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Digital light processing of yttria-stabilized zirconia: Modeling photoinitiator decay

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A digital process was developed to facilitate additive manufacturing for ceramic materials using digital light processing (DLP). A numerical model that predicts DLP sample properties can be generated from manufacturing inputs to forecast the effect of resin age on mechanical strength of the printed part based on data collected from experiments. Key parameters for printing the green bodies included determining the depth of cure, layer thickness, material composition, and solids loading. Thermogravimetric analyses were used to develop debinding and sintering curves. Debinding is used to remove the volatile organics comprising the photopolymer resin. Sintering is performed after debinding to increase density and mechanical strength of the printed parts. The sintered parts were then subjected to characterization and mechanical testing. The ensemble of data for various DLP-printed ceramic materials were added to a database. A design of experiments can be generated from the manufacturing process defined in the database with selected changeable parameters randomized over a range. Because the database is defined with an architecture to capture manufacturing processes, it can persist as a more generic platform for manufacturing digital twins. This can ease the development of future digital twins and can grow as a common repository for the insights gained from manufacturing research. Creating a digital twin of a DLP system for 3D printing parts enables manufacturers to simulate and assess the impact of resin age on printing parameters and part quality, facilitating optimization, predictive maintenance, and cost reduction.

KEYWORDS

digital twin, digital light processing, ceramics, additive manufacturing, response surface modeling

1 Introduction

Additive manufacturing, a revolutionary approach to fabricating complex structures, has found a niche in ceramic materials through the advent of Digital Light Process (DLP) printing. This innovative digital process has been tailored to facilitate the additive manufacturing of ceramics, specifically Yttria-stabilized Zirconia (YSZ). In this study, we delve into the development of a digital model capable of predicting the properties of DLP-printed YSZ samples. The model's foundation lies in manufacturing inputs and key parameters governing the production of ceramic-resin green bodies.

Following the printing process are the stages of debinding and sintering, which contribute to the enhancement of density and mechanical strength in the final printed parts. Following the manufacturing process, the sintered parts underwent comprehensive characterization and mechanical testing. While other studies have been performed using DLP for YSZ printed parts, the effect of resin age on the mechanical properties has not been evaluated. This study compares the mechanical strength of resin at 114 days from production to 324 days from production. Understanding how resin age affects printing quality can help in forecasting when maintenance or resin replacement might be needed in the actual system. This predictive maintenance approach can save time and resources by avoiding unexpected downtimes, part failures, and procurement inefficiencies. Assessing the effect of resin age digitally can potentially save costs associated with physical testing and experimentation. It enables fabricators of 3D printed parts to identify optimal resin usage strategies and minimize waste, thus reducing overall production costs.

In this study, sample characterization results were uploaded to a unique digital model built around a data ontology specific to advanced manufacturing methods. The use of a data ontology allows the data to be managed in a manner that both strictly controls the validity and completeness of the manufacturing data, but also provides the flexibility to define variants of This digital twin framework organized the varying manufacturing inputs, detected factors that changed between experiments, and generated a predictive model of YSZ strength in bending based on days since material feedstock synthesis and ambient humidity. The ontology is explored in its role to define both the data that is involved in the details of manufacturing and also the performance characteristics of interest with specific designs of experiment that tie them together.

The digital twin framework realized several advantages that would not be accomplished traditionally: the completeness of the data was enforced by the ontology meaning each experiment is fully defined with material properties, preform geometry, and all manufacturing settings, which is important for future reuse of data; the data was preprocessed automatically for analysis with a Gaussian process model; and, data entry efforts resulted in a queryable model that would return the predicted strength in bending value of YSZ samples (and accompanying measure of uncertainty) for a given combination of ambient humidity and days since synthesis of feedstock materials.

