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# Research on the deep peak-shaving cost allocation mechanism considering the responsibility of the load side

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With the goal of carbon reduction, China has carried out a series of institutional reforms and innovations in renewable energy consumption. However, the existing allocation rules for peak-shaving costs concentrate on the power side only. In the context of high energy penetration rates, peak-shaving cost significantly increases, and the economic pressure on the power side sharply increases. As the beneficiaries of peak shaving, the load side, while enjoying clean energy, also needs to bear the responsibility of peak shaving and share part of the peak-shaving cost. In this regard, this paper proposes a peakshaving cost allocation mechanism considering load-side participation. First, it uses the marginal contribution theory to establish the peak-shaving value evaluation model of the power and load. Then, based on the waveform similarity theory, it sets two indicators "Fluctuation Trend Similarity" and "Waveform Amplitude Difference" to evaluate each load's renewable energy consumption responsibility. Finally, the peak-shaving cost allocation rules on the power source side and the load side are obtained. An example shows that the proposed allocation mechanism can initially realize the uniform distribution of power and load in peak-shaving cost. Furthermore, the method can promote the fairness of the peak-shaving market and guide users to reasonably participate in the peak-shaving market.

#### KEYWORDS

deep peak-shaving, value assessment, benefit distribution, load side, market rules

## **1** Introduction

Under the high proportion of new energy access, thermal power units in the power system are often in a deep peak-shaving state, which generates a large amount of peak-shaving cost. Thermal power units that are in the deep peak-shaving state do not need to bear the peak-shaving cost, so the new energy units bear the cost mostly. The cost of peak shaving has caused the new energy units to operate under heavy pressure, and there is a risk of discarding new energy. As a public product, peak-shaving contribution benefits all members in the power system, so the cost caused by it needs to be shared by all members of the power system. In some European countries such as Germany, peak-shaving service cost is included in the user's electricity bill in the form of incremental electricity prices (Jiamei Li and Xian, 2022), which alleviates the economic pressure of the power generation side. In China, there have been many studies on the allocation mechanism

of peak-shaving costs in recent years. He et al. (2021) proposed a cost allocation method that considered the peak-shaving influence coefficient, by synthesizing the peak-shaving cost of each thermal power unit. In solving the problem of peak-shaving cost compensation for pumped storage power plants, Zhang et al. (2022) proposed the concept of quantifying the peak-shaving value of participating units. Jian et al. (2018) proposed a new mechanism based on Kaldor's improvement theory for the distribution of deep peak-shaving benefits and established a compensation fee rule that was convenient for engineering realization. Xie et al. (2012), Zhao et al. (2013), and Dong et al. (2016) studied the problem of peak-shaving cost allocation when wind power is connected to the grid and established a model division based on game theory. Shao et al. (2018) established a peak-shaving scheduling model based on the direct demand factors and indirect factors of peak shaving. It used the cooperative game method to apportion the peakshaving cost, effectively measuring the differences in the demand for peak-shaving auxiliary services by different subjects. Aiming at the problem of unfair peak-shaving cost allocation caused by renewable energy grid-connected, Hu et al. (2019) introduced the concept of active peak-shaving capability and proposed a new peak-shaving cost allocation method combined with peak-shaving characteristics of fluctuating power and conventional power. Chen et al. (2021) analyzed peak-shaving cost from the perspective of thermal power flexibility transformation and provided a theory for thermal power to participate in peak-shaving auxiliary services. Ye et al. (2022) used the theory of power generation rights to formulate crossprovincial wind power trading strategies and proposed a market mechanism conducive to cost compensation for peak-shaving units (units providing peak-shaving service). Jing et al. (2022) proposed a method for estimating system peak-shaving costs under high wind power penetration while considering flexible resource investment and peak-shaving markets. However, it is still limited to research on the peak regulation mechanism of the power side. Dong et al. (2017) studied storage sizing with a peak-shaving policy for wind farms based on the cyclic Markov chain model and indirectly analyzed the cost of energy storage caused by wind power. Li et al. (2022) considered the problem of the design of the peak-shaving market mechanism when the virtual power plant is connected to the grid. Xie et al. (2013) proposed a peak-shaving cost compensation method based on the combination of Shapley value and peakshaving mileage, but the peak-shaving value cannot be assessed on the load side. Liu et al. (2017)proposed a peak-shaving cost allocation mechanism based on the proportion of generator power generation. Luo et al. (2021) proposed a compensation mechanism for peak-shaving fees based on dynamic peak-shaving benchmarks but did not find a corresponding solution to the overflow peakshaving fee. Yang et al. (2022) analyzed the profit model of electric vehicle-type loads participating in the peak-shaving market, but there is little research on its peak-shaving responsibility. Li et al. (2020) proposed a peak-shaving model of fire-storage combination, without considering the load's responsibility for renewable energy consumption.

