INORGANIC MATERIALS FOR ENERGY AND ENVIRONMENTAL CATALYSIS

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INORGANIC MATERIALS FOR ENERGY AND ENVIRONMENTAL CATALYSIS

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Editorial: Inorganic materials for energy and environmental applications

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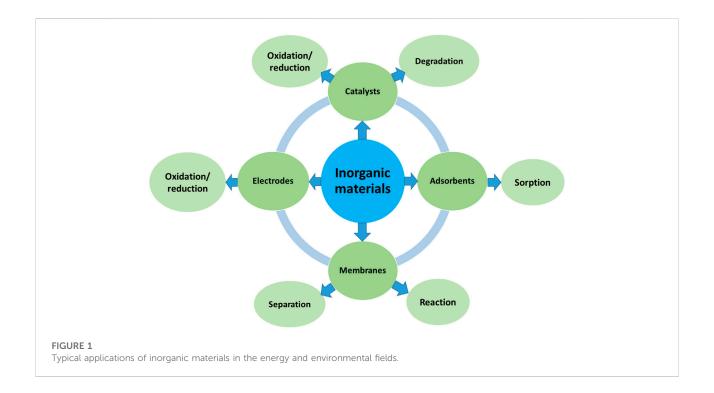
Editorial on the ResearchTopic

Inorganic materials for energy andenvironmental applications

Inorganic materials have played significant roles in both energy conversion and environmental decontamination, relevant to chemical and environmental engineering. These inorganic materials are diverse, such as metals, metal oxides, nonmetallic oxides, sulphides, nitrides, phosphides and haloids. Inorganic materials often have high thermal stabilities, unique physicochemical properties and diverse nanostructures, making them highly desirable in various heterogeneous adsorption and catalytic applications (Goodman et al., 2020). As a result, they have been widely used as heterogeneous catalysts and/or adsorbents for CO₂ conversion, fuel production, pollutant degradation or adsorption (He et al., 2020; Yang et al., 2021). Figure 1 summarizes the typical applications of inorganic materials in the energy and environmental fields, including as catalysts (Kuang et al., 2020), electrodes (Li et al., 2020), adsorbents (Zito and Shipley, 2015) and membranes (Song et al., 2016) for energy conversion via oxidation/reduction, or environmental decontamination via adsorption, rejection, oxidation or reduction (Zeng et al., 2020; Xu et al., 2021).

Numerous metals and metal oxides have been employed as electro- or photo-catalysts for energy conversion and pollutant degradation. Qi et al. developed a porous ${\rm Ti_4O_7}$ electrocatalytic membrane by employing Ti powder as the reducing agent to thermally reduce ${\rm TiO_2}$ in vacuum. The prepared electrocatalytic membrane showed a high oxygen evolution potential (~2.7 V/SHE). Wang et al. develop a new iron cathode electro-Fenton process coupled with a pH-regulation divided electrolysis cell for p-nitrophenol degradation. In the electrochemical Fenton system, an iron plate was used as the cathode to inhibit the release of iron ions and promote the reduction of ${\rm Fe^{3+}}$ to ${\rm Fe^{2+}}$. Therefore, excellent electrocatalytic degradation performance towards organic pollutants was achieved. Wang and Wang synthesized a NiO modified BiVO₄ nanocomposite by a hydrothermal and calcination method. The as-prepared nanocomposite showed enhanced photoelectrochemical performance due to the unique NiO lamellar structure that provided a large number of active sites.

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Wang et al. used a sol-gel self-combustion method to prepare carboxylate-rich carbon-modified Fe₃O₄ magnetic catalysts for heterogeneous Fenton degradation of organic pollutants. The prepared Fe₃O₄-based catalysts displayed improved heterogeneous Fenton degradation performance due to the enhanced pollutant adsorption. Zhu et al. synthesized a CdS/microcrystalline cellulose nanocomposite photocatalyst using an ultrasonic-assisted method. The prepared nanocomposite photocatalyst displayed enhanced pollutant degradation performance under visible light due to the heterojunction formation that efficiently separates the photogenerated electrons and holes of the photocatalyst. Wang et al. prepared a Co₃O₄/Ti cathode by electrodeposition for electrocatalytic reduction of nitrate, in which the NO₃⁻ was reduced to N₂ and NH₄⁺ by the catalysis of Co₃O₄/Ti, and then NH₄⁺ was selectively oxidized into N₂ assisted by chloride ions and using IrO2-RuO2/Ti as the anode. Qiu et al. prepared Pt-modified TiO2 nanotubes as catalysts for photocatalytic degradation of Rhodamine B (RhB) under UV light. It was reported that the superoxide radical anions (O_2^{-}) , photogenerated hole (h+) and hydroxyl radical (OH-) were the main active species contributing for RhB degradation.

In addition, metal and metal oxide based or modified materials have also been used for other catalytic applications. Bai et al. reported the Fischer–Tropsch synthesis performance of Co-based catalysts supported on graphitized ordered mesoporous carbon. The high catalytic performance resulted from the highly crystallized graphitic structure of the mesoporous carbon and the uniform dispersion of CoO on the support. Dai et al. used ion-exchange, *in situ* modification and complexation-excessive impregnation modification methods to modify SAPO-11 molecular sieves with

Ni. The Ni-modified SAPO-11 molecular sieves were supported by NiWS catalysts for hydroisomerization of n-Hexadecane. The complexation-excessive impregnation modification method led to the best hydroisomerization performance. Huang et al. studied the effect of $\rm Ga_2O_3$ on the hydrodesulfurization performance of 4,6-dimethyldibenzothiophene catalyzed by the stepwise impregnation method. $\rm Ga_2O_3$ promoted Ni and Mo species to disperse uniformly and doping of more Ni atoms into the $\rm MoS_2$ crystals, increasing the average stacking number and the length of $\rm MoS_2$. As a result, enhanced hydrodesulfurization performance was achieved due to the formation of more NiMoS active phases in the system.

Adsorption is a simple but effective way for environmental decontamination (Zhang et al., 2018; Samadi et al., 2021). Various inorganic materials have been used for contaminant removal by adsorption. Zhang et al. prepared a series of nanostructured Fe-Cu binary oxides for arsenic removal. The crystallinity and structure of the Fe-Cu binary oxides had a significant impact on the arsenic adsorption performance. The oxides with lower crystallinity showed higher surface hydroxyl density and better adsorption performance. Li et al. reviewed the preparation, classification and applications of templated materials, particularly adsorbents in wastewater treatment. The templating method can endow materials with high specific area and unique porous structures, thereby enhancing the material sorption performance towards aqueous pollutants. Wei et al. reviewed the composite adsorbents for fluoride removal, including the adsorbent types (i.e., metal biopolymers, carbon-based, and others), oxides/hydroxides, preparation sorption performance. The adsorption mechanisms for fluoride removal involving electrostatic

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attraction, ion exchange, complexation, and hydrogen bonding were also discussed.

Recently, with the promotion of the circular economy, waste based materials have attracted growing interest for various applications, such as fertilizers (Ye et al., 2019), carbon capture (Ji et al., 2018), membrane separation (Ni et al., 2022). Yu et al. prepared new biochar from excess sludge, followed by acetic acid modification. The modified sludgebiochar displayed improved porosity enriched-COOH functional groups, thereby enhancing its adsorption performance to uranium. However, the catalytic performance of the sorbent was not discussed. Zeng et al. fabricated porous glass-ceramics based on coal fly ash without using pore forming agents by direct overfiring, in which borax was used to destroy the structure of quartz and amorphous vitreous body in coal fly ash and thus reduce the sintering temperature by the B-O bond. Chen et al. fabricated a nonsintered ceramsite from pyrite tailings for phosphorus removal. Both Plackett-Burman Design (PBD) and Box-Behnken Design (BBD) based response surface methodology were used to optimize the fabrication parameters.

Cellulase plays a key role in the production of fuel ethanol by enzymatic hydrolysis of lignocellulose, and immobilization of cellulase on the nanocarriers is an effective way to improve the hydrolysis efficiency. Wang et al. reviewed the significant roles of surfactants in oriented immobilization of cellulase on nanocarriers as well as a surfactant reversed micelle system.

In summary, this Research Topic discussed various inorganic materials as catalysts or adsorbents with unique nanostructures and functionalities for energy conversion and environmental decontamination. In the future, inorganic materials will continue to play a vital role in addressing global energy and environmental challenges, such as climate change, energy shortages and environmental pollution. Engineering new high performance heterogeneous catalysts and understanding the limiting factors and their mechanisms in the catalytic reaction are two key research directions that should be paid more attention to.

Author contributions

SZ, QZ and C-CW contributed to the writing of this editorial.

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Efficient Sorption of Arsenic on Nanostructured Fe-Cu Binary Oxides: Influence of Structure and Crystallinity

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To study the structure-performance relationship, a series of nanostructured Fe-Cu binary oxides (FCBOs) were prepared by varying synthesis conditions. The obtained binary oxides were well characterized using X-ray diffraction (XRD), transmission electron microscope (TEM), Brunner-Emmet-Teller (BET), magnetic and Zeta potential measurement techniques. Both As(V) and As(III) sorption on the FCBOs were evaluated by batch tests. Results show that the surface structure and crystallinity of FCBOs are greatly dependent on preparation conditions. The crystallinity of FCBOs gradually increases as the synthesis pH value increasing from 9.0 to 13.0, from amorphous phase to well-crystalline one. Simultaneously, the morphology change of FCBOs from irregular agglomerate to relatively uniform polyhedron has been observed. The sorption of arsenic is greatly influenced by the crystallinity and structure of FCBOs. decreasing with increasing degree of crystallinity. The amorphous FCBO has higher surface hydroxyl density than well-crystalline one, which might be the reason of higher sorption performance. As(V) is sorbed by the FCBOs via formation of inner-sphere surface complexes and As(III) is sorbed through formation of both inner- and outer-sphere surface complexes. This investigation provides new insights into structure-performance relationship of the FCBO system, which are beneficial to develop new and efficient sorbents.

