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# Multi-objective optimal scheduling considering low-carbon operation of air conditioner load with dynamic carbon emission factors

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As global temperatures rise and climate change becomes more severely. People realize that air conditioning systems as a controllable resource and play an increasingly important role in reducing carbon emissions. In the past, the operation optimization of air conditioning systems was mainly oriented to user comfort and electricity costs ignoring the long-term impact on the environment. This article aims to establish a multi-objective model of airconditioning load to ensure user temperature comfort performance and reduce the total cost (i.e., electricity cost and carbon emission cost) simultaneously. Multi Sand Cat Swarm Optimization (MSCSO) algorithm combined with gray target decision-making (GTD) is used to explore optimal solution. Meanwhile four competitive strategies are applied to validate the effectiveness of the proposed method, i.e., genetic algorithm (GA), MSCSOcomfort objective, MSCSO-total electricity cost objective and unoptimization. The simulation results show that the MSCSO-GTD based objective method can significantly reduce total costs while taking into account appropriate indoor temperature comfort.

#### KEYWORDS

low-carbon operation, economic scheduling, air conditioning system, multiobjective optimization, dynamic carbon emission factor

## **1** Introduction

With increasing societal attention to energy sustainability (Wang et al., 2022) and global warming (Wiriyasart and Kaewluan, 2024), experts in the power systems field are continuously exploring new methods to reduce carbon emissions and steer the power systems towards a more sustainable direction (Hu and Yi, 2023). The building industry accounts for approximately 40% of the global electricity consumption with air conditioning constituting over 50% of the total energy consumption within buildings (Wijaya et al., 2022; Silva et al., 2023). According to statistics, there are currently 1.2 billion air conditioners in daily use globally and this number is expected to rise to 4.5 billion by 2050 (Fikiin, 2018). Against the backdrop of the carbon neutrality goals outlined in the Paris Agreement (Reyseliani et al., 2022). Meanwhile the government and related enterprise focusing on carbon emission reduction, and cost accounting for carbon emissions is the necessary

premise of carbon reduction and objects which should further attention (Hu et al., 2022). Air conditioning systems as a significant burden on the power system, not only directly impact the stability and efficiency of the power system but also have profound implications for the environmental carbon emission levels (Yang ZX. et al., 2022).

Currently, research on carbon emissions in the power sector has become one of the hot topics in the field of power systems. Past studies primarily focused on assessing and reducing the carbon footprint of the overall power system (Shi et al., 2023). However, current optimization scheduling of air conditioning systems often emphasizes improving user comfort (Hernández et al., 2022) and reducing electricity costs with relatively less attention given to their contribution to carbon emission reduction as referenced (Jung and Jazizadeh, 2019; Huang et al., 2022). Air conditioning systems have significant potential to reduce the cost of carbon source energy and lower overall energy costs. Additionally the aggregation and coordinated control of air conditioning systems not only quickly alleviate peak load pressures on the power grid (Xie et al., 2022) but also provide various load transfer and adjustment assistance methods, contributing to the stable and efficient operation of the grid (Dong et al., 2023). Against the backdrop of the "dual carbon goals" aiming to reduce carbon emissions in the power system while ensuring its efficiency. It is necessary to reexamine the strategies for controlling the operation of air conditioning systems.

Li et al. (2021) proposed a single-objective optimization method during air conditioning usage, which combined weighted user comfort and energy consumption to minimize overall consumption. This approach provides a comprehensive assessment of air conditioning usage. In WuCao et al. (2023), a personal comfort model was established to optimize and control air conditioners. This model optimizes air conditioning operation based on electricity prices, outdoor temperatures, and user preferences, significantly reducing electricity costs while effectively maintaining user comfort. Satisfactory decision results are achieved using a multi-objective air conditioning optimization method based on user comfort and energy consumption. Bingham et al. (2017), Ohta and Sato (2018), Elnour et al. (202) employed a neural network-based model to control building air conditioning systems reducing energy consumption by up to 46% without compromising indoor comfort and air quality, providing valuable insights for reducing energy costs in air conditioning systems. Hu et al. (2019) explored air conditioning frequency control in response to smart grids building upon real-time dynamic electricity prices, endowing air conditioning with price responsiveness and grid interactivity. Lin et al. (2022) presented a multi-objective optimization model based on air conditioning energy consumption and thermal comfort, yielding well-balanced decision results.