The perfect market rules should include all members in the power system. However, the aforementioned studies have very little research on load-side peak-shaving cost and lack the method of



peak-shaving value evaluation of various market members. Based on these, this article considers a user-side new energy source. Based on this, this article attempts to propose a peak-shaving mechanism that considers the responsibility for the consumption of new energy on the side. The innovation points of this mechanism are to evaluate the peak-shaving value of each member in the power system through the principle of marginal contribution value in Shapley and determine the peak-shaving costs of each user based on the degree of the user's consumption of new energy. The main contributions are summarized as follows:

- 1. This paper establishes a fast calculation model of the peakshaving cost based on existing research.
- This paper uses the contribution margin theory in Shapley's method to define the responsibilities of power and load and realizes the allocation of peak-shaving costs on both sides according to the responsibility.
- 3. For the problem of internal peak-shaving cost allocation on the load side, this paper uses the waveform similarity theory to analyze the impact of the load electricity consumption behavior on the consumption of renewable energy, so as to determine the new energy consumption responsibility of each load through the two indexes: fluctuation trend similarity and waveform amplitude difference. The results of the share of peak-shaving cost on the load side are determined by the two indexes.

This paper validates the effectiveness of the proposed method through a system example analysis of nine market members. The results will help market-oriented reforms under the background of renewable energy power system construction (**Figure 1**).

# 2 Value evaluation and modeling of power and load

# 2.1 Value analysis of the peak-shaving service of power and load

The existing mechanism stipulates that the fee for paid peakshaving auxiliary services shall be borne by renewable energy plants and other types of power plants that do not meet the peak-shaving requirements. It is not easy to effectively define and calculate the cost sharing when loads participate in peak-shaving auxiliary services. From a market perspective, each participant should bear the peakshaving cost according to its impact on peak shaving. The peakshaving value analysis is the quantification process of this impact. In the problem of benefit distribution or cost sharing, according to the cooperative game theory, for an alliance S, the value of any member to the alliance is the marginal contribution of the member, that is, the increase or decrease of the alliance value after the alliance loses the member. Therefore, in the peak-shaving auxiliary service market, the responsibility of each participant in the market should be expressed by its marginal contribution to peak shaving; that is, the peak-shaving value of any participant is the added value of its peak ancillary service fee. After calculating the added value of all participants, the user and the power generation side are classified into two categories. The ratio of the two categories is the weight ratio of the peak-shaving service fee on the power generation side and the load side. For the actual peak-shaving market, all market members form an indissoluble alliance S, the overall peak-shaving value of the alliance is v(S), and its peak-shaving fee is  $F_{\{S\}}$ . After losing alliance S, the peak-shaving fee does not exist, so the overall peak-shaving value of the alliance is considered to be equal to its overall peak-shaving fee

$$v\{S\} = F_{\{S\}}.$$
 (1)

When the alliance is stable, for a certain peak-shaving market member *i*, its peak-shaving value is  $v\{S_i\}$ , and it is too challenging to solve  $v\{S_i\}$  directly. Using the marginal contribution theory mentioned above, the member's peak-shaving value is calculated as follows:

$$v\{ S_i\} = F_{\{S\}} - F_{\{S/i\}}, \tag{2}$$

where  $F_{\{S/i\}}$  represents the peak-shaving fee of alliance S after excluding member *i*.

For the power side, after a certain generating unit is excluded, the power generation it undertakes should be supplemented by an additional generation of other peak-shaving units. At this time, the load factor of the peak-shaving unit increases, and the peak-shaving cost is negatively correlated with the load factor of the peak-shaving unit. The peak-shaving cost is reduced. On the premise that all market members are rational, the additional electricity generated by each peak-shaving unit should be optimized according to the principle of maximizing the peak-shaving cost reduction. On the load side, assuming that the system loses a certain load *i*, the reduced power consumption corresponds to the reduction of all peak-shaving units' output to make up for it. At this time, the load factor of the peak-shaving unit decreases. The peak-shaving cost is negatively related to the load factor of the peak-shaving unit, so the



peak-shaving cost increases. The load factor drop value of each peakshaving unit needs to be optimized to minimize the increase in the peak-shaving amount. The specific process is shown in **Figure 2**.