The predictive model resulting from the digital twin was tested with a random sampling of characterization results withheld from the modeling engine and used as a verification set. The model is reliable within the bounds of uncertainty returned by the Gaussian process. While a trend of decreasing strength was observed in the samples due to both increasing humidity and feedstock age, the strength of the whole set of materials was well below results expected based on published performance characteristics of YSZ. A discussion of factors that likely led to under performance is included. Future work should take greater care to apply a debinding/sintering heat treatment sourced from literature instead of manufacturersupplied settings.

2 Materials and methods

2.1 Yttria-stabilized zirconia

YSZ is a material of interest for the design and manufacture of various energy systems. YSZ has unique balance of physical properties, encompassing electrical (Lanagan et al., 1989), thermal (Tojo et al., 1999; Hayashi et al., 2005), mechanical (Ren and Pan, 2014), and optical (Alaniz et al., 2009) properties. Because of its electrical performance it has been implemented in energy products such as solid oxide fuel cells (Butz, 2009) and because of its mechanical resilience at high temperatures it has been used as a thermal barrier coating (Zhao et al., 2006; Liu et al., 2019; Chen, 2006), both of which are of interest for energy applications. YSZ has been manufactured via traditional sintering (Laberty-Robert et al., 2003), colloidal suspension extrusion (Peng et al., 2018; Ghazanfari et al., 2017), and digital light processing (Coppola et al., 2022). In this study, 3 mol% YSZ was used for the DLP printing. Biomedical applications for this material include dental crowns Snyder (2022).

The YSZ used in this study was used to generate samples via a three-dimensional printing method that cures layers of photosensitive resin. As such, the green body for samples generated in this study makes use of granular YSZ suspended in a slurry of photosensitive resin which creates a layer-by-layer scaffolding to define geometry. The organic resin scaffold is later removed via postprocessing techniques, leaving only the YSZ in the final sample.

2.2 Digital light processing

DLP is an additive manufacturing method that uses ultraviolet light to cure thin layers of photosensitive liquid polymer resin to form solid samples (Zhao et al., 2020). Thanks to the possibility for far greater light intensity than other photocuring techniques, DLP printing can be used to fabricate parts from resin slurries that are made semiopaque through the addition of ceramic and metallic powders. The cured polymer-ceramic/metallic green bodies resultant from printing can then undergo the subsequent postprocesses of debinding to remove the polymer matrix and sintering to solidify the remaining material, resulting in printed parts consisting purely of the ceramic or metal. This method has been successfully applied to alumina (Santoliquido et al., 2019; Shuai et al., 2020), silicone oxycarbide (Schmidt and Colombo, 2018; He et al., 2020), zeolite (Guillen et al., 2023), zirconia compounds and barium titanate (Mamatha et al., 2022; Mu et al., 2022). An illustration of the components of the printing stage of the process is shown in Figure 1.

2.2.1 Resin matrix

The photosensitive resin that acts as a temporary matrix for the YSZ acts is hardened via the interaction of the resin polymer and an additive photoinitiator. The photoinitiator is a constituent that is reactive to light exposure. When the photoinitiator is activated by light energy it generates molecular constituents that attract areas of the free floating polymer chains that make up the resin. The photoinitiators selected for these resins bind to them in such a way that multiple polymer chains can bind to a



single activated element (Allen, 1996). As free floating polymers in the path of the directed light are bound together in large networks with cross linked elements, the engineering-scale effect of this process is that the material is hardened and fixed in those regions. These photoinitiating additives are known to degrade along with other resin elements over time after the resin mixture is formulated (Nagaoka et al., 2020).

2.3 Digital representation of manufacturing processes

2.3.1 Ontology

A digital approach to manufacturing often raises the issue of ontologies. An ontology is a set of concepts and classes that define the entities in a domain, their relationships, and their properties. Ontologies in manufacturing have been explored as a method to query information from manufacturing data (Usman et al., 2013), to automate manufacturing design and decision making (Sanfilippo et al., 2019), and to create interoperability among different manufacturing design software applications (Chungoora et al., 2013).