Kuo et al. (2017) developed a low-carbon and economic dispatch planing for isolated power systems, which offers a significant tool for this field. Utilizing dynamic approaches for carbon assessment, the study captures the characteristics of the electricity grid's generation mix (Khan et al., 2018). When air conditioner operates as a controllable load, a dual-layer economic scheduling model is introduced, emphasizing source-load coordination for carbon reduction (Zh et al., 2023). In the field of low-carbon behavior modeling, relevant theoretical models have been established. These models utilize generic algorithms such as GA and particle swarm optimization (PSO) to maximize profits for all stakeholders and minimize carbon emissions (Yang et al., 2023). Additionally, to optimize the parameters of low-carbon models, metaheuristic algorithms are employed including genetic algorithms, particle swarm optimization and so on. Ding (2023) exhibited a certain advantage in optimizing the parameters of low-carbon models during to the simplicity and lower computational costs of these methods.

This study aims to investigate an innovative operational control strategy for air conditioner focusing on the key performance indicator of minimizing carbon emission costs. The proposed approach introduces a multi-objective optimization scheduling method that relies on dynamic carbon emission factors while considering collaborative operations with air conditioning vendors. The primary contributions/nolvelties of this methodology are outlined as follows:

- Different to fixed carbon emission factor, the dynamic carbon emission factor is introducted to accurately and fairly evaluate the carbon emmission of air conditioners in hour-level. It offers an effective guidance for low-carbon and low-cost operation of air conditioner loads;
- ➤ Unique to single objective optimization, the total cost (including electric cost and carbon emission cost) and users' comfort are intergrated as a multiple objectives to guide th optimal operations of air conditioners;
- ➤The proposed MSCSO algorithm in combination with the Grey Target Decision, aims to obtain the optimal weighted balanced solution. By considering both indoor temperature comfort and the reduction of total electricity costs, it seeks to find a solution that achieves the best balance between these objectives, thereby maximizing overall efficiency and benefits.

The remaining sections of this paper are organized as follows: Section 2 presents the modelling of air conditioning operational characteristics and optimization objectives. Section 3 introduces the workflow of the MSCSO algorithm combined with the Grey Target Decision algorithm. Section 4 provides case simulations for the optimization of the operation of four air conditioners. Finally, Section 5 offers a summary of this paper.

### 2 Air conditioner operation characteristics and optimization objective modeling

# 2.1 Characteristics related to air conditioning operation

Yang et al. (2022b) shows that air conditioning operation is actually a dynamic process. If continuous operating characteristics cannot be maintained, it will affect the user's comfort experience (Lu et al., 2023) and increase energy consumption costs (Yuan et al., 2023). During the air conditioning operation control process, the direct load of the air conditioner Direct Load Control (DLC) (Alrasheedi et al., 2024) is a strategy used to manage and balance loads in power systems. It involves adjusting the load of the power system by proactively intervening in the



operation of air conditioning equipment to respond to changes in system demand or to optimize system operation.

In air-conditioning direct load control, it is achieved in the following two ways:

- > Heating mode: When the indoor real-time temperature is lower than the lower limit temperature, the air conditioner turns on the heating mode. The indoor temperature gradually increases until it reaches the upper limit temperature and the air conditioner stops working; until the indoor temperature drops to the lower limit temperature again, the air conditioner turns on the heating mode again and then the cycle repeats.
- Cooling mode: When the indoor real-time temperature is higher than the upper limit temperature, the air conditioner turns on the cooling mode. The indoor temperature gradually decreases until it reaches the lower limit temperature and the air conditioner stops working; until the indoor temperature rises to the upper limit temperature again, the air conditioner turns on the cooling mode again. And then the cycle repeats.

In the paper, the background of the simulation of air conditioning load optimization operation is based on summer. So only the cooling mode needs to be considered, its working state is shown in Figure 1.

# 2.2 Real-time calculation of indoor temperature

The operating status of the air conditioner can be adjusted through changes in indoor temperature in the process of direct load control of air conditioners. The real-time indoor temperature is mainly related to the outdoor temperature, room thermal parameters, air conditioning load operating status and rated power, which can be described by Eq. 1 as follows:

$$T_{\rm in}(t+1) = \begin{cases} T_{\rm out}(t+1) - (T_{\rm out}(t+1) - T_{\rm in}(t))e^{\frac{-M}{R_{\rm re}C_{\rm re}}} & S_{\rm op}(t) = 0\\ T_{\rm out}(t+1) - (T_{\rm out}(t+1) - T_{\rm in}(t) - R_{\rm re}P_{\rm e}\eta_{\rm cop})e^{\frac{-M}{R_{\rm re}C_{\rm re}}} S_{\rm op}(t) = 1 \end{cases}$$
(1)

