



## A Holistic Modeling Approach to **Project the Evolution of Inlet-Interrupted Coastlines Over the** 21<sup>st</sup> Century

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Approximately one-guarter of the World's sandy beaches, most of which are interrupted by tidal inlets, are eroding. Understanding the long-term (50–100 year) evolution of inletinterrupted coasts in a changing climate is, therefore of great importance for coastal zone planners and managers. This study, therefore, focuses on the development and piloting of an innovative model that can simulate the climate-change driven evolution of inlet-interrupted coasts at 50-100 year time scales, while taking into account the contributions from catchment-estuary-coastal systems in a holistic manner. In this new model, the evolution of inlet-interrupted coasts is determined by: (1) computing the variation of total sediment volume exchange between the inlet-estuary system and its adjacent coast, and (2) distributing the computed sediment volume along the inlet-interrupted coast as a spatially and temporally varying quantity. The exchange volume, as computed here, consists of three major components: variation in fluvial sediment supply, basin (or estuarine) infilling due to the sea-level rise-induced increase in accommodation space, and estuarine sediment volume change due to variations in river discharge. To pilot the model, it is here applied to three different catchmentestuary-coastal systems: the Alsea estuary (Oregon, United States), Dyfi estuary (Wales, United Kigdom), and Kalutara inlet (Sri Lanka). Results indicate that all three systems will experience sediment deficits by 2100 (i.e., sediment importing estuaries). However, processes and system characteristics governing the total sediment exchange volume, and thus coastline change, vary markedly among the systems due to differences in geomorphic settings and projected climatic conditions. These results underline the importance of accounting for the different governing processes when assessing the future evolution of inlet-interrupted coastlines.

Keywords: anthropogenic activities, climate change, coastline change, numerical modeling, tidal inlets

## INTRODUCTION

Open sandy coasts are complex coastal systems that are continually changing under the influence of both natural and anthropogenic drivers (Stive, 2004; Ranasinghe et al., 2013; Ranasinghe, 2016; Anthony et al., 2015; Besset et al., 2019). The majority of the world's sandy coasts are interrupted by inlets (Aubrey and Weishar, 1988; Davis and Fitzgerald, 2003; Woodroffe, 2003; FitzGerald et al., 2015; Duong et al., 2016; McSweeney et al., 2017). Both oceanic and terrestrial processes contribute to the long term (50-100 year) evolution of these inlet-interrupted coasts (Stive et al., 1998; Stive and Wang, 2003; Ranasinghe et al., 2013). Moreover, future changes in temperature and precipitation due to climate change, and anthropogenic activities at catchment scale can alter the fluvial sediment supply to the coast, which in turn will affect the evolution of inletadjacent coastlines. While being spatio-temporally dynamic due to their sensitivity to both oceanic and terrestrial processes, inletinterrupted coasts are also highly utilized, often containing public and private property, roads, bridges, and ports and marinas (McGranahan et al., 2007; Wong et al., 2014; Neumann et al., 2015). Significant changes in coastline position at these systems are therefore likely to lead to severe socio-economic impacts. To avoid such impacts and associated losses, a good understanding, and the ability to reliably predict the long-term evolution of inlet-interrupted coasts is of great importance for coastal zone planners and managers.

The key oceanic processes that may affect inlet-interrupted coasts include mean sea-level change, tides and waves, and longshore sediment transport (Hayes, 1980; Davis and Fox, 1981; Davis and Hayes, 1984; Davis, 1989; Davis and Barnard, 2000, 2003), while the key terrestrial processes that may affect these coasts include river flow, fluvial sediment supply, land use/agricultural patterns, and land management (Cowell et al., 2003; Syvitski et al., 2009; Green, 2013). While the influence of oceanic processes on the evolution of inlet-interrupted coasts is well known and well accepted, the effect that terrestrial processes may have on coastal evolution is less well studied. Nevertheless, there are a number of studies that have investigated the evolution of delta systems while taking into account the changes in fluvial sediment supply (e.g., Ericson et al., 2006; Yang et al., 2006, 2018; Syvitski and Saito, 2007; Syvitski, 2008; Overeem and Syvitski, 2009; Syvitski et al., 2009; Barnard et al., 2012, 2013a,b; Anthony et al., 2013, 2015, 2019; Tessler et al., 2015; Szabo et al., 2016; Dunn et al., 2018, 2019).

Essentially, there are three major components to be considered in the source to sink sediment pathway from the catchment to the coast (**Figure 1**): (1) catchment-scale sediment production fed by weathering and soil erosion, (2) the transition zone characterized by fluvial sedimentation and reworking, and (3) the deposition and redistribution zone dominated by sediment exchange between the estuary and its adjacent coast. The longterm evolution of most inlet-interrupted coastlines is affected by processes that govern the behavior of all these zones making up the complete sediment pathway. However, it should also be noted that some inlet-interrupted coasts (e.g., estuary-inlet systems in the Southeast of the United States) are not affected by the fluvial sediment supply. Such systems are characterized by low fluvial sediment supply and contain small deltas at the heads of estuaries that sequester the coarse sediment delivered by rivers. In such systems, it is not necessary to consider the fluvial sediment delivery aspects to determine the long-term evolution of inlet-interrupted coasts.

Globally, rivers contribute about 95% of the sediment received by the oceans (Syvitski et al., 2003). Generation of this sediment starts in the mountains, where rocks weather into sediment through mechanical, chemical and biological processes (Syvitski and Milliman, 2007). Climate change is expected to result in increased temperatures (Stocker et al., 2013b), which will affect both chemical and mechanical weathering, thus increasing the rate of soil erosion at the catchment scale (Syvitski et al., 2003; Syvitski and Milliman, 2007). Future changes in precipitation will also affect the amount of soil eroded at catchment scale. The rate of sediment generation at catchment scale also depends on anthropogenic activities, such as land clearance for agriculture, urbanization, road construction and de-and reforestation (Syvitski and Milliman, 2007; Syvitski et al., 2009; Overeem et al., 2013). All these climate-change impacts and anthropogenic activities will alter the magnitude of sediment production at catchment scale, which, in turn, will affect the sediment volume received by the coast.

Sediment generated in the catchment is transported to the coast by rivers. Climate-change driven variations in future precipitation will alter the river discharge, thus affecting the throughput of eroded soil material at catchment scale (Syvitski et al., 2003; Kettner et al., 2005; Shrestha et al., 2013). Anthropogenic activities, however, will exert significant influences on the ultimate fluvial sediment supply to the coast. Activities that reduce the fluvial sediment supply capacity include anthropogenic sediment retention by dams, river sand mining, reduction in sedimentation area due to levee/dyke construction, and reduction in river flow due to water withdrawal for irrigation/drinking water supply. On the other hand, activities such as increased surface runoff due to urbanization and deforestation would increase the fluvial sediment loads (Verstraeten and Poesen, 2001; Vörösmarty et al., 2003; Syvitski, 2005; Syvitski and Milliman, 2007; Syvitski and Saito, 2007; Slagel and Griggs, 2008; Syvitski et al., 2009; Walling, 2009; Overeem et al., 2013; Chu, 2014; Ranasinghe et al., 2019). In combination, these anthropogenic activities and climate-change driven impacts can change the total fluvial sediment throughput from the catchment to the coast.