While efforts to create an ontology to link design engineering and manufacturing methods (Chhim et al., 2019) have been explored, the ontology efforts of this project are geared toward making a single model of a manufacturing process that can be be used for experimental design generation (via the response surface method), manufacturing, and simulation, all in the service of sample performance prediction. The ontology is called Advanced Manufacturing Basic Entity Relationships (AMBER) and is based on the ontology Data Integration Aggregated Model and Ontology for Nuclear Deployment (DIAMOND), funded by an award from the Department of Energy's Office of Nuclear Energy (Browning et al., 2020). Both ontologies make use of the Basic Formal Ontology (BFO) entities (Arp et al., 2015) near the root for future interoperability with other BFO-compatible models. A diagram of the classes in the ontology is shown in Figure 2. The classes in the ontology are built around representing the properties and relationships that describe factors relevant both to the manufacturing of samples with DLP, and also the data modeling activities and numeric models necessary for making predictions from the relationship between these factors and the resultant performance of the samples.

The AMBER ontology is implemented in the Deep Lynx data lake (Darrington et al., 2020), a DOE-funded open source software utility. Deep Lynx allows ontologies to initialize a database, which can be used for storage, querying, and version control. For this project, the elements of a manufacturing build, decomposed by the definition and constraints of the process that generated it, feedstock material properties, and preform geometry, are all located in the same knowledge graph. The ontology also defines entities to store the resultant characteristics, that may be physical or simulated, and the predictive models themselves that are generated from the relationship between manufacturing inputs and outputs.

2.3.2 Predictive modeling

The response surface method (RSM) has been used widely in the search for optimal manufacturing parameters (Sik Shim, 2021; Geng et al., 2017; Al-Ahmari et al., 2016; Seo et al., 2017; Jagadish et al., 2016; Öktem et al., 2005). The method uses a constellation of techniques to systematically approach the discovery of optimal resultants in parameterized systems; the components of modern RSM involve generating a design of experiments, carrying out the designs, and using statistical techniques to correlate the relationship between design parameters and experimental resultant values. Typically, for techniques in which design parameters can be set continuously and independently within a set of ranges, the designs are generated using the central composite design or Box-Behnken design (de Oliveira et al., 2019). These methods define efficient designs that explore the contribution of parameters of interest across their available ranges. An alternative experimental design method was used for this study due to the constraints imposed by the manufacturing technique. Although layer height is of interest, batches of samples printed together must have the same basic layer height in order to print together. Because manufacturing was carried out in batches, there are discrete layer heights. As such the design method used in this study is a single parameter design.

Typically, once the experiments are carried out and the results recorded, the response surface is generated using a simple least squares regression. This study opts instead for a Gaussian Process Model (GPM), in order to create surfaces that not only predict regions of results inside the design envelope but also return uncertainty measurements as surfaces that bound the prediction surface. The RSM models were generated using utilities on the stochastic tools module (Slaughter et al., 2023) of the Multiphysics Object-Oriented Simulation Environment (MOOSE) simulation library (Lindsay et al., 2022). The library's GPM is implemented as follows:

Given a set of input parameters $X = \{\vec{x}_1, \vec{x}_m\}$, and a set of corresponding outputs of the form $Y = \{\vec{y}_1, \vec{y}_m\}$ that result from the function or process Y = f(X) the Gaussian model should return a new set of results $Y_* = \{\vec{y}_{*1}, \vec{y}_{*n}\}$ given new input parameters $X_* = \{\vec{x}_{*1}, \vec{x}_{*n}\}$ without incurring the cost of evaluating $Y_* = f(X_*)$.

