

Optimal Placement and Sizing of Distributed Generators Based on Equilibrium Optimizer

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To solve the problems of environmental pollution and energy consumption, there is an urgent need to develop clean and renewable energy to maintain the sustainable development of society. Therefore, distributed generation (DG) has attracted engineers' extensive attention. However, DG output of is usually random and intermittent. When connected to different locations, different sizing, and different distribution networks, it will have varying impact on the safe and stable operation of the power system. When choosing the optimal DG access scheme, planners must consider the impact of size, type, and location to ensure that power grid operation is safe, stable, reliable, and efficient. Therefore, this article proposes an objective function considering power losses, voltage profile, and pollution emission, which is solved by equilibrium optimizer (EO). Finally, the effectiveness of the proposed strategy is verified based on IEEE 33 and 69-bus distribution networks. The results show that the strategy can effectively improve the pollution emission of the system, effectively reduce power loss, and improve the voltage profile.

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1 INTRODUCTION

In the continuous development of power systems, the traditional model of centralized power generation leads to thermal power, consuming greater amounts of non-renewable resources, fossil energy shortages and intensified environmental degradation. This trend has been unable to comply with the demands of today's power system, so global energy transformation is imperative (Chan and Phang, 1987; Krismanto et al., 2018; Yang et al., 2021).

On the other hand, at present, most of the large power grids, with centralized power generation as their dominant feature, is adopted domestically and internationally. The power system is evolving toward large-scale, centralized, ultra-high voltage units. The disadvantages of the power system are made clear with the construction of the power grid. Some power supply sources are located far away, in cities with low population density. Long transmission distances lead to high power loss and difficulty in ensuring power quality, which makes users in remote areas unable to obtain ideal power supply services and leads to low utilization of economic investment (Wang et al., 2014; Bikash et al., 2019; Bikash et al., 2020).

In addition, although DG can provide power for the power grid and improve system reliability (Kumar et al., 2019), several factors (different network distribution structure ; huge node numbers; large power load; randomness of DG access; power distribution network management) lead to construction difficulties, schedule complications, and problems at various points of failure caused by

1





negative impacts on the power system. In the case of serious disturbances, large-scale power failure may result, causing disastrous consequences (Chandrasekhar and Sydulu, 2012; Aman et al., 2014; Velasquez et al., 2016). In addition, multiple types of DG are usually connected to the distribution network, in order to take full advantage of DG and make the system run more reliably, safely, and stably (Aman et al., 2012; Murty and Kumar, 2015; Iqbal et al., 2018). Currently, wind turbines are the most mature photovoltaic (PV) system, and so is often the first choice for installation. However, their output power is largely affected by illumination and wind speed, causing randomness, intermittency, and uncertainty. Access to the distribution network brings many uncertain factors (Gandomkar et al., 2005; Afzalan et al., 2012). Inappropriate sizing of DG and unreliable access to any node of the distribution



network will increase network losses and damage the voltage profile and network harmonics (Zhu et al., 2006; Ameli et al., 2014; Poornazaryan et al., 2016). How to rationally configure sizing and access nodes for different types of DG, so as to most effectively reduce construction costs and maintenance costs, improve voltage profile of the system, correctly use the direct value of power supply provided by DG, and scientifically and reasonably connect DG to the distribution network has become an urgent problem to be solved.

Currently, the DG planning process is highly nonlinear and contains many discrete optimization variables and multiple complex constraint optimization problems. In light of this, the traditional interior-point method makes it difficult to obtain high-quality plans. To address this deficiency, some scholars adopt heuristic algorithms (Acharya et al., 2016; Das et al., 2016). Heuristic algorithms are used to find optimal solutions by constant updating and iteration. It has the advantage of not relying on the accurate system model and is widely used to solve problems of high complexity . The optimization method can be divided into two types: single individual search and population search. Because population search has multiple search individuals, its efficiency is increased (Ogunjuyigbe et al., 2016; Ben Hamida et al., 2018). Past research (Moradi and Abedini, 2016) suggests DG site is the appropriate selection, based on the influence of the injected active power of each node on the active power losses, which significantly reduces the amount of calculation for site selection. Genetic algorithm is then adopted to fix DG volume, which effectively reduces the active power losses of the system. Meena et al.(2017) proposed an improved artificial bee colony algorithm to plan the DG, taking into account access sizing, a-node and power factor. Results of the IEEE 33 and 69-bus distribution networks tests showed that power losses of the test system were significantly optimized. Yanez-Borjas et al. (2021) proposed a cooperative complementary optimization scheme for DG and capacitor, which is solved by the dragonfly algorithm. This scheme can