The final segment of the sediment pathway from catchment to the coast is the deposition and redistribution of sediment within the estuary and the adjacent inlet-interrupted coast. The estuarine accommodation volume is affected by both the sediment input from the river and anthropogenic influences within the estuary, such as sand mining, construction of causeways, bridges, and finger canals (Davis and Barnard, 2000; Barnard and Kvitek, 2010; Dallas and Barnard, 2011). Climatechange induced sea-level rise will increase the accommodation space within the estuary. The net sediment volume imported or exported by the estuary is, therefore, a direct function of the relative magnitudes of the sediment demand from the



FIGURE 1 | Schematic representation of the sediment pathway from source to the coast. The three colors used in the figure denote the major components (i.e., zones) related to this sediment pathway: (1) catchment-scale sediment production zone fed by soil erosion (in green), (2) transition zone of sediment throughput (in blue), and (3) deposition and redistribution zone dominated by sediment exchange between the estuary and its adjacent coast (in brown). Two-way arrows in brown denote sediment exchange between the estuary and its adjacent throughput is adjacent inlet-interrupted coast.

increased accommodation space, fluvial sediment supply, and the anthropogenic activities within the estuary. Depending on whether the estuary is a sediment importing or exporting system, the inlet-interrupted coast may, respectively, recede or prograde (Ranasinghe et al., 2013; Ranasinghe, 2016). The spatio-temporal alongshore variation of the coastline recession/progradation is

a function of the relationship between the sediment volume exchange between the estuary and the adjacent coast and wave driven longshore sediment transport capacity in the vicinity of the inlet (Dalrymple, 1992; Dalrymple and Choi, 2003, 2007).

Due to the complex interplay and dependencies between coastline change and catchment, estuarine and coastal processes, any modeling technique that attempts to simulate long-term evolution of inlet interrupted coasts would benefit by considering the holistic behavior of Catchment-Estuary-Coastal (CEC) systems. However, only a limited number of studies to date have considered these systems in a holistic way (e.g., Shennan et al., 2003; Samaras and Koutitas, 2012; Ranasinghe et al., 2013). To investigate the interactions between the subsystems (catchment/fluvial, estuarine, and coastal), a range of modeling approaches are theoretically possible. In one end member, for each subsystem, models representing the relevant processes in as much detail as possible, resolving time and space scales as finely as possible, could be coupled together. Highly detailed models are available for some of the processes in some of the subsystems. For example, models representing flow and sediment transport on time and space scales that allow explicit simulation of hydrodynamics (based directly on approximations to the Navier Stokes equations) could theoretically be employed to represent fluvial, estuarine and coastal morphodynamics. Although the term "process-based" has often been used to describe such highly detailed models currently being used in practice (e.g., Delft3D, Mike21). Since a wide range of modeling approaches are in fact used to simulate physical processes, whether represented on the finest scales practical or on larger scales, here we avoid using the term "process based" and use the more generic term "highly detailed" instead.

There are three obstacles to coupling together an array of highly detailed models in the context of this study. First, processes in the subsystems involve physical, ecological, and human dynamics-and their couplings, but highly detailed models are not available for all of the relevant dynamics and couplings. Second, even when based on state-of-the-art representations of smallscale processes and parameterizations for sub-grid processes, highly detailed models, like all models, are imperfect. Model imperfections can cascade up through the scales when explicitly representing dynamics on scales much smaller than those of interest, especially where long-term simulations are concerned, limiting the quantitative reliability of model results on the scales of interest (Murray, 2007). Finally, limits on computational power make the use of a highly detailed modeling approach to simulate holistic behavior of CEC systems at 50-100 year time scales a daunting task. Therefore, presently available highly detailed modeling approaches are not capable of providing the probabilistic estimates of coastline change via multiple model realizations, which are needed by coastal zone planners/managers for risk-informed decision making (Ranasinghe, 2016, 2020).

To holistically model CEC systems, here we use an approach which represents the aggregated effects that processes occurring on much smaller scales have on the scales of interest, rather than explicitly resolving the interactions between myriad degrees of freedom that can be identified on much smaller scales. This approach embraces the way modeling (conceptual, analytical and numerical) has most often been done in Earthsurface science (Murray, 2013). For example, when simulating interactions on a macroscopic scale, e.g., hydrodynamics, we use parameterizations representing the collective effects at macroscopic scales of interactions between the many degrees of freedom that appear at microscales. For example, the Navier Stokes equations are in a sense parameterizations describing the interactions between macroscopic variables (e.g., pressure, density) that emerge from the collective dynamics at microscales (e.g., molecular dynamics). Thus, the modeling approach adopted here might best be termed "Appropriate Complexity" (French et al., 2016), since it embraces the philosophy of representing processes and interactions at scales commensurate with those of the phenomena of interest to effectively address dynamics at that scale. In this sense, models resolving hydrodynamic and sediment dynamics on fine time and space scales have an appropriate level of complexity for addressing questions across a range of scales, but models that aggregate the effects of those detailed processes to address questions on much larger scales are also appropriate. Compared to more highly detailed models, models in Earth-surface science using a more synthesized (Paola, 2000) or scale-aggregated approach have often been called "Reduced Complexity" models. We recognize that this term has its drawbacks (French et al., 2016), including the fact that all models are "reduced complexity" compared to the natural (or anthropogenic) systems they are representing.

The Scale-aggregated Model for Inlet-interrupted Coasts (SMIC) presented by Ranasinghe et al. (2013) is the first of its kind that treats CEC systems holistically while giving due consideration to the description of physics governing the behavior of the integrated system. Although SMIC provides a platform to probe into CEC systems holistically, its utility to address the long-term evolution of inlet-interrupted coasts under climate change impacts and anthropogenic activities is limited by (a) its applicability to only small tidal inlets, (b) its simplistic method of quantifying the fluvial sediment supply, and (c) the omission of alongshore spatio-temporal variation in coastline change. The present study attempts to address these shortcomings by developing a more generally applicable modeling tool that can simulate the climate-change driven evolution of inlet-interrupted coasts at macro (50-100 year) time scales.

It should be noted that the model developed here is partly data driven, using empirically-based parameterizations representing the behaviors of some component subsystems (e.g., terrestrial sediment yield). Representing the emergent effects of much smaller scale processes with empirically-based parameterizations can potentially be more quantitatively reliable than basing a model explicitly on the smaller scale dynamics (even if computational power were not a limitation), avoiding the possible cascade of model imperfections (Murray, 2007).

It is important to note that inlet-interrupted coasts include both mainland and barrier island coasts. For inlet-interrupted coasts along the mainland, sediment deposition and redistribution processes are closely linked with the type of estuary they are attached to (Ranasinghe et al., 2013; FitzGerald et al., 2014). The scope of this study is restricted to the

long-term evolution of inlet-interrupted coastlines attached to bar-built (barrier) estuaries, which are commonly found along mainland sandy coasts located in wave-dominated, micro-tidal environments. Examples of bar-built estuaries can be seen along the eastern coast of the United States (near mid-latitudes), the Gulf of Mexico, Australia, Brazil, India, and in the regions of Amazon and Nile River (Ranasinghe et al., 1999; Davis and Fitzgerald, 2003; Woodroffe, 2003).

This study concentrates on coastlines interrupted by (a) estuaries with low-lying margins, and (b) small tidal inlets. Estuaries with low-lying margins contain tidal flats and salt marshes along their margins as well as banks with mild slopes. In these systems, increased sea level would lead to a significant increase in surface area of the estuary surrounded by mildly sloping banks, leading to an increase in the tidal prism, and consequently affecting the inlet cross-section area (O'Brien, 1969). On the other hand, small tidal inlets can be considered as a unique subset of barrier estuaries that (generally) have little or no intertidal flats, tidal marshes or ebb-tidal deltas (Duong et al., 2016, 2017, 2018).

### MATERIALS AND METHODS

Part of the future coastline change at tidal inlets will arise from changes in the net volume of sediment exchanged between inletestuary systems and their adjacent coast (Stive et al., 1998; Stive and Wang, 2003), driven by climate change and anthropogenic activities. This exchange sediment volume can be discretized into three main components: (1) basin (or estuary) infilling volume due to the sea level rise-induced increase in accommodation space, (2) basin (or estuary) volume change due to variation in river discharge, and (3) change in net annual fluvial sediment supply (Ranasinghe et al., 2013). Depending on whether the estuary is in sediment importing or exporting mode (relative to the ocean side of the estuary), and the magnitude of the aforementioned three sediment budget components, an inletaffected coastline will experience a certain amount of coastline recession or progradation. In addition, the entire coastal profile is expected to respond to sea-level rise by moving landward and upward (Bruun, 1962); a process now commonly referred to as the Bruun effect. The model developed in this study mainly revolves around the physics-based representation of these processes and the way they interact with each other in driving coastline change.