where  $T_{in}(t)$  is the indoor temperature in the *t*th period;  $T_{out}(t + 1)$  represents the outdoor temperature in the (t + 1) th period;  $R_{re}(\Omega)$ 

and  $C_{\rm re}$  (F) are the indoor equivalent of thermal resistance and heat capacity, respectively;  $\Delta t$  (h) represents the duration of opening or closing;  $P_{\rm e}$  (kW) and  $\eta_{\rm cop}$  represent the rated power of the air conditioner load and coefficient of refrigeration efficiency respectively;  $s_{\rm op}(t)$  denotes the operational state of the air conditioning load during the t-th time interval;  $s_{\rm op}(t) = 0$  and  $s_{\rm op}(t) = 1$  represent the standby and operational states, respectively.

# 2.2.1 Determining the operating state of the air conditioning load

Although the operating status of the air conditioner and the start-stop status are not equivalent. The operating status of the air-conditioning load at the next moment can be determined through the indoor temperature and start-stop status at that moment. The determination method is described by Eq. 2 as follows:

$$S_{\rm op}(t+1) = \begin{cases} 0 \ S_{\rm turn}(t+1) = 0 \ or T_{\rm in}(t) < T_{\rm min} \\ 1 \ S_{\rm turn}(t) = 0 \ and S_{\rm turn}(t+1) = 1 \ and T_{\rm in}(t) \ge T_{\rm max} \\ S_{\rm op}(t) \ S_{\rm turn}(t) = 1 \ and S_{\rm turn}(t+1) = 1 \ and T_{\rm min} \le T_{\rm in}(t) \le T_{\rm max} \\ 1 \ S_{\rm turn}(t) = 1 \ and S_{\rm turn}(t+1) = 1 \ and T_{\rm in}(t) \ge T_{\rm max} \end{cases}$$
(2)

where  $s_{turn}(t)$  represents the on/off state of the air conditioning load during the *t*th time interval where  $s_{turn}(t) = 0$  and  $s_{turn}(t) = 1$  indicate the states of being turned off and turned on, respectively. Similarly.

According to the condition  $s_{op}(t + 1) = 1$  in Eq. 2, it indicates that the air conditioning load is in the operational state in the next time step. Combining this with the condition in For Eq. 1 that the air conditioning load is in the turned-on state, we can calculate the duration of the air conditioning system's operation when it is in the operational state, which can be expressed by Eq. 3:

$$\tau_{\rm on} = R_{\rm re} C_{\rm re} \ln \frac{T_{\rm max} - T_{\rm out} (t+1) + R_{\rm re} P_{\rm e} \eta_{\rm cop}}{T_{\rm out} (t+1) - T_{\rm min} + R_{\rm re} P_{\rm e} \eta_{\rm cop}}$$
(3)

where  $\tau_{on}$  represents the working time when the air conditioning system is in working state.

#### 2.2.2 Dynamic carbon emission factor

Currently in China, there are challenges associated with the average carbon emission factors for electricity including delayed data updates and difficulties in reflecting temporal and spatial variations, it has not been updated since 2012 and has lost its timeliness taking the example of the regional grid's average carbon emission factor. Moreover, its broad coverage makes it challenging to adequately consider the development disparities and temporal characteristics of non-fossil energy generation especially new energy sources in different regions.

The existing values represent fixed annual figures lacking the capability to address dynamic issues. In this paper, we propose a dynamic carbon emission factor that utilizes a spatiotemporal data model for the power grid. This approach enables the coupling and correlation analysis of electricity and carbon emissions within the grid. By leveraging real-time grid dynamic flow data, the dynamic carbon emission factor can be calculated on an hourly and minuteby-minute basis allowing for dynamic assessments of carbon emissions across different time periods and regions. This methodology is more conducive to accurate carbon emission cost calculations and the equitable distribution of carbon emission



responsibilities. The dynamic carbon emission factor can be predicted and released to users in advance. Users adjust their electricity consumption behavior on an hourly basis. After perceiving the differences in carbon emission factors for electricity consumption in different time periods in the future, users, within the range allowed by their own adjustment capabilities, respond with the goal of maximizing their carbon reduction, aiming to minimize their carbon footprint.