effectively compensate the active power and reactive power gap of the system in close range, thus improving the voltage stability margin and maximum load sizing of the distribution network and reducing system power loss.

However, distribution network load shows certain rules relating to people's living habits, so it is necessary to assess its regularity. In addition, the output of wind turbines and PV units is significantly affected by the natural environment, so timing modeling for those items is necessary.

In this article, we first establish time-series power output models for wind turbines and PV systems, time-series load models, constant power output models for fuel cells, and miniature steam turbines. We next constructed a multiobjective mathematical optimization model of DG location and constant volume. Considering power losses, we used established voltage profile and pollution emission, and equilibrium optimizer (EO) to solve the model. Finally, the simulation based on IEEE 33 and 69-bus distribution networks shows that the proposed strategy can effectively improve the active power losses and voltage profile of the distribution network while considering environmental pollution emission and demonstrates that the proposed strategy can effectively solve the multi-objective programming problem.

2 PROBLEM FORMULATION

2.1 Load and DG Output Timing Model 2.1.1 Output Timing Model of Wind Turbine

If the time-series characteristics of wind turbine are not considered, the location and sizing model can be expressed as a power source with constant output active power, but consuming reactive power. However, in practical engineering, output of wind turbine is significantly affected by the natural environment. If its timing characteristics are not considered, it does not have engineering practicability. At this stage, wind speed characteristics are usually described by the Weibull distribution of two parameters, which is shown as follows:

$$F(\nu) = 1 - \exp\left[-\left(\frac{\nu}{A_{\rm WT}}\right)^{kW}\right] \tag{1}$$

where kW is the shape parameter of Weibull distribution; A_{WT} is the scale parameter; and v is the wind speed at the rotating force surface of the impeller axis.

Logarithmically transformed:

$$\ln\left[\ln\left(\frac{1}{1-F(\nu)}\right)\right] = k\ln(\nu) - kW\ln A_{\rm WT}$$
(2)

Further equivalent transformation:

$$v = A_{\rm WT} \exp\left(\frac{\ln\{-\ln[1-F(v)]\}}{kW}\right)$$
(3)

Finally, the probability density function can be expressed as

TABLE 1 | Five types of power generation emissions.

| Generator | Pollution emissions (lb/MW•h) | | | | |
|------------------------|-------------------------------|----------------------|-----------------|--|--|
| | CO ₂ | SO ₂ | NO _x | | |
| Wind turbine | 0 | 0 | 0 | | |
| PV station | 0 | 0 | 0 | | |
| Micro turbine | 1,596 | 0.008 | 0.440 | | |
| Fuel cell | 1.106 | 8 × 10 ⁻⁶ | 1.149 | | |
| Conventional generator | 621 | 6.465 | 2.875 | | |

$$f(v) = \left(\frac{kW}{A_{\rm WT}}\right) \left(\frac{v}{A_{\rm WT}}\right)^{kW-1} \exp\left[-\left(\frac{v}{A_{\rm WT}}\right)^{kW}\right]$$
(4)

The output power of wind turbine mainly depends on wind speed, which can be expressed as the following segmented function (Abu-Mouti and El-Hawary, 2011):

$$P(v) = \begin{cases} 0 & (v \le v_{ci} \text{ or } v \ge v_{co}) \\ P_{r} \frac{v - v_{ci}}{v_{R} - v_{ci}} & (v_{ci} \le v \le v_{R}) \\ P_{r} & (v_{R} \le v \le v_{co}) \end{cases}$$
(5)

where P(v) is the power output of the wind turbine; v_{ci} is the cut wind speed; v_{co} is cutting out wind speed; v_R is rated wind speed; and P_r is the rated output power. The wind turbine output curve is modeled according to the mean value of seasonal wind speed, and the fan output curve is obtained as shown in **Figure 1** (Abu-Mouti and El-Hawary, 2011).