## Change in Total Sediment Volume Exchange Between a Barrier-Estuary System and Its Inlet-Interrupted Coast

Assuming the system is presently in dynamic equilibrium, the first step in determining the evolution of an inlet-interrupted coastline is to compute the change in the net annual volume of sediment exchanged between the inlet-estuary system and its adjacent coast. This calculation presumes that any given inlet-estuary system would tend toward and eventually reach its natural equilibrium. Hence, any excess amount of sediment would be exported to its adjacent coast. If there is a deficit in sediment (from the equilibrium value), an inlet-estuary system will import sand from its adjacent coast. This sediment volume can be computed by the summation of the three different processes mentioned above, and given by the following equation (Ranasinghe et al., 2013):

$$\Delta V_{\rm T} = \Delta V_{\rm BI} + \Delta V_{\rm BV} + \Delta V_{\rm FS} \tag{1}$$

where  $\Delta V_{\rm T}$  is the cumulative change in the total sedimentvolume exchange between the estuary and its adjacent coast,  $\Delta V_{\rm BI}$  is the sediment demand of the basin due to sea-level rise-driven change in basin volume (i.e., basin infilling volume),  $\Delta V_{\rm BV}$  is the change in basin infill sediment volume due to variation in river discharge, and  $\Delta V_{\rm FS}$  is the change in fluvial sediment supply due to combined effects of climate change and anthropogenic activities (all volumes in m<sup>3</sup>).

Sea-level rise may affect the tides as well. However, possible changes in tides due to rising sea level are projected to be marginal. For example, Pickering et al. (2017) have shown that for 2.0 m of sea-level rise, the possible changes in the mean high water level of tides are less than 0.1 m. Therefore, this aspect was not considered in this study. Further, the nodal tidal elevation changes (e.g., Baart et al., 2012; Peng et al., 2019) are also not taken into account in the present model.

The schematic diagram presented below (Figure 2) shows the connectivity among these processes and the sediment-volume components comprising  $\Delta V_{\rm T}$ .

## Basin Infilling Volume Due to Sea-Level Rise-Induced Increase in Accommodation Space

Accommodation space is the additional volume created within the basin (or estuary) due to an increase relative mean sea level [ $\Delta RSL$  (m)]. This increase in volume, given by  $A_b$ . $\Delta RSL$ ; where,  $A_b$  is the basin surface area (m<sup>2</sup>), results in an extra sediment demand by the estuary [ $\Delta V_{BI}$  (m<sup>3</sup>); Factor 1 in **Figure 2**]. Taking into account also the time lag between sealevel rise (hydrodynamic forcing) and the associated basin infilling (morphological response),  $\Delta V_{BI}$  can be expressed by the following equation, where the negative sign indicates sediment imported into the inlet-estuary system.

$$\Delta V_{\rm BI} = -fac \left( A_{\rm b} \Delta RSL \right) \tag{2}$$

where "fac" (0 < fac < 1) accounts for the morphological response lag. In this study, it is taken as 0.5 (following the argumentation and formulations in Ranasinghe et al. (2013) for the original SMIC model) in all model simulations.

**Basin Volume Change Due to Variations in River Flow** Changes in river discharge  $[\Delta Q_R \ (m^3)]$  will affect the infill volume of the estuary. Such changes in river discharge would alter the tidal flow volume during the ebbing phase of the tide, and subsequently, the estuarine and inlet velocities. Due to the tendency of velocities in a basin-inlet system (averaged over the net cross section) to approach an equilibrium value, the basin-inlet system will change its cross-section by either scouring or accretion, until the equilibrium cross section is reached. Depending on the sign of change in future river discharge [i.e.,



increase (+)/decrease (-)], a particular volume of sediment  $[\Delta V_{BV}(m^3)$ ; Factor 2 in **Figure 2**] would be exchanged between the inlet-basin system and its adjacent coast to accommodate this basin-inlet cross-sectional change. This sediment volume ( $\Delta V_{BV}$ ) can be computed as follows (Ranasinghe et al., 2013):

$$\Delta V_{\rm BV} = \frac{\Delta Q_{\rm R} V_{\rm B}}{(P+Q_{\rm R})} \tag{3}$$

where  $Q_{\rm R}$  is the present river flow into the basin during ebb (m<sup>3</sup>),  $\Delta Q_{\rm R}$  is the climate change-driven variation in river flow during ebb (m<sup>3</sup>),  $V_{\rm B}$  is the present basin volume (m<sup>3</sup>), and *P* is the mean equilibrium ebb-tidal prism (m<sup>3</sup>).

## Determining equilibrium tidal prism for estuaries with low-lying margins

The above sediment volume  $\Delta V_{BV}$  depends on the equilibrium tidal prism. This equilibrium tidal prism in estuaries with low-lying margins is linked with the concurrent sea level and cross-sectional area of the tidal inlet and channels in the basin. When the sea level is gradually increasing, as it is doing now (Stocker et al., 2013b), it is necessary to determine the equilibrium tidal prism at these inlet-estuary systems for the increased mean sea level, so that the corresponding basin volume change and subsequent amount of sediment exchange can be correctly computed. **Figure 3** illustrates the non-linear, iterative calculation

procedure adopted here to represent this phenomenon, followed by a description of the associated physical processes.

The total ebb-tidal prism (*P*) consists of two components: (1) the volume of water flowing out of the estuary system due to tidal forcing alone ( $P_{\rm T}$ ), and (2) the volume of water supplied by the river flow during the ebbing phase of the tide ( $P_{\rm R}$ ).

$$P = P_{\rm T} + P_{\rm R} \tag{4}$$

Owing to the low-lying margins of these systems, the basin surface area of the estuary  $(A_b)$  will change with sea-level rise. Therefore, a look-up table for the basin surface area was developed with the aid of a Digital Elevation Model (DEM), to determine the basin surface area  $(A_b)$  associated with different sea levels.

Assuming there is no phase lag in tidal elevations within the systems, which is a reasonable assumption for not-verylong estuaries (Dronkers, 1964) the ebb-tidal prism ( $P_T$ ) corresponding to this new basin surface area can be calculated according to the relationship presented by Keulegan (1951).

$$P_{\rm T} = A_{\rm b}(2a_{\rm b}) \tag{5}$$

where  $A_b$  is the surface area of the estuary and  $a_b$  is the mean tidal amplitude within the estuary.

Tidal inlets throughout the world exhibit several consistent relationships that have allowed coastal engineers and



FIGURE 3 | Flowchart of the iteration procedure to determine equilibrium tidal prism at estuaries with low-lying margins (modified from Bamunawala et al., 2018b).

marine geologists to formulate predictive models. One such widely-known relationship is O'Brien's relationship between inlet channel cross-sectional area (a) and tidal prism (P) (O'Brien, 1969).

$$a = c_1 P^{c_2} \tag{6}$$

where  $c_1$  and  $c_2$  are empirical coefficients.

It should be noted that there can be instances where the estuary systems deviate from the above a-P relationship (e.g., Hume and Herdendorf, 1993; Gao and Collins, 1994). Townend (2005) suggested that the deviation from the a-P relationship can be attributed to the state of the respective estuary system's response to contemporary processes over the Holocene. Besides, there are some other systems, of which the geological constraints do not accommodate the eroding of the inlet channel. In such cases, the tidal prism has to change to maintain the equilibrium conditions.

Thus, when *P* changes, the inlet cross-sectional area *a* will also need to change. According to Keulegan (1951), such changes in the inlet cross-sectional area could also affect tidal attenuation characteristics in the inlet channel as attenuation is a function of the inlet-channel geometry. Table 2 of Keulegan (1951) provides a look-up table for an expression (left-hand side of the equation below), which includes the coefficient of repletion (*K*), basin surface area ( $A_b$ ), inlet channel cross-sectional area (*a*) and

oceanic tidal amplitude (*H*) for a given inlet-channel length ( $L_c$ ), inlet-channel hydraulic radius (r) and Manning's roughness (n).

$$\frac{A_{\rm b}K\sqrt{H}}{a} \times 10^{-4} = f(n, r, L_{\rm c}) \tag{7}$$

This relationship allows determining the coefficient of repletion (*K*). The resulting tidal amplitude within the basin  $(a_b)$  can then be computed using:

$$\frac{a_{\rm b}}{H} = \sin(\tau) \tag{8}$$

where  $sin(\tau)$  is a function of the coefficient of repletion (*K*), and can be determined through another look-up table (Table 4) provided in Keulegan (1951).