In much the same way a multivariate Gaussian distribution is fully defined by its mean and covariance matrix, the Gaussian



Process [shown in Equation 1] is defined by two functions: the mean function and the covariance function, where $\mu(\vec{x})$ are the parameters from the training set and $\mu(\vec{x'})$ are the parameters being evaluated. The mean function $\mu(\vec{x})$ and the covariance function $k(\vec{x}, \vec{x'})$ are tuned on the training data.

$$\mathcal{GP}\left(\mu\left(\vec{x}\right), k\left(\vec{x}, \vec{x'}\right)\right) \tag{1}$$

The mean function returns the mean value for any combination of parameters. The covariance function is meant to describe the relationship that the input parameters in the study have to one another. The output of the covariance function (also called a kernel function) is a covariance matrix that describes the complete set of parameters (every parameter's relationship to every other parameter). The complete set of covariance matrices available from the kernel function are as follows in Equations 2–4:

$$\mathbf{K}(X \cup X_{\star}, X \cup X_{\star}) = \begin{bmatrix} k(\vec{x}_{1}, \vec{x}_{1}) & \cdots & k(\vec{x}_{1}, \vec{x}_{m}) & k(\vec{x}_{1}, \vec{x}_{\star}) & \cdots & k(\vec{x}_{1}, \vec{x}_{\star n}) \\ \vdots & \vdots & \vdots \\ k(\vec{x}_{m}, \vec{x}_{1}) & \cdots & k(\vec{x}_{m}, \vec{x}_{m}) & k(\vec{x}_{m}, \vec{x}_{m}) \\ k(\vec{x}_{\star 1}, \vec{x}_{1}) & \cdots & k(\vec{x}_{\star n}, \vec{x}_{\star n}) \\ \vdots & \vdots \\ k(\vec{x}_{\star n}, \vec{x}_{1}) & \cdots & k(\vec{x}_{\star n}, \vec{x}_{m}) \\ \end{bmatrix} \begin{pmatrix} k(\vec{x}_{\star}, \vec{x}_{\star}) & \cdots & k(\vec{x}_{\star n}, \vec{x}_{\star n}) \\ k(\vec{x}_{\star n}, \vec{x}_{\star}) & \cdots & k(\vec{x}_{\star n}, \vec{x}_{\star n}) \\ k(\vec{x}_{\star n}, \vec{x}_{\star 1}) & \cdots & k(\vec{x}_{\star n}, \vec{x}_{\star n}) \\ \end{bmatrix}$$
(2)

$$= \begin{bmatrix} \mathbf{K}(X,X) & \mathbf{K}(X,X_{\star}) \\ \hline \mathbf{K}(X_{\star},X) & \mathbf{K}(X_{\star},X_{\star}) \end{bmatrix}$$
(3)

$$= \begin{bmatrix} \mathbf{K} & \mathbf{K}_{\star} \\ \hline \mathbf{K}_{\star}^{T} & \mathbf{K}_{\star\star} \end{bmatrix}$$
(4)

With this definition of the covariance function and its output, along with the assumption that the distribution of the training data and the evaluation data will be roughly the same the model can undergo conditioning. The Gaussian Process Model starts with an infinite collection of functions such that any random selection of output variables from the collection will produce a normal distribution. In the conditioning process functions are winnowed down from the infinite set to only those functions that agree with the training and evaluation sets, according to the following in Equations 5, 6:

$$\mu_{\star} = \mu + \mathbf{K}_{\star} \mathbf{K}^{-1} \left(Y - \mu \right) \tag{5}$$

$$\Sigma_{\star} = \mathbf{K}_{\star\star} - \mathbf{K}_{\star}^{T} \mathbf{K}^{-1} \mathbf{K}_{\star}$$
(6)

and the output of the model will be given as shown in Equation 7

}

$$V_{\star} \sim \mathcal{N}(\mu_{\star}, \Sigma_{\star})$$
 (7)