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INTRODUCTION

Arsenic contamination has emerged as one of global environmental issues in the last decades due to its high toxicity (Smedley and Kinniburgh, 2002). In natural waters, arsenic exists mainly in two inorganic forms as arsenate [As(V)] and arsenite [As(III)]. In view of the serious adverse effects of arsenic, a number of treatment techniques such as coagulation/precipitation, ion exchange, adsorption, membrane filtration and biological treatment, have been exploited for arsenic removal from drinking water and wastewater. Among them, adsorption is commonly and extensively used, due to its simplicity in operation, high efficiency and cost-effectiveness (Mohan and Pittman, 2007; Hu et al., 2015). Various adsorbents have been developed and used for arsenic removal (Mohan and Pittman, 2007). Recently, metal (hydr)oxides such as Fe (hydr)oxides (Sowers et al., 2017; Usman et al., 2020), feroxyhyte (Usman et al., 2021), Al oxides (Han et al., 2013; Mertens et al., 2016), TiO₂ (Guan et al., 2012; Yan et al., 2015), ZrO₂ (Hristovski et al., 2008; Cui et al., 2012; Shehzad et al., 2019), CeO₂ (Srivastava, 2010; Li et al., 2012), CuO

(Martinson and Reddy, 2009; Yu et al., 2012; Reddy et al., 2013) etc., have attracted considerable attention because they exhibit strong sorption properties towards arsenic.

More recently, composite sorbents containing two or more metal oxides have been emphasized for their enhanced sorption performance and synergistic effect. For example, an Fe-Mn binary oxide prepared by Zhang and coworkers demonstrates a greater enhancement in both As(V) and As(III) removal (Zhang et al., 2014); amorphous Fe-Ti bimetal oxides synthesized by Rao and coworkers have higher performance in both As(V) and As(III) removal than pure component oxides (Rao et al., 2015); a Ce-Mn binary oxide synthesized by Chen and coworkers exhibits higher arsenic removal efficiency than parent oxides (Chen et al., 2018); an Fe-Ni-Mn trimetal oxide reported by Nasir and coworkers is found to be efficient for As(III) removal (Nasir et al., 2018); an Fe-Cu-Mn trimetal oxide fabricated by Zhang and coworkers displays high sorption capacity for both As(V) and As(III) (Zhang et al., 2020).

Many literatures demonstrated that the sorption ability of metal oxides was strongly affected by their structure and crystallinity. Therefore, it is very necessary to study systemically the structureperformance relationship of synthesized metal oxides. Some researchers have investigated this relationship of single metal oxide system (Jegadeesan et al., 2010; Dou et al., 2016). However, very few researches have been done about binary metal oxide systems (Dou et al., 2018). In our previous study, a novel amorphous Fe (III)-Cu (II) binary oxide prepared with a Cu/Fe molar ratio of 1:2 was found to have high sorption ability towards arsenic (Zhang G et al., 2013). Moreover, it was superior to its parent components (ferrihydrite and cupric oxide) and crystalline CuFe₂O₄ (Tu et al., 2012; Wei et al., 2019). This Fe(III)-Cu(II) binary oxide system is very interesting because it can exist as a pure compound of CuFe₂O₄ or a mixture of ferrihydrite and cupric (hydr)oxide, depending on preparation conditions (Tu et al., 2012; Zhang G et al., 2013), which is very different from other binary systems (Zhang et al., 2014; Rao et al., 2015). Therefore, to investigate the structure-performance relationship of Fe(III)-Cu(II) binary oxide system is very vital, which will facilitate further understanding the arsenic sorption behaviors on binary oxide system and developing new composite adsorbents. To our best knowledge, until now, no information about the structure-performance relationship of Fe (III)-Cu (II) binary oxide is available in literatures.

Therefore, the main objectives of this study are 1) to synthesize a series of Fe-Cu binary oxides with different structure and crystallinity degree by varying the synthesis solution pH; 2) to characterize the morphology and crystallinity of as-synthesized binary oxides using a variety of techniques; 3) to evaluate the arsenic adsorption behavior and performance of binary oxides by batch tests; and finally 4) to investigate the structure-performance relationship of Fe-Cu binary oxide system.

MATERIALS AND METHODS

Materials

Analytical grade chemicals including FeCl₃.6H₂O, CuSO₄.5H₂O and NaOH were purchased from Sinopharm Chemical Reagent Beijing Co., Ltd. (Beijing, China). They were directly used and no

further purification was done. As (V) and As (III) stock solutions were prepared with deionized water using $Na_2HAsO_4.7H_2O$ and $NaAsO_2$, respectively. Arsenic working solutions were freshly prepared by diluting stock solutions with deionized water. Glass vessels were used as reactors. Before use, reactors were firstly cleaned using $1\%\ HNO_3$ solution and then washed several times with deionized water.

Preparation of Fe-Cu Binary Oxides (FCBOs)

A series of FCBOs with a Fe/Cu molar ratio of 2:1 were prepared at different pHs, according to a slightly modified method described by Zhang G et al. (2013). Specifically, about 10.8 g ferric chloride hexahydrate (FeCl₃.6H₂O) and 5.0 g copper (II) sulfate pentahydrate (CuSO₄.5H₂O) were dissolved in 400 ml deionized water. Under vigorous mechanical-stirring, NaOH solution (3 M) was added dropwise to raise the pH of mixture to a predetermined value (9.0 or 11.0 or 12.0 or 13.0). The formed suspensions were continuously stirred for 0.5 h, aged at 100°C for 6 h using a hot water bath. After cooling, the prepared suspensions were washed several times with distilled water. Afterwards, they were treated by filtration and dried at 55°C for about 24 h. The dried FCBOs were crushed into fine powders $(0.5-50 \mu m)$ and stored in a desiccator. According to the synthesis pH value, these FCBOs are denoted as FC1, FC2, FC3, and FC4, respectively.

Characterization of FCBOs

X-ray diffraction analyses were performed on a Rigaku D/Max-3A diffractometer using Ni-filtered copper Kα one radiation (XRD, Rigaku, Japan). The morphology of FCBOs was analyzed using a transmission electron microscope (TEM, Hitachi H-800, Japan). Specific saturation magnetization (M_s) and magnetization remanence (M_r) measure of particles' magnetism, was determined using vibrating sample magnetometer at room temperature (VSM, Model 7,307 Lakeshore, United States). Specific surface area was determined by nitrogen adsorption (BET-method) using a area surface analyzer (Nova 2000e; Quantachrome Instruments, United States). A zeta potential analyzer (Zatasizer 2000; Malvern, UK) was used to analyze zeta potential of the FCBOs.

The density of surface hydroxyl sites was determined by a surface titration method (Dou et al., 2016). Fe-Cu binary oxide (0.3000 g) was added into 50 ml of 0.05 mol/L NaOH solution. Its accurate molar concentration was titrated using a 0.0500 mol/L Na₂CO₃ solution-calibrated HCl solution (0.0502 mol/L). After 4 h shaking at 130 rpm with the temperature maintained at 25°C, the mixture solution was passed through a 0.45 μm membrane. The filtrate was titrated using the HCl solution and residual NaOH in it was neutralized until pH up to 7.0, then the amount of surface hydroxyl can be calculated based on the amount of NaOH consumed.

Batch Sorption Experiments

A series of batch experiments were performed to investigate the sorption of arsenic on FCBOs. A certain amount of FCBO was put

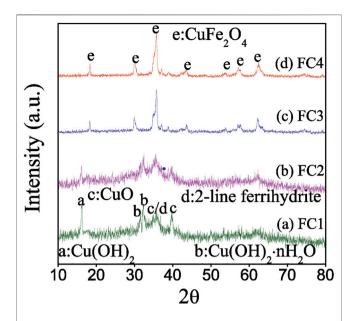


FIGURE 1 | X-ray diffraction patterns of the Fe-Cu binary oxides: (a) FC1, (b) FC2, (c) FC3 and (d) FC4. (a: $Cu(OH)_2$, b: $Cu(OH)_2$ - nH_2O , c: CuO, d: 2-line ferrihydrite and e: $CuFe_2O_4$).

into 100 ml glass vessels containing 50 ml arsenic solution of different concentrations. The vessels were then oscillated on a shaker at 170 rpm for 24 h. After reaction, all samples collected were filtrated using 0.45 μ m membrane and then were analyzed for arsenic. More detailed description of sorption experiments can be seen in the Supplementary Material.

Analytical Methods

Prior to arsenic analysis, the aqueous samples were diluted to a concentration below $100 \,\mu\text{g/L}$, acidified with concentrated HNO₃, and stored in acid-washed glass vessels. Arsenic concentration was determined using an inductively coupled plasma mass spectrometry machine (ICP-MS, ELAN DRC II, Perkin Elmer Co. United States).

RESULTS AND DISCUSSION

Properties of the FCBOs

X-ray diffraction patterns of the as-prepared FCBOs are presented in **Figure 1**. For FC1, five broad peaks at approximately 16.2, 31.7, 32.3, 35.8 and 39.8° are observed. The characteristic peak at 16.2° belongs to the copper hydroxide (Cu(OH)₂) (JCPDS 80-0656); the peaks at 31.7 and 32.3° are attributed to the hydrated copper hydroxide (Cu(OH)₂·nH₂O) (JCPDS: 42-0638); the peak at 35.8° might be ascribed to both copper oxide (CuO) (JCPDS: 45-0937) and 2-line ferrihydrite formation (Hofmann et al., 2004); the peak at 39.8° might belong to the CuO (JCPDS: 45-0937). Obviously, the FC1 exists mainly as an amorphous mixture of 2-line ferrihydrite and copper (hydr)oxides. The X-ray diffraction pattern of FC2 is closely similar to that of FC1. However, the intensity of peaks belonging to copper hydrated hydroxide, hydroxide and oxide decreases with an

increase in synthesis pH value. When the synthesis pH reaches 12.0 (FC3), these peaks disappear almost completely, and new diffraction peaks appear at 18.3, 30.0, 35.8, 43.6, 53.7, 57.8 and 62.4°, respectively. These characteristic peaks are attributed to the well-crystalline copper ferrite (CuFe $_2$ O $_4$) (JCPDS: 34-0425). With a further increase in synthesis pH value from 12.0 to 13.0 (FC4), the intensity of these peaks increases, indicating a greater crystallinity.