It should be noted that Eqs 7 and 8 inherently assume that the presence of a narrow and relatively straight inlet channel which connects the ocean to an estuary/lagoon that is significantly wide compared to the inlet channel.

Use of the above computed tidal amplitude in Eq. (5) provides the new tidal prism (for the considered mean sea level), which will consequently result in a new inlet cross-sectional area as per Eq. (6). A new inlet cross-sectional area will have a different coefficient of repletion (K) and, thus a new tidal amplitude within the basin. Therefore, Eqs (5-8) are here used iteratively, until the difference between two subsequent computed inlet crosssectional areas (for a given mean sea level) is less than 1% of the former value (**Figure 3**).

#### **Change in Fluvial Sediment Supply**

Climate change and anthropogenic activities could result in significant changes in the annual fluvial sediment volume [ $\Delta Q_S$  (m<sup>3</sup>)] supplied to the coast (Vörösmarty et al., 2003; Syvitski, 2005; Palmer et al., 2008; Ranasinghe et al., 2019). Consequently, these changes will affect the total volume of sediment exchanged between the inlet-estuary system and its neighboring coast [ $\Delta V_{FS}$  (m<sup>3</sup>); Factor 3 in **Figure 2**] over the period considered [t (in years)]. The changes in fluvial sediment volume are here calculated as (Ranasinghe et al., 2013):

$$\Delta V_{\rm FS} = \int_{0}^{t} \Delta Q_{\rm S}(t) \, dt \tag{9}$$

#### Assessment of fluvial sediment supply to coasts

Sediment generation and fluvial sediment throughput at catchment scale are affected by both climate change-driven impacts and anthropogenic activities (Syvitski et al., 2003, 2009; Syvitski and Milliman, 2007; Shrestha et al., 2013). Bamunawala et al. (2018a) illustrated that the empirical BQART model presented by Syvitski and Milliman (2007) can be used effectively to assess the annual fluvial sediment supply to the coast while considering both climate change-driven impacts and human activities. This empirical model is based on 488 globally-distributed datasets. For catchments with a mean annual temperature greater than or equal to  $2^{\circ}$ C, the BQART model estimates the annual sediment volume ( $Q_{\rm S}$ ) transported downstream to the coast by the following equation:

$$Q_{\rm S} = \omega B Q^{0.31} A^{0.5} R T \tag{10}$$

where  $\omega$  is 0.02 or 0.0006 for the sediment volume ( $Q_S$ ), expressed in kg/s or MT/year, respectively, Q is the annual river discharge from the catchment considered (km<sup>3</sup>/yr), A is the catchment area (km<sup>2</sup>), R is the relief of the catchment (km), and T is the catchment-wide mean annual temperature (°C).

Term "B" in the above equation represents the catchment sediment production and comprises glacial erosion (I), catchment lithology (L) that accounts for its soil type and erodibility, a reservoir trapping-efficiency factor ( $T_E$ ), and human-induced erosion factor ( $E_h$ ), which is expressed as the following equation:

$$B = IL(1 - T_{\rm E})E_{\rm h} \tag{11}$$

Glacial erosion (*I*) in the above equation is expressed as follows:

$$I = 1 + (0.09A_{\rm g}) \tag{12}$$

where  $A_{g}$  is the percentage of ice cover of the catchment area.

Syvitski and Milliman (2007) stated that the human-induced erosion factor ( $E_h$ ; anthropogenic factor) depends on land-use practices, socio-economic conditions and population density. In their study,  $E_h$  values were determined based on the Gross National Product (per capita) and population density. Based

on the global dataset used, the optimum range of  $E_{\rm h}$  was suggested to be 0.3–2.0.

In this study, however, instead of using coarse countrywide estimates of Gross National Product (GNP)/capita and population density to estimate the human-induced soil erosion factor ( $E_h$ ), the human footprint index (HFPI), which is based on high-resolution spatial information published by the Wildlife Conservation Society [WCS] and Columbia University Center for International Earth Science Information Network [CIESIN] (2005) is used to achieve a better representation of anthropogenic influences on sedimentation (Balthazar et al., 2013; Bamunawala et al., 2018a). The HFPI is developed by using several global datasets such as population distribution, urban areas, roads, navigable rivers, electrical infrastructures and agricultural land use (Sanderson et al., 2002).

#### **Reference Conditions for Baseline Simulations**

The modeling approach presented above is used here to compute the total sediment exchange volume between the inlet-estuary system and its adjacent coastline for the 2020–2100 period. In order to compute these future changes, first, baseline conditions need to be established. Here, CEC system conditions at 2019 were used as the reference condition in all sediment-volume computations. However, as both mean annual temperature (T) and cumulative river discharge (Q) show significant inter-annual variability, using T and Q values specifically for the year 2019 as the reference conditions for these two variables. As there is no significant inter-annual variability in mean sea level, all future changes in sea level over the 2020–2100 period were computed relative to the 2019 mean sea level.

# Modeling the Spatio-Temporal Evolution of Inlet-Interrupted Coastlines

Changes in the total sediment exchange between barrier estuaries and their adjacent coasts ( $\Delta V_{\rm T}$ ) will act as sediment source/sink at the coast, which, in turn, will contribute to the evolution of the inlet-interrupted coast. The extent and magnitude of such coastline variations are also related to the wave-driven longshore sediment transport capacity in the vicinity of the inlet. Many studies have indicated that potential climate-change impacts during the 21<sup>st</sup> century may result in changing mean wave conditions across the world's oceans (Mori et al., 2010; Hemer et al., 2013; Semedo et al., 2013; Casas-Prat et al., 2018; Morim et al., 2019). Such changes in wave conditions could result in variations in longshore sediment transport rates and gradients therein (e.g., Hemer et al., 2012; Casas-Prat and Sierra, 2013; Erikson et al., 2015; Grabemann et al., 2015; Wolf et al., 2015; Dastgheib et al., 2016; Shimura et al., 2016). However, all available wave projections only provide averaged changes of wave conditions [i.e., not for individual Representative Concentration Pathways (RCPs)] over the last two/three decades of the 21st century (i.e., not for the entire 21st century). Furthermore, projected changes in offshore wave conditions are rather small for most of the global coastline, especially where sandy coasts are concerned, implying that associated changes in nearshore waves

would also be small. Therefore, in this study, which considers all RCPs over the entire 21<sup>st</sup> century, it is assumed that the ambient rates of longshore sediment transport remain invariant throughout the 21<sup>st</sup> century, and thus, the projected changes in coastlines are computed based on the present-day longshore sediment transport rates. With this assumption, the conceptual framework used to compute the spatio-temporal variations of inlet-interrupted coastlines is described below.

Following the overarching objective of this study, a simplified framework of a generically applicable coastline model that provides first-order estimates of coastline variations at macro time scales was developed. It represents the general changes of the inlet-interrupted coastline by considering the total change in sediment volume exchange between the inlet-estuary system and the adjacent coast ( $\Delta V_T$ ), while assuming uniform shoreline orientations along up- and down-drift coasts and the lack of any coastal structures.

The maximum extent of inlet-affected coastline in both updrift and down-drift directions from an inlet is constrained by the existence of headlands, rock outcrops, inlets or by other prominent changes in mean shoreline orientation. Following the method adopted in the SMIC applications by Ranasinghe et al. (2013), the maximum extent of this inlet-affected coastline distance was considered to be ~25 km. If there is no known gradient in the net annual alongshore sediment transport rate along the coastline (i.e., both up- and down-drift coasts), it can be assumed that the coastal cell concerned is presently in equilibrium at annual time scales.