The particular kernel function used for this study was the radial basis function. It contains the additional terms (or hyperparameters) l, which is a length scale term which correlates loosely to the standard deviation of a given model parameter and affects the smoothness of the fitted model; σ_f^2 , which represents the true signal variance and acts as an overall length scale term; and σ_n^2 , which acts as a signal noise term which generally improves model fitting even when acting on relatively noiseless data. The radial basis function is shown as follows in Equations 8, 9:

$$k(x,x') = \sigma_f^2 \exp\left(-\frac{r_\ell(x,x')^2}{2}\right) + \sigma_n^2 \,\delta_{x,x'} \tag{8}$$

where $r_{\ell}(x, x')$ is expanded as

$$r_{\ell}(x,x') = \sqrt{\sum_{n} \left(\frac{x_i - x'_i}{\ell_i}\right)^2}$$
(9)

In this study's implementation, the Gaussian process pulls its training data from the digital representation of a set of experiments. It prompts the user for initial hyperparameter values, trains the model, and stores the model executable in the graph for future reference and execution. Although the Gaussian process requires more data preparation and more operations than a simple fit using linear or polynomial regression, the digital twin framework uses the GPM in order to deliver models that return uncertainty

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TABLE I FINITING parameters used across att s	amptes in the study.			
Layer height (µm)	LED power (%)	Pixel value (%)		
20	30	100		
Exposure per layer (s)	Delay before exposure (s)	Delay after exposure (ms)		
2	30	500		
Transport speed (µm/s)	Transport acceleration (μ m/s ²)	Transport distance margin (μm)		
20,000	20,000	50,000		
Up/down distance (µm)	Up/down speed (µm/s)	Up/down acceleration (µm/s²)		
20,000	10,000	7,500		
Slow up distance (µm)	Slow up speed (µm/s)	Slow down distance (µm)		
2000	300	500		
Slow down speed (µm/s)	Scale	Fans PWM freq (Hz)		
200	1	0		
Anti-aliasing	Power calibration mask	Power mask type		
Enabled	Enabled	Load		
Z-axis min accuracy (nm)	Z-axis homing spd (µm/s)	Z-axis homing acc (μm/s²)		
15,000	10,000	10,000		
Z-axis zero current (mA)	Z-axis zero spd (μm/s)	Z -axis zero acc (μ m/ s^2)		
800	10,000	10,000		
Z-axis zero slow spd (µm/s)	Z-axis zero slow duration (s)	Z-axis max manual spd (μm/s)		
20	40	10,000		
Foil tension distance (µm)	Transport error margin (µm)	Transport jog spd (µm/s)		
2000	15,000	15,000		
Transport jog acc (μ m/s ²)	Min transport distance (µm)	Transport calc height (µm)		
15,000	0	200		
Delayed transport	Pump PWM freq (Hz)	Pump PWM duty cycle (%)		
Enabled	60	80		
Transport max speed (µm/s)	Refill pump freq (Hz)	Refill pump duty cycle (%)		
100,000	60	100		
Refill sensor level (ppm) Current refill level		Refill sensor margin (ppm)		
465,000	Update	5,000		
Max refill pump duration (s)	Max refill foil distance (µm)	End pump back		
500	750,000	Enabled		
End pump back spd (μm/s)	End pump back dist (µm)	End pump back duration (s)		
5,000	2,000,000	600		

Temperature (C°)	Rate (C°/hr)	Time (min)		
25-150	25↑	300		
150	dwell	30		
150-290	8↑	1,050		
290	dwell	90		
290-400	8 ↑	825		
400	dwell	60		
400-600	12 ↑	1,000		
600-1,000	60 ↑	400		
1,000	dwell	60		
1,000–25	100↓	600		
25-1,000	200 ↑	300		
1,000–1,500	100 ↑	300		
1,500	dwell	180		
1,500–20	200↓	450		

TABLE 2 Debind/sinter profile, shaded cells indicate the sintering phase.

bounds along with every point of evaluation. In the digital twin's implementation, the manual data management usually involved with using the Gaussian model is handled by an interface that automates most onerous data preparation tasks.