Transmission electron micrographs (TEMs) of the FCBOs are shown in **Figure 2**. It can be seen that the FCBO particles produced at pH 9.0 (FC1, **Figure 2A**) are agglomerates of smaller nanoparticles. The morphology of FC2 (**Figure 2B**) is very similar to that of FC1. When the synthesis pH increases from 11.0 to 12.0, the major of amorphous particles (FC3, **Figure 2C**) becomes crystallized grains with visible grain boundaries and polyhedron shapes. For FC4 (**Figure 2D**), much more uniform grains are observed, suggesting well-crystalline CuFe₂O₄ particles are dominant under this condition. These results agree with those of XRD analysis.

The magnetic hysteresis curves of FCBOs are depicted in Figure 3. The hysteresis loops of FC3 and FC4 show a normal S-shape type, while those of FC1 and FC2 exhibit a nonhysteresis straight line, indicating that they are paramagnetic or superparamagnetic. The parameters of magnetic properties are summarized in Table 1. It can be seen that the saturation magnetization (M_s) increases with increasing synthesis pH value. For FC1 and FC2, they demonstrate very weak magnetism and the value of saturation magnetization is less than 0.4 emu/g. As the synthesis pH increases from 11.0 to 12.0, the saturation magnetization of FC3 rises sharply to 19.5 emu/g, which is far higher than that of FC2 and is very close to the CuFe₂O₄ nanoparticle (20.6 emu/g) synthesized via citrate-nitrate combustion method (Anandan et al., 2017). The magnetism of FC4 is the strongest and the saturation magnetization is as high as 26.9 emu/g. These results indicate that the magnetic properties of the FCBOs are closely related to their crystallinity.

The results of BET surface area measurements of the FCBOs are listed in **Table 1**. It can be clearly seen that the BET surface area of FCBOs decreases gradually with an increase in synthesis pH value. The BET surface area of FC1 is $268 \text{ m}^2/\text{g}$. However, the surface area of FC4 is only $90 \text{ m}^2/\text{g}$. It seems that the BET surface area of FCBOs is inversely proportional to its crystallinity.

Sorption Envelope

The influence of solution pH on arsenic sorption was investigated and the results are shown in **Figure 4**. For all FCBOs, the sorption of As (V) depends evidently on solution pH value. The greatest sorption occurs under acidic conditions and decreases with increasing solution pH, which is a typical characteristic for anions sorption by metal oxides and oxyhydroxides (Ren et al., 2011; Jordan et al., 2014). Over the tested pH range (3.0–11.0), As(V) mainly exists as negatively charged $H_2AsO_4^-$ and $HAsO_4^{2-}$ in water (pKa of dissociation is 2.20, 6.97 and 11.53, respectively). Under weak acidic conditions, the surface of the FCBO is positively charged because of protonation and $H_2AsO_4^-$ is dominant species in aqueous solution, which is beneficial for electrostatic attraction between the surface of FCBO and the

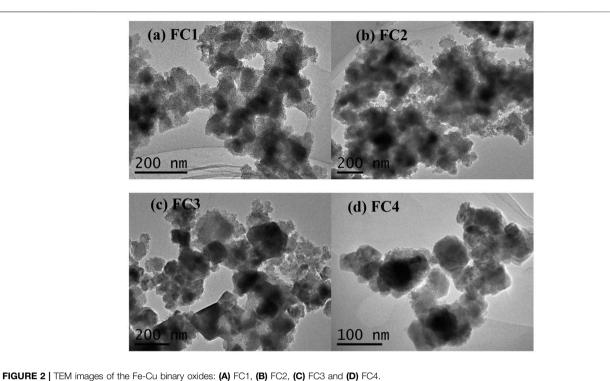
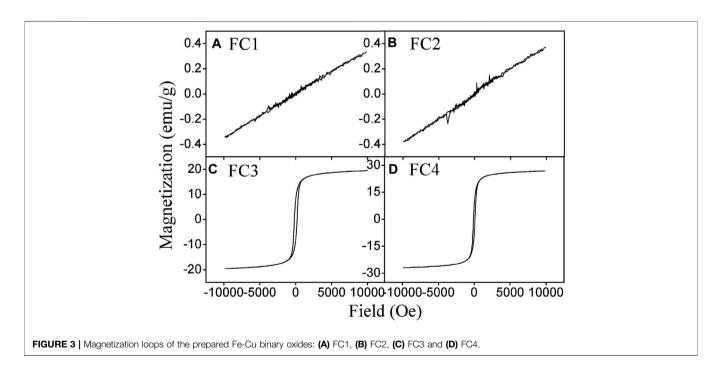


FIGURE 2 | TENT IT lages of the Fe-Cu binary Oxides. (A) FOT, (b) FOZ, (c) FOS and (b) FO4



aqueous $H_2AsO_4^-$. With an increase in solution pH, the surface of FCBO becomes less positively charged and even negatively charged. At the same time, $HAsO_4^{\ 2^-}$ (a more negatively charged As (V) species) becomes to be dominant. Therefore, the attraction between the surface of FCBO and As (V) species weakens and as a consequence, As (V) sorption decreases.

Compared to As (V), the influence of solution pH on As (III) sorption is markedly different. Its sorption enhances gradually as solution pH increases and a maximum sorption occurs at about pH 9.1. Afterwards, further increase in pH decreases the sorption of As (III). Similar phenomena have been reported for the As (III) sorption by other binary metal oxides (Ren et al.,

TABLE 1 | Saturation magnetization and BET specific surface area of the as-prepared Fe-Cu binary oxide samples.

Samples	Synthesis pH	Saturation magnetization (emu g ⁻¹)	Specific surface area (m² g ⁻¹)
FC1	9.0	0.34	268
FC2	11.0	0.37	202
FC3	12.0	19.52	130
FC4	13.0	26.88	90

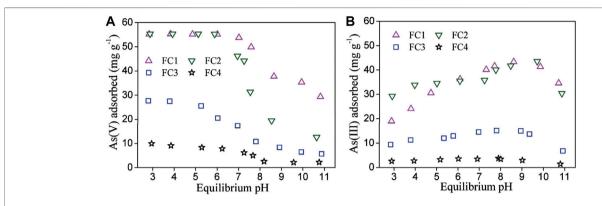


FIGURE 4 | Effect of solution pH on (A) As (V) and (B) As (III) sorption by Fe-Cu binary oxides. Initial arsenic concentration = 11.0 mg/L, adsorbent dose = 200 mg/L and $T = 25 \pm 1^{\circ}C$.

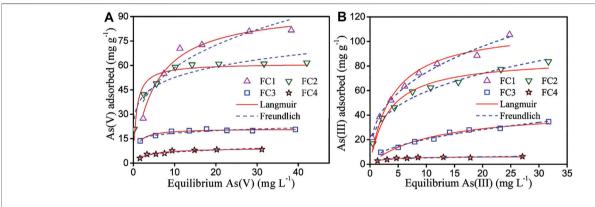


FIGURE 5 | Adsorption isotherm of (A) As (V) and (B) As (III) by Fe-Cu binary oxides. Initial arsenic concentration = 2-60 mg/L, adsorbent dose = 200 mg/L, pH = 7.0 ± 0.1 and T = 25 ± 1°C.

2011). Generally, a maximal sorption of weak acid anions onto metal oxides occurs at pH values close to pk_{a1} of the acid. The pk_{a1} of H_3AsO_3 is 9.2. The reduction in As (III) sorption at pH above 9.1 may be ascribed to the Coulombic repulsion between the negative surface of FCBOs ($pH_{pzc} = 7.3$ -9.0) and negatively charged As (III), whereas the predominant form of As (III) species is $H_2AsO_3^-$.