According to the principle of carbon emission flow transmission in the power grid, the schematic diagram is shown in Figure 2. For each node, according to the proportional sharing principle, considering the active power input externally, the average converted carbon emission intensity of the injected node is defined as the carbon emission factor intensity. The carbon emission intensity of node branch power and node access load (Si et al., 2023), which can be expressed by Eq. 4:

$$\delta_{i} = \frac{P_{g} \times \delta_{g} + \sum_{j \in \phi_{i}} P_{ji} \times \delta_{j}}{P_{g} + \sum_{j \in \phi_{i}} P_{ji}}$$
(4)

where  $\delta_i$  (kgCO<sub>2</sub>/kWh) and  $\delta_j$  (kgCO<sub>2</sub>/kWh) represent the power carbon emission factors of the *i*th and *j*th load nodes respectively,  $P_g$  (kW) represents the active power output of the power plant,  $\delta_g$  (kgCO<sub>2</sub>/kWh) connected to the *g*th load node are the power carbon emission factors of the connected power plants,  $P_{ji}$  (kW) represents the power carbon emission factors from active power is injected into the branch from the *j*th node to the *i*th node,  $\phi_i$ represents the set of connected nodes of the branch from the *i*th node.

### 2.3 Optimization target modeling

This section models the carbon emission flow calculation model as the foundation. Under the premise of satisfying constraints on user air conditioning cluster switch states and switch durations, economic costs for users are fully taken into account. At the same time, the section aims to maximize user comfort and minimize carbon emission costs. Therefore building upon the carbon emission flow, this section formulates a multi-objective model for low-carbon operation of air conditioning loads. The objective function of the model considering user comfort and reducing the overall electricity cost that including carbon emission costs is expressed by Eq. 5: where Eq. 6 represents the associated constraints of Eq. 5.

$$\begin{cases} \min f_{1} = \sum_{n=1}^{N} \sum_{t=1}^{H} \omega_{n}(t) \times \sqrt{\left[T_{n}^{\operatorname{avg}}(t) - T_{n}^{\operatorname{set}}(t)\right]^{2}} \\ \min f_{2} = \sum_{n=1}^{N} \sum_{t=1}^{H} s_{\operatorname{op},n}(t) \times \tau_{\operatorname{on},n} \times P_{n} \times \left[\psi_{e}(t) + \psi_{c}(t) \times \sigma_{n}(t)\right] \end{cases}$$
(5)

$$\begin{cases} s_{op,n}(t) = 1 \\ n = 1, 2, \dots, N \\ t = 1, 2, \dots, H \\ N = 4 \\ H = 24 \end{cases}$$
(6)

where  $f_1$  represents the user temperature comfort deviation function;  $f_2$  represents the comprehensive electricity cost function of electricity cost and carbon emissions; N is the number of air conditioner;  $\omega_n(t)$  is the indoor temperature demand weight of the *n*th user in the *t*th period;  $T_n^{avg}(t)$  (°C) and  $T_n^{set}(t)$  (°C) are the average indoor temperature and preset indoor temperature of the *n*th air conditioner in the *t*th period respectively;  $s_{op,n}(t)$  is the working status of the *n*th user in the *t*th period, when the value is 1, the air conditioner is working,  $\tau_{on,n}(h)$  represents the duration of the *n*th user's air conditioning load; *H* (h) represents the number of hours in a day;  $\sigma_n(t)$  (kgCO<sub>2</sub>/kWh) is the carbon emission factor for the *n*th user in the *t*th time period;  $\psi_e(t)$  (CNY/kWh) and  $\psi_c(t)$  (CNY/kgCO<sub>2</sub>) represent the electricity price and carbon emission price for the *t*th time, respectively.

# 3 MSCSO algorithm combined with gray target decision-making algorithm

### 3.1 Basic principles of MSCSO algorithm

The MSCSO algorithm is an intelligent optimization algorithm that imitates the foraging behavior of sand cats in nature. This algorithm simulates the two stages of sand cat foraging behavior: searching for prey and attacking prey (Seyyedabbasi and Kiani, 2023).

#### 3.1.1 Initialization

In a D-dimensional problem, a sand cat represents a  $1 \times D$  matrix, where each sand cat corresponds to a solution to the problem. The sand cat population matrix  $Cat_i = [x_1, x_2, ..., x_D]$ , i = pop(1, 2..., N)where *pop* represents the population size and N is the maximum population size. During the operation of the MSCSO algorithm based on the size of the problem  $(N_{pop} \times N_D)$ . The sand cat population



matrix  $Cat_i = [x_1, x_2, ..., x_D]$  is initialized. The specific form of the initialization matrix is expressed by Eq. 7:

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$$Cat_{i} = \begin{bmatrix} X_{1} \\ \vdots \\ X_{i} \\ \vdots \\ X_{N} \end{bmatrix}_{N \times D} = \begin{bmatrix} x_{11} & x_{1j} & x_{1D} \\ \vdots & \vdots & \vdots \\ x_{1j} & x_{ij} & x_{iD} \\ \vdots & \vdots & \vdots \\ x_{1j} & x_{nj} & x_{ND} \end{bmatrix}_{N \times D}$$
(7)

where  $X_i$  represents the *i*th sand cat group;  $x_{ij}$  represents the dimension of the *i*th population in the sand cat population.