In **Figure 2**,  $F_{\{S/i-1\}}$  or  $F_{\{S/i-2\}}$  represents the overall peak-shaving fee of the alliance after losing a member on the power generation side, and  $F_{\{S/i+1\}}$  or  $F_{\{S/i+2\}}$  indicates the overall peak-shaving fee of the alliance after losing a member on the load side.

### 2.2 Peak-shaving value evaluation model

Based on the value analysis of power and load, the peak-shaving value evaluation model is constructed as follows:

$$P_{T,i} = \{P_{T,i,1}, P_{T,i,2}, \dots, P_{T,i,t}\},$$
(3)

where  $P_{T,i}$  is the power generation sequence of a generating unit.

$$P_{T,n} = \{P_{T,n,1}, P_{T,n,2}, \dots, P_{T,n,t}, n \neq i\},$$
(4)

where  $P_{T,n}$  is the power generation sequence of the remaining units. At the same time, the total amount  $\Delta P_{T,n}$  is set as the decision

variable.  $\Delta P_{T,n}$  can be calculated by the following formula:

$$\Delta P_{T,n} = \left\{ \Delta P_{T,n,1}, \Delta P_{T,n,2}, \dots, \Delta P_{T,n,t}, n \neq i \right\}.$$
(5)

After removing the set  $P_{T,i}$ , the power generation sequence of the remaining units  $P'_{T,n}$  is

$$P'_{T,n} = P_{T,n} + \Delta P_{T,n}, n \neq i.$$
(6)

At the same time, the objective function is

$$\nu \{S_i\} = F_{\{S\}} - F_{\{S/i\}} \Leftrightarrow 
\nu \{S_i\} = \max \{F(P_{T,i,t}, t) - F(P'_{T,i,t}, t)\}.$$
(7)

Constraints are as follows:

s.t 
$$\begin{cases} \sum_{n=1,n\neq i}^{N_g} \Delta P_{T,n,1} = P_{T,i,1} \\ \sum_{n=1,n\neq i}^{N_g} \Delta P_{T,n,2} = P_{T,i,2} \\ \dots \\ \sum_{n=1,n\neq i}^{N_g} \Delta P_{T,n,m} = P_{T,i,m} \end{cases}$$
(8)

where  $N_g$  is the number of the power plant.

Suppose the load sequence  $P_{L,i}$  of a specific load is

$$P_{L,i} = \{P_{L,i,1}, P_{L,i,2} \dots P_{L,i,n}\}.$$
(9)

After removing load *i*, the reduction output of the remaining generating units  $\triangle P_{T,n}$  is the decision variable, and  $\triangle P_{T,n}$  can be calculated by the following formula:

$$-\Delta P_{T,n} = \left\{ \Delta P_{T,n,1}, \Delta P_{T,n,2}, \dots \Delta P_{T,n,t}, n \neq i \right\}.$$
(10)

After removing the set  $P_{L,i}$ , the power generation sequence of the remaining units  $P'_{T,n}$  is

$$P'_{T,n} = P_{T,n} + \Delta P_{T,n}, n \neq i.$$
<sup>(11)</sup>

At the same time, the objective function is

$$\nu \{S_i\} = F_{\{S\}} - F_{\{S/i\}} \Leftrightarrow 
\nu \{S_i\} = \min \{F(P_{T,i,t}, t) - F(P'_{T,i,t}, t)\}.$$
(12)

Constraints are as follows:

s.t 
$$\begin{cases} \sum_{n=1,n\neq i}^{N_g} \Delta P_{T,n,1} = P_{L,i,1} \\ \sum_{n=1,n\neq i}^{N_g} \Delta P_{T,n,2} = P_{L,i,2} \\ \dots \\ \sum_{n=1,n\neq i}^{N_g} \Delta P_{T,n,m} = P_{L,i,m} \end{cases}$$
(13)