2.4 Manufacture of physical samples

2.4.1 Sample geometry

Miniature three-point bend bars ($25 \text{ mm} \times 4 \text{ mm} \times 1 \text{ mm}$) were printed using an Admatec Admaflex 130 DLP printer with commercially available photocurable YSZ resin (Admatec, Alkmaar, Netherlands). The samples printed in the study were designed using the ASTM C1161-18 design specification (ASTM International, 2018). This is a prismatic geometry optimized for testing the flexural strength of ceramic samples at ambient temperatures. The tesselated geometry was stored in the digital twin architecture as an STL file and also exported as a batch to the printer. Since the Admatec 130 build plate can accommodate 20 samples arranged in a grid pattern, 20 became the batch size wherein the layer height was held constant.

2.4.2 Feedstock formulation and print settings

The print settings given in Table 1 were applied to all samples.

The layer height was determined by a depth of cure test in which a small amount of the slurry is placed on the printing surface and exposed to a certain duration of light exposure. The cured material is measured from the printing base After printing, each sample was post-processed with the same thermal treatment that debinds the organic resin matrix and then sinters the remaining ceramic



material to its final density. The profile of this heat application is listed in Table 2.

One of the factors impacting the quality of printed samples is exposure to atmospheric humidity. The room in which the printing took place did not have a dehumidifier for the printing area nor for the lab space. Because of this, average humidity values during the time of printing (from 12:00 to 18:00, each day) was considered as a variable in the modeling effort, and as an element of the digital twin framework.

2.5 Mechanical testing

2.5.1 Flexural strength

Flexural strength is the ultimate strength (the stress at which a tested sample breaks or cracks) when subjected to a bending load. The flexural strength and the tensile strength of a material, especially a ceramic, are correlated values (Leguillon et al., 2015). The general standard practice for materials that are brittle, such as ceramics, is to use determine material performance for an application from flexural strength, as these measures tend to be the most representative of application performance (Yamaguchi et al., 2019).

Samples were measured for flexural strength using a three-point configuration as illustrated in Figure 3. Conducting three-point bend tests on ceramic materials, as opposed to tensile tests, is driven by several considerations rooted in the inherent characteristics of ceramics. Primarily, ceramics exhibit brittleness, and their tensile strength is notably lower than their compressive strength. Tensile loading can lead to premature and catastrophic failure due to the limited capacity of ceramics to withstand tensile stress. The high friction jaws used in tensile testing lead to many samples cracking, making this technique impractical for this study. In contrast, threepoint bend tests provide a controlled environment for studying

Days	114	143	175	205	236	273	324
Humidity (%)	51	37	40	44	62	49	34
		*50.275					
		*61.896		111.326	96.393	56.985	*110.389
	*20.009	89.629	*117.785	124.939	107.027	76.538	^{<i>T</i>} 145.004
	*30.337	146.793	*122.669	141.539	117.671	94.23	145.251
	90.259	152.957	*123.581	150.44	119.977	104.218	149.645
	^T 90.804	159.699	146.211	150.909	120.104	105.895	155.593
	^T 113.717	160.17	153.555	151.968	133.599	114.405	155.967
	118.642	172.906	158.241	153.526	138.35	118.799	156.761
	123.733	177.145	158.368	154.516	140.989	133.107	156.78
	125.815	178.561	159.588	156.865	142.973	133.972	159.409
	126.276	186.418	164.161	158.345	151.516	^{<i>T</i>} 134.565	162.62
MPa	127.171	^T 186.811	165.436	^{<i>T</i>} 166.89	156.192	136.695	163.231
	127.273	198.395	167.076	171.518	^{<i>T</i>} 158.21	142.59	165.764
	127.602	199.791	168.161	174.172	159.065	146.99	169.915
	^T 130.425	204.586	169.017	177.424	170.406	152.016	170.904
	131.437	209.837	174.752	180.567	170.949	157.836	175.632
	136.102	^T 220.923	178.212	^{<i>T</i>} 183.195	181.52	158.131	180.142
	138.558	^{<i>T</i>} 221.284	186.058	183.276	^{<i>T</i>} 186.312	164.166	182.722
	142.871	226.269	190.457	187.49	186.354	169.966	^T 183.565
	147.432	235.105	194.898	195.942	193.42	179.725	190.437
	*406.74	236.888	*218.689	201.104	197.376	198.757	192.845
		248.215					
		249.586					