The fitness function of the sand cat population is  $F = f(Cat_i) = f(x_1, x_2, ..., x_D)$ , and the specific matrix form is expressed by Eq. 8:

$$F = \begin{bmatrix} F_{1} \\ \cdot \\ F_{i} \\ \cdot \\ F_{N} \end{bmatrix}_{N \times 1} = \begin{bmatrix} f(x_{11}, x_{12}, \dots, x_{1D}) \\ \cdot \\ f(x_{i1}, x_{i2}, \dots, x_{iD}) \\ \cdot \\ f(x_{n1}, x_{n2}, \dots, x_{nD}) \end{bmatrix}_{N \times 1}$$
(8)

#### 3.1.2 Searching for prey stage

In the stage of searching for prey, the sand cat's hearing can explore the location of the prey by perceiving hearing within 2 kHz.

In the mathematical model, According to the working principle of the algorithm the process of gradually decreasing linearly from 2 to 0 after iteration is simulated and represents this process using sensitive Factors  $\xrightarrow{\bullet}$  The mathematical form is expressed by Eq. 9:

$$\underset{s_c}{\longrightarrow} = s_b - \frac{2 \times s_b \times K_P}{K_{\text{max}}} \tag{9}$$

where  $s_b$  represents the maximum hearing limit of the simulated sand cat which is set to 2;  $K_P$  represents the current number of iterations;  $K_{\text{max}}$  represents the maximum number of iterations.

During the search process in order to ensure that the search space falls into a local optimum, this search process requires position updating based on random position changes during the search process. This behavior can be defined by the different sensitivity ranges of each sand cat using Eq. 10:

$$\underset{s_{a}}{\longrightarrow} = \underset{s_{c}}{\longrightarrow} \times rand(0,1) \tag{10}$$

The parameter variable that realizes the transformation of searching for prey and attacking prey is expressed as  $\overrightarrow{s}$ . This parameter variable can balance the transformation of the two stages and is expressed by Eq. 11:

$$\overrightarrow{s} = \left| 2 \times \overrightarrow{s_a} - \overrightarrow{s_c} \right| \tag{11}$$

When searching for prey position in the algorithm, the sand cat can iterate its position based on the current position, sensitivity range and optimal solution which can be expressed by Eq. 12:

Air conditioner	No.	<i>R<sub>ac</sub></i> (℃/kW)	C <sub>ac</sub> (kWh/°C)	N <sub>ac</sub>	P <sub>ac</sub> (kW)	Working hours
Air conditioner number	1	5.47	0.14	2.1	4.0	09:00-18:00
	2	5.51	0.17	1.2	2.3	09:00-18:00
	3	6.20	0.16	1.8	3.5	00:00-08:00, 18:00-24:00
	4	5.73	0.21	1.5	2.7	00:00-08:00, 18:00-24:00

#### TABLE 1 Air conditioning related parameters

TABLE 2 Electricity prices and carbon prices at each moment within 24-h.

Time (hour)	1	2	3	4	5	6	7	8	9	10	11	12
Electricity prices (CNY/kWh)	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.5	0.7	0.7	0.7	0.5
Dynamic CEFs (kgCO <sub>2</sub> /kWh)	0.75	0.75	0.8	0.8	0.7	0.7	0.65	0.5	0.45	0.4	0.35	0.3
Time (hour)	13	14	15	16	17	18	19	20	21	22	23	24
Electricity prices (CNY/kWh)	0.5	0.5	0.5	0.7	0.7	0.7	0.7	0.9	0.9	0.9	0.5	0.3
Dynamic CEFs (kgCO <sub>2</sub> /kWh)	0.25	0.2	0.25	0.3	0.4	0.5	0.6	0.7	0.7	0.75	0.75	0.8

The meaning of the bold values represent from 13:00 to 24:00.

$$\overrightarrow{X}(t+1) = \overrightarrow{s_a} \cdot \left( \overrightarrow{L_b} - \operatorname{rand}(0,1) \cdot \overrightarrow{L_c} \right)$$
(12)

where  $\xrightarrow{s_a}$  represents the sensitivity range;  $\xrightarrow{L_b}$  represents the optimal solution;  $\xrightarrow{T}$  represents the current position.