Let  $\alpha$ : $\beta$  be the weight ratio of the peak-shaving cost that should be borne by the power generation side and the load side.

$$\alpha:\beta = \left(\sum_{i=m}^{n} \nu\{S_i\}\right): \left(\sum_{i=j}^{k} \nu\{S_i\}\right).$$
(14)

According to formulas 3–8, 14, the cost to be borne by the power generation side is as follows:

$$F_{Gen} = \frac{\alpha}{\alpha + \beta} * F.$$
(15)

From formulas Eqs 9–13 and Eq. 14, the cost to be borne by the load side is as follows:

$$F_{Cus} = \frac{\beta}{\alpha + \beta} * F,$$
(16)

where *F* is the total peak-shaving fee,  $F_{Gen}$  is the cost of the power generation side, and  $F_{Cus}$  is the cost of the load side.

### 3 Apportionment method of peak-shaving cost considering the responsibility of the load side

## 3.1 Calculation of peak-shaving fee

The thermal power unit running at a low-load factor generates the deep peak-shaving fee F. When the output of thermal power unit is lower than the paid peak-shaving benchmark, the difference between the paid peak-shaving benchmark and the actual thermal power unit output is called the paid peak-shaving electricity. The peak-shaving fee is the sum of the products of the paid peak-shaving electricity of each gear and the peak-shaving marginal electricity price of each gear. The calculation model is as follows:

$$F(P_{i,t},t) = \sum_{t=1}^{T} \sum_{i=1}^{N_g} \left( \rho_t^{\alpha_1} \Delta P_{i,t}^{\mathrm{I}} + \rho_t^{\alpha_2} \Delta P_{i,t}^{\mathrm{II}} \right) * \Delta T, \tag{17}$$

where  $\Delta T$  is the sampling period,  $P_{i,t}$  is the output sequence of peak-shaving unit *i*,  $P_{i, \max}$  is the upper limits of output of peak-shaving unit *i*,  $P_{i, \min}$  is the lower limits of output of peak-shaving unit *i*,  $\beta_1$ {%} is the first-grade paid peak-shaving load factor of unit *i*,  $\beta_2$ {%} is the second-grade paid peak-shaving load factor of unit *i*,  $\beta_1$ {%} is the rated capacity of unit *i*,  $\rho_t^{\alpha_1}$  is the system marginal clearing price of the first level,  $\Delta P_{i,t}^{I}$  is the sistem marginal clearing price of the second level, and  $\Delta P_{i,t}^{II}$  is the second-level paid peak-shaving electricity of unit *i* at time *t*.

When  $P_{i,t} \in (\beta_1 \% * S_{N,i}, P_{i,\max})$ , the values of  $\Delta P_{i,t}^{I}$  and  $\Delta P_{i,t}^{II}$  are as follows:

$$\begin{cases} \Delta P_{i,t}^{\mathrm{I}} = 0\\ \Delta P_{i,t}^{\mathrm{II}} = 0. \end{cases}$$
(18)

When  $P_{i,t} \in (\beta_2 \% * S_{N,i}, \beta_1 \% * S_{N,i})$ , the values of  $\Delta P_{i,t}^{I}$  and  $\Delta P_{i,t}^{II}$  are as follows:

$$\begin{cases} \Delta P_{i,t}^{I} = \beta_{1} \% * S_{N,i} - P_{i,t} \\ \Delta P_{i,t}^{II} = 0. \end{cases}$$
(19)

When  $P_{i,t} \in (P_{i,\min}, \beta_2 \%^* S_{N,i})$ , the values of  $\Delta P_{i,t}^{I}$  and  $\Delta P_{i,t}^{II}$  are as follows:

$$\begin{cases} \Delta P_{i,t}^{I} = (\beta_{1}\% - \beta_{2}\%) * S_{N,i} \\ \Delta P_{i,t}^{II} = \beta_{2}\% * S_{N,i} - P_{i,t}. \end{cases}$$
(20)