2.1.2 Output Timing Model of Photovoltaic System

The output power P_{PV} of PV system can be approximated by the following formula (Abu-Mouti and El-Hawary, 2011):

$$P_{\rm PV} = P_{\rm stc} \frac{I_{\rm r,t}}{I_{\rm stc}} \left[1 + \alpha_{\rm T} \left(T_{\rm t} - T_{\rm stc} \right) \right] \tag{6}$$

where P_{stc} is the output power of PV system when solar radiation intensity $I_{\text{stc}} = 1000 \text{W/m}^2$ and temperature $T_{\text{stc}} = 25^{\circ}\text{C}$; $I_{\text{r,t}}$ is the radiation intensity during actual operation; α_{T} is the power temperature coefficient of the PV system; and T_{t} is the actual operating temperature of the PV power supply. In addition, the output curve of PV system obtained by fitting irradiance of typical days in four seasons is shown in **Figure 2** (Abu-Mouti and El-Hawary, 2011). It is worth noting that this kind of DG is regarded as injecting active power into the parallel node only in the site selection and sizing.

2.1.3 Load Time Series Model

The load size shows certain regularity due to people's living habits. **Figure 3** shows the typical load curve of resident load in four seasons (Abu-Mouti and El-Hawary, 2011).

2.2 Objective Function

The operation of DG connected to the distribution network can effectively reduce system power loss and improve the voltage profile. In addition, rational use of DG can effectively utilize fossil fuels and reduce emission of carbon and sulfur pollutants.





Therefore, we propose a DG location and volume multi-objective programming model considering power losses, voltage profile, and pollution emission. The aim of this model is to optimize the power loss and voltage profile of the system to the greatest extent possible and maximize consumption of new energy.

2.2.1 Power Losses

When the power system operates under the heavy load conditions, power loss will also increase, seriously affecting its economical operation. However, with the increase of DG permeability to the distribution network, the distance of power flow can be effectively reduced, so as to significantly reduce power loss. However, the size of DG connected to the distribution network cannot increase indefinitely. When it exceeds a certain value, power loss will increase instead and affect the stability of the power system. Therefore, we used the power loss index to measure the optimization effect for network loss, which can be described as follows (Ugranh and Karatepe, 2013):

$$PLRI = \frac{PL_{w/DG}}{PL_{wo/DG}}$$
(7)

$$PL_{W/DG} = \sum_{t=1}^{T} \sum_{i=1}^{N_{n_i}} I_{dg,n_i}^2 R_{n_i}$$
(8)

$$PL_{wo/DG} = \sum_{t=1}^{T} \sum_{n_i=1}^{N_{n_i}} I_{n_i}^2 R_{n_i}$$
(9)

where $PL_{w/DG}$ and $PL_{wo/DG}$ is the active power loss of the distribution network before and after installation of DG; N_{n_i} is the number of nodes in the distribution network; and I_{dg,n_i} and I_{n_i} injection the *n*th node after DG installation and before DG installation, respectively. R_{n_i} is the Resistance of the n_i th node; *T* is the number of simulation periods, and the value is 96.