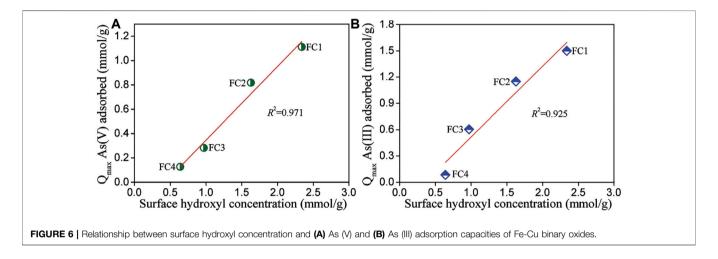
Sorption Isotherm

The sorption isotherms of arsenic on the FCBOs are depicted in **Figure 5**. Obviously, the sorption of arsenic by the FCBO is closely related with its crystallinity. The FC1 has the strongest uptake ability for both As(V) and As(III) and the maximum sorption

capacities are 83.3 and 112.2 mg/g at pH 7.0 (Langmuir model), respectively. The arsenic uptake ability of FCBOs decreases in the following order: FC1>FC2>FC3>FC4. Furtherly, the maximum sorption capacities of FC1 and FC2 are far larger than those of FC3 and FC4. The sorption performance of metal oxides depends generally on their surface area. However, the decrease in arsenic uptake by the FCBOs is not completely proportional to the reduction of specific surface area. This can be explained as follows. The specific surface area of the FCBOs is determined by N₂ molecule, which is smaller than the arsenic molecule. Partial surfaces of the FCBOs are inaccessible to arsenic molecule. Additionally, the As(V) and As(III) maximal sorption capacities

	TABLE 2 Langmuir and Freundlich isotherm	parameters for As (V) and As (III) ad	dsorption on Fe-Cu binary oxides at pH 7.0 ± 0.1 .
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Adsorbent As species		Langmuir model			Freundlich model		
		q _{max} (mg/g)	K _L (L/mg)	R ²	$K_{\rm F} ({\rm mg^{1-1/n} L^{1/n} g^{-1}})$	1/n	R ²
FC1	As(V)	83.3	0.19	0.977	58.9	0.31	0.844
FC2	As(V)	61.3	1.40	0.900	35.5	0.17	0.884
FC3	As(V)	21.1	1.03	0.935	14.0	0.12	0.806
FC4	As(V)	9.5	0.31	0.935	3.5	0.28	0.842
FC1	As(III)	112.2	0.25	0.936	32.6	0.36	0.988
FC2	As(III)	86.5	0.30	0.961	28.4	0.32	0.974
FC3	As(III)	45.3	0.09	0.959	6.9	0.47	0.980
FC4	As(III)	6.4	0.55	0.920	3.1	0.22	0.819



of Fe-Cu binary oxide synthesized at pH 7.5 are 82.7 and 122.3 mg/g, respectively (Zhang G et al., 2013). Obviously, the arsenic sorption ability of FC1 is to very close to that of Fe-Cu binary oxide prepared under neutral condition.

Both Langmuir and Freundlich models (seen in the Supplementary Material) were employed to fit the isotherm data. The fitting results and obtained parameters are shown in **Figure 5** and **Table 2**, respectively.

For As (V), the Langmuir model is more favorable for fitting the data, giving higher correlation coefficients (\mathbb{R}^2). However, the Freundlich model is more suitable to describe the adsorption of As(III) on Fe-Cu binary oxides except for FC4, according to the correlation coefficients. The As (V) adsorption is likely a monolayer adsorption because the Langmuir model supposes that the adsorption process is a monolayer adsorption. While As (III) adsorption is a multilayer adsorption since the Freundlich model presumes that adsorption occurs on the heterogeneous surface and follows multilayer adsorption.

Relationship Between Surface Hydroxyl Concentration and Arsenic Adsorption Capacity

The surface of metal oxides in water is easily hydroxylated, due to the dissociation of chemisorbed water molecules, and the formed surface hydroxyl groups are responsible for anions adsorption from water by the exchange with hydroxide ions (Tamura et al., 1999). To reveal the relationship between surface hydroxyl concentration and arsenic adsorption capacity of FCBOs, the amounts of surface hydroxyl groups were determined by titration method and the results are demonstrated in Figure 6. It can be seen that FC1 has the largest amount of surface hydroxyl groups per unit weight (2.34 mmol/g), followed by FC2 (1.63 mmol/g), FC3 (0.97 mmol/g), and FC4 (0.64 mmol/g). Evidently, surface hydroxyl concentration of FCBO is negatively correlated with its crystallinity. However, arsenic sorption capacity of FCBO is well positively correlated with its surface hydroxyl concentration. The data was fitted using a linear equation and the coefficient of determination (R^2) of linear regression for As (V) and As(III) is 0.971 and 0.925, respectively. It should be noted that the intercept is negative, indicating that not all surface hydroxyl groups are efficient for arsenic, especially for FCBO with high crystallinity. This could be explained as follows. The space structure of arsenic species (H2AsO4, HAsO₄²⁻ or H₃AsO₃) is remarkably larger than that of hydrogen ions, which was used to determine the amounts of surface hydroxyl groups. Therefore, partial hydroxyl groups on the surfaces could not be available for the arsenic molecules. To some extent, the arsenic sorption capacity of FCBO could be evaluated by the amounts of surface hydroxyl groups.

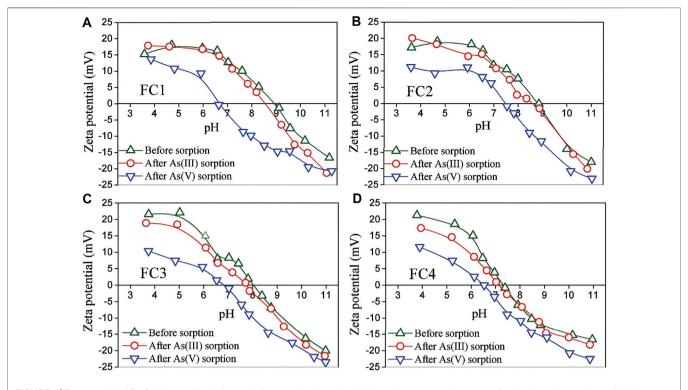
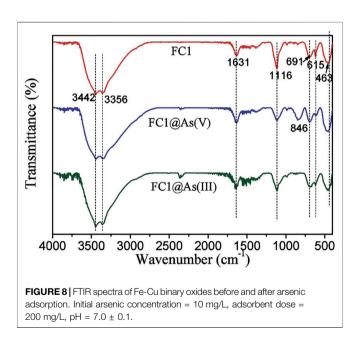


FIGURE 7 | Zeta potential of Fe-Cu binary oxides before and after arsenic adsorption. Initial arsenic concentration = 10 mg/L, adsorbent dose = 200 mg/L, ionic strength = 0.01 M NaNO₃, equilibrium time = 72 h.

Zeta Potential and FTIR Analysis Before and After Arsenic Adsorption

The zeta potentials of synthesized Fe-Cu binary oxides before and after reaction with arsenic were measured. As presented in Figure 7, the pH_{pzc} (pH at point of zero charge) of the virgin FC1, FC2, FC3 and FC4 were about 9.0, 8.8, 8.1 and 7.3, respectively. Evidently, the pH_{pzc} of the FCBOs decreases with increasing in crystallinity. This could be explained as follows. The pH_{pzc} values of CuO and Cu(OH)₂ are commonly over 9.2 (Martinson and Reddy, 2009; Kosmulski, 2009; Yu et al., 2012), and the pH_{pzc} of amorphous ferrihydrite is mostly in the range of 7.6-8.7 (Kosmulski, 2009; Antelo et al., 2010). As a mixture of these compounds, the amorphous FC1 and FC2 show relatively higher pH_{pzc} values. However, the crystalline CuFe₂O₄ illustrates a lower pHpzc value, which is consistent with previously reported values (Zhang T et al., 2013; Tu et al., 2014; Sun et al., 2015). For the FC1, a remarkable decrease in pH_{pzc} value has been observed after reaction with As(V) and the pH_{pzc} of As(V)adsorbed FC1 is about 6.7. Apparently, As (V) is specifically adsorbed by the FC1, since the specific sorption of anions leads to a shift of the pH_{pzc} of adsorbent to a lower pH value (Hsia et al., 1999; Ren et al., 2011). However, a slight decrease in pH_{pzc} of FC1 has been found after reaction with As(III). Commonly, the adsorption of uncharged As(III) species can not result a significant shift in pH_{pzc} of adsorbents (Ren et al., 2011). The slight decrease in pH_{pzc} might be explained as follows. A small part of As (III) adsorbed on the FC1 was oxidized to As(V) by the



dissolved oxygen because the experiments were conducted in an open system and the present CuO content might catalyze this reaction. For the FC2, FC3 and FC4, similar phenomena have been observed.

FTIR spectra of the FC1 before and after arsenic adsorption are depicted in **Figure 8**. For the pristine FC1, the peaks at 3,442

and 3,356 cm⁻¹ may belong to the vibration of O-H stretching and the peak at 1,631 cm⁻¹ may be ascribed to the deformation vibration of water molecules, implying that the surface of FC1 sorbed water molecules through physical adsorption; the peak at 1,116 cm⁻¹ may be assigned to the vibration of SO_4^{2-} (Lefevre, 2004); the three peaks at 691, 615 and 463 cm⁻¹ may be ascribed to the overlap of the HO- deformation vibration of ferrihydrite and Cu-O stretching (Kliche and Popovic, 1990). After As (V) adsorption, the intensity of peak at 1,116 cm⁻¹ weakens and a new peak appears at 846 cm⁻¹, which may be due to the vibration (As-OH) of As-O-M groups (Goldberg and Johnston, 2001). This result suggests that the As (V) is mainly sorbed through the formation of inner-sphere surface complexes. While no significant change has been observed after As (III) adsorption. Similar phenomena were also observed for arsenic adsorption by other metal oxides (Ren et al., 2011).

Based on the analyses of zeta potentials and FTIR sepctra, it could be reasonably concluded that the As (V) is specifically sorbed by the FCBOs via formation of inner-sphere surface complexes, while As (III) is sorbed through formation of both inner- and outer-sphere surface complexes.

CONCLUSION

A series of Fe-Cu binary oxides were prepared under different solution pH values. The crystallinity and saturation magnetization of prepared Fe-Cu binary oxide increased with an increase in synthetic pH value. Simultaneously, the morphology of FCBO changed gradually from irregular agglomerate to relatively uniform polyhedron. The adsorption of arsenic on FCBOs is remarkably affected by the surface structure and crystallinity, decreasing as the degree of crystallinity increases. Surface hydroxyl density of FCBOs is an important parameter to evaluate its arsenic adsorption ability. Nevertheless, the adsorption ability may be overestimated if only this parameter is used. As (V) is sorbed by the FCBOs via formation of inner-sphere surface complexes and As (III) is

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sorbed through formation of both inner- and outer-sphere surface complexes. This investigation provides new insights into structure-performance relationship of FCBOs system, which are beneficial to develop new and efficient sorbents. However, the characterization of FCBOs is still not insufficient in this study and more powerful techniques such as X-Ray Absorption Fine Structure (XAFS) are needed to reveal further the structure-performance relationship of FCBOs system in future study.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/**Supplementary Material** further inquiries can be directed to the corresponding authors.