### 3.2 Allocation method of peak-shaving cost on the power side

For the internal allocation of peak-shaving cost on the power side, each generating unit is calculated according to the proportion of the correction value of the on-grid electricity in each generator's peak-shaving billing cycle to the total. Among them, for thermal power units, if the load factor is higher than the minimum peak load factor requirement, the correction method is

$$S'_{T,j} = \sum_{j=1}^{5} \left( S_{T,j,1} * K_1 + S_{T,j,2} * K_2 + S_{T,j,3} * K_3 \right),$$
(21)

where  $S'_{T,j}$  is the correction value of the thermal power unit *j*'s ongrid power,  $S_{T,j,1}$  is the power generation of thermal power unit *j* when the load factor is between 50{%} and 70{%},  $K_1$  is the correction coefficient of the power level of the gear, and the value is 1,  $S_{T,j,2}$  is the power generation of the thermal power unit *j* when the load factor is between 70{%} and 80{%},  $K_2$  is the correction coefficient of the power level of the gear, and the value is 1.5,  $S_{T,j,3}$  is the power generation of thermal power unit *j* when the load factor is between 80{%} and 100{%}, and  $K_3$  is the correction factor for the electric quantity of this gear, and the value is 2. For renewable energy units, the power correction method is

$$S'_{Wk} = S_{W,k}^* d^* p^* z,$$
 (22)

where  $S'_{W,k}$  is the correction value of the on-grid power of renewable energy unit k;  $S_{W,k}$  is the actual power generation of renewable energy unit k; and d, p, and z are the heating period, utilization hours, and electricity price correction factor with or without subsidies, respectively. After the aforementioned formula corrects the electricity, the cost all thermal power units should bear is as follows:

$$F_{Gen,T,j} = \frac{S'_{T,j}}{\sum_{j=1}^{N_g} S'_{T,j} + \sum_{k=1}^{N_w} S'_{W,k}} F_{Gen},$$
(23)

and the cost all wind power units should bear is as follows:

$$F_{Gen,W,k} = \frac{S'_{W,k}}{\sum_{j=1}^{N_g} S'_{T,j} + \sum_{k=1}^{N_w} S'_{W,k}} F_{Gen},$$
(24)

where  $F_{Gen,T,j}$  is the cost that the non-renewable energy unit should bear and  $F_{Gen,W,k}$  is the cost that the renewable energy unit should bear.

# 3.3 Allocation method of peak-shaving cost on the load side

Based on the theoretical analysis of the waveform similarity, this paper sets up two indicators. One is the similarity of the fluctuation trend, and the other is the difference of the waveform amplitude. The difference between the original load curve and the ideal curve is analyzed through these two indicators. Then, these two indicators are combined to determine the impact of each load's power consumption behavior on peak regulation. Finally, the user side cost is determined.

#### 3.3.1 Idealized load power consumption curve

When the electric curve of the load is entirely consistent with the waveform of the renewable energy power generation curve, the fluctuations of the two uncertain factors of the power system at this time calm each other, which means that the load's power consumption behavior is ideal. The transformation method of the load-idealized curve is as follows:

$$\frac{P'_{L,i,t} - P'_{L,i,t-1}}{P'_{L,i,t-1}} = \frac{P_{W,t} - P_{W,t-1}}{P_{W,t-1}}t = 2, 3, \dots, T,$$
(25)

where  $P_{L,i,t}$  is the original power consumption sequence of load *i*,  $P'_{L,i,t}$  is the idealized power consumption sequence of load *i*, and  $P_{W,t}$  is the renewable energy generation sequence. According to the principle of equal electric quantity,  $P'_{L,i,t}$  and  $P_{L,i,t}$  satisfy the following relationship:

$$\sum_{t=1}^{T} P_{L,i,t}' = \sum_{t=1}^{T} P_{L,i,t}.$$
(26)

### 3.3.2 Fluctuation trend similarity coefficient

The fluctuation trend similarity coefficient  $\theta$  represents the similarity of the change of the load curve and the ideal curve waveform. The larger the indicator, the more similar. The calculation formula is as follows:

$$\theta_{L_{i}} = \frac{\sum_{t=1}^{T} \Delta P_{L,i,t}' \Delta P_{L,i,t}}{\sqrt{\sum_{t=1}^{T} \left(\Delta P_{L,i,t}'\right)^{2}} \sqrt{\sum_{t=1}^{T} \left(\Delta P_{L,i,t}\right)^{2}}}.$$
(27)

Among them,  $\Delta P'_{L,i,t}$  should be calculated from the idealized power consumption sequence of load  $P'_{L,i,t}$  using the following formula:

$$\Delta P'_{L,i,t} = \left\{ P'_{L,i,2} - P'_{L,i,1}, \dots, P'_{L,i,t+1} - P'_{L,i,t} \right\} \quad t = 1 \dots n - 1.$$
(28)