#### 3.1.3 Attacking prey stage

During the process of attacking prey, the sand cat uses a 360degree range around its current position as a rotation angle. This involves randomly selecting an angle for the attack, ensuring both the avoidance of getting stuck in local optima and a more accurate emulation of the sand cat's hunting behavior by Eqs 13, 14.

$$\overrightarrow{L_r} = |rand(0,1) \cdot \overrightarrow{L_b} - \overrightarrow{L_c}|$$
(13)

$$\overrightarrow{X}(t+1) = \overrightarrow{L_{b}} - \overrightarrow{s_{a}} \cdot \overrightarrow{L_{r}} \cdot \cos(\theta) \quad \theta \in (0, 360^{\circ})$$
(14)

where  $\overrightarrow{L_r}$  represents the random position updated by the sand cat;  $\theta$  represents the search angle.

# 3.1.4 Transformation into exploring and attacking prey stages

The parameter variables that realize the conversion of searching for prey and attacking prey are expressed as  $\frac{1}{s}$ ,  $|\frac{1}{s}| > 1$  means exploring prey,  $|\frac{1}{s}| \le 1$  means attacking prey which progress can be expressed by Eq. 15.

$$\overrightarrow{X}(t+1) = \begin{cases} \overrightarrow{s_a} \cdot \left( \overrightarrow{L_b} - \operatorname{rand}(0, 1) \cdot \overrightarrow{L_c} \right) | \overrightarrow{s} | > 1 \\ \overrightarrow{L_b} - \overrightarrow{s_a} \cdot \overrightarrow{L_r} \cdot \cos(\theta) | \overrightarrow{s} | \le 1 \end{cases}$$
(15)

# 3.2 Basic principles of gray target decision-making

By employing the MSCSO algorithm for two objectives and obtaining numerous solutions based on diverse requirements, this paper adopts an approach that combines Grey Target Decision to derive the optimal decision solution.

The Grey Target Decision method is primarily based on considering multiple scenarios and objectives. Essentially, the grey target represents the region of satisfactory outcomes, with a designated target center in a sequence set. The proximity to the target center reflects the superiority of the outcome, where closer distances indicate better performance. The core concept revolves around identifying data in a set of sequences that is closest to the target value, forming a reference sequence. Subsequently, a grey target is constructed using this reference sequence with the reference sequence as the target center. The distance between each data sequence in the information space and the target center is referred to as the target center distance and the solutions are ranked based on the magnitude of these distances.

#### 3.2.1 Establishing sample matrix

For the MSCSO algorithm targeting two objectives from the set of numerous solutions obtained based on different requirements: msolutions can be obtained; each solution contains n objectives. Within the *i*th solution, the *j*th objective value is designated as an element of a newly created sample matrix denoted as  $x_i(j)$  (i = 1, 2, ..., m; j = 1, 2, ..., n). The sample matrix is denoted as  $X = [x_i(j)]_{m \times n}$ , the specific solution method is using with Eqs 16, 17, as follows

$$X = [x_i(j)]_{m \times n} = X_{\min} + \frac{x_i(j) - x(j)_{\min}}{x(j)_{\max} - x(j)_{\min}} (X_{\max} - X_{\min}) \quad (16)$$

$$\boldsymbol{X} = [x_i(j)]_{m \times n} = \begin{bmatrix} x_1(1) & x_1(2) & \dots & x_m(n) \\ x_2(1) & x_2(2) & \dots & x_m(n) \\ \dots & \dots & \dots & \dots \\ x_m(1) & x_m(2) & \dots & x_m(n) \end{bmatrix}_{m \times n}$$
(17)

where  $X_{\text{max}}$ ,  $X_{\text{min}}$  represent the maximum and minimum values of the normalized fitness function;  $x(j)_{\text{max}}$ ,  $x(j)_{\text{min}}$  represent the maximum and minimum target values of the *j*th non-dominated solution; *X* is a sample matrix containing the normalized fitness values of all solutions.



(A) Hourly electricity prices and carbon prices; (B) Hourly ideal indoor and outdoor temperature.