TABLE 3 Per-sample flexural strength values (MPa) gathered from bending tests organized by days since slurry synthesis. Outlier values are marked with an asterisk *. Validation samples are marked with a T.

fracture mechanics, including crack initiation and propagation, which is essential for understanding how ceramics fail. Fracture mechanics in ceramics are better captured through three-point bend tests, as these tests facilitate the controlled study of crack propagation. Tensile tests may not effectively capture critical flaw sizes or stress intensity factors crucial for assessing the fracture process in brittle materials.

Practically, ceramics are often employed in structural applications where they experience bending or flexural loads rather than tension. three-point bend tests simulate these realworld loading conditions, offering more relevant insights into how ceramics behave in practical applications. Additionally, the geometry of ceramic components frequently involves bending, making three-point bend tests more representative of actual service conditions. Moreover, the size and shape of samples for three-point bend tests are more manageable, requiring smaller specimens compared to the larger cross-sectional areas needed for tensile tests. Interpreting data from three-point bend tests is often more straightforward, with a more uniform stress distribution across the sample compared to tensile tests. This simplicity aids in relating the test results to the material's properties.



TABLE 4 Printing parameters used across all samples in the study.

Scale (<i>l</i>)	Signal variance (σ_f^2)	Noise variance (σ_n^2)
1	1	0.3

Standardization further supports the preference for threepoint bend tests in ceramics. Widely recognized testing methods, such as ASTM C1161-18, recommend three-point bend tests as the preferred approach for determining flexural strength and modulus of rupture. This standardization ensures consistency and comparability of results across different studies and laboratories, contributing to the robustness of data obtained from such tests.

3 Results

3.1 Sample performance

Seven sets of samples were printed from the same slurry batch which was synthesized on 15 May 2023. The sets were

printed at the following days since synthesis: 114, 143, 175, 205, 236, 273, and 324. The long gap between synthesis and the first batch print was due do a shipping delay with the Admatech slurry. The flexural strength values from each sample are shown in Table 3. Each set was subjected to the interquartile range test for outliers, and the outliers were thrown out of the model development and analysis. The general trend of the progressively older samples is decreasing strength. Another thirteen samples were randomly selected and withheld as validation samples to test the confidence interval.

The observed strength of the samples is well under the strength in bending for DLP-printed samples previously committed to literature. (Coppola et al., 2022; Zhang et al., 2020). The average strength in bending for samples in this study is about 160 MPa, while published results for DLP-printed samples for 3% mol YSZ have exceeded 350 MPa by Zhang et al. and exceeded 750 MPa by Coppola et al. Beyond humidity control, it is likely that the debindsintering profile suggested by the manufacturer (shown in Table 2) led to poor densification of the material. Both listed studies sintered samples at a higher temperature than that suggested for our slurry by the manufacturer. Future work should control for the humidity during printing and also use the heat treatment parameters that



FIGURE 5

The results of the GPM shown inside the range of non-constant output. The color surface represents the predicted strength in bending value. The x-axis represents humidity and the y-axis represents days since synthesis. The grey surfaces represent the upper and lower 95% confidence bounds. The black dots are measured experimental values.



led to optimum performance in published studies instead of slurry supplier recommendations.