 $\Delta P_{L,i,t}$  should be calculated from the original power consumption sequence of load  $P_{L,i,t}$  using the following formula:

$$\Delta P_{L,i,t} = \{ P_{L,i,2} - P_{L,i,1}, \dots, P_{L,i,t+1} - P_{L,i,t} \} \quad t = 1 \dots n - 1.$$
 (29)

### 3.3.3 Waveform amplitude difference coefficient

The coefficient  $\theta$  based on the similarity algorithm of the string is sensitive to the fluctuation trend and not sensitive to the amplitude of the fluctuation. Therefore, setting Jensen–Shannon distance  $\tau$ measures the difference in the amplitude difference between the two distributions. The larger the indicator, the more different.

$$\tau_{L,i} = \frac{1}{2} \begin{pmatrix} \sum_{t=1}^{T} \left| \frac{P_{L,i,t}'}{P_{L,All,i}} \log_2 \frac{P_{L,i,t}'}{P_{L,i,t}} \right| \\ + \sum_{t=1}^{T} \left| \frac{P_{L,i,t}}{P_{L,All,i}} \log_2 \frac{P_{L,i,t}}{P_{L,i,t}'} \right| \end{pmatrix},$$
(30)

where  $\tau_{L,i}$  is the amplitude difference between load *i* and its own ideal power curve waveform and  $P_{L,AII,i}$  is the total power generation of load *i*.

According to formulas 27–30, the similarity between each load and the renewable energy generation curve is expressed as a two-dimensional vector ( $\theta$ ,  $\tau$ ).  $\theta$  represents the gap between the trends of the two curves, and  $\tau$  represents the difference between the amplitude distributions of the two curves. The formula for calculating the unbalanced electricity in the  $\theta$  direction is

$$\Delta S_{i,\theta} = (1 - \theta_{L,i}) \int_{1}^{T} \left| f_{L,i}'(t) - f_{LW,i}'(t) \right| dt.$$
(31)

The formula for calculating the unbalanced electricity in the  $\tau$  direction is

$$\Delta S_{i,\tau} = \tau_{L,i} \int_{-1}^{T} f_{L,i}(t) \, dt.$$
(32)

Comprehensive unbalanced electricity  $\Delta S_i$  is calculated by the following formula

$$\Delta S_i = \frac{1}{2} \sqrt{\Delta S_{i,\theta}^2 + \Delta S_{i,\tau}^2},\tag{33}$$

where  $\Delta S_{i,\theta}$  is the unbalanced power consumption of load *i* in the direction of  $\theta$ ,  $\Delta S_{i,\tau}$  is the unbalanced power consumption of load *i* in the direction of  $\tau$ ,  $f_{L,i}(t)$  is the function of the power consumption

Unit number	Max output/MW	Min output/MW	Ramp rate/MW per min	Minimum boot time/h	Minimum downtime/h
А	500	90	3.5	8	6
В	250	100	4	12	6
С	400	_	_	—	—
1	50	—	_	_	_
2	100	_	_	—	—
3	150		_	_	_

TABLE 1 Unit parameters.



curve of load *i* after interpolation,  $f'_{L,i}(t)$  is the derivative function of the interpolated power consumption curve of load *i*,  $f'_{LW,i}(t)$  is the derivative function of the renewable energy generation curve, and  $\Delta S_i$  is the total unbalanced power consumption of load *i*. Based on the aforementioned analysis, for any load, the peak-shaving cost it should bear is

$$F_{Cus,i} = \frac{\Delta S_i}{\sum_{i=1}^k \Delta S_i} * F_{Cus},\tag{34}$$

where  $F_{Cus,i}$  is the peak-shaving cost that load *i* should bear and  $F_{Cus}$  is the total peak-shaving cost on the load side.

# 4 Case analysis

### 4.1 Calculation overview

This paper uses a regional system including six power producers and three typical power users for verification and analysis. The parameter power units are shown in **Table 1**. The outputs of nonrenewable energy plants are shown in **Figure 3**. The outputs of renewable energy plants are shown in **Figure 4**. The typical load curves are shown in **Figure 5**.