2.2.2 Voltage Profile Index

DG can effectively improve voltage profile and voltage amplitude by providing active power and reactive power to the load in a short distance. However, when power injected into the distribution network by DG is too large, it will also lead to voltage exceeding the stable range and endanger system stability. Therefore, this article uses voltage profile index to describe this optimization effect, as detailed here (Ugranlı and Karatepe, 2013):

$$VPII = \frac{VP_{\rm w/DG}}{VP_{\rm wo/DG}} \tag{10}$$

$$VP_{w/DG} = \sum_{t=1}^{T} \sum_{n_i=1}^{N_{n_i}} \left(V_{dg,n_i} - V_{rated} \right)^2$$
(11)

$$VP_{\rm wo/DG} = \sum_{t=1}^{T} \sum_{n_i=1}^{N_{n_i}} \left(V_{n_i} - V_{\rm rated} \right)^2$$
(12)

where $VP_{w/DG}$ and $VP_{wo/DG}$ is the total voltage deviation before and after the installation of DG in the distribution network; V_{dg,n_i} and V_{n_i} are the voltage of the n_i th node before and after the installation of DG in the distribution network, respectively; and V_{rated} is the rated voltage of the system, with a value of 1 p.u.

2.2.3 Environmental Emission Reduction Index

Compared with traditional centralized power generation, DG can effectively absorb renewable energy distributed in the natural environment, reduce dependence on fossil fuels and effectively reduce emission of pollutants containing carbon and sulfur. The present study uses pollution emission indicators to describe this optimization effect, described as follows (Ugranlı and Karatepe, 2013):

$$EIRI_{p} = \frac{PE_{w/DG}}{PE_{wo/DG}}$$
(13)

$$PE_{w/DG} = \sum_{t=1}^{T} \sum_{j=1}^{N_j} PG_{dg,j} AE_{pj}$$
(14)

$$PE_{wo/DG} = \sum_{t=1}^{T} \sum_{j=1}^{N_j} PG_j AE_{pj}$$
(15)

where $PE_{w/DG}$ is the total mass of pollutants discharged from the installation of DG; $PE_{wo/DG}$ is the total mass of pollutants discharged from traditional centralized power generation; $PG_{dg,j}$ is the active power output by DG at the *j*th node; PG_j is the active power output at the *j*th node of traditional centralized power generation; and AE_{pj} is the total mass of pollutant discharged from the *j*th node of the power supply.

TABLE 2 | Optimization results of EO.

| DG location | DG sizing (kVA) | Losses function | Voltage function | Emission function | Fitness function |
|-------------|--------------------------------------|--|---|---|--|
| 11 | 70.558 | 0.827 | 0.8887 | 0.2476 | 0.697,575 |
| 32 | 160.829 | | | | |
| 73.7187 | 2 | | | | |
| 70.7129 | 19 | | | | |
| 30 | 12 | | | | |
| 50 | 26 | | | | |
| | 11 32 73.7187 70.7129 30 | (kVA) 11 70.558 32 160.829 73.7187 2 70.7129 19 30 12 | (kVA) 11 70.558 0.827 32 160.829 73.7187 2 70.7129 19 30 12 | (kVA) 0.827 0.8887 11 70.558 0.827 0.8887 32 160.829 73.7187 2 70.7129 19 30 12 | (kVA) 0.827 0.8887 0.2476 32 160.829 |

The mass of carbon dioxide, sulfur dioxide, and nitride emitted can be obtained by adding the weight coefficient (Ugranlı and Karatepe, 2013):

$$EIRI = \sum_{p=1}^{N_p} \mathrm{ew}_p EIRI_p \tag{16}$$

$$0 \le \operatorname{ew}_p \le 1 \text{ and } \sum_{p=1}^{N_p} \operatorname{ew}_p = 1 \tag{17}$$

where ew_p is the weight coefficient between carbon dioxide, sulfur dioxide, and nitride, which is 0.5, 0.25, and 0.25, respectively; and N_p is the type and quantity of pollutants, and the value is 3. The five types of generation emissions are listed in **Table 1**.

2.2.4 Multi-Objective Function

In this article, we proposed a multi-objective performance optimization index, in order to obtain DG location and volume planning scheme, taking into account the three optimization indexes noted above, as described by Ugranlı and Karatepe (2013):

$$\begin{cases} \min MPI = w_1 PLRI + w_2 VPII + w_3 EIRI \\ s.t. \ 0 \le w \le 1 \\ w_1 + w_2 + w_3 = 1 \end{cases}$$
(18)

where w is the weight coefficient of each optimization objective, w_1 , w_2 , and w_3 . The values are 0.5, 0.25, and 0.25, respectively. It is worth noting that w is adjusted accordingly according to the actual engineering needs.