Within the development of this simplified coastline change model, it is assumed that the longshore sediment transport (LST) occurs uniformly over the cross-shore profile. **Figure 4** illustrates the hypothetical equilibrium cross-shore profile. Given that the change in total sediment volume exchange ( $\Delta V_T$ ) is computed annually (Eqs 1–12),  $\Delta V_T$  is first divided into a number of equal fragments ( $n_v$ ). This volume fragment ( $V_{fr}$ ), which is calculated using Eq. [13] was then distributed along the coastline.

$$V_{\rm fr} = \frac{\Delta V_{\rm T}}{n_{\rm v}} \tag{13}$$

Depending on the equivalent longshore transport capacity ( $\Delta Q_{\text{LST}}$ ; calculated using Eq. 14), all or part of this volume fragment is transported along the coast.

$$\Delta Q_{\rm LST} = \frac{Q_{\rm LST}}{n_{\rm v}} \tag{14}$$

Following the assumption of a balanced sediment budget within the coastal cell, any volume of sediment that gets transported in the down-drift direction will result in coastal progradation at the farthermost section of the down-drift coast. If the volume fragment is larger than the equivalent longshore transport capacity ( $\Delta Q_{\text{LST}}$ ), the surplus volume ( $\Delta V$ ; computed using Eq. 15) will result in a seaward translation of the coastline position ( $\Delta y$ ) within the considered alongshore distance ( $\Delta x$ ) (**Figure 4**). This also holds when  $V_{\text{fr}} < \Delta Q_{\text{LST}}$ , which will lead to coastline recession.

$$\Delta V = V_{\rm fr} - \Delta Q_{\rm LST} \tag{15}$$

Assuming that the shoreline moves cross-shore parallel to itself while maintaining its equilibrium profile, the following relationship can be derived to determine the resulting change in coastline position ( $\Delta y$ ).

$$\min(\Delta V, V_{\rm fr}) = \Delta x (D\Delta y)$$

where *D* is the depth of closure.

The above procedure is repeated  $n_V$  times, so that the total change in sediment volume exchange between the estuary and adjacent coast ( $\Delta V_T$ ) is fully distributed along the coastal cell. These computations are closely connected to an expression for the longshore sediment transport rate ( $Q_{LST}$ ), which, in turn, is related to the longshore current generated by oblique incident breaking waves.  $Q_{LST}$  is thus presented as:

$$Q_{\rm LST} = Q_0 \sin(2\alpha_{\rm b}) \tag{16}$$

where  $Q_0$  is the amplitude of the longshore sediment transport rate (m<sup>3</sup>/yr), and  $\alpha_b$  is the breaking wave angle between wave crest line and coastline, which can be expressed as follows, assuming small-angles:

$$\alpha_{\rm b} = \alpha_0 - \frac{\Delta y}{\Delta x} \tag{17}$$

where  $\alpha_0$  (rad) is the angle of breaking wave crests (relative to the coastline).

Since the local coastline position  $(\Delta y)$  would be updated with the alongshore distribution of each volume fragment, breaking wave angle  $(\alpha_b)$  and longshore sediment transport rate  $(Q_{LST})$  are also updated after completion of the distribution of each volume fragment. If the present-day longshore sediment transport rate and the corresponding angle of breaking wave crest  $(\alpha_0)$  are known, the above-described procedure can be implemented to distribute the sediment volume along the inlet-interrupted coast. If such information is not available, the amplitude of the longshore sediment transport rate  $(Q_0)$  can be reasonably estimated by using a bulk longshore sediment transport equation such as the CERC formula (CERC, 1984), the Kamphuis formula (Kamphuis, 1991), and the Bayram formula (Bayram et al., 2007). An example of such formulation of  $Q_0$  [from the US Army corps, Coastal Engineering Research Centre (CERC), published in the Shore Protection Manual (CERC, 1984)] is shown in Eq. (18).

$$Q_{0} = \frac{0.77\sqrt{g}}{32(1-p)\left(\frac{\rho_{s}}{\rho} - 1\right)\sqrt{\gamma_{b}}} \times H_{sb}^{2.5}$$
(18)

where  $H_{\rm sb}$  is the significant wave height at breaker line (m),  $\gamma_b$  is the breaking parameter for irregular waves (0.55),  $\rho_{\rm s}$  is the density of sand (2, 650 kg/m<sup>3</sup>),  $\rho$  is the density of seawater (1, 030 kg/m<sup>3</sup>), p is the porosity of sand (0.4), and g is the gravitational acceleration (9.81 m/s<sup>2</sup>).

In addition to the above-described coastline change, regional relative sea-level rise ( $\Delta RSL$ ) will shift the active cross-shore profile upward and landward, which, in the absence of sediment sources supplying sand to the coast, will result in additional coastline recession (Bruun, 1962). The magnitude of this



so-called Bruun effect driven coastline recession is expressed according to the following equation:

$$\Delta C_{\rm BE} = \frac{\Delta RSL}{\tan\left(\beta\right)} \tag{19}$$

where  $\Delta C_{\text{BE}}$  is the coastline recession (m),  $\Delta RSL$  is the sea-level rise (m), and  $\beta$  is the average slope of the active beach profile from the shoreline to the depth of closure (*D*; **Figure 4**). It is important to note the the coastline change computed in this way will represent only the change that would be due to climate change impacts and will not be inclusive of any ambient coastline change that would occur even without any future variations in system forcing (e.g., due to alongshore gradients in LST, cross-shore feeding of sediment, fluvial sediment supply).

#### **Input Data Sources**

The reduced-complexity model presented in sections "Change in Total Sediment Volume Exchange Between a Barrier-Estuary System and Its Inlet-Interrupted Coast" and "Modeling the Spatio-Temporal Evolution of Inlet-Interrupted Coastlines," requires four main drivers to project the long-term evolution of inlet-interrupted coasts: annual mean temperature (*T*), annual cumulative river discharge (*Q*), change in regional relative sealevel ( $\Delta RSL$ ), and anthropogenic activities in the catchment, as represented by the human-induced erosion factor (*E*<sub>h</sub>).

Temperature and runoff projections were obtained from General Circulation Models (GCMs) of the Coupled Model Intercomparison Project Phase 5 [CMIP5 data portal; Earth System Grid-Centre for Enabling Technologies (ESG-CET); available on the webpage http://pcmdi9.llnl.gov/]. Projected daily/monthly values of temperature and surface runoff were obtained for all four Representative Concentration Pathways (RCPs). Initially, the GCMs with both temperature and surface runoff projections for all RCPs over the 2010–2100 period were considered as data sources. Of these, GCMs with spatial resolution finer than  $2.5^{\circ}$  were selected to obtain the necessary climate inputs (*T* and *Q*). Where possible, the suitability of the above-selected data sources was assessed regionally, by considering the guidelines published on the appropriateness of GCMs in respective areas (e.g., CSIRO and Bureau of Meteorology, 2015, for Australia).

According to Nicholls et al. (2014), the regional relative sealevel changes ( $\Delta RSL$ ) can be calculated according to the following equation:

$$\Delta RSL = \Delta SL_{\rm G} + \Delta SL_{\rm RM} + \Delta SL_{\rm RG} + \Delta SL_{\rm VLM}$$
(20)

where  $\Delta RSL$  is the change in relative sea level,  $\Delta SL_G$  is the change in global mean sea level,  $\Delta SL_{\rm RM}$  is the regional variation in sea level from the global mean due to meteo-oceanographic factors,  $\Delta SL_{\rm RG}$  is the regional variation in sea level due to changes in the earth's gravitational field, and  $\Delta SL_{\rm VLM}$  is the change in sea level due to vertical land movement (all values in meters).

