2		
Mixers	0.3		
Rotary and belt filters	0.2		
Screens	0.05		



TABLE 4 | Sensitivity analysis parameters for FW fermentation process integrated with CHP.

Parameters	Optimistic	Base case	Pessimistic
Plant distance-miles radius (km radius)	8 (12.9)	12 (19.3)	24 (38.6)
Plant Capacity- Mg/day	1,000	2000	3,000
Lig. fertilizer resale value-¢/gal (¢/L)	40 (10.6)	30 (7.9)	20 (5.3)
Ethanol yield (% w/w) wet basis	2.9	2.2	1.5
Fix capital cost (\$MM)	407	585	757

- CHP feedstock: bio compost with 40% moisture content
- Contingency factor: 20% from total installed equipment and indirect cost
- Construction period: 2.5 years with total capital investment spent with 8, 60 and 32% for first, second and third year respectively.
- Startup period: 6 months with considering 50% of revenues, 75% variable cost and 100% fixed expenses will be achieved.

There were three major cost areas used in the discounted cash flow analysis to estimate MSE (\$/gal): Total projet investment (TPI), variabel cost (\$/y) and the fixed operating cost (\$/y). The detailed investment costs are shown in **Table 1** upon assumption.

Variable cost consists of the raw material cost, transportation cost, and utility cost. The utility cost depends on the energy balance of the whole process and the prices for each utulity component as shown in **Table 2**. The fixed cost consists of operating labor cost, laboratory cost, overhead, maintenance, local taxes, and insurances. The labor costs depend on the number of operators required per equipment, as listed in **Table 3**.

Economies of scale will be performed to evaluate the reduction of the product value while increasing daily feedstock volume from 10 to 5,000 Mg. From this analysis, the range of optimum feedstock value with the lower MSE value will be estimated for the future study.

# Sensitivity Analysis

Further analysis is required to identify which parameter has the most significant impact on MSE value. A sensitivity analysis is a method used by modifying one parameter value while



maintaining others. **Table 4** shows the sensitivity analysis parameters selected for this analysis. These parameters are identified as a powerful impact on plant economic performance.

# **RESULTS AND DISCUSSION**

# **Economic Analysis**

This plant is designed with 2000 Mg/day of FW as a feedstock. The mass and energy balance was obtained from the simulation result. From the discounted cash flow analysis, the MSE price was estimated to \$1.88 per gallon (\$0.50 per liter) with yielding an NPV of zero and 10% IRR. Results from this analysis reveals that the integrated process is found to be the most economical process



compared to the other studies from Muhammad (Muhammad 2019).

The CHP integrated plant has a value for total installed equipment cost (TIEC) and total project investment (TPI) of \$221 MM and \$400 MM respectively. In addition to that, the annual utility cost (\$/y) without credit power and heat from CHP was \$30 MM annually as detailed in **Figure 4**. However, this value reduces more than 50% by using energy generated from CHP. This finding shows that the fermentation process integrated with CHP has a significant impact on reducing the product cost.

Economies of scale for this study are represented in **Figure 5**. From the graph, there is a power relationship of -0.557 between MSE and feedstock size. It also shows that with the feedstock rate varying between 10 and 4,000 Mg per day, the MSE of ethanol ranges from \$74.16 to \$0.10 per gallon of ethanol. The MSE keep decreasing because there is surplus of electricity that exceeds demand. Thus, it will be sold to the grid. However, higher feedstock capacity is impossible due to the logistic problem. FW is made up of organic materials that are easily contaminated by other organisms. Therefore, proper storage is required in a loading area. Therefore it will incur the cost of operation and is not economically viable.

# Sensitivity Analysis

**Figure 6** shows the sensitivity analysis for this study. From the tornado chart, it indicates that feedstock plant capacity is the most influential parameter in estimating the MSE value. Increasing the amount of FW feedstock to the plant from

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1,000 Mg/day to 3,000 Mg/day will decrease the value of MSE from \$5.44 to \$0.27 per gallon.

# CONCLUSIONS

This techno-economic analysis evaluates the cost of integrated CHP with FW fermentation process in producing ethanol as the primary product. From the discussions above, waste stream can be converted into heat and power energy and utilized back to the process. This process could reduce the annual utilities cost by up to 50%. The results from discounted cash flow analysis showed that the MSE value for an integrated system is lower compared to previous study as discussed above given by \$1.88 per gallon (\$0.50 per liter) and \$2.41 per gallon (\$0.64 per liter) respectively. This finding would justify that integrated CHP with ethanol production plant is more economically attractive and more energy efficient.

Additionally, from the sensitivity analysis, results showed that the variability of feedstock plant capacity at  $\pm 100\%$  would give an MSE value in the range of \$0.27 to \$5.44 per gallon. Based on the economics of scale, the graph shows that the MSE value is decreasing when the feedstock plant capacity increases. As expected, it occurs because of surplus electricity which will be sold to the grid to improve profitability. However, a higher amount of feedstock will require an extensive storage facility which is not modeled in this study. Therefore, further optimization study is recommended to be done to find the optimal feedstock plant including the storage facilities. This information is one of the essential aspects for the investors and shareholders for future consideration.

# DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

# **AUTHOR CONTRIBUTIONS**

NS conducted the research, conducted the analysis, and drafted the manuscript. KR conceived the project, provided supervision, and edited the manuscript.

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