AUTHOR CONTRIBUTIONS

GZ: Conceptualization, Writing—Original draft preparation. ZW: Investigation, Formal analysis. QQ: Investigation. YW: Conceptualization, Writing—Reviewing and Editing.

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SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: https://www.frontiersin.org/articles/10.3389/fchem.2021.840446/full#supplementary-material

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An Eco-friendly Iron Cathode Electro-Fenton System Coupled With a pH-Regulation Electrolysis Cell for p-nitrophenol Degradation

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The high consumption of salt reagents and strict pH control are still bottlenecks for the full-scale application of the Fenton reaction. In this work, a novel eco-friendly iron cathode electrochemical Fenton (ICEF) system coupled with a pH-regulation divided electrolysis cell was developed. In a pH-regulation divided electrolysis system, the desired pH for an effective Fenton reaction and for a neutral treated media could be obtained by H₂O splitting into H⁺ and OH⁻ at the anode and cathode, respectively. In an ICEF system, an iron plate was used as the cathode to inhibit the release of iron ions and promote the reduction of Fe³⁺ to Fe²⁺. It was found that when a potential of 1.2 V/SCE was applied on the iron cathode, 98% of p-nitrophenol was removed in the combined system after 30 min with continuously adding 200 mg/L of H₂O₂. Meanwhile, a COD and TOC removal efficiency of 79 and 60% was obtained, respectively. In this case, the conductivity just slightly increased from 4.35 to 4.37 mS/cm, minimizing the increase of water salinity, as compared with the conventional Fenton process. Generally, this combined system was eco-friendly, energy-efficient, and has the potential of being a promising technology for the removal of bio-refractory organic pollutants from wastewaters.

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INTRODUCTION

Over the past few decades, advanced oxidation processes (AOPs) have attracted increasing interests for wastewater treatment since the highly oxidative hydroxyl radical (${}^{\bullet}$ OH, ${\rm E}^0$ = 2.80 V/SHE) was generated *in situ* and found to be capable of degrading any refractory organic molecules present in the aqueous solution until total mineralization at the kinetic constant values as high as $10^8 \sim 10^{10} \, {\rm M}^{-1} {\rm s}^{-1}$ (Andreozzi et al., 1999; Oturan and Aaron, 2014; Gao et al., 2018). Among various AOPs, the conventional Fenton reaction process has been most widely applied for the treatment of wastewater streams because it exhibits the advantages of fast reaction rates, mild operating conditions, and simplicity to control (Bello et al., 2019). The Fenton reaction mainly proceeds via two steps (Neyens and Baeyens, 2003; Moreira et al., 2017; Gao et al., 2020). The first stage is characterized by the rapid formation of ${}^{\bullet}$ OH from the homogeneous reaction between Fe²⁺ and H₂O₂ (Eq. 1), most of the pollutant degradation is achieved in this stage. The second stage is characterized by a slow reaction between Fe³⁺ and H₂O₂ for the regeneration of Fe²⁺ (Eq. 2), maintaining the continuous Fenton reaction (Babuponnusami and Muthukumar, 2014; Bello et al., 2019).

Iron Cathode Electro-Fenton System

$$\begin{split} Fe^{2^{+}} + H_{2}O_{2} &\rightarrow Fe^{3^{+}} + OH^{-} + {}^{\bullet}OH \ k_{1} = 63 - 76 \left(L \ mol^{-1} s^{-1}\right) \\ (1) \\ Fe^{3^{+}} + H_{2}O_{2} &\rightarrow Fe^{2^{+}} + {}^{\bullet}HO_{2} + H^{+} \ k_{2} = 0.001 - 0.01 \left(L \ mol^{-1} s^{-1}\right) \end{split}$$

However, the Fenton process has some drawbacks, which greatly hamper its industrial application (Babuponnusami and Muthukumar, 2014; Gao et al., 2020). The addition of concentrated acid reagent is indispensable to adjust the solution pH to ~3.0, that is the optimum condition for the Fenton reaction. However, working in such acidic pH requires the addition of a large amount of acid. In addition, massive alkaline reagents were also consumed for the subsequent neutralization of the treated solution. In addition, the employment of iron salt inevitably increases water salinity (Li et al., 2013). The increased salt content probably makes this wastewater unacceptable for natural environments or poses significant pressure on the subsequent reverse osmosis unit (Wang et al., 2014; Fang et al., 2018). Besides, most of the Fenton reagents are added at once while over-dosage of either H_2O_2 or iron ions would lead to side reactions (**Eq. 3** and **Eq. 4**). As a result, Fe3+ is massively accumulated from the oxidation of Fe²⁺ in the Fenton reaction system since Fe²⁺ regeneration from Fe³⁺ is very slow (Qiang et al., 2003). Thus, the reduction of Fe³⁺ to Fe²⁺ greatly limits the treatment performance of the Fenton reaction for pollutants degradation.

$$Fe^{2+} + {}^{\bullet}OH \rightarrow Fe^{3+} + OH^{-} k3 = 3.2 \times 10^{8} (L \text{ mol}^{-1}\text{s}^{-1}) (3)$$

$${}^{\bullet}OH + H_{2}O_{2} \rightarrow {}^{\bullet}HO_{2} + H_{2}O k_{4} = 3.3 \times 10^{7} (L \text{ mol}^{-1}\text{s}^{-1})$$

Over the recent decades, there has been growing interest in the research community to address the above limitations of the conventional Fenton process. The development heterogeneous Fenton system has been demonstrated to be a feasible strategy to avoid salt reagents addition, where iron oxides and other metal oxides such as goethite (a-FeOOH), magnetite (Fe₃O₄), hematite (α-Fe₂O₃), and maghemite (γ-Fe₂O₃) have been commonly utilized as heterogeneous catalysts (Davarnejad and Azizi, 2016; He et al., 2016; Hassani et al., 2018; Görmez et al., 2019; Cai et al., 2021; Chen et al., 2021). Unlike the homogenous Fenton system, in a heterogeneous Fenton system, iron sources are immobilized within/on the catalyst structure, and the Fenton reaction occurs when the H₂O₂ molecule is in contact with the iron sites of the carrier, so that it is not necessary to continuously add the iron salts and pH limitation is reduced to some extent (Ganiyu et al., 2018; Cai et al., 2021; Hu et al., 2021). In spite of this, the most heterogeneous Fenton catalysts still operate optimally at pH 3-5 and its catalytic performance is reduced in near-neutral water bodies because the catalyst turnover frequency is reduced by up to 100-fold under neutral conditions (Cai et al., 2021; Chen et al., 2021).

Electro-Fenton is an emerging technology with well-known outstanding oxidation power, where the electron is utilized as the reagent to facilitate the regeneration of Fe²⁺ at the cathode (Eq. 5). Thus, this process exhibits higher performance in

comparison with the conventional Fenton system because of the high utilization efficiency of Fe²⁺ (Oturan et al., 2000; Yuan et al., 2006; Brillas et al., 2009). Consequently, much more •OH can be produced at a much smaller amount of iron salt addition. In fact, the addition of iron salts can be completely avoided with using a metal iron plate as the sacrificial anode material, where the electrochemically released Fe²⁺ can serve as the Fenton catalyst. In spite of this, the produced ferric sludge amount cannot be controlled effectively. Besides, concentrated acid and basic reagents are still required to regulate the solution pH. In fact, in the typical electrolysis system, OH⁻ and H⁺ are produced at the cathode and anode, respectively, which can be separated well in the divided electrolysis cell. Inspired by this characteristic, the divided electrolysis cell can be used as the pH-regulation unit before and after the Fenton system to automatically acidify and neutralize the wastewaters without the requirement of chemicals. Besides, in the acid solution, the acidic dissolution of the metal iron plate can release the iron ions into the solution. Under the cathodic polarization of metal iron, the released iron ion amount can be well regulated. At the same time, Fe³⁺ can be also reduced to Fe²⁺ at the iron cathode. These collectively eliminate the limitations of the conventional Fenton process and promote its treatment efficiency for pollutants.

$$Fe^{3+} + e^{-} \to Fe^{2+}$$
 (5)

In this study, a novel electro-Fenton process coupled with a pH-regulation divided electrolysis cell was developed for p-nitrophenol (PNP) degradation. In the pH-regulation divided electrolysis cell with a PTFE membrane as the separated material, the desired pH for an effective Fenton reaction and for a neutral treated media could be obtained by $\rm H_2O$ splitting into $\rm H^+$ and $\rm OH^-$ at the anode and cathode, respectively. In the electro-Fenton process with external addition of $\rm H_2O_2$, metal iron and a DSA electrode were applied as the cathode and anode, respectively, where the cathodic polarization of the metal iron electrode could effectively reduce the release of iron ions with diminishing ferric sludge generation.