The regional relative sea-level change projections by 2100 ( $\Delta RSL$ ) were obtained from Figure TS.23 of Stocker et al. (2013a), while the corresponding global mean sea level change ( $\Delta SL_{\rm G}$ ) was obtained from Table SPM. 2 of Stocker et al. (2013b). The difference between those two sets of values provide the cumulative contribution of  $\Delta SL_{\rm RM}$ ,  $\Delta SL_{\rm RG}$ , and partly

 $\Delta SL_{\rm VLM}$  (excluding any local subsidence/rebound) for 2100. Those differences were linearly distributed from the year 2000 to obtain the yearly cumulative contribution of  $\Delta SL_{\rm RM}$ ,  $\Delta SL_{\rm RG}$ , and  $\Delta SL_{\rm VLM}$ . Those linearly distributed values were then added to the yearly changes in global mean sea level ( $\Delta SL_{\rm G}$ ), following the method presented by Mehvar et al. (2016), to obtain yearly projections of regional relative sea-level changes. The yearly changes in global mean sea level ( $\Delta SL_{\rm G}$ ) are calculated following Nicholls et al. (2014) as:

$$\Delta SL_{\rm G} = a_1 t + a_2 t^2 \tag{21}$$

where;  $\Delta SL_G$  is the change in global sea level (m) since 2000, "*t*" is the number of years since 2000,  $a_1$  is the trend in sea level change (m/yr), and  $a_2$  is the change in the rate of sea-level change trend (m/yr<sup>2</sup>). The relevant coefficients were obtained from Mehvar et al. (2016).

The HFPI data were obtained from the WCS-CIESN database, which is available at a spatial resolution of 30 arc-seconds and is regionally normalized to account for the interaction between the natural environment and human influences (Sanderson et al., 2002). Global and continental-scale raster files of HFPI data are available at https://doi.org/10.7927/H4M61H5F.

### **Case Study Sites and Input Data**

The above-introduced reduced-complexity model was applied at three selected systems representing (a) barrier estuaries with low-lying margins (Alsea estuary, Oregon, United States, and Dyfi estuary, Wales, United Kingdom) and (b) small tidal inlets (Kalutara inlet, Sri Lanka). **Table 1** summarizes the key properties of these systems and **Figure 5** shows the locations of the selected case study sites, their respective watershed areas and HFPI.

**TABLE 1** | Properties of the selected barrier estuary systems (reference conditions).

Parameter	Alsea	Dyfi	Kalutara
Mean ebb-tidal prism (P in 10 <sup>6</sup> m <sup>3</sup> )	9.0	71.1	6.2
Basin surface area (A <sub>b</sub> in 10 <sup>6</sup> km <sup>2</sup> )	9.1	17.3	1.75
Basin volume (V <sub>B</sub> in 10 <sup>6</sup> m <sup>3</sup> )	20.0	44.98	5.25
Catchment area (A in km <sup>2</sup> )	1,225	670	2,778
Catchment relief (R in km)	1.25	0.66	2.25
Lithology factor (L)	1.0	0.75	0.5
Anthropogenic factor (E <sub>h</sub> )	0.67	0.93	0.93
Beach profile slope ( $\tan \beta$ )	0.02	0.02	0.02
Depth of closure (h <sub>DoC</sub> in m)	15	15	15

Values of mean ebb-tidal prism, basin surface area and basin volume for Alsea, Dyfi, and Kalutara CEC systems were obtained from O'Neil (1987), National Rivers Authority Welsh Region (1995), and Duong (2015), respectively. Catchment area values were determined by the respective watershed shapefiles. Catchment relief values were determined by the use of one arc-second resolution digital elevation models obtained from the USGS Earth Explorer tool (Farr et al., 2007). Catchmentaveraged lithological factors for the selected systems were obtained from Syvitski and Milliman (2007). Catchment wide anthropogenic factors (E<sub>h</sub>) were obtained by rescaling the Human FootPrint Index (HFPI), given in Wildlife Conservation Society [WCS] and Columbia University Center for International Earth Science Information Network [CIESIN] (2005). The active coastal-profile slope values and depths of closure values were obtained from Athanasiou et al. (2019). Present-day HFPI values within the catchment were rescaled linearly to fit the optimum scale of  $E_h$  suggested by Syvitski and Milliman (2007). These rescaled HFPI values were then averaged over the catchment to determine a representative factor for human-induced erosion ( $E_h$ ). Given the contemporary rate of population growth and urbanization, it is safe to assume that  $E_h$  will increase by 2100. Owing to numerous uncertainties associated with such projections (e.g., Veerbeek, 2017), the value of  $E_h$  by 2100 was assumed to increase by 15% of its presentday value.

The *T* and *Q* values were obtained by an ensemble of four selected GCMs (viz., GFDL-CM3, GFDL-ESM2G, and GFDL-ESM2M from NOAA, United States, and IPSL-CM5A-MR from IPSL in France). **Table 2** presents the averaged *T* and *Q* projections for the reference (2010–2019), mid-century (2046–2065), and end-century (2081–2100) periods, indicating the variation of the respective model inputs across the  $21^{st}$  century for different RCPs.

**Figure 6** shows the projected variations of regional relative sea-level ( $\Delta RSL$ ) at the selected study locations for the four RCPs.

## RESULTS

Model hindcasted coastline changes are presented in section "Model Hindcasts for the 1986–2005 Period." Results of model applications at the three case study locations are presented in sections "Projected Variation of Total Sediment Volume Exchange ( $\Delta V_T$ ): 2020–2100" and "Projected Coastline Change at the Case Study Locations: 2020–2100." Section " Projected Variation of Total Sediment Volume Exchange ( $\Delta V_T$ ): 2020– 2100" presents, for each system, the projected variations in the total sediment volume exchange between the estuary and the adjacent coast ( $\Delta V_T$ ), together with an assessment of the predominant sediment volume component at each case study location. Section "Projected Coastline Change at the Case Study Locations: 2020–2100" presents the projected changes in coastline position at each location by 2060 and 2100.

# Model Hindcasts for the 1986–2005 Period

As a model validation exercise, the above-presented modeling technique was applied to a historical period (1986–2005) to compare the model hindcasts with observed shoreline change at the studied mainland barrier estuary systems. To achieve this objective, the following simplifications were made when obtaining the model inputs/reference conditions.

For the historical period (1986–2005), the ensemble of GCMs described in section "Case Study Sites and Input Data" was used to obtain the yearly values of T and Q. The reference conditions for the T and Q for this hindcast period were taken as the mean value of the GCM ensemble over the 1976–1985 period. The rate of global mean sea-level rise was taken as 2.1 mm/yr for the 1986–2005 period, following the projections presented in Chapter 4 of the IPCC Special Report on the Ocean and Cryosphere in a Changing Climate (i.e., Oppenheimer et al., 2019). The present value of HFPI was considered as a constant



throughout the historical period. The model hindcasted coastline change rates at the three case study locations were compared with satellite-image derived ambient shoreline change rates presented by Luijendijk et al. (2018).

The results of the comparison are shown in **Table 3**. This comparison indicates that the modeled coastline change at all three systems for the validation period compare well with ambient shoreline change rates presented by Luijendijk et al. (2018) over the same period, providing confidence in the model.

# Projected Variation of Total Sediment Volume Exchange ( $\Delta V_T$ ): 2020–2100

**Figures 7–9** show the projected change in total sediment volume exchange  $(\Delta V_{\rm T})$  between each case study estuary and the adjacent coast over the 21<sup>st</sup> century (left) and the individual contributions of the three main sediment volume components [i.e., basin infilling  $(\Delta V_{\rm BI})$ , basin volume change  $(\Delta V_{\rm BV})$ , and fluvial sedimentation  $(\Delta V_{\rm FS})$ ].

The model projections indicate that the Alsea estuary system will import sediment from its adjacent coast throughout the  $21^{st}$  century. The maximum and minimum projected volumes of sediment imports by 2100 are -1.25 million cubic meters (MCM) (RCP 8.5) and -1.0 MCM (RCP 2.6). The results also

indicate that  $\Delta V_{\rm T}$  at the Alsea estuary system is predominantly governed by the process of basin infilling ( $\Delta V_{\rm BI}$ ) and that the projected variations of  $\Delta V_{\rm BV}$  have trivial impacts on  $\Delta V_{\rm T}$  for all RCPs. The increased supply of fluvial sediment toward the end-century period slightly reduce sediment demand due to basin infilling for all RCPs. These increases in fluvial sediment supply toward the end-of-the-century are governed by the projected increments in temperature (**Table 2**) and the increase in humaninduced erosion factor.