2.3 Constraint

When DG is connected to the distribution network for operation, the power flow of the original system will change. In order to ensure the stable operation of the system, the following constraints need to be considered.

2.3.1 Power Balance

$$\begin{cases} P_{\mathrm{G}i} + P_{\mathrm{D}\mathrm{G}i} = P_{\mathrm{L}i} + U_i \sum_{j=1}^{N} U_j \big(G_{ij} \cos\theta_{ij} + B_{ij} \sin\theta_{ij} \big) \\ Q_{\mathrm{G}i} + Q_{\mathrm{D}\mathrm{G}i} = Q_{\mathrm{L}i} + U_i \sum_{j=1}^{N} U_j \big(G_{ij} \sin\theta_{ij} - B_{ij} \cos\theta_{ij} \big) \end{cases}$$
(19)

where P_{Gi} and Q_{Gi} , respectively, represent the active power output and reactive power output of the power supply at *i*th node in the distribution network. P_{DGi} and Q_{DGi} are, respectively, the active power and reactive power of DG output at *i*th node. U_i is the voltage of the *i*th node; G_{ij} and B_{ij} represent the admittance and susceptance between the *i*th node and the *j*th node; θ_{ij} is the power angle between *i*th node and the *j*th node; and P_{Li} and Q_{Li} , respectively, represent the active power and reactive power required by the load on *i*th node in the distribution network (Ugranlı and Karatepe, 2013).

2.3.2 DG Sizing

Due to the limitation of the working principle, structure and production model of the production DG, and the influence of environmental factors on the operation of the production DG, power dispatching cannot be completely controlled, which will have a great impact on power flow, relay protection, voltage, and waveform of the original power grid. Therefore, the power allowed to access the power grid DG is limited (Ugranlı and Karatepe, 2013).

$$\begin{cases} P_{i\text{DGmin}} \le P_{i\text{DG}} \le P_{i\text{DGmax}} (i = 1, 2, \dots, N) \\ 0.8 * P_{i\text{load}} \le P_{i\text{DGmax}} \end{cases}$$
(20)

where P_{iDGmin} represents the minimum size of DG connected by the *i*th node; P_{iDG} represents the active power sent to the power grid by DG connected to the *i*th node; and P_{iDGmax} represents the maximum size of the DG connected by the *i*th node. P_{iload} is the total load on the *i*th node.

2.3.3 Transmission Line Sizing Constraints

$$|S_l| \le \left|S_l^{\max}\right| \tag{21}$$

where S_l is the apparent power flowing through the *l*th line and S_l^{max} is the maximum apparent power allowed to flow through the *l*th line (Ugranlı and Karatepe, 2013).

2.3.4 Voltage Constraints

In order to ensure the safe and stable operation of the system, it is necessary to limit voltage within the safe range, which can be described as follows (Ugranlı and Karatepe, 2013):

$$U_{\mathrm{DG}k}^{\mathrm{min}} \le U_{\mathrm{DG}k} \le U_{\mathrm{DG}k}^{\mathrm{max}} \tag{22}$$

where $U_{\text{DGk}}^{\text{max}}$ and $U_{\text{DGk}}^{\text{min}}$ are the upper and lower voltage limits of the *k*th node after DG is configured, and their values are 1.05 and 0.9 p.u., respectively.

3 EQUILIBRIUM OPTIMIZER

Equilibrium optimizer (EO) is an optimization algorithm inspired by the physical phenomenon of dynamic balance of



mass in control volume, and its specific optimization process is as follows (Faramarzi et al., 2020):

and size of particles, as shown in the following formula (Faramarzi et al., 2020):

 Population initialization: similar to most meta-heuristics, EO uses the initial population to start the optimization process. The initial state is randomly and uniformly constructed in the search space according to the number $C_i^0 = C_{\min} + \operatorname{rand}_i (C_{\max} - C_{\min}), i = 1, 2, \cdots, n$ (23)

where C_{\min} and C_{\max} are the lower and upper limits of the variables to be optimized, respectively; rand_i is a random vector between [0,1]; and *n* is the population number.



