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\*CORRESPONDENCE Umair Khan, ⊠ Umairkhan@iba-suk.edu.pk

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# Significance of non-uniform heat source/sink and cattaneo-christov model on hybrid nanofluid flow in a Darcy-forchheimer porous medium between two parallel rotating disks

# Sawan Kumar Rawat<sup>1</sup>, Moh Yaseen<sup>2</sup>, Umair Khan<sup>3,4</sup>\*, Manoj Kumar<sup>5</sup>, Sayed M. Eldin<sup>6</sup>, Abeer M. Alotaibi<sup>7</sup> and Ahmed M. Galal<sup>8,9</sup>

<sup>1</sup>Department of Mathematics, Graphic Era Deemed to be University, Dehradun, Uttarakhand, India, <sup>2</sup>Department of Applied Sceince, Meerut Institute of Engineering and Technology, Meerut, Uttar Pradesh, India, <sup>3</sup>Department of Mathematical Sciences, Faculty of Science and Technology, Universiti Kebangsaan Malaysia (UKM), Bangi, Selangor, Malaysia, <sup>4</sup>Department of Mathematics and Social Sciences, Sukkur IBA University, Sukkur, Sindh, Pakistan, <sup>5</sup>Department of Mathematics, Statistics and Computer Science, G. B. Pant University of Agriculture and Technology, Pantnagar, Uttarakhand, India, <sup>6</sup>Center of Research, Faculty of Engineering, Future University in Egypt, New Cairo, Egypt, <sup>7</sup>Department of Mathematics, Faculty of Science, University of Tabuk, Saudi Arabia, <sup>8</sup>Department of Mechanical Engineering, College of Engineering in Wadi Alddawasir, Prince Sattam bin Abdulaziz University, Al-Kharj, Saudi Arabia, <sup>9</sup>Production Engineering and Mechanical Design Department, Faculty of Engineering, Mansoura University, Mansoura, Egypt

The suspension of nanoparticles in fluid influences several properties of the resulting fluid. Many production and manufacturing applications need knowledge of the heat transference mechanism in nanofluids. The current paper concerns the influence of non-uniform heat source/sink on (MoS<sub>2</sub>-Go/water flow) hybrid nanofluid flow and (Go/water flow) nanofluid flow in a Darcy-Forchheimer porous medium between two parallel and infinite spinning disks in the occurrence of radiation. The Cattaneo-Christov model is utilized to analyze heat and mass transmission. The Cattaneo-Christov model introduces the time lag factors in the process of heat and mass transmission, known as the thermal relaxation parameter and solutal relaxation parameter, respectively. The governing equations are numerically solved employing the "bvp4c function in MATLAB." The effect of the primary relevant parameters on the velocity, temperature, nanoparticle concentration, and is graphically depicted. Finally, a table is drawn to show the relationships of various critical factors on the Nusselt number, and Sherwood number. Results reveal that an increase in the thermal relaxation parameter reduces the heat transmission rate at both the upper and lower plate. Furthermore, an increase in the nanoparticle's volume fraction causes enhancement in thermal conduction, which increases the heat transmission rate at the upper disk. The results of this study will be helpful to many transportation processes, architectural design systems, enhanced oil recovery systems, medical fields that utilize nanofluids, and so on.

#### KEYWORDS

rotating disks, hybrid nanofluid, cattaneo-christov model, Darcy-forchheimer porous medium, non-uniform heat source/sink

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## **1** Introduction

To address today's escalating energy demands, the variety of industries has risen exponentially. Optimizing heating performance is an essential alternative for improving cooling and heating efficiency in nuclear and chemical reactors, electronic equipment, and so on. To extract the most out of these applications, scientists and researchers are very much concerned about boosting heating efficiency. Turkyilmazoglu (2022a) studied the influence of a horizontal uniform magnetic field in the flow instigated by a rotating disk. In another study, Turkyilmazoglu (2022b) investigated the influence of heat source/ sink in the convective flow of fluids due to a vertical flat surface/ cone immersed in porous media. Ali et al. (2019a) utilized the Bingham and Carreau models to investigate the complex rheology of slime. Asghar et al. (2020a) utilized the couple stress fluid model to study the movement of microorganisms in two-dimensional channel. Ali et al. (2019b) investigated the optimum speed of microorgamisms through Carreau fluid models with under magnetic and porous effects. Javid et al. (2019) studied and gave the numerical solution of magnetically induced flow of fluid confined inside two curled peristaltic walls. Asghar et al. (2020b) studied the non-Newtonian fluid flow confined within a complex wavy walls of a 2-dimensional channel using Taylor's swimming sheet model. Asghar et al. (2022a) studied the non-Newtonian Couple stress fluid in 2-dimensional inclined channel with magnetic and electrical field. Some other remarkable studies on applications of fluid models on bio-medical fields can be refered from Refs. (Asghar et al., 2020c; Asghar et al., 2022d; Asghar et al., 2022b; Asghar et al., 2022c; Asghar et al., 2023; Wu et al., 2020; Shah et al., 2022). Two decades-long, exploration of nanofluids (Choi, 1995) has confirmed that they have superior heat transmission potential. The varied characteristics of nanoparticles (NPs) may be adjusted by modifying their size (diameter), substance (metallic oxides, non-metallic, metallic, etc.), and nanoparticle dispersion in the working fluid. Keeping in mind the properties, Rahman et al. (2022) studied the influence of suction and magnetic field on several water-based nanofluids over a decelerating rotating disk. They studied the different waterbased nanofluids (NFs) with copper oxide, copper, alumina, silver, and titania. The primary issue with single nanoparticle NFs is that they have either better rheological characteristics or superior thermal networks. Mono nanoparticles lack all of the desirable characteristics needed for some applications. The features of nanofluids may be improved by adjusting the nanoparticle volume fraction; however, this has a limitation as the difficulty arises in the trade-off due rise in viscosity. This is a constraint, which may be overcome by combining more than one variety of NPs in the working fluid. Later, the researcher's developed hybrid nanofluids (HNFs) that optimize the exclusive features of many varieties of nanoparticles.