The model projections indicate that the Dyfi estuary system will also import sediment from the adjacent coast throughout the  $21^{st}$  century. The maximum and minimum projected volumes of sediment imports by 2100 are -5.0 MCM (RCP 8.5) and -2.5 MCM (RCP 2.6). The results here too indicate that  $\Delta V_T$ at the Dyfi estuary system is governed by the basin sediment demand ( $\Delta V_{BI}$ ), while projected variations of  $\Delta V_{BV}$  and  $\Delta V_{FS}$ have trivial impacts on  $\Delta V_T$  for all RCPs. The river catchment area of this CEC system is relatively small compared with the estuary surface area. Hence, despite the projected increments in temperature (**Table 2**) and the increase in human-induced erosion, fluvial sediment supply by the Dyfi River catchment contributes little to the sediment volume demand due to basin infilling for all RCPs. TABLE 2 | Average annual mean temperature and cumulative runoff at the selected case study locations over the present, mid-21<sup>st</sup> century and end 21<sup>st</sup> century time slices.

System	Period	Mean annual temperature (°C)			Annual cumulative runoff (km <sup>3</sup> )				
		RCP 2.6	RCP 4.5	RCP 6.0	RCP 8.5	RCP 2.6	RCP 4.5	RCP 6.0	RCP 8.5
Alsea, United States	2010-2019	11.11	11.07	10.86	10.91	0.437	0.449	0.467	0.431
	2046-2065	11.66	12.01	11.72	12.56	0.459	0.431	0.438	0.446
	2081-2100	11.69	12.51	12.86	14.12	0.458	0.458	0.459	0.421
Dyfi, United Kingdom	2010-2019	10.30	10.16	10.37	10.29	0.134	0.130	0.126	0.131
	2046-2065	10.71	11.24	10.83	11.55	0.128	0.127	0.130	0.133
	2081-2100	10.57	11.42	11.75	13.06	0.133	0.127	0.126	0.128
Kalutara inlet, SL	2010-2019	26.85	26.92	26.89	26.83	0.799	0.685	0.707	0.812
	2046-2065	27.32	27.79	27.47	28.17	0.805	0.837	0.935	0.999
	2081-2100	27.36	28.01	28.40	29.61	0.793	0.878	0.897	1.054

The temperature and runoff values in the table were obtained by averaging the annual ensembles of the four selected GCMs over the respective time slices.



The model projections indicate that the Kalutara estuary system will also import sediment from the adjacent coast throughout the  $21^{st}$  century. The maximum and minimum projected volumes of sediment imports by 2100 are -7.0 MCM (RCP 2.6) and -3.0 MCM (RCP 8.5). The results here indicate that  $\Delta V_{\rm T}$  at the Kalutara estuary system is governed by the fluvial

sediment supply ( $\Delta V_{\text{FS}}$ ), while projected variations of  $\Delta V_{\text{BV}}$  and  $\Delta V_{\text{BI}}$  have trivial impacts on  $\Delta V_{\text{T}}$  for all RCPs. However, it should be noted that the fluvial sediment supply from the Kalu River catchment is significantly affected by river sand mining (Bamunawala et al., 2018b), which is taken into account in these simulations (423,000 m<sup>3</sup>/yr). Model projections show that,

**TABLE 3** | Comparison of the model hindcasted rates of coastline change over

 1986–2005 with the ambient shoreline change rates presented by Luijendijk et al.

 (2018) over the same period.

CEC system	Rate of coastline change over 1986–2005 (m/yr)				
	Luijendijk et al. (2018)	RC model hindcast			
Alsea estuary (United States)	-0.7	-0.5			
Dyfi estuary (United Kingdom)	-1.0	-0.8			
Kalutara estuary (Sri Lanka)	-1.0	-0.7			

Negative rates of coastline change indicate coastline recession.

despite river sand mining, Kalutara estuary will export sediment to the adjacent coast during the end-century period for RCP 8.5. This is due to the significant increments of the projected *T* and *Q* (**Table 2**) over 2091–2100 (relative to the reference period), which substantially increases  $\Delta V_{\text{FS}}$ , and to a lesser degree  $\Delta V_{\text{BV}}$ .

## Projected Coastline Change at the Case Study Locations: 2020–2100

The  $\Delta V_{\rm T}$  values computed in section "Projected Variation of Total Sediment Volume Exchange ( $\Delta V_{\rm T}$ ): 2020–2100" were used to determine the changes in the position of the coastlines adjacent to the three case studies (**Figure 10**). All the coastline change projections presented here exclude ambient coastline changes. Therefore, the actual (resultant) coastline changes by 2060 and 2100 might be different to what is computed and presented in **Figure 10**.

At the Alsea estuary, the sediment volume demand of the basin (i.e.,  $\Delta V_{\rm T}$ ) acts as a sink at the inlet. However, the magnitude of  $\Delta V_{\rm T}$  is smaller than the existing LST capacity at the inlet. Therefore, the down-drift coast will be subjected to additional coastline recession driven by the  $\Delta V_{\rm T}$ , over and above that due to the Bruun effect. The total recession along the down-drift coast may vary between 71 m (RCP 2.6) and 75 m (RCP 8.5) by 2100. The up-drift coast is only affected by the coastline recession due

to the Bruun effect, which is projected to vary between 50 m (RCP 2.6) and 70 m (RCP 8.5) by 2100.

At the Dyfi estuary too,  $\Delta V_{\rm T}$  causes the inlet to act as a sediment sink. As the magnitude of  $\Delta V_{\rm T}$  here is greater than the existing LST capacity at the inlet, both the up- and downdrift coast should provide sediment to the basin. Thus, both the up- and down-drift coasts will be subjected to additional coastline recession driven by the  $\Delta V_{\rm T}$ , over and above that of Bruun effect. The extent of additional coastline recession along the down-drift coastline is constrained by the longshore sediment transport capacity while that along the up-drift coast corresponds to the deficit in sediment volume (i.e., the difference between the estuarine sediment demand and longshore sediment transport capacity). The model projections indicate that the down-drift coast at the Dyfi estuary may erode by 78 m (RCP 2.6) to 96 m (RCP 8.5) by 2100. However, the up-drift coast is projected to erode between 85 m (RCP 2.6) and 140 m (RCP 8.5) by 2100.

The Kalutara estuary is also projected to act as a sediment sink during all but the end-century period for RCP 8.5. Since these projected magnitudes of  $\Delta V_{\rm T}$  values are less than the existing LST capacity at the inlet, the down-drift coast will be subjected to additional coastline recession driven by  $\Delta V_{\rm T}$ , over and above the Bruun effect. Under RCP 8.5, the inlet acts as a sediment source during the end-century period, thus reducing recession due to Bruun effect along the down-drift coast. The projected coastline recession along the down-drift coast vary between 82 m (RCP 2.6) and 110 m (RCP 8.5) by 2100. The updrift coast is only affected by the coastline recession due to the Bruun effect, which varies between 50 m (RCP 2.6) and 70 m (RCP 8.5) by 2100.

## DISCUSSION

Application of the newly developed model to the three barrier estuary case-studies indicates that macro-time-scale evolution of



**FIGURE 7** Projected change in total sediment volume exchange ( $\Delta V_T$ ) between the Alsea estuary and the adjacent coast **(left)**, and the relative contributions of the three different sediment volume components **(right)** over the 21<sup>st</sup> century for RCP 2.6, 4.5, 6.0, and 8.5. Negative and positive values of  $\Delta V_T$  indicate sediment imported to the estuary from the adjacent coast and sediment exported from the estuary to the adjacent coast, respectively.







inlet-interrupted coasts under the influences of climate changedriven impacts and anthropogenic activities would vary markedly from system to system. Although the coastlines at these case study sites are projected to erode by the end of this century, the physical processes governing the erosion are different among the three systems.