EXPERIMENTAL SECTION

Materials

An iron plate (Fe, >99%) of 50×50 mm was purchased from Tengfeng Metallic Material Co. Ltd. (Hebei, China). p-nitrophenol (PNP, $C_6H_5NO_3$, 99%) was supplied from Shanghai Yien Chemical Technology Co. Ltd. 1,10-phenanthroline ($C_{12}H_8N_2\cdot H_2O$, 99%), glacial acetic acid ($C_2H_4O_2$, 99%), sodium acetate (CH₃COONa, 99%), ferrous sulfate (FeSO₄.7H₂O, 99%), hydroxylamine hydrochloride (HONH₃Cl, 98.5%), sodium sulfate (Na₂SO₄, 99%), hydrogen peroxide (H_2O_2 , 30%), titanium oxalate, potassium ($K_2TiO(C_2O_4)_2$, 98%), ferrous ammonium sulfate hexahydrate (Fe(NH₄)₂·(SO₄)₂·6H₂O, 99%), potassium permanganate (KMnO₄, 99%), sulfuric acid (H_2SO_4 , 98%), and sodium

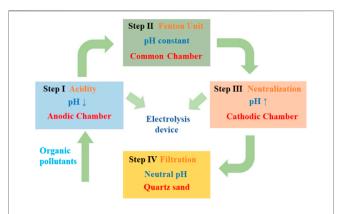


FIGURE 1 | Scheme of the iron cathode electrochemical Fenton (ICEF) system (steps 2 and 4) coupled with the pH-regulation divided electrolysis system (steps 1 and 3).

hydroxide (NaOH, 98%) were provided by Sinopharm Chemical Reagent Co. Ltd., China. All chemicals were analytical grade and were used without further purification. Ultrapure water (18.2 M Ω cm) was used to prepare reaction solutions for all the experiments.

Experimental Procedures

As shown in Figure 1, the combined electrochemical treatment process mainly consisted of four steps. Prior to step 1, a 100 mg/L PNP solution with pH 7.0 was performed in the beaker, 3 g/L of Na₂SO₄ was used as the electrolyte solution. In step 1, pH adjustment was carried out in the divided electrolysis cell, which used a plexiglass rectangular tank with the cathode and anode chambers isolated by a PTFE microfiltration membrane. The anode consisted of a 50 × 80 mm boron-doped diamond (BDD) electrode while the cathode consisted of titanium mesh of the same dimensions with the distance of 25 mm; the PTFE membrane was between the anode and cathode. The galvanostatic electrolysis reactions were performed by a DC power supply (voltage 0-30.0 V, electric current 0-5.0 A). In step 1, the PNP solution concurrently entered into the cathode and anode chambers, pH was reduced to near 3.0 in the anodic chamber within 1 min. In step 2, the solution with the reduced pH was added into the iron cathode electrochemical Fenton (ICEF) system for PNP degradation with a chamber volume of 500 ml using a three-electrode potentiostat (Model CHI1130C, Chenhua instrument Co. Ltd. Shanghai, China) coupled with a saturated calomel reference electrode (SCE), where the cathodic potential was precisely controlled by the potentiostat and SCE. The working electrode was a 50 × 50 mm iron plate, and the counter electrode was a 50 × 50 mm DSA (Ti-RuO₂-IrO₂) mesh; 200 mg/L of H₂O₂ was continuously added by a pump within 15 min. In step 3, after the treatment of PNP solution in the ICEF system, the solution was transferred into the cathode chamber of the divided electrolysis cell to increase the pH. In addition, the pH of the cathode effluent was further regulated to neutral (~9.0) by NaOH solution. In step 4, the neutral solution was passed through a filter device to remove iron ions, which was carried out in a container filled with quartz sand (80-120 mm).

The removal ratio of p-nitrophenol, COD, or TOC $(\eta, \%)$ was calculated via Eq. 8.

$$\eta = \frac{C_0 - C_t}{C_0} \times 100\%$$
 (6)

Analytical Determinations

The concentrations of PNP were determined by high performance liquid chromatography (HPLC-1100, Agilent) with an Eclipse XDB-C18 column (4.6 mm \times 150 mm, 5 μ m), (Nakatsuji et al., 2015). The mobile phase was methanol/water (50/50), the flow rate was 1.0 ml/min, and the UV detector was set at 314 nm. The chemical oxygen demand (COD) was detected using a COD analyzer (ASH 6B-80, China) [37]. A total organic carbon analyzer (multi N/C® 2,100, Analytik Jena AG) was applied to monitor total organic carbon (TOC). (Kavitha and Palanivelu, 2004). The concentration of H₂O₂ was measured by the potassium titanium (IV) oxalate method at 400 nm with a UV-Vis spectrophotometer (UV 6000 PC Yuanxi instrument Co. Ltd. Shanghai, China) (Wang and Chu, 2011). Fe²⁺ and Fe (tot) were determined at 510 nm using a modified phenanthroline method with an Fe²⁺ detection limit of 0.5 µM, and Fe³⁺ concentration was estimated as the difference between Fe (tot) and Fe²⁺ (Xin et al., 2018). Solution pH and conductivity were measured by a water quality analyzer. The reaction was quenched in the collected samples by immediately adding 1.0 mol/L of NaOH since Fenton oxidation cannot occur at pH > 10.0. For COD measurements, the samples were pretreated with NaOH to remove any residual H₂O₂. All experiments were performed twice at least, with relative errors less than 3%.

RESULTS AND DISCUSSION

pH-Regulation in a Divided Electrolysis Cell

For the Fenton reaction, it is recommended to acidify the solution pH to ~3.0 for •OH production and then neutralize the solution for the precipitation of Fe³⁺ (Chen et al., 2021). In this study, we developed a divided electrolysis cell using a hydrophilic PTFE microfilter membrane as the separated material. In this system, H₂O splitting reactions at the anode and cathode could produce H⁺ and OH (Eq. 7 and Eq. 8), respectively, which could be used to regulate the solution pH required for the Fenton reaction. Thus, the substrate solution pH could reduce to nearly 3.0 when it flowed through the anode chamber in step 1 (Figure 1). After the Fenton reaction, the solution pH was raised to promote the formation of Fe(OH)₃ in step 3. The above pH adjustment objective could be achieved by regulating the applied current density and flow velocity. Here, a neutral solution containing 100 mg/L of PNP and 3 g/L of Na₂SO₄ electrolyte was pumped into the electrolysis device at a flow rate of 20 ml/min by a peristaltic pump, where the residence time was 1 min. The current density applied is the key parameter for the electrochemical pH regulation because it fundamentally affects the yield of H⁺ in the anode compartment and OH⁻ in the cathode compartment, respectively. As shown in Figure 2A, the pH of the anode effluent continuously decreased with the increase of current density; as the current density increased from 0.5 to 6 mA/cm², the

Iron Cathode Electro-Fenton System

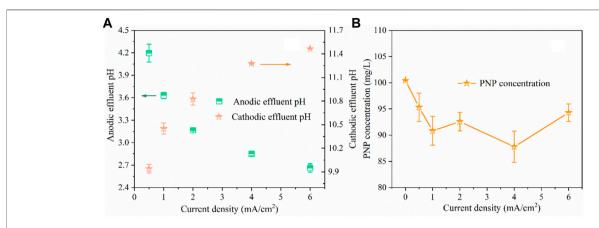


FIGURE 2 | The influence of current density on effluent pH (A) and PNP concentration (B). (PNP concentration = 100 mg/L, Na₂SO₄ = 3 g/L, pH₀ = 7.0, anode compartment flow velocity = 20 ml/min, cathode compartment flow velocity = 20 ml/min).

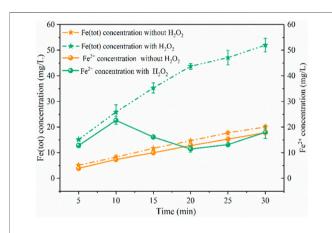


FIGURE 3 | Concentration variations of iron ions under different conditions. (PNP = 100 mg/L, Na $_2$ SO $_4$ = 3 g/L, pH $_0$ = 3.0).

pH of anodic effluent decreased from 4.2 to 2.7, while the cathodic effluent pH increased from 9.9 to 11.5. This was consistent with what we expected, because as the current increased, effective watersplitting resulted in more H^+ produced at the anode and more OH^- produced at the cathode. In particular, when the applied current density was 2 mA/cm^2 , an acidic effluent with pH of 3–3.2 was automatically attained at the steady state (Neyens and Baeyens, 2003). It has been demonstrated that the Fenton process is inhibited at extremely acidic environments due to the formation of $(Fe(H_2O))^{2+}$ and Fe(III)-hydroxyl complexes, $Fe(OH)^{2+}$. Thus, to achieve the most favorable Fenton reaction condition, an applied current density of 2 mA/cm^2 was adopted in this study.

$$2H_2O + 2e^- \rightarrow 2OH^- + H_2\uparrow$$
 (7)

$$2H_2O - 4e^- \rightarrow 4H^+ + O_2 \uparrow \tag{8}$$

The results in **Figure 2B** show that the PNP degradation efficiency increased as the current density increased initially from 0 to 1 mA/cm², but it became nearly constant when the current density was elevated above 1 mA/cm². Specifically, as the current density increased from 0.5 to 1 mA/cm², the PNP removal

efficiency increased from 5 to 10%. Nevertheless, further increasing the current density to 6 mA/cm² did not increase the further removal of PNP. In this case, the BDD anode had little effect on the degradation of pollutants in this system because of a too short residence time.