### 3.2.2 Determine the target center

Select the target value as a cost indicator, that is expressed by Eq. 18.

$$y_{i}(j) = \frac{w(j) - x_{i}(j)}{\max\left\{\max_{1 \le i \le m} x_{i}(j) - w(j), w(j) - \min_{1 \le i \le m} x_{i}(j)\right\}}$$
(18)

where w(j) expressed as the average value of each column of the sample matrix by Eq. 19

$$w(j) = \frac{\sum_{i=1}^{m} x_i(j)}{m} \tag{19}$$

Based on this, the decision matrix is defined as  $Y = y_i(j)$  (i = 1, 2, ..., m; j = 1, 2, ..., n). The maximum value in

each column represents an element of the target center vector. Thus the target center vector can be obtained by Eq. 20 as follows:

$$y_o = \{y(1)_{\max}, \dots, y(j)_{\max}, \dots, y(n)_{\max}\}$$
 (20)

where  $y(j)_{max}$  represents the maximum value of the *j*th objective function.

### 3.2.3 Find the best decision

The method of minimum center distance is used to determine the optimal solution of the target value (Liu et al., 2022) by Eq. 21.

$$d_{i} = |y_{i} - y_{o}| = \sum_{i=1}^{n} w(j) |y_{i}(j) - y_{o}|$$
(21)



FIGURE 6 Indoor temperature changes of different air conditioners under different strategies. (A) air conditioner 1; (B) air conditioner 2; (C) air conditioner 3; (D) air conditioner 4.



(A) Variation chart of different air conditioning comfort indexes under different strategies. (B) Change chart of total cost of electricity under different strategies.



Figure 3 shows the chart flow of the MSCSO algorithm combined with gray target decision-making. where  $d_i$  represents the minimum center distance which helps us explore the optimal solution.

# 3.3 MSCSO algorithm combined with gray target decision-making flow chart

MSCSO algorithm

## 4 Case studies

During the simulation optimization process, the relevant parameters of the air conditioner are set as shown in Table 1. The hourly electricity price and carbon price are designed for 24 h a day as shown in Table 2, (Zhang et al., 2023). Dynamic carbon emission factor exhibit a trend of being low during the day and high during the night clean and renewable energies are considered such as solar power generation. During the day, the proportion of renewable energy generation is larger resulting in a small electric carbon factor. On the contrary when solar resources disappear at night, the system becomes more reliant on traditional power supply primarily provided by fossil fuel-based power generation equipment such as coal-fired power plants the proportion of renewable energy generation is relatively low at night and the carbon emission factor is large in Figure 4A.

The ideal indoor temperature and actual outdoor temperature are also set as shown in Figure 4B. The maximum number of iterations and the number of populations of all algorithms are exactly the same, the maximum number of iterations  $K_{\text{max}} = 500$  and the number of populations Pop = 200. Figure 5A shows simulation of the air conditioner operating State. There are two dimensions in Pareto fronts in Figure 5B. It shows the MSCSO-GTD strategy's trade-off ability in multi-objective solution sets.

Figure 5A shows simulation of the air conditioner operating State. There are two dimensions in Pareto fronts in Figure 5B. It shows the MSCSO-GTD strategy's trade-off ability in multi-objective solution sets. In Figure 5B, the solutions obtained from MSCSO- $f_1$  are close to the minimum value on the comfort index axis, while the values on the total cost axis are the highest. This indicates that this decision method places special emphasis on the weight of comfort, diminishing the impact of total cost. Similarly, the solutions obtained from MSCSO- $f_2$  are close to the minimum value on the total cost axis, while the values on the comfort index axis are the highest. This suggests that this

decision method prioritizes the weight of total cost, mitigating the influence of comfort. It is worth noting that the solutions without optimization and those obtained from MSCSO- $f_1$  are similar indicating that under regular default conditions, the system automatically tends to prioritize user comfort neglecting the impact of total cost. This study provides insights into balancing these two aspects. Compared to the GA algorithm, MSCSO-GTD- $f_1$ ,  $f_2$  achieves a more balanced consideration of user comfort and total cost issues, aligning well with the optimal expectations of users and society regarding air conditioning usage.

The indoor temperature variations of different air conditioners under different strategies are shown in Figure 6. For air conditioners 1 and 2 during the working hours from 9:00 to 18:00, MSCSO-GTD $f_1, f_2$  strategy results in the indoor average temperature being very close to the set ideal temperature compared to other strategies. Similarly, for air conditioners 3 and 4, during the working hours from 00:00 to 08:00 and 18:00 to 24:00. MSCSO-GTD- $f_1, f_2$  strategy also leads to the indoor average temperature being very close to the set ideal temperature with a temperature deviation within 2.5°C in Figure 5B. This indicates that MSCSO-GTD- $f_1, f_2$  can significantly meet the requirements in terms of user comfort.