Many studies have used hybrid nanofluid combinations of metallic and non-metal oxide nanoparticles to maximize thermal performance and nanoparticle stability. The development of nanoclusters increases the relative viscosity of HNFs, and HNFs have superior thermal conductivity than solitary nanoparticle nanofluids and base fluids (Ranga Babu et al., 2017). Ranga Babu et al. (2017) also marked out that metal nanoparticles make a nanolayer atop metallic oxide nanoparticles, and it

produces a thermal interfacial layer between weak boundaries of the working fluid and hybrid NPs, resulting in significant thermal conductivity augmentation. Devi and Devi (2016) studied the significance of Newtonian heating in HNF flow over a three-dimensional stretched surface. They analyzed the comparative behavior of Cu-Al<sub>2</sub>O<sub>3</sub>/water and Cu/water. They concluded that HNF has a higher heat transmission rate (HTR) compared to NF. Waqas et al. (2021) also explained and gave the solution to a HNF flow problem over a rotating disk with nonlinear radiation. They studied the model with water as a base fluid and SWCNT- TiO2 and MWCNT- CoFe2O4 NPs. Khan et al. (2020c) expounded on the HNF flow over a thick moving surface instigated by mixed convection. They modeled the flow with water as a main fluid and SiO<sub>2</sub> and MoS<sub>2</sub> NPs. Masood et al. (2021) discussed the significance of a HNF flow over a stretched surface near a stagnation point. They studied the problem with heat generation/absorption and water as a working fluid with polystyrene and titanium oxide NPs. Alrabaiah et al. (2022) inspected the HNF flow inside a conical slit of a cone and a disk. They modeled the flow with water and magnesium oxide, and silver NPs. Yaseen et al. (2022c) expounded on the significance of the magnetic field on HNF flow and NF flow between two parallel plates. They studied the flow problem with MoS<sub>2</sub>-SiO<sub>2</sub>/H<sub>2</sub>O-C<sub>2</sub>H<sub>6</sub>O<sub>2</sub> for HNF flow and MoS<sub>2</sub>/H<sub>2</sub>O for NF flow. Qureshi et al. (2021) investigated the HNF flow between two moving co-axial orthogonal disks. They considered the flow problem with water as a main fluid and titania and copper NPs and studied the significance of the magnetic field. Rashid et al. (2021) inspected the HNF flow over a cylinder in motion. They considered the flow problem with water as a main fluid and Titania and silver NPs. Khan et al. (2022) explicated the significance of suction in a HNF flow between two parallel plates. They considered the flow problem with water as a base fluid and carbon nanotubes and Fe<sub>3</sub>O<sub>4</sub> NPs.

Technological advancements have considerably enhanced human interaction with fundamental tasks such as heating and cooling food and materials, transportation, and manufacturing. The heat altercation process in equipment or applications intended to suit social requirements is a key aspect typically seen in the aforementioned activities. This has been a significant issue for manufacturers over the decades, particularly recently, in improving the thermal control of various maneuvers in the electronic sector, power systems, thermal sector, and medicinal bids. For a long period, the Fourier law (Fourier, 1822) was used to analyze the heat transmission attributes. Years later, Cattaneo (Cattaneo, 1948) altered the Fourier law by including a parameter related to the time lag in the traditional Fourier law, which states that the heat transfer mechanism permits heat to be carried at a restricted pace through the transmission of heat waves. Later, Christov, (Christov, 2009) used thermal relaxation time and the upper convective derivative of Oldroyd to overcome the limitation of the Cattaneo rule and arrive at a material invariant formulation. The developments by Cattaneo (Cattaneo, 1948) and Christov (Christov, 2009) have led the way for researchers to study the HTR with a time lag factor and it is called the Cattaneo-Christov heat flux model (CCM). Very recently, Turkyilmazoglu (2021) provided an analytical explanation of the application of CCM in cooling and its role in enhancing the HTR from surfaces. In recent times; Khan et al. (2020b) explicated the consequence of the thermal stratification and CCM in the water-based



NF flow over a surface having an exponential stretching rate. They analyzed the behavior of NF with three diverse NPs, namely, copper, Titania, and alumina; Yaseen et al. (2022a) studied the difference in HTR of MoS<sub>2</sub>/Kerosene oil and MoS<sub>2</sub>-SiO<sub>2</sub>/Kerosene oil flow between two spinning disks with CCM. They concluded that at the lower disk, the HTR of the hybrid nanofluid transcends the HTR of the nanofluid. (Ashraf and Ghehsareh (2021) explored the significance of CCM in the flow of Casson fluid past a heated surface; Kumar et al. (2021) studied the flow of water-based NF with carbon nanotubes (multi and singlewalled) between two spinning disks in a porous medium with CCM. Bai et al. (2022) derived the analytical solution of an Oldroyd-B nanofluid flow problem through a vibrating tensile plate with CCM. Naz et al. (2022) also discussed the analytical solution of a Carreau nanoliquid flow problem over a rotating and stretchable disk with CCM. Some more interesting research on CCM can be found in Refs. (Irfan et al., 2018; Garia et al., 2021; Khan et al., 2021; Madhukesh et al., 2021).

According to the preceding discussion, it can be inferred that only a few studies are published to study the significance of HNF between two spinning disks. Authors have developed a model to analyze the HNF flow (MoS<sub>2</sub>-Go/water flow) and NF flow (Go/water flow) between two parallel and infinite spinning disks. Furthermore, as a novelty, the significance of non-uniform heat source/sink, CCM, thermal radiation, magnetic field, and Darcy-Forchheimer porous medium are also studied. This research paper also aims to analyze the HTR and mass transmission rate (MTR) of HNF flow (MoS<sub>2</sub>-Go/ water flow) and NF flow (Go/water flow) at both disks. The numerical solution is sought *via* the bvp4c solver in MATLAB. As per the author's information, such a comparative analysis of the HNF flow (MoS<sub>2</sub>-Go/water) and NF flow (Go/water) between two parallel and infinite spinning disks has never been reported before and the results are new and novel.

## 2 Flow model and governing equations

## 2.1 Assumptions of the problem

Consider the three-dimensional incompressible, steady, and axisymmetric flow of the HNF (MoS2-Go/water) and NF (Go/ water) between the two spinning infinite disks placed along parallel lines (see Figure 1). The notation  $(r, \Theta, z)$  has been used for the cylindrical coordinate system (see Figure 1). The flow is exposed to a magnetic field *B*<sub>o</sub> in the *z*-direction. As a novelty, to develop the model, the Darcy-Forchheimer law is used for porous medium. In addition, the non-uniform heat source/sink, Cattaneo-Christov double diffusion model, and thermal radiation is used to investigate HTR and MTR. Moreover, the last term in the energy equation (Eq. 5) denotes the non-uniform heat source/sink term (q''') and it is explained later. The lower disk and upper disk are placed at z = 0and z = H (see Eq. 7). In the boundary conditions,  $a_1$  and  $a_2$  denote the shrinkage rates of the lower and upper disks in the radial direction, respectively. Furthermore,  $b_1$  and  $b_2$  are taken as the angular velocities of the lower and upper disks, respectively. The outer surfaces of the disks are assumed to be convectively heated by hot liquids having temperatures  $T_w$  (lower disk) and  $T_H$  (upper disk), with  $h_1$  (lower disk) and  $h_2$  (upper disk) as their heat transfer coefficients. In addition,  $C_w$ and C<sub>H</sub> denote the NPs concentration at the lower and upper disks, respectively.