Model projections show that the future sediment exchange between the estuary and the coast at both the Alsea and Dyfi estuary systems will be governed by the sediment demand due to basin infilling, although, the Alsea inlet system will also be partially influenced by fluvial sediment supply, especially toward the latter part of the 21<sup>st</sup> century. Due to the small projected changes in annual cumulative river discharges and the size of the basin volumes, both these systems are not affected by the sediment demand due to variations in basin volume size. The projected future sediment exchange behavior at the Kalutara estuary system is rather different and is governed by the fluvial sediment supply. Due to the combined effects of the projected increments in temperature and river discharge, and anthropogenic activities, the Kalutara river catchment may generate a surplus of sediment throughout the 21<sup>st</sup> century. However, if the present practice of river sand mining continues, the catchment generated sediment surplus will be significantly reduced, resulting in eroding the adjacent coast. Due to the relatively small basin size (both volume and surface area), effects of sediment demand due to variations in basin volume size and basin infilling are negligible at the Kalutara CEC system.

The coastline change projections presented by Vousdoukas et al. (2020) indicate 50 m of erosion along both up-and downdrift coast of the Alsea estuary by 2100 for RCP 8.5. The same



FIGURE 10 | Projected changes of the coastline adjacent to Alsea estuary (top), Dyfi estuary (middle), and Kalutara estuary (bottom) (excluding ambient coastline change). The two solid lines in each subplot represent the coastline position by 2060 and 2100 (in the same order, moving landward from the most seaward line). The dotted line in each subplot represents the initial (reference) coastline position considered.

study indicates 100 and 150 m erosion along both up-and downdrift coast of the Dyfi estuary and Kalutara inlet, respectively for RCP 8.5 by 2100. It should, however, be noted that the global assessment of sandy coastline variation presented by Vousdoukas et al. (2020) does not consider any estuarine effects and also incorporates a correction factor for Bruun effect-driven coastline recession. As a result, the model projections of the present study will, by necessity, differ from the coastline variation presented by Vousdoukas et al. (2020) at the study locations.

In the model presented here, everything seaward of the shoreline is considered as the "outside world," in order to avoid making this model over-complicated by bringing in complex ebb delta dynamics. Moreover, there are no significant ebb deltas in the three selected CEC systems. In general terms, the presence of ebb deltas would not affect the computation of sediment exchange volumes. However, if there is a significant ebb delta, in which the sand is mobile, part of the sediment demand of the inlet-estuary system (for an importing estuary) could be met by sand supply from the ebb delta. This will affect the coastline change projections by reducing the volume of sediment eroded from the coast. In such situations, the projections given by this model can be considered as pessimistic estimates of coastline recession. At sediment exporting inlet-estuary systems, part of the sediment supplied to the coast may contribute to the development of the ebb delta. Therefore, coastline changes projected by the model under these circumstances will overpredict coastline accretions (i.e., optimistic estimates).

It should also be noted that the simplified one-line coastline change model presented in this study only provides preliminary (i.e., first-order) estimates of variations along the inlet-interrupted coasts. This simplified modeling framework uses a relatively shallow profile (up to the depth of closure) and does not account for any local changes in coastline orientation (i.e., straight shoreline segments are assumed) or the presence of any coastal structures. Since the model projections are based on the total change in exchange volume between the inlet-estuary system and the adjacent coast, results presented here are the changes in coastline the would occur in addition to the ambient coastline change. Thus, the actual coastline changes by 2060 and 2100 might be different to that presented in this manuscript. In addition, for computational efficiency, the coastline change modeling used here treats the coastline up-drift and down-drift of the inlet separately, and as sequences of linear shoreline segments. This treatment results in a rather coarse representation of coastline change and does not resolve subtle coastline curvatures that are coupled with gradients in net alongshore sediment transport and shoreline change rates, which has implications for the way in which erosion or progradation might propagate along the coast. Coupling the terrestrial and estuarine model components with a coastline change model that is able to simulate more realistic changes in coastline shape and orientation [e.g., Coastline Evolution Model (CEM); Ashton and Murray, 2006; the Coastal One-line Vector Evolution Model (COVE); Hurst et al., 2015, or ShorelineS, Roelvink et al., 2020], will improve model predictions significantly. Usage of such a coastline change model will enable more realistic forecasts of changes in coastline shape and orientation, which equate to the capacity to predict shoreline-change hot spots, in response to future changes in wave climate (Slott et al., 2006; Hurst et al., 2015; Anderson et al., 2018; Antolínez et al., 2018). Besides, future changes in wave climate may also alter the in longshore sediment transport rates and gradients therein. Such variations in LST may affect the evolution

of inlet-interrupted coasts and thus need to be considered via detailed site-specific assessments of coastline change.

Results of this study show that fundamental CEC system properties such as basin volume and surface area, river catchment area and projected climatic conditions over the river catchment are closely related to the long-term evolution of inletinterrupted coasts. The existence of any generally applicable relationships/dependencies between these properties/forcing and coastline change could be investigated by applying the model presented here at a larger number of CEC systems with diverse environmental and geographical settings.

There are significant uncertainties in future climate change and anthropogenic activities that need to be borne in mind when considering the projections of coastline change provided here, especially at small tidal-inlet systems, which are highly sensitive to changes in forcing conditions. As a result [in addition to the uncertainties associated with the modeling technique(s) adopted], projections of inlet-interrupted coastline changes will inherit the variabilities in climate change forcing and anthropogenic activities (i.e., input uncertainties) considered. In some situations, for example, to inform catchment/coastal zone management decisions, it may be desirable to have a quantitative understanding of the separate contribution of climate change and anthropogenic activities to the total uncertainty of the coastline change projections. This may be achieved via a Variance Based Sensitivity Analysis (VBSA) using Sobol indices (Sobol', 2001) as done by Le Cozannet et al. (2019).

## CONCLUSION

A new model that can rapidly simulate the climate-change driven evolution of inlet-interrupted coasts at 50–100 year time scales, while taking into account the contributions from catchment-estuary-coastal systems in a holistic manner has been developed and piloted at three different case study locations. The spatio-temporal evolution of inlet-interrupted coasts is simulated by (1) computing the variation of total sediment volume exchange between the inlet-estuary system and its adjacent coast ( $\Delta V_{\rm T}$ ), and (2) distributing the computed  $\Delta V_{\rm T}$ along the inlet-interrupted coast as a spatially and temporally varying quantity. The exchange volume  $\Delta V_{\rm T}$  is calculated as a function of variations in fluvial sediment supply ( $\Delta V_{\rm FS}$ ), basin (or estuarine) infilling due to the sea-level rise-induced increase in accommodation space ( $\Delta V_{\rm BI}$ ), and estuarine sediment volume change due to variations in river discharge ( $\Delta V_{\rm BV}$ ).

The three case study locations considered in this study are: the Alsea estuary (Oregon, United States), Dyfi estuary (Wales, United Kingdom), and Kalutara inlet (Sri Lanka), which broadly represent some of the barrier estuary systems and geomorphic settings found across the world. The model was first validated at the three case study locations against the satellite image derived ambient shoreline change rates presented by Luijendijk et al. (2018) over 1986–2005. Subsequently, the model was applied in forecast mode at the case study sites, with the aim of investigating system behavior under projected climate-change impacts and anthropogenic activities. Results indicated that all three systems will experience sediment deficits by 2100 (i.e., sediment importing estuaries) leading to coastline recession along the inlet-adjacent coasts. However, the processes and system characteristics governing the total sediment exchange volume, and thus coastline change, vary among the systems due to differences in geomorphic settings and projected climatic conditions. Therefore, the results of this study demonstrate the importance of carefully considering catchment and estuarine processes (i.e., fluvial sediment supply, basin infilling and basin volume change) in obtaining projections of coastline change at inlet-interrupted coasts at macro time scales.

## DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation, to any qualified researcher.

## **AUTHOR CONTRIBUTIONS**

JB, AD, AS, and RR conceived and designed the study. JB developed the model, carried out all model applications, and wrote the first draft of the manuscript. SM provided specific guidance on the catchment hydrology aspects of the study. TD provided specific guidance on the SMIC model adaptation, and QA'd the new code. TS assisted with GCM data collection and catchment delineation. All authors provided feedback on the manuscript and contributed text.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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