Iron Plate Immersed in Water Without Electricity

As shown in Figure 3, when the solution pH reduced to nearly 3.0, the iron plate immersed in water without power could produce 20 mg/L of Fe (tot) within 30 min, of which 89% was Fe(II). In this process, the iron plate would be dissolved by H⁺ to generate Fe²⁺ under acidic conditions through Eq. 9, and the oxidation of Fe²⁺ to Fe³⁺ by O₂ was slow and the solution pH increased slightly from 3.0 to 3.2. The average production rate of Fe (tot) (approximately 0.33 mg/min) and Fe²⁺ (approximately 0.3 mg/min) was stable and closed within 30 min, indicating the stable release of Fe²⁺ by the iron plate under the acid solution. Under the same conditions, Fe (tot) significantly increased to 52 mg/L after 200 mg/L of H₂O₂ was continuously added into the solution within 15 min. The average production rate of Fe (tot) was stable within 20 min (approximately 1.1 mg/min), which was three times higher than that without the addition of H₂O₂. But these two reactions exhibited a similar average production rate of Fe (tot), approximately 0.41 mg/min, within the reaction period of 20-30 min, which may be ascribed to the fact that most of the H₂O₂ was consumed within 20 min. As for Fe²⁺ concentration, it continuously increased within 10 min with the production rate of approximately 1.13 mg/min and decreased from 23 to 11 mg/L between 10 and 20 min, which was explained by the consumption of Fe²⁺ during the Fenton reaction process (Eq. 1). And after 20 min, the concentration continuously increased, finally reaching 18 mg/L at 30 min, accounting for 35% of the Fe (tot). Within 20-30 min, the Fe (tot) concentration increased by 8 mg/L, close to the value of Fe²⁺ increase (7 mg/L), this can also be explained by the fact that little H2O2 remained after 20 min and the increase of Fe (tot) concentration was mostly due

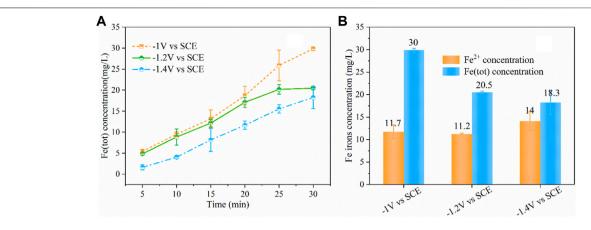


FIGURE 4 | Concentration variations of Fe (tot) under different cathodic potentials (A), concentration of Fe irons at 30 min under different cathodic potentials (B). (PNP = 100 mg/L, Na₂SO₄ = 3 g/L, pH₀ = 3.0).

to the Fe^{2+} released (**Eq. 9**). The above results revealed that the presence of H_2O_2 could facilitate the release of iron ions from Fe^0 in the acid solution. In this case, a large amount of iron sludge was produced and side reactions (**Eq. 3**) might consume produced \bullet OH, leading to inferior degradation of pollutants.

$$Fe + 2H^+ \rightarrow Fe^{2+} + H_2$$
 (9)

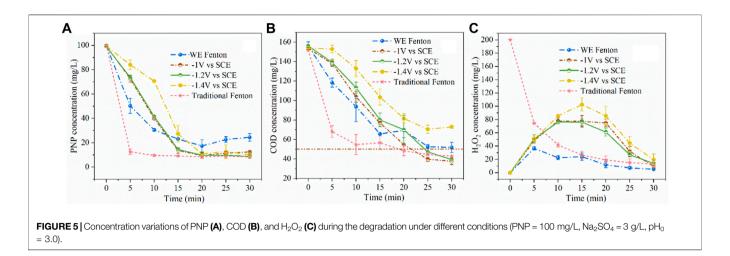
Effect of Different Potential Applied to Iron Plate Cathode in ICEF System

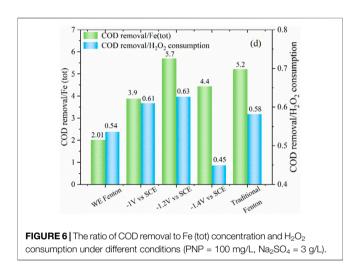
To further reduce the release of iron ions from the iron cathode and improve the regeneration of Fe²⁺ from Fe³⁺, we developed a novel iron cathode electro-Fenton system, applying a potential on the iron cathode. Figure 4A shows that concentration variations of Fe (tot) under different cathodic potentials, it was found that as the applied cathodic potential increased, the produced Fe (tot) decreased continuously. At the cathodic potential of -1.0 and -1.2 V/SCE, the produced Fe (tot) concentration was 30 and 21 mg/L within 30 min, which reduced by 42 and 61%, respectively, compared with no electricity input. Further increasing the cathodic potential from -1.2 to -1.4 V/SCE resulted in the slight decrease of Fe (tot) concentration to 18 mg/L. The production rate of Fe (tot) (0.43 mg/min) at the cathodic potential of -1.2 V/SCE was significantly higher than -1.4 V/SCE (0.29 mg/min) within the initial 20 min, while the value was apparently decreased to 0.17 mg/min within 20-30 min, and the rate slightly increased to 0.33 mg/min during the same time at -1.4V/ SCE. Figure 4B shows the Fe²⁺ and Fe (tot) concentrations produced at 30 min under different cathodic potentials. It was found that the ratio of Fe²⁺ to Fe (tot) concentration enhanced significantly from 0.39 to 0.77 with the decrease of cathodic potential from -1.0 to -1.4V/SCE. This can be explained by the fact that the regeneration from Fe³⁺ to Fe²⁺ increased with the decrease of cathodic potential.

The results of PNP concentration versus time are shown in **Figure 5A**. It was found that only 75% of PNP was degraded

within 30 min under the conditions of the iron plate immersed in water with 200 mg/L of H₂O₂ without electricity (WE Fenton process). And PNP removal efficiency was enhanced to 87, 91, and 90% at cathodic potentials of -1.0, -1.2, and -1.4 V/SCE, respectively (Kavitha and Palanivelu, 2004). However, it is noted that the removal efficiency was inferior initially then reached similar levels as the others after 20 min at -1.4 V/SCE. In addition, COD removal efficiency was basically the same in the case of -1 and -1.2 V/SCE, whereas the treatment at -1.4V/SCE exhibited an inferior degradation rate. As shown in Figure 5B, the COD removal efficiency was 67% without electricity, and increased to 76 and 75% at the cathodic potentials of -1.0 and -1.2 V/SCE, respectively, with residual COD concentration below 50 mg/L. However, when the cathodic potential was decreased to -1.4 V/SCE, the COD concentration reduced from 154 to 73 mg/L within 30 min, which can be ascribed to the inferior production of Fe (tot) for the Fenton reaction. According to the above results, -1.2 V/ SCE was chosen as the optimal cathodic potential, and the released Fe (tot) concentration decreased by approximately 61% with the COD concentration further decreasing from 52 to 40 mg/L as compared with the WE Fenton process. The degradation of the 100 mg/L PNP solution was carried out in the traditional Fenton system with initially adding 20 mg/L of Fe^{2+} and 200 mg/L of H_2O_2 at p H_0 3.0. It was found that PNP was destructed quickly within 5 min and exhibited faster decay of PNP and COD than the present combined process within 20 min. However, its final COD removal efficiency was outperformed by the present combined process at 30 min and was slightly surpassed by the latter (Babuponnusami and Muthukumar, 2014).

The variation of $\mathrm{H_2O_2}$ concentration is shown in **Figure 5C**. It was observed that when applying potential at the iron cathode, the $\mathrm{H_2O_2}$ concentration increased initially within 15 min and then decreased afterwards in the late reaction stage. As compared with the WE Fenton reaction system, the $\mathrm{H_2O_2}$ concentration was higher, which was probably due to the smaller release of iron ions from the iron





cathode. As the applied cathodic potential decreased from -1.0 to -1.4 V/SCE, the remaining concentration of H₂O₂ was slightly higher over the whole reaction period, which was also associated with the production of iron ions. In the traditional Fenton system, the concentration of H2O2 significantly decreased from 200 to 126 mg/L within 5 min, which corresponded to the quick reaction between Fe²⁺ and H₂O₂, and the remaining H₂O₂ concentration at 30 min was 13 mg/L. From Figure 6, it could be clearly observed that as the cathodic potential decreased from -1.0 to -1.2 V/SCE, the ratio of COD removal to produced Fe (tot) and H2O2 consumption was increased from 3.9 to 5.7 and 0.61 to 0.63, while the value significantly decreased to 4.4 and 0.45 at a higher cathode potential of 1.4 V/SCE. These results demonstrated that -1.2 V/SCE was the optimal cathodic potential with suitable Fe (tot) production for the electro-Fenton reaction, which exhibited slightly higher COD removal/Fe (tot) and COD removal/H2O2 consumption for the traditional Fenton reaction system. In the WE Fenton process, the much lower value, i.e., 2 for COD removal/Fe (tot) and 0.54 for COD removal/ H_2O_2 consumption, was obtained, respectively.

The Divided Electrolysis Cell and ICEF Combined System

According to the aforementioned experimental results, the optimal current density for solution pH regulation and cathodic potential for the ICEF reaction have been obtained. The results of PNP and COD concentration time are shown in Figure 7A. It was found that the PNP concentration of the anodic effluent slightly decreased from 100 to 91 mg/L while the COD removal efficiency was only 5%, owing to the oxidation at the BDD anode. During the combined process, the removal efficiency of PNP and COD attained 93 and 72% within 30 min, and the PNP pollutant was further destructed after filtration because of the coagulation of iron ions with the concentration decreased from 6 to 2 mg/L. Figure 7B shows the TOC removal efficiency of traditional Fenton and ICFE systems, the removal efficiency was 42% within 5 min by traditional Fenton but maintained relatively stable in the remaining time, finally the value reached 48%. This can be explained by the rapid consumption rate of Fenton reagents. However, the TOC removal efficiency achieved 60% in the combined system, which was much higher than traditional Fenton (Kavitha and Palanivelu, 2004). The high removal efficiency of PNP (98%), COD (79%), and TOC (60%) revealed more efficient degradation of pollutants in the combined system than the traditional Fenton system.