Based on the aforesaid points, the flow equations are (see Bhattacharyya et al., 2020; Mabood et al., 2021; Yaseen et al., 2022a): *Continuity equation:* 

$$\frac{\partial u}{\partial r} + \frac{\partial w}{\partial z} + \frac{u}{r} = 0 \tag{1}$$

Momentum equations:

$$\rho_{hnf}\left(u\frac{\partial u}{\partial r}+w\frac{\partial u}{\partial z}-\frac{v^{2}}{r}\right) = -\frac{\partial p}{\partial r}+\mu_{hnf}\left(\frac{\partial^{2} u}{\partial r^{2}}+\frac{\partial^{2} u}{\partial z^{2}}+\frac{1}{r}\frac{\partial u}{\partial r}-\frac{u}{r^{2}}\right)$$
$$-\sigma_{hnf}B_{0}^{2}u-\frac{\mu_{hnf}}{k_{fn}}u-\frac{\rho_{hnf}F}{\sqrt{k_{fn}}}u^{2} \qquad (2)$$

$$\rho_{hnf}\left(u\frac{\partial v}{\partial r} + w\frac{\partial v}{\partial z} + \frac{uv}{r}\right) = \mu_{hnf}\left(\frac{\partial^2 v}{\partial r^2} + \frac{\partial^2 v}{\partial z^2} + \frac{1}{r}\frac{\partial v}{\partial r} - \frac{v}{r^2}\right) - \sigma_{hnf}B_0^2 v$$
$$-\frac{\mu_{hnf}}{k_{fn}}v - \frac{\rho_{hnf}F}{\sqrt{k_{fn}}}v^2 \tag{3}$$

$$\rho_{hnf}\left(w\frac{\partial w}{\partial z}+u\frac{\partial w}{\partial r}\right) = -\frac{\partial p}{\partial z}+\mu_{hnf}\left(\frac{\partial^2 w}{\partial r^2}+\frac{1}{r}\frac{\partial w}{\partial r}+\frac{\partial^2 w}{\partial z^2}\right)$$
(4)

Energy equation:

$$u\frac{\partial T}{\partial r} + w\frac{\partial T}{\partial z} + \gamma_t \left( \frac{\partial T}{\partial r} \left( w\frac{\partial u}{\partial z} + u\frac{\partial u}{\partial r} \right) + \frac{\partial T}{\partial z} \left( w\frac{\partial w}{\partial z} + u\frac{\partial w}{\partial r} \right) \right) \\ + 2uw\frac{\partial^2 T}{\partial z\partial r} + u^2 \frac{\partial^2 T}{\partial r^2} + w^2 \frac{\partial^2 T}{\partial z^2} \right) \\ = \frac{1}{\left(\rho C_p\right)_{hmf}} \left( k_{hmf} + \frac{16\sigma^* T_H^3}{3k^*} \right) \left( \frac{\partial^2 T}{\partial r^2} + \frac{\partial^2 T}{\partial z^2} + \frac{1}{r} \frac{\partial T}{\partial r} \right) + \frac{q^{\prime\prime\prime\prime}}{\left(\rho C_p\right)_{hmf}}$$
(5)

Concertation equation:

$$u\frac{\partial C}{\partial r} + w\frac{\partial C}{\partial z} + \gamma_c \left( \frac{\partial C}{\partial r} \left( w\frac{\partial u}{\partial z} + u\frac{\partial u}{\partial r} \right) + \frac{\partial C}{\partial z} \left( w\frac{\partial w}{\partial z} + u\frac{\partial w}{\partial r} \right) + 2uw\frac{\partial^2 C}{\partial z\partial r} + u^2\frac{\partial^2 C}{\partial r^2} + w^2\frac{\partial^2 C}{\partial z^2} \right)$$
$$= D \left[ \frac{1}{r}\frac{\partial C}{\partial r} + \frac{\partial^2 C}{\partial r^2} + \frac{\partial^2 C}{\partial z^2} \right]$$
(6)

with Boundary conditions (BCs):

$$u = a_1 r, v = b_1 r, w = 0, k_{hnf} \frac{\partial T}{\partial z} = -h_1 (T_w - T), C = C_w \text{ at } z = 0$$
$$u = a_2 r, v = b_2 r, w = 0, k_{hnf} \frac{\partial T}{\partial z} = -h_2 (T - T_H), C = C_H \text{ at } z = H$$
$$(7)$$

where "(u, v, w) are the velocity components along with  $(r, \Theta, z)$  directions," respectively, "*C* is nanoparticles concentration," "*T* is temperature," "p is pressure," " $k^*$  is the mean absorption coefficient," " $\sigma^*$  is the Stefan-Boltzmann constant," "*F* is the Forchheimer coefficient and  $k_{fh}$  is the porous medium permeability," respectively, "*D* is diffusion coefficient," " $\gamma_t$  is the thermal relaxation time," and " $\gamma_c$  is the solutal relaxation time." Furthermore, "*k* is thermal conductivity,  $\mu$  is dynamic viscosity,  $C_p$  is heat capacity,  $\rho$  is density,  $\sigma$  is electrical conductivity." Moreover, subscript *hnf* is for hybrid nanofluid, *nf* is for nanofluid, and *f*, *bf* is for fluid. In addition, the last term in the energy Eq. 5 i.e.,  $q^{m}$  denotes the significance of "non-uniform heat source/sink" and it is demarcated as follows (Yaseen et al., 2022b):

$$q^{\prime\prime\prime} = \frac{k_{hmf} u_w (T_w - T_H)}{r v_{hmf}} \left\{ A^* \frac{df}{\partial \xi} + B^* \theta \right\}$$
(8)

where  $u_w = b_1 r$  and the heat source/sink corresponding to space coefficients and corresponding to temperature dependence are signified by constants  $A^*$  and  $B^*$ , respectively. As a result, the heat

TABLE 1 Thermo-physical properties of water,  $\mathsf{MOS}_2$  and Go nanoparticles (Khan et al., 2020d).

	ho(Kg/m <sup>3</sup> )	C <sub>p</sub> (J/KgK)	<i>k</i> (W/mK)	$\sigma$ ( $\Omega$ .m) $^{-1}$
Water	997.1	4,179	.613	.05
Go	1800	717	5,000	$6.30  imes 10^7$
MoS <sub>2</sub>	5,060	397.746	904.4	$2.09  imes 10^4$

source phenomena is characterized by  $A^* > 0$  and  $B^* > 0$ , whereas the heat sink phenomena is characterized by  $A^* < 0$  and  $B^* < 0$ .