In **Table 1**, numbers A–B are peak-shaving thermal power plants, C is hydropower plants, and 1–3 are renewable energy plants. The peak-shaving benchmark of thermal power units for peak regulation is set as follows:  $50\{\%\}$  of the load factor is the first-grade paid peak-shaving service boundary, and  $40\{\%\}$  is the





### TABLE 2 Cost comparison of different allocation methods.

Market member	nber Original method 1		Original method 2		New method	
	Cost	Profit	Cost	Profit	Cost	Profit
Unit 1	40,323.33	0	39,389.41	0	27,783.13	0
Unit 2	80,646.67	0	90,668.57	0	64,579.57	0
Unit 3	120,970	0	111,882.02	0	78,850.33	0
Unit A	0	223,280	0	223,280	0	223,280
Unit B	0	18,660	0	18,660	0	18,660
Unit C	0		0	0	0	0
Load	0		0	0	70,740.97	0

second-grade paid peak-shaving service boundary. The highest price for each level of peak regulation is 0.4 RMB/kWh and 1 RMB/kWh, respectively. The on-grid electricity price of renewable energy is 0.3749 RMB/kWh, and the power correction coefficients of each renewable energy are d = 2, p = 1, and z = 0.5.

# 4.2 Analysis of peak-shaving cost apportionment results

The calculation examples show the division of peak-shaving responsibilities for power and load. The specific calculation results are as follows.











# 4.2.1 Responsibility division and apportionment results for power and load peak regulation

The calculated peak-shaving cost is shown in **Figure 6** according to **Table 1**, **Figure 4**, and Eqs 17–20.

In **Figure 6**, the peak-shaving depth of the thermal power unit mainly determines the peak-shaving fee. When the first-tier paid peak-shaving capacity of the system is insufficient, it will enter the second-tier peak-shaving interval. At this time, the peak-shaving cost curve has a peak moment. Before allocating the peak-shaving cost of the load side, the respective peak-shaving responsibilities of the power and load sides should be divided. The peak-shaving value expresses the peak-shaving responsibility of a certain market participant. The ratio of the total peak-shaving value on the power side to the total peak-shaving costs. As the operating conditions of the system change from time to time, the peak-shaving value of market participants also changes dynamically. **Figure 7** shows the



In **Figure** 7, the blue and red histograms are the power and load peak-shaving values, respectively; the green needle graphs are the weight ratios of power and load peak-shaving responsibilities by time. The example uses the intraday weight ratio average (2.44:1) for calculation. Under this weight ratio, the cost comparison of different allocation methods is shown in **Table 2**.

In **Table 2**, original method 1 is based entirely on the allocation of electricity division. This allocation method is the most basic and original allocation method, which to some extent reflects the responsibility of peak shaving. However, there is no more detailed evaluation of peak-shaving responsibility. Original method 2 only allocates peak-shaving costs on the power source side based on the correction electricity value, which is currently implemented in most regions of China. It corrects and compensates for units with poor efficiency. There is still no detailed evaluation



Market member	Original method 1		Original method 2		New method	
	Cost	Profit	Cost	Profit	Cost	Profit
Load 1	0	0	0	0	17,350	0
Load 2	0	0	0	0	9,788	0
Load 3	0	0	0	0	43,602	0

#### TABLE 3 Load-side internal cost allocation result.

of peak-shaving responsibilities. The new method considers the peak-shaving responsibilities on both sides of the power and load and establishes a detailed peak-shaving responsibility evaluation model.

In the scenario, the weight ratio of power and load peak-shaving responsibilities is 2.44:1. Considering the output of peak-shaving thermal power units, thermal power units A and B both meet the peak-shaving requirements and do not need to bear peak-shaving costs; hydropower unit C is not involved in the apportionment mechanism, so the peak-shaving cost is 0. Based on the renewable energy output, the renewable energy on-grid electricity from large to small is Unit 3 > Unit 2 > Unit 1. In **Figures 8**, **9**, the results of cost allocations match the ranking results of power plants' on-grid electricity.

Considering the apportionment mode of user-side participation, the total apportioned cost of the power side is reduced from 241,940 yuan to 171,213.03 yuan. Unit 1 reduces the cost by 11,606.28 yuan; Unit 2 reduces the cost by 26,089 yuan; and Unit 3 reduces the cost by 33,031.69 Yuan. The results show that the new method diminishes the peak-shaving cost of the renewable energy power generation side by 18.52{%} on average. Compared with **Figures 8**, **9**, the sort of peak adjustment costs of each renewable energy unit before and after load participation remains unchanged. However, for large-capacity renewable units, the reduced cost is more than other small-capacity units, which encourages the future construction of large-capacity renewable energy sources.