As illustrated in Figure 7A showing the changes in comfort index for different air conditioners under different strategies. Figure 7B displays the variations in total power cost under different strategies, confirming that MSCSO-GTD- $f_1$ ,  $f_2$  compared to other strategies. It exhibits a certain advantage in power cost savings. Particularly compared to the unoptimized and MSCSO- $f_1$  strategies, power costs can be saved by approximately 16%–30%.

Figure 8 depicts the cost and comfort index under different strategies. The trends exhibited by the four air conditioners under different strategy optimizations are generally similar. It can be observed that without optimization, both carbon emission costs and electricity costs are high which contradicts the low-carbon concept. MSCSO-f<sub>1</sub>, MSCSO-f<sub>2</sub> demonstrate significant advantages in their respective optimized indicators. However they cannot achieve a balanced decision in terms of the other corresponding indicator. In the context of the low-carbon operation of the air conditioners studied in this paper, a crucial aspect is reducing carbon emission costs. MSCSO-f1 and MSCSO-f2 show significant disadvantages in reducing carbon emission costs. In comparison, MSCSO-GTD-f1, f2 exhibits an advantage in carbon emission cost savings of approximately 75%-90% compared to these two single-objective decision methods. This aligns with the objective of the low-carbon operation research conducted in this paper. Compared to GA, MSCSO-GTD-f<sub>1</sub>, f<sub>2</sub> holds an advantage in both carbon emission costs and electricity costs, resulting in an overall cost savings of around 10%. Particularly, it demonstrates a significant potential of MSCSO-GTD-f1, f2 for carbon reduction in the aspect of carbon emission costs. Meanwhile the comfort index for users can still maintain a satisfactory level. MSCSO-GTD algorithm is excellent in global and local search, and can effectively maintain the balance between global and local search performance. This advantage is shown in this paper as follows: Compared with unoptimized and genetic algorithms, MSCSO-GTD has the lowest carbon emission cost, and the obtained solution can also well meet the user comfort and total cost optimization, which reflects the huge advantages of the algorithm in maintaining the balance between global and local search performance, and the algorithm has fast convergence speed and accuracy.

# 5 Conclusion

This paper considers the multi-objective decision-making problem of low-carbon operation of air-conditioning load. How to better achieve the decision-making balance problem for the two goals of user comfort and total electricity cost on the basis of being as low -carbon as possible, using MSCSO-GTD and dynamic electric carbon The research method of combining factors explored the dual-objective balance problem of low-carbon cost measurement, user comfort and total electricity cost. Finally the following conclusions were obtained:

- > The algorithm employed in this paper belongs to heuristic algorithms and has demonstrated excellent optimization results in the context of weak optimization problems presented in this paper. However, when dealing with the output optimization of devices such as generators in a distribution network, more complex constraints, such as start-stop constraints and ramping constraints, need to be considered. In such cases, the algorithm proposed in this paper may not be as applicable.
- Compared to the single-objective MSCSO, the proposed dualobjective MSCSO-GTD can overcome the limitations of overlooking other objectives in the single-objective research process. Most importantly, the method proposed for lowcarbon cost control exhibits significant potential;
- Compared with the non-optimized and GA algorithm, more satisfactory optimization indicators were achieved in the test for the optimized operation of four air conditioners, especially in terms of low-carbon cost control. The respective comparisons were close to 20% and 13% reduction; in the total cost indicators, there are reductions of nearly 33% and 20%, respectively;
- ➤ Compared with the electricity price, the carbon unit price is lower; the electricity price plays a dominant role in the algorithmic equilibrium decision-making process in many cases, resulting in sometimes unsatisfactory optimization results guided by the carbon price. A higher carbon unit price may achieve a more effective low-carbon economy, carbon runs the guiding role. With the continuous increase in the proportion of new energy installations and the establishment of a more robust carbon trading market in the electricity system, enhanced price incentives, and more standardized carbon trading, the low points in both electricity user net loads and dynamic carbon emission factors may overlap in the future.

# Data availability statement

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding author.

# Author contributions

XS: Writing-original draft, Writing-review and editing. JL: Writing-review and editing. YY: Writing-review and editing. JT:

Writing-original draft. BQ: Writing-review and editing. XL: Writing-review and editing. ZW: Writing-review and editing.

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## **Conflict of interest**

Authors XS, JL, and YY were employed by Yunnan Power Grid Co., Ltd. Authors JT, BQ, XL, and ZW were employed by Electric Power Research Institute of CSG.

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