# 2.2 Properties of hybrid nanofluid and nanofluid

This study describes the analysis of HNF and NF. The thermal characteristics of HNF and NF are influenced by the base fluid (water) and NPs; as well as by the volume fraction of MoS<sub>2</sub> and Go NPs, as shown in Table 1 (Khan et al., 2020d). The Shape of MoS<sub>2</sub> and Go NPs is taken as spherical. In this paper, the volume fraction of Go NPs and MoS<sub>2</sub> NPs is denoted by  $\phi_1$  and  $\phi_2$ , respectively. Furthermore,  $s_1$  is used for Go NPs, and  $s_2$  is used for MoS<sub>2</sub> NPs. The MoS<sub>2</sub> belongs to the transition metal class and Go belongs to the oxide class. The combination of MoS<sub>2</sub> and Go NPs is taken because metal nanoparticles make a nanolayer atop oxide nanoparticles, and it produces a thermal interfacial layer between weak boundaries of the working fluid and hybrid NPs, resulting in thermal conductivity augmentation.

# 2.2.1 Thermophysical correlations of Go/water nanofluid

The thermophysical correlations of the NF model used are as follows (Rawat and Kumar, 2020):

$$\frac{\mu_{nf}}{\mu_{f}} = \frac{1}{\left(1 - \varphi_{1}\right)^{2.5}}, \ \rho_{nf} = (1 - \varphi_{1})\rho_{f} + \varphi_{1}\rho_{s1}, \ \frac{k_{nf}}{k_{f}}$$

$$= \left[\frac{k_{s1} + 2k_{f} - 2\varphi_{1}(k_{f} - k_{s1})}{k_{s1} + 2k_{f} + \varphi_{1}(k_{f} - k_{s1})}\right]$$
(9)
$$\frac{\sigma_{nf}}{\sigma_{f}} = 1 + \frac{3(\sigma - 1)\varphi_{1}}{2 + \sigma - (\sigma - 1)\varphi_{1}} \text{ where } \sigma = \sigma_{s1} / \sigma_{f}, \ (\rho C_{p})_{nf}$$

$$= (1 - \varphi_{1})(\rho C_{p})_{f} + \varphi_{1}(\rho C_{p})_{s1}$$
(10)

#### 2.2.2 Thermophysical correlations of MoS2-Go/ water hybrid nanofluid

The thermophysical correlations of the HNF model used are as follows (Khan et al., 2020c):

$$\rho_{hnf} = (1 - \varphi_2) \Big[ (1 - \varphi_1) \rho_f + \varphi_1 \rho_{s1} \Big] + \varphi_2 \rho_{s2}, \frac{\mu_{hnf}}{\mu_f} \\
= \frac{1}{(1 - \varphi_1)^{2.5} (1 - \varphi_2)^{2.5}}$$
(11)  

$$\frac{k_{hnf}}{k_{bf}} = \Bigg[ \frac{k_{s2} + 2k_{bf} - 2\varphi_2 (k_{bf} - k_{s2})}{k_{s2} + 2k_{bf} + \varphi_2 (k_{bf} - k_{s2})} \Bigg] \text{where} \frac{k_{bf}}{k_f} \\
= \Bigg[ \frac{k_{s1} + 2k_f - 2\varphi_1 (k_f - k_{s1})}{k_{s1} + 2k_f + \varphi_1 (k_f - k_{s1})} \Bigg]$$
(12)



$$\frac{\sigma_{hmf}}{\sigma_{bf}} = \left[\frac{\sigma_{s2} + 2\sigma_{bf} - 2\varphi_2(\sigma_{bf} - \sigma_{s2})}{\sigma_{s2} + 2\sigma_{bf} + \varphi_2(\sigma_{bf} - \sigma_{s2})}\right] \text{where } \frac{\sigma_{bf}}{\sigma_f}$$
$$= \left[\frac{\sigma_{s1} + 2\sigma_f - 2\varphi_1(\sigma_f - \sigma_{s1})}{\sigma_{s1} + 2\sigma_f + \varphi_1(\sigma_f - \sigma_{s1})}\right]$$
(13)
$$\left(\rho C_p\right)_{hmf} = (1 - \varphi_2) \left[(1 - \varphi_1)(\rho C_p)_f + \varphi_1(\rho C_p)_{s1}\right] + \varphi_2(\rho C_p)_{s2}$$
(14)

## 2.3 Similarity transformations

The transformations listed below are utilized to transform the governing equations (Yaseen et al., 2022a):

$$u = rb_{1}f'(\eta), v = rb_{1}g(\eta), w = -2Hb_{1}f(\eta), P$$
  
=  $b_{1}\rho_{hnf}v_{hnf}\left[P(\eta) + \frac{r^{2}\varepsilon}{2H^{2}}\right], \xi = \frac{z}{H}, \theta = \frac{T - T_{H}}{T_{w} - T_{H}}, \phi = \frac{C - C_{H}}{C_{w} - C_{H}}$   
(15)

Eq. 1 is satisfied, and Eqs 2, 3, 4, 5, 6, 7 reduce to

$$Re\frac{\omega_2}{\omega_1}\left(f'^2 - 2ff'' - g^2 + \frac{\omega_3}{\omega_2}Mf' + F^*f'^2\right) + Re\lambda f' = -\varepsilon + f'''$$
(16)

$$g'' - Re\lambda g = Re\frac{\omega_2}{\omega_1} \left( \frac{\omega_3}{\omega_2} gM + gF^* - 2(g'f - f'g) \right)$$
(17)

$$P' + 4\frac{\omega_2}{\omega_1} Reff' + 2f'' = 0$$
 (18)

$$\left(\omega_5 + R_d - \omega_4 \operatorname{PrRe}\tau_E f^2\right)\theta'' + \frac{\operatorname{Re}\omega_5\omega_2}{\omega_1} \left\{A^*f' + B^*\theta\right\}$$
(19)