3.2 Digital twin

The use of the term "twin" in digital twin implies the that there is another entity to which the digital system is coupled. Each digital twin should have a corresponding physical twin or process twin. Digital twins are digital representations of the state of a physical system, but also "designed around a twoway flow of information that occurs when object sensors provide relevant data to the system processor and then happens again when insights created by the processor are shared back with the original source object." (IBM, 2021) AMMONOID, in this study, becomes a digital twin as it mirrors the features of the materials, geometry, and manufacturing parameters and records characterized data, but also exports control settings from the digital twin to the DLP printer to manufacture the samples according to the design of experiments generated in the digital system. In this study, all the material parameters, printer settings, and preform geometry values are saved such that the experiments could be replicated. The Gaussian model takes in ambient humidity and days since sythesis as inputs and predicts strength in bending as the output.

The use of the AMMONOID digital framework to record and model the experimental work resulted in a knowledge graph of the sample geometry, material properties, settings, post-processes, and experimental results of characterization. The graph also holds the resulting predictive model files that were generated using the GPM. A representation of the digital model is shown in Figure 4.

The digital model functions to store and query the manufacturing data, but also to prepare the manufacturing data for use by the GPM. The digital twin enforces completeness of the input parameters and resultant data, then formats the data as input to the modeling engine. Figure 4 shows nodes colored by their class types from the AMBER ontology (which are all displayed in Figure 2). This graph organization allows the data to be saved in a context outside of any particular study or design of experiment. Future studies that add more data with similar or dissimilar manufacturing parameters, materials, or preform geometry can find their way in the graph. By forced gathering of all manufacturing parameters in the study, future models that focus on parameters beside humidity and days since expiration for YSZ can make use of the data. This framework also creates a clear thread between the particular components of inputs and methods that generated a predictive model and the model itself. Changes to the upstream data can trigger a notification that a component of the model has been altered and that the model needs to be refit. This framework led to a progressive set of models that became more and more refined as new characterization results were added to the platform.

3.3 Outcome of RSM model

Different iterations of the model were trained until the 95% confidence intervals captured 95% of values. The final hyperparameter values are shown in Table 4. A randomized set of 10% of the characterized values was withheld from the model to use as a validation set. Twelve of the thirteen samples fell within the bounds of the 95% confidence interval, for a capture rate of 92%. The only sample to fall outside the interval is the sample with the strength of 90.804 in the 114 days set.

Since the model was trained on both humidity and days since synthesis, the resultant model can be viewed as a 3D response surface, or as a 2D graph with one value held constant. The output of the GPM is shown in Figure 5. The model demonstrates the GPM's ability to return confidence data which narrows in regions where training data is richer.

The 3D model, unsurprisingly, shows a peak in sample performance when both the humidity and the days since synthesis are lowest. Figure 6 shows the 2D cross sections of the surface at various single-value selections of the parameter that demonstrate trends for each variable, and also variability in the model results for different regions of the parameter space. The model demonstrates both a general negative correlation between humidity and strength and days since synthesis and strength. The areas of highest confidence (as represented by the narrowest confidence interval bands) show the decline in strength most strongly.

The outcome of the experimental results, the digital twin, and the RSM show that the use of these research modalities in conjunction provide a unique enabling of advanced manufacturing research for high energy applications. Manufacturing researchers and technicians, in the normal course of sample production, create a searchable knowledge graph of their data for future study. They also are able to create data-driven predictive models of the performance characteristics of the samples they are creating. In summary, creating a digital twin of a DLP system for 3D printing allows for comprehensive exploration and understanding of how resin age affects printing performance and part quality, leading to more efficient and optimized production processes.

Data availability statement

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

Author contributions

BH: Conceptualization, Data curation, Funding acquisition, Methodology, Project administration, Software, Visualization, Writing-original draft, Writing-review and editing. DP: Conceptualization, Methodology, Writing-original draft, Writing-review and editing. AM: Data curation, Formal Analysis, Methodology, Writing-review and editing. JS: Data curation, Software, Writing-review and editing.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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