# 4.2.2 Allocation results of peak-shaving cost on the load side

According to the content of Chapter 2.3, the original power consumption curve of each load and the load-idealized curve are shown in **Figure 10**.

In **Figure 10**, the power consumption curve after equal power conversion is the load-idealized curve. The load-idealized curve is consistent with the waveform of the renewable energy total power generation curve, and the total power consumption is equal to the power consumption of the load curve before conversion. The total power consumptions of loads 1–3 are 2381.83 MW, 2403.21 MW, and 3397.90 MW, respectively.

Calculated according to formulas 27-30, the similarity vectors between loads 1-3 and their load-idealized curve are (0.07, 0.12), (0.29, 0.14), and (-0.25, 0.25). Each vector is in two-dimension, and the position relationship is shown in **Figure 11**.

It can be seen intuitively from **Figure 11** that the volatility trend similarity is load 2 > load 1 > load 3, and the waveform amplitude difference is load 3 > load 2 > load 1. After calculating the similarity vector between each load and its load-idealized curve, the peak-shaving unbalanced power of each load is obtained by Eqs 31–33.

The smoothing of each load output sequence is carried out after cubic spline interpolation. The curve is shown in **Figure 12**.

According to the interpolation results and Eq. 34, the total peakshaving unbalanced power and the sharing ratio of each load are shown in **Figure 13**.

On the load side, the peak-shaving cost borne by any load should be apportioned according to the proportion of the load's peak-shaving unbalanced power consumption. **Figure 13** shows each load's peak-shaving unbalanced power within a day in the blue histogram. The sharing ratio corresponding to the waveform similarity between each load and the renewable energy output curve is shown in the red histogram. The peak cost ratios are 26.86{%}, 21.06{%}, and 52.08{%}. The calculation results of internal cost allocation on the load side are shown in **Table 3**.

It can be seen from the calculation results that the fluctuation trend similarity between the power consumption curve of load 1 and the renewable energy output curve is 0.07, and the waveform amplitude difference is 0.12. Although the power consumption curve of load 1 is stable, it has no outstanding contribution to the consumption of renewable energy. So, load 1 bears the second highest fee. The similarity of the fluctuation trend of load 2 is 0.29, and the difference in waveform amplitude is 0.14. However, its power consumption trend has played a certain role in renewable energy consumption, so it bears the minimum fee. The similarity of the fluctuation trend of load 3 is -0.25, and the amplitude difference of the waveform amplitude is 0.25. The power trend could be more conducive to the consumption of renewable energy. Its waveform amplitude has a large difference, which increases the burden of renewable energy consumption in the system, so it bears the highest fee. Based on the aforementioned analysis, the peakshaving responsibility on the load side is ranked from large to small as load 3 > load 1 > load 2. The final cost allocation result is consistent with the ranking of responsibilities, which achieves the unified right and responsibility of peak-shaving cost allocation on the load side.

## 5 Conclusion

In the context of low-carbon power system construction, this paper proposes a peak-shaving cost allocation mechanism that considers the responsibility of renewable energy consumption on the load side. First, according to the peak-shaving value of market participants, the weight ratio of peak-shaving value on the power and load side is divided. Then, according to the similarity between the load curve and load-idealized curve, this paper calculates the peak-shaving cost that each load should bear. Finally, the calculation example shows that this method achieves the distribution purpose of "allocation according to rights and allocation according to responsibilities." Meanwhile, the new method implements the allocation idea "who benefits, who bears." The method proposed in this paper incorporates the load side into the main body of peakshaving cost allocation. It is conducive to regulating the rational use of electricity by power users, promoting the development of renewable energy, and contributing to the construction of the future low-carbon power system.

## Data availability statement

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

## Author contributions

LC and WY contributed to the conception and design of the study. ZY performed the statistical analysis. ZY wrote the first draft of the manuscript. WY, ZY, XY, XZ, CG, and GW wrote sections of the manuscript. All authors contributed to the article and approved the submitted version.

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## **Conflict of interest**

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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