+ 
$$\omega_4 \operatorname{PrRe}(2f\theta' - \tau_E(ff'\theta')) = 0$$

$$\phi'' = Re\tau_c Sc \left( f f' \phi' + f^2 \phi'' \right) - 2 \text{ReS} c f \phi'$$
(20)

The BCs are obtained as follows:

$$\begin{split} f(\eta) &= 0, f'(\eta) = k_1, g(\eta) = 1, \theta'(\eta) = -\frac{\gamma_1}{\omega_5} (1 - \theta(\eta)), P(\eta) = 0, \phi(\eta) = 1 \text{ at } \eta = 0 \\ f(\eta) &= 0, f'(\eta) = k_2, g(\eta) = \Omega, \theta'(\eta) = -\frac{\gamma_2}{\omega_5} \theta(\eta), \phi(\eta) = 0 \text{ at } \eta = 1 \end{split}$$

$$\end{split}$$

$$(21)$$

In the aforementioned equations, " $Re(=\frac{b_1H^2}{v_f})$  represents In the aforementioned equations,  $Re(-\frac{v_f}{v_f})$  represents Reynold number,  $F^*(=\frac{Fr}{\sqrt{k_{fn}}})$  represents the inertial coefficient,  $Pr(=\frac{v_f}{\alpha_f})$  is the Prandtl number,  $\lambda(=\frac{v_f}{b_k f_{fn}})$  is the porosity parameter,  $M(=\frac{\sigma_f B_0^2}{\rho_f b_1})$  represents the magnetic field parameter,  $A^*$  and  $B^*$  represents heat source/sink parameters,  $R_d(=\frac{16\sigma^*T_{f1}^3}{3k_f k^*})$ represents thermal radiation parameter,  $\tau_E (= 4\gamma_t b_1)$  represents the thermal relaxation parameter,  $\tau_C (= 4\gamma_c b_1)$  represents the solutal relaxation parameter,  $t_C(=\pm \gamma_c o_1)$  represents the solutal relaxation parameter,  $k_1(=\frac{a_1}{b_1})$  and  $k_2(=\frac{a_2}{b_1})$  represent shrinking parameters,  $\Omega(=\frac{b_2}{b_1})$  is the rotation parameter,  $\gamma_1(=\frac{Hh_1}{k_f})$  and  $\gamma_2(=\frac{Hh_2}{k_f})$  are Biot numbers,  $Sc(=\frac{v_f}{D})$  represents Schmidt number and  $\omega_1 = \frac{\mu_f}{\mu_{hnf}}, \omega_2 = \frac{\rho_{hnf}}{\rho_f}, \omega_3 = \frac{\sigma_{hnf}}{\sigma_f}, \omega_4 = \frac{(\rho C_p)_{hnf}}{(\rho C_p)_f}, \omega_5 = \frac{k_{hnf}}{k_f}$  are constants". Eq. 16 is then differentiated w.r.t  $\eta$  for the elimination of  $\varepsilon$ 

(pressure variable), and we get:

Ω	f" (0) (Khan et al., 2018)	f''(0) [present]	-g'(0) (Khan et al., 2018)	-g'(0) [present]
-1	.06666314	.06666303	2.0009522	2.00095213
-0.8	.08394207	.08394201	1.8025885	1.80258846
-0.3	.10395088	.10395088	1.3044236	1.30442355
0	.09997221	.09997221	1.0042776	1.00427756
0.5	.06663419	.06663416	.5026135	.50261344

TABLE 2 The comparison of the values f''(0) and g'(0) for the various value of  $\Omega$  and the rest parameters are, Pr = 6.2,  $\phi_1 = \phi_2 = M = F^* = \lambda = \tau = k_1 = k_2 = \gamma_1 = \gamma_2 = 0$ .













$$\omega_1(f^{i\nu} - \lambda \text{Re}f'') + \omega_2 \text{Re}\left(2ff''' + 2gg' - M\frac{\omega_3}{\omega_2}f'' - 2f'f''F^*\right) = 0$$
(22)

Eqs 16–21 define the  $\varepsilon$  (pressure variable) as follows:

$$\varepsilon = f'''(0) - \operatorname{Re}\frac{\omega_2}{\omega_1} \left( f'(0)^2 - 2f''(0)f(0) - g(0)^2 + F^*f'(0)^2 + \frac{\omega_3}{\omega_2} Mf'(0) \right) - \lambda \operatorname{Re} f'(0)$$
(23)

To solve Eqn. (18) for *P*, use integration from 0 to  $\eta$  and obtain the following form:

$$P = -2\left\{ \left( f' - f'(0) \right) + \frac{\omega_2}{\omega_1} \operatorname{Re}(f)^2 \right\} = 0$$
 (24)



Effect of nanoparticles volume fraction  $\varphi$  on  $f(\eta)$ .



# 3 Engineering parameters

### 3.1 Nusselt numbers

The Nusselt numbers at the lower disk  $(Nu_{r0})$  and upper disk  $(Nu_{r1})$  are (Mabood et al., 2021) and (Yaseen et al., 2022a):

$$Nu_{r0} = -(\omega_4 + R_d)\theta'(0) \text{ and } Nu_{r1} = -(\omega_4 + R_d)\theta'(1)$$
 (24a)

## 3.2 Sherwood numbers

The Sherwood numbers at the lower disk  $(Sh_{r0})$  and upper disk  $(Sh_{r1})$  are defined as (Khan et al., 2020a):











$$Sh_{r0} = -\phi'(0) \text{ and } Sh_{r1} = -\phi'(1)$$
 (25)

## 4 Methodology of numerical approach

This section focuses on the methodology used for deducing solutions as well as code validation. The equations are at first modeled as PDEs and later, converted into ODEs *via* similarity variables. The numerical solution of the Eqs 16, 17, 18, 19, 20 along with BCs (21) is deduced with the "bvp4c function" (a built-in package in MATLAB), the more specific details of the bvp4c function can be referred from the Shampine et al. (2003). The "bvp4c function" uses a finite difference scheme together with a precision of fourth order with the help of the "3-stage Lobatto IIIA formula". To deduce the solution of the model, the ODEs obtained after similarity transformation are reduced into first-order ODEs by the following substitution:

Utilizing the new variables, the Eqs 16, 17, 18, 19, 20 are reduced to first-order ODEs and the following MATLAB syntax is used:

$$\begin{pmatrix} yy_{1} \\ yy_{2} \\ yy_{3} \\ yy_{4} \end{pmatrix} = \begin{pmatrix} Re\frac{\omega_{2}}{\omega_{1}} \left( -2y_{1}y_{4} - 2y_{5}y_{6} + \frac{\omega_{3}}{\omega_{2}}My_{3} + 2F^{*}y_{2}y_{3} \right) + \lambda Rey_{3}; \\ Re\frac{\omega_{2}}{\omega_{1}} \left( -2y_{1}y_{4} - 2y_{5}y_{6} + \frac{\omega_{3}}{\omega_{2}}My_{3} + 2F^{*}y_{2}y_{3} \right); \\ Re\frac{\omega_{5}\omega_{2}}{\omega_{1}} \left( A_{1}y_{2} + B_{1}y_{7} \right) + \omega_{4}PrRe\left( 2y_{1}y_{8} - \tau_{E}y_{1}y_{2}y_{8} \right) \\ - \frac{Re\frac{\omega_{5}\omega_{2}}{\omega_{1}} \left( A_{1}y_{2} + B_{1}y_{7} \right) + \omega_{4}PrRe\left( 2y_{1}y_{8} - \tau_{E}y_{1}y_{2}y_{8} \right)}{\omega_{4} + R_{d} - \omega_{3}\tau_{E}PrRey_{1}^{2}}; \\ \frac{Re\tau_{c}Sc \times y_{1}y_{2}y_{10} - 2ReScy_{1}y_{10}}{1 - Re\tau_{c}Scy_{1}^{2}}; \end{pmatrix}$$
(27)









The above system Eq. 27 is subjected to the following BCs at the lower disk ( $\eta = 0$ ) and upper disk ( $\eta = 1$ ):

$$y_{1} = 0, y_{2} = k_{1}, y_{5} = 1, y_{8} = -\frac{\gamma_{1}}{\omega_{5}} (1 - y_{7}), y_{9} = 1 \text{ at } \eta = 0$$
  

$$y_{1} = 0, y_{2} = k_{2}, y_{5} = \Omega, y_{8} = -\frac{\gamma_{2}}{\omega_{5}} y_{7}, y_{9} = 0 \text{ at } \eta = 1$$

$$(28)$$

From new variables in Eq. 26 and BCs Eq. 28, it is seen that the following conditions at the ( $\eta = 0$ ) and ( $\eta = 1$ ) are missing:

 $y_3(0), y_3(1), y_4(0), y_4(1), y_6(0), y_6(1), y_7(0), y_7(1), y_{10}(0), and y_{10}(1)$ (29)

Furthermore, the values of missing conditions are guessed to initiate the process of finding the solution and other parameters present in the Eqs 27, 28 are set to find the desired solution. The process of iteration is repeated and the solution is accepted only when the conditions in Eq. 28 are satisfied. The process of finding the solution is shown *via* a flow chart in Figure 2. To validate the model and the code used to find the numerical solution, an assessment in Table 2 is outlined with the published computations of (Khan et al., 2018) study as a limiting case to validate the numerical code utilized to solve the current model. The comparative results are quite consistent, ensuring that the current conclusions are valid.

## 5 Results and discussion

This section focuses on the numerical outcomes and graphical and tabular results are interpreted physically. Authors have used





### 5.1 Velocity distribution

Figures 3, 4, 5, 6, 7, 8, 9, 10, 11 show the fluctuation of dimensionless velocity against the similarity variable while altering distinct flow-regulating parameters one at a time while leaving others unchanged. Figures 3, 4, 5 depict the influence of porosity parameter  $\lambda$ on axial velocity distribution  $f(\eta)$ , radial velocity distribution  $f'(\eta)$ , and tangential velocity distribution  $g(\eta)$ , respectively. Within the core areas of the boundary layer region (BLR), there is a noticeable decrease in the axial velocity distribution  $f(\eta)$  and tangential velocity distribution  $g(\eta)$  with growing values of  $\lambda$ . The radial velocity shows transitioning nature in BLR and the transition point lies near  $\eta \sim 0.5$ .  $f'(\eta)$  rises near the lower disk and behavior changes near the upper disk w.r.t to growing values of  $\lambda$ . Physically, the porosity parameter is linked to the friction force. Resistance increases with a rise in the porosity parameter, and therefore the velocity falls. Figures 6, 7, 8 elucidate the effectiveness of magnetic parameter *M* on  $f(\eta)$ ,  $f'(\eta)$  and  $g(\eta)$ . The increasing magnitude of



parameter *M* is responsible for the decrease in velocity  $f(\eta)$  and  $g(\eta)$ . The radial velocity  $f'(\eta)$  shows transitioning nature in BLR w.r.t parameter *M*. The decrease in the velocity  $f(\eta)$  and  $g(\eta)$  is related to the generation of Lorentz force. The presence of magnetic force generates the Lorentz force opposite to the flow direction, hence it opposes the motion, and hence velocity decreases.

Figures 9, 10, 11 elucidate the effectiveness of volume fraction on velocity distribution. On increasing the volume fraction of each nanoparticle Go ( $\varphi_1$ ), and MoS<sub>2</sub> ( $\varphi_2$ ) in equal quantity ( $\varphi$ ), the axial velocity  $f(\eta)$  decreases and tangential velocity  $g(\eta)$  increases, whereas radial velocity  $f'(\eta)$  shows transitioning nature in BLR, i.e., it first decreases and then increases. The increasing nanoparticles volume fraction in the base fluid causes the hindrance for the motion in the axial direction, hence the velocity  $f(\eta)$  decreases. On contrary, the tangential velocity  $g(\eta)$  increases, because the addition of nanoparticles causes the outward movement of fluid. In Figures 3, 4, 5, 6, 7, 8, 9, 10, 11, the authors have presented a comparison in velocity profiles of HNF (MoS2-Go/water flow) and NF (Go/water flow). HNF is seen to have the higher axial velocity  $f(\eta)$ and NF has the higher tangential velocity  $g(\eta)$ . Near the lower disk, HNF has a higher radial velocity, but as fluid approaches the upper disk, NF has a higher radial velocity.