(2) Balance pool and candidate solution: the balance pool collects the top four particles in the fitness value of the current solution and the average value of these four particles as the candidate solution of the update formula, as shown in the following formula (Faramarzi et al., 2020):

$$C_{\rm eq, \ pool} = \{C_{\rm eq,1}, C_{\rm eq,2}, C_{\rm eq,3}, C_{\rm eq,4}, C_{\rm eq, \ ave}\}$$
(24)

where $C_{eq,1}$, $C_{eq,2}$, $C_{eq,3}$, $C_{eq,4}$ are the optimal solutions found in the current iteration, which are mainly used to improve global exploration ability; and $C_{eq, ave}$ is the average values of the above four solutions, which are mainly used to improve local development ability.

(3) Exponential coefficient *F*: The exponential coefficient can balance global exploration and local development capabilities well, and its specific calculation formula is as follows (Faramarzi et al., 2020):

$$F = \exp\left[-\lambda \left(t - t_0\right)\right] \tag{25}$$

$$t_0 = \frac{1}{\lambda} \ln \left(-a_1 \text{sign} \, (\text{ rand } -0.5) \left[1 - e^{-\lambda t} \right] \right) + t \qquad (26)$$

$$t = \left(1 - \frac{iter}{maxiter}\right)^{\left(a_2 \frac{iter}{maxiter}\right)}$$
(27)

where a_1 and a_2 are the weight coefficients of global exploration and local development, respectively. When the value is larger, the corresponding ability is stronger. Generally, they are 2 and 1, respectively; *iter* is the current number of iterations, and *maxiter* is the maximum number of iterations; λ is a random number between [0, 1].

(4) Generation rate *G*: The generation rate is an important indicator in the mass balance equation. In order to further improve the local development sizing, it is designed as follows (Faramarzi et al., 2020):

$$G = G_0 e^{-\lambda(t-t_0)} \tag{28}$$

$$G_0 = GCP(C_{\rm eq} - \lambda C) \tag{29}$$

$$GCP = \begin{cases} 0.5r_1, & r_2 \ge GP \\ 0, & r_2 < GP \end{cases}$$
(30)

where r_1 , r_2 , and λ are random numbers [0, 1]; *GCP* is the generation rate control parameter; and *GP* is the generation probability. When the value is 0.5, the exploration and development ability reach a balance.

(5) Update formula: After abstracting and improving the original physical theory, the updated formula of EO is established as (Faramarzi et al., 2020)

$$C = C_{\rm eq} + F\left(C - C_{\rm eq}\right) + \frac{G}{\lambda V}\left(1 - F\right)$$
(31)

where C_{eq} is randomly selected from the equilibrium pool and λ is a random number between [0,1].

4 CASE STUDIES

In order to verify the effectiveness of the proposed strategy, simulation verification was carried out based on IEEE 33 and 69-bus distribution networks. The test system is shown in **Figures 4**, **5**. The configured DG includes four types: PV system (2 nodes installed), wind turbine (2 nodes installed), fuel cell (1 node installed), and micro gas turbine (1 node installed). It is important to note that fuel cells and micro gas turbines can adjust their power output by controlling the waste products of fuel input, and the output is relatively stable, which can effectively compensate for the randomness of the output of PV units and wind turbines.

| Generator | DG location | DG sizing (kVA) | Losses function | Voltage function | Emission function | Fitness function | | |
|-------------------------|-------------|--------------------|-----------------|------------------|-------------------|------------------|--|--|
| The first PV | 2 | 10.2699 | 0.2393 | 0.2916 | 0.6613 | 0.3579 | | |
| The second PV | 61 | 487.819 | | | | | | |
| The first wind turbine | 36 | 21.258 | | | | | | |
| The second wind turbine | 63 | 162.98 | | | | | | |
| Micro turbine | 62 | 500 | | | | | | |
| Fuel cell | 66 | 500 | | | | | | |

TABLE 3 | Optimization results of EO.