#### 5.2 Temperature distribution

Figures 12, 13, 14, 15, 16, 17 show the fluctuation of dimensionless temperature  $\theta(\eta)$  against the similarity variable while altering distinct flow-regulating parameters one at a time while leaving others unchanged. Figures 12, 13, 14 depict the influence of porosity parameter  $\lambda$ , magnetic parameter M, and radiation parameter  $R_d$  on the temperature profile. It is observed that with an increment in the aforesaid parameters, the temperature  $\theta(\eta)$  falls near the lower disk and rises near the upper disk. The effect of resistance forces due to the porosity parameter and the effect of generated Lorentz force due to the magnetic field is significant near



A* B*	B*	R <sub>d</sub>	$ au_E$	$ au_C$	Sc	$oldsymbol{\phi}_1$	$\phi_2$	Hybrid nanofluid			Nanofluid				
								Lower disk Upper disk		Lower disk		Upper disk			
								Nu <sub>r0</sub>	$Sh_{r0}$	$Nu_{r1}$	$Sh_{r1}$	Nu <sub>r0</sub>	$Sh_{r0}$	$Nu_{r1}$	$Sh_{r1}$
-1	-2	0.2	1	10	300	.03	.03	.057107		.000849		.057708		.000970	
-0.6	-1.6							.056925		.001055		.057502		.001219	
-0.2	-1.2							.056643		.001438		.057182		.001672	
2	3							.057153		00352		.057958		00365	
2.4	3.4							.056760		00413		.057598		00416	
2.8	3.8							.056207		00510		.057123		00495	
3	4	0.2						.056731	1.362876	00421	.2360413	.056977	1.362876	00519	.2360413
		0.6						.073872		00424		.075884		00489	
		1						.090865		00484		.094490		00551	
		0.2	41					.055367		00667		.056418		00622	
			81					.054603		00814		.055761		00745	
			161					.047451		02197		.049522		01933	
			1	40					1.372419		.1824050		1.349601		.1897056
				100					1.409904		.0722179		1.383349		.0796101
				10	100				1.149931		.6515081		1.142216		.6562210
					200				1.272361		.4019200		1.257269		.4086483
					500				1.455823		.0718406		1.424433		.0758839
					300	.09	.09	.054332	1.301495	00389	.256299	.056149	1.272015	00399	.266096
						.15	.15	.053425	1.211009	00234	.288401	.0555	1.202725	00297	.291286
						.21	.21	.052689	1.107517	00143	.329396	.054883	1.134009	00227	.31828

the upper disk, which opposes the motion of the flow and increases friction. As a result, the temperature rises near the upper disk with increasing porosity parameter  $\lambda$  and magnetic parameter M. Figure depicts that augmenting parameter  $R_d$  causes the temperature to decrease first, then after a transition point, it increases. This means that near the upper disk, the heat carried by radiation supplies energy to the particles, increasing their kinetic energy and velocity, and causing an increase in the temperature.

Figure 15 depicts that an increase in the thermal relaxation parameter  $\tau_E$  lead the temperature  $\theta(\eta)$  to rise near the lower disk but for the same, the temperature falls near the upper disk. The nonzero thermal relaxation parameter  $\tau_E$  denotes time lag during heat transfer. For the zero value of  $\tau_E$ , the heat transfer is governed by Fourier's law. The results depict that near the lower disk the more time lag in heat transfer implies higher temperature but the same condition near the upper disk relates to the lower temperature. Figure 16 elucidates the effectiveness of volume fraction on temperature  $\theta(\eta)$ . On increasing the volume fraction of each nanoparticle Go ( $\varphi_1$ ), and  $MoS_2(\varphi_2)$  in equal quantity  $(\varphi)$ , the temperature falls near the lower disk and surges near the upper one. The rise in the temperature near the upper disk can be attributed to the enhancement in the thermal conduction of the HNF or NF due to an increase in the nanoparticles in the base fluid. Figure 17 depicts that for the case of heat source  $(A^* > 0, B^* > 0)$ , the temperature  $\theta(\eta)$  shows transitioning nature in BLR. Temperature first increases then decreases for increasing  $A^*$  and  $B^*(A^*>0, B^*>0)$ . Whereas, for the case of the heat sink  $(A^* < 0, B^* < 0)$ , the temperature increases for increasing magnitude of heat sink parameters. In Figures 12, 13, 14, 15, 16, 17, the authors have presented a comparison of temperature profiles of HNF (MoS<sub>2</sub>-Go/water flow) and NF (Go/water flow). Near the lower disk, HNF has a higher thermal profile  $\theta(\eta)$ , but as fluid approaches the upper disk, NF has a higher thermal profile  $\theta(\eta)$ .

### 5.3 Nanoparticle concentration distribution

Figures 18, 19, 20 show the fluctuation of dimensionless concentration of nanoparticles against the similarity variable while altering distinct flow regulating parameters one at a time while leaving others unchanged. Figures 18, 19 depict the influence of the solutal relaxation parameter  $\tau_C$  and Schmidt number Sc on the concentration  $\phi(\eta)$ . Figure 18 depicts that increasing values of the solutal relaxation parameter  $\tau_C$  leads concentration to fall. The non-zero values of the solutal relaxation parameter  $\tau_C$  denote the presence of time lag during mass transfer. The increasing time lag during mass transfer has an adverse effect on concentration. The increasing time lag during mass transfer leads to a fall in the concentration profile. Figure 19 depicts that increasing values of Sc cause concentration to fall. The concentration decreases as Sc increases. The Schmidt number is an important parameter to consider as it physically connects the depths of the hydrodynamic layer and the mass transfer boundary layer. The momentum diffusion of particles in fluid increases as the strength of the Schmidt number increases in fluid flow. As a result, concentration falls. Figure 20 depicts that on increasing the volume fraction of each nanoparticle Go ( $\varphi_1$ ), and MoS<sub>2</sub> ( $\varphi_2$ ) in equal quantity ( $\varphi$ ), the concentration falls. The reason for this behavior can be attributed to the fact the mixing of more nanoparticles causes the HNF or NF to be more viscous and flow is resisted, hence the concentration of NPs falls. In Figures 18, 19, 20, the authors have presented a comparison in concentration profiles of HNF (MoS<sub>2</sub>-Go/water flow) and NF (Go/ water flow). It is seen that NF has a higher concentration profile  $\phi(\eta)$  as compared to HNF.

#### 5.4 Streamlines and engineering parameters

Figure 21 visualizes the streamlines pattern of HNF (MoS<sub>2</sub>-Go/water flow) and NF (Go/water flow). The streamlines represent the movement of the suspended particles in the stream and which are driven by it. The direction of velocity at each point in the streamline is given by the tangent at that location. The denser streamlines indicate that the fluid velocity is greater than when it is open out. The HNF is seen to have slightly less dense streamlines in the present case which means more nanoparticles cause fluid to be more viscous and flow is resisted.

Table 3 elucidates the effectiveness of pertinent parameters on the Nusselt and Sherwood number. Nusselt number corresponds to the heat transmission rate (HTR) and the Sherwood number corresponds to the mass transmission rate (MTR) in the BLR at both disks. At the higher magnitude of the heat sink parameter, the HTR rises for HNF and NF at the lower disk but contrary behavior is seen at the upper disk. Whereas, the HTR decreases for HNF and NF at both the upper and lower disk. At the higher values of radiation parameter  $R_d$ , HTR increases at the lower disk and decreases at the upper disk. An increase in the volume fraction of each nanoparticle *Go* ( $\varphi_1$ ), and MoS<sub>2</sub> ( $\varphi_2$ ) in equal quantity ( $\varphi$ ) enhances the thermal conductivity of the THNF due to an increase in the nanoparticles in the base fluid. The rising thermal conductivity enhances the MTR and HTR at the upper disk. It is also observed that at the higher values of the thermal relaxation parameter  $\tau_E$ , HTR reduces at both disks. The non-zero values of the thermal relaxation parameter  $\tau_E$  denote the time lag during heat transfer. Thus on augmenting  $\tau_E$ , HTR at both disks reduces. Moreover, on increasing the magnitude of the Schmidt number Sc and solutal relaxation parameter  $\tau_c$ , the MTR reduces at upper disks, whereas, on increasing the magnitude of the same parameters, the MTR rises at the lower disk.

## 6 Conclusion

The current problem concerns the influence of a non-uniform heat source/sink in the flow of a HNF ( $MoS_2$ -Go/water flow) and NF (Go/water flow) between two parallel and infinite spinning disks with the Cattaneo-Christov model in a porous medium in the presence of the magnetic field, and radiation. The numerical solution is deduced by employing the "bvp4c" function in MATLAB. Some vital conclusions are listed below.

- Radial velocity shows decreasing behavior near the lower disk and increasing behavior near the upper disk for increasing values of porosity parameter, magnetic parameter, and nanoparticles volume fraction.
- The heat transmission and mass transmission rate is higher at the lower disk.
- A higher magnitude of the heat sink parameter causes the rate of heat transmission to rise at the lower disk.
- The increase in nanoparticle volume fraction causes an enhancement in the rate of heat transmission at the upper

disk and the time lag during heat transfer is negatively correlated with the heat transmission rate at both disks.

• The combination of heat sink parameter and thermal relxation parameter can be used to modulate the heat trnamission rate at the surface.

## 6.1 Future scope of research

The present study discuss the flow of nanofluid and hybrid nanofluid without the nanoparticle aggregation effect. The study can de extended with proper modeling of fluid flow by utilization of validated thermophysical correlations for nanoparticle aggregation effect.

## Data availability statement

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

## Author contributions

SR and MY: Conceptualization, methodology, software, formal analysis, writing-original draft. MK and SE: Writing-original draft, data curation, investigation, visualization, validation. UK: Conceptualization, writing-original draft, writing-review and editing, supervision, resources. AA: Validation, investigation, writing-review and editing, formal analysis. AG: Writing-review

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## Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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## Nomenclature

## Alphabetical Symbols

A\*, B\* Heat source/sink parameter  $a_1$  shrinkage rate of the lower disk  $a_2$  shrinkage rate of the upper disk  $b_1$  angular velocity of the lower disk  $b_2$  angular velocity of the upper disk Bo Magnetic field strength C Nanoparticles concentration Cw Nanoparticles concentration at lower disk C<sub>H</sub> Nanoparticles concentration at the upper disk  $C_p$  Heat capacity **D** Diffusion coefficient F Forchheimer coefficient  $F^{\star}$  inertial coefficient f Axial velocity f' Radial velocity  $h_1$  heat transfer coefficient of hot liquid at lower plate  $h_2$  heat transfer coefficients of hot liquid at the upper plate H Distance between disks g Tangential velocity k Thermal conductivity  $k^*$  Mean absorption coefficient  $k_{fh}$  Permeability of the porous medium  $k_1$ ,  $k_2$  Shrinking parameters M Magnetic field parameter  $Nu_{ro}$ ,  $Nu_{r1}$  Nusselt numbers **p** Pressure Pr Prandtl number (q''') Non-uniform heat source/sink term  $R_d$  Radiation parameter Re Reynolds number Sh<sub>ro</sub>, Sh<sub>r1</sub> Sherwood numbers Sc Schmidt number T Temperature  $T_w$  Temperature of hot liquid at lower disk  $T_H$  Temperature of hot liquid at lower disk (*u*, *v*, *w*) Components of velocity  $(r, \theta, z)$  cylindrical coordinate system

# Greek Symbols

 $\Omega$  Rotation parameter  $\lambda$  Porosity parameter  $\gamma_t$  Thermal relaxation time  $\gamma_c$  Solutal relaxation time  $y_1, y_2$  Biot numbers  $\tau_E$  thermal relaxation parameter  $\tau_c$  solutal relaxation parameter  $\phi$  Dimensionless concentration  $\varphi_1$  Volume fraction of Go nanoparticles  $\varphi_2$  Volume fraction of  $MoS_2$  nanoparticles  $\Theta$  Dimensionless temperature  $\mu$  Dynamic viscosity  $\varepsilon$  Pressure variable  $\rho$  Density  $\sigma^*$  Stefan–Boltzmann constant  $\sigma$  Electrical conductivity  $\boldsymbol{\xi}$  Similarity variable  $\omega_i$  (*i* = 1 – 5) Constant

## Subscripts

bf, f Base fluidnf Nanofluidhnf Hybrid nanofluid

## Superscripts

' Derivative w. r. to  $\eta$ 

## Abbreviations

NPs Nanoparticles NFs Nanofluids HNFs Hybrid Nanofluids HTR Heat transmission rate CCM Cattaneo-Christov model MTR Mass transmission rate BLR Boundary layer region MoS<sub>2</sub> Molybdenum disulfide Go Graphene oxide