In addition, the objective function, constraints, and size of the test system jointly affect the complexity of the problem to be solved. The population size and iteration times of the algorithm determine the solution efficiency of the problem. If the population size and iteration times of the algorithm are too large, it will lead to low solution efficiency. On the other



hand, if small population size and iteration times are set, the planning scheme can be obtained quickly, but the optimal solution has a high probability of not occurring. Therefore, we used the trial-and-error method to select population size iteration times. The objective function is established as follows:

$$f_{\rm try} = \omega_{\rm t1} \left(\omega_1 P L R I + \omega_2 V P I I + \omega_3 E I R I \right) + \omega_{\rm t2} t_{\rm run} \tag{32}$$

where $t_{\rm run}$ is the running time, and ω_{t1} and ω_{t2} is the weight coefficient between the two. Because this study used offline optimization, ω_{t1} and ω_{t2} is 0.8 and 0.2, respectively. After many tests, the population size and iteration times of EO were finally set to 200 and 100, respectively. In addition, the total active power loss of IEEE 33 and 69-distribution network in four typical days was 4,061.87 and 4,449.99 kW, respectively. The total voltage deviation was 66.1991 and 71.3853 p.u., respectively, and the total load was 3.715 and 3.802 MW, respectively. In addition, all case studies were carried out in MATLAB 2018b environment on a personal computer with 3.40 GHz Intel(R) Core (TM) i5-8400 CPU, 32 GB RAM.

4.1 IEEE 33-Bus Distribution Networks

Table 2 and Figure 6, respectively, show the IEEE 33 bus distribution network planning scheme for grid-connected operation and the voltage distribution of the system. As seen in Figure 6 and Table 2, after EO optimization and configuration of different types of DG, the total active power loss and annual average voltage distribution of the distribution network throughout the year improved significantly. The results show that the planning scheme avoids areas with heavy reactive load, avoids more serious reactive power shortage in these areas, and ensures system stability. In addition, the voltage profile curves with and without DG installation, which effectively proves that DG has a significant optimization effect on improving the voltage

profile of the distribution network, because DG is always installed near the load. **Figure** 7 shows the convergence curves of EO. It can be seen that EO has an excellent search mechanism and can converge to the minimum value with fewer iterations to avoid falling into the local optimum.

4.2 IEEE 69-Bus Distribution Networks

In order to further verify the optimization effect of EO on larger and more complex systems, **Table 3** and **Figure 8** give the IEEE 69-bus distribution network planning scheme and voltage profile, respectively. **Table 3** and **Figure 8**, **9** show that EO still has a strong search effect in systems with larger nodes, which can effectively improve the power loss and voltage profile of the distribution network. It can effectively improve the stability of the system and reduce the emission of carbon and sulfur pollutants, which brings the best comprehensive optimization effect to the distribution network.

5 CONCLUSION

Considering that active power losses, voltage profile, and pollution emission are elements of DG planning, EO is used to solve the problem. Its main contributions are as follows:

- (1) The DG planning model, incorporating active power loss, voltage profile, and pollution emission is established. The introduction of pollution emission can effectively reduce carbon and nitrogen emissions in the system.
- (2) Through IEEE 33 and 69-bus distribution networks tests, it was verified that EO has strong global search effect and convergence ability and can avoid falling into local optimization under a complex objective function.
- (3) After the installation of four DG units, PV system, wind turbine, micro turbine, and fuel cell, the micro turbine and fuel cell are connected to the system to stabilize the output of PV system and wind turbine. Finally, the results show that power loss of the distribution network after EO is significantly reduced, effectively verifying the effectiveness of the algorithm, and significantly improving the voltage profile.

This research does not involve energy storage systems. The assembly of energy storage systems in new energy stations can effectively suppress the problem of fluctuation of output of scenic resources. Therefore, examination of new energy stations equipped with energy storage systems should be a focus of future research.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material. Further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

WZ: writing-reviewing and editing; SW: supervision and fundings.

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Conflict of Interest: WZ was employed by Yunnan Provincial Energy Investment Group Co.Ltd.

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