For traditional Fenton, pH was adjusted to the desired values with $\rm H_2SO_4$ and NaOH solution while ferrous sulfate was used as the iron ions source (Gao et al., 2020). As shown in **Figure 8**, the conductivity was increased from 4.35 to 4.68 mS/cm after acidification during traditional Fenton, and the value continuously enhanced to 4.95 after the Fenton reaction, while the pH slightly decreased from 3.07 to 2.73, which can be explained by the large quantity of organic acids production. The pH of the effluent was neutralized to approximately 9.0 with the conductivity reduced to 4.76 mS/cm, which might be caused by acid-base

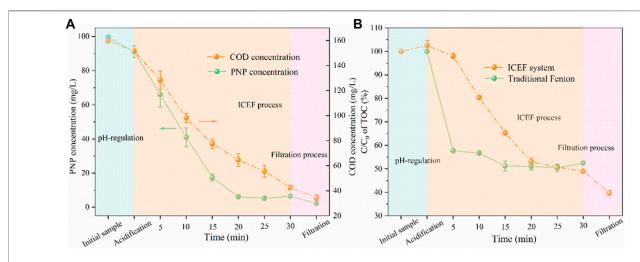
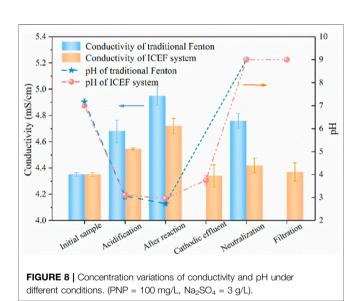


FIGURE 7 | Concentration variations of PNP and COD (A) and TOC concentration reduction (B) during the EIC-EF system degradation (PNP = 100 mg/L, Na₂SO₄ = 3 g/L, pH₀ = 7.0).

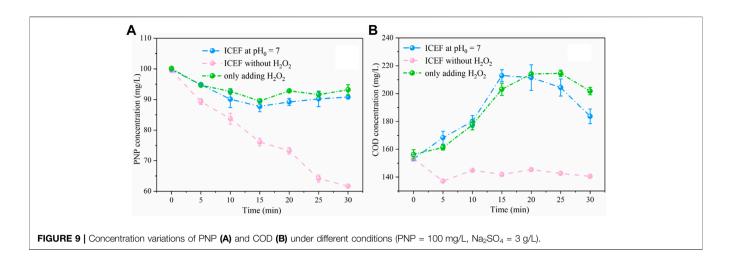


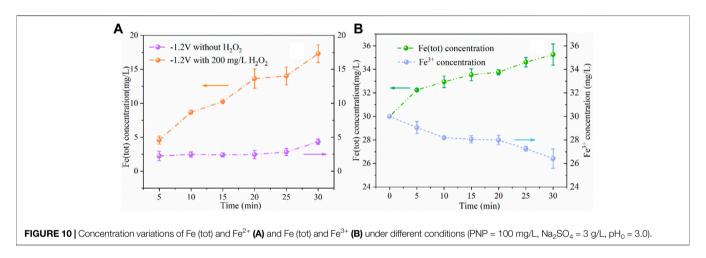
neutralization. As for the present combined process, the conductivity of the anodic effluent increased to 4.55 mS/cm with the pH decreasing from 7.0 to 3.1, the cathodic effluent pH only slightly increased from 2.95 to 3.75 at the same current density (2 mA/cm²), owing to the buffering effect of organic acids on pH. During the neutralization process, pH was further adjusted to neutral (~9.0) by the NaOH solution (Chen et al., 2021), driving the complete precipitation of Fe(OH)₃. In this case, the conductivity further decreased to 4.37 mS/cm. Generally, the salinity of traditional Fenton increased by 9% compared with the initial solution while the present combined process remained basically unchanged after the reaction, avoiding the obvious increase of water salinity caused by the addition of a large amount of chemical reagents in traditional Fenton.

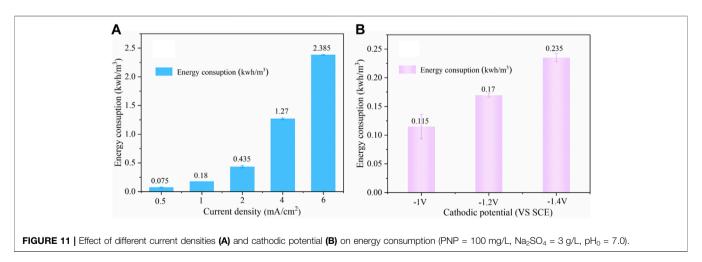
Mechanism Discussion

A set of experiments was performed to verify the main mechanism of pollutant degradation. As shown in Figures 9A,B, the PNP removal efficiency was only 9% without frontend pH adjustment, owing to basically no Fe²⁺ production under the neutral solution, indicating that the pH-regulation process is indispensable for the ICEF system. In addition, only 7% of PNP was oxidized by H₂O₂ in solution. In the above two reaction system, COD concentration slightly increased after the reaction, which was possibly subject to formation of some intermediates which interfered with the COD concentration. The direct oxidation of PNP by the DSA anode was also examined without H_2O_2 at $pH_0 = 3.0$, the removal efficiency of PNP and COD concentration were 38 and 13%, respectively. Thus, the direct PNP degradation at the anode was ruled out, indicating that PNP in solution was mainly oxidized by •OH produced by the Fenton reaction.

To further investigate the effect of cathode potential on iron ion concentration, we conducted the following experiments. As shown in Figure 10A, at the cathode potential of -1.2V/SCE without adding H₂O₂, the produced Fe (tot) concentration was 4 mg/L, which reduced by 80% compared with no electricity as shown in Figure 3 (20 mg/L). And in the case of adding 200 mg/L of H₂O₂ and applying the cathode potential of -1.2 V/SCE, the Fe (tot) concentration increased to 17 mg/L. There are two reasons for this phenomenon, one is that the iron plate would react with H_2O_2 in the presence of H^+ through Eq. 10 (Pan et al., 2019); the other is that the presence of H2O2 promoted the conversion of Fe²⁺ to Fe³⁺ and the generated Fe³⁺ may further react with the iron plate to produce Fe^{2+} through Eq. 11. As shown in Figure 10B, 30 mg/L of Fe^{3+} was also added into the solution at the cathodic potential of -1.2 V/SCE without H₂O₂, the Fe (tot) concentration slightly increased to 35 mg/L within 30 min and Fe³⁺ concentration reduced to 26 mg/L. The results demonstrated that the reaction between Fe3+ and Fe0 contributed marginally to







the release of iron ions during the ICEF process, while the direct oxidation of ${\rm Fe^0}$ by ${\rm H_2O_2}$ probably dominated the release of iron ions from the iron plate. As a result, in the WE Fenton system, ${\rm H_2O_2}$ was not only consumed for the Fenton reaction but also for the release of ${\rm Fe^{2+}}$ by the reaction with the iron plate. Thus, a part

of H₂O₂ cannot be utilized for •OH production via the Fenton reaction, leading to the inferior degradation efficiency of PNP.

$$Fe + H_2O_2 + 2H^+ \rightarrow Fe^{2+} + 2H_2O$$
 (10)

$$Fe^{3+} + Fe \rightarrow Fe^{2+} \tag{11}$$

Environmental Implication

In the present combined system, the cost for electricity played an important role in the overall operating cost of the process. Apparently, the overall energy consumption is the sum of the pH adjustment unit and Fenton reaction process, the power consumption of per ton of wastewater was calculated based on Eq. 12 (Wang and Chu, 2011).

$$E = \frac{UIT}{V} \times 10^{-3} \tag{12}$$

where E is the energy consumption, U is the voltage measured during the reaction (V), I is the applied current (A), t is the electrolysis time (h), and V is the volume of reaction solution (m³).

As shown in Figure 11A, during the pH-regulation process, current density had a significant impact on energy consumption, the value increased from 0.075 to 2.385 kWh/m³ as the current density increased from 0.5 to 6 mA/cm². In the present combined system, a pH of 3.0-3.2 was automatically attained by electrolysis with the energy consumption of 0.435 kWh/m³. Figure 11B shows that the energy consumption was increased from 0.115 to 0.235 kWh/m³ with the cathodic potential decreasing from -1.0 to -1.4 V/SCE. We can infer that the pH-regulation took up most energy consumption (72%) in our system, and the whole system power consumption of per ton of wastewater was 0.605 kWh/m3, which translates into a cost of \$0.04/m³ based on the average US industrial electricity rate (\$0.0653/kWh). Iron sheet is very cheap and highly reusable (\$1.4), which can counteract the cost. The cost of H₂O₂ was \$0.16 with 0.6 L of consumption per ton of water, while the unit price of H₂O₂ was \$0.27/L. Furthermore, in situ electrochemical synthesis of highly concentrated H₂O₂ (Yamanaka et al., 2003; Chen et al., 2017) could be used as a replacement for externally supplied H₂O₂ in the future, eliminating the chemical cost.

The specific energy consumption was calculated in terms of the removal of 1 kg of COD from PNP wastewater by the Fenton process (kWh/kg COD) using **Eq. 13**, where U, I, and t are the average voltage (V), applied current (A), and electrolysis time (s), respectively (Kurt et al., 2007; Zhao et al., 2016).

$$SEC = \frac{U \times I \times T}{(COD_0 \times V_0 - COD_t \times V_t) \times 3.6}$$
 (13)

After pH adjustment and the 30-min ICEF process, the PNP mineralization shows an SEC value of 4.92 kWh/kg COD, the results in this study demonstrated that the ICEF system was environmentally friendly, efficient, and inexpensive in comparison. It was proven that the operation of the system greatly enhanced the treatment of PNP wastewater. Compared to traditional Fenton and other electro-Fenton systems, the ICEF system has its own merits. Firstly, the pH-regulation divided electrolysis cell with the PTFE membrane as the separating material was simple and convenient compared to

others, an acidic pH of 3.0–3.2 was automatically attained at a steady state within 1 min, which is suitable for most Fenton-like reactions (Babuponnusami and Muthukumar, 2014). In contrast, \sim 60 min was required in the divided electrolysis cell using an ion exchange membrane as the separating material (Liu et al., 2007). Secondly, the cathode potential applied on the iron plate can decrease amounts of iron irons released under acid solution and precisely control the Fe (tot) production, avoiding the addition of iron salt and increase of water salinity. All these advantages together suggest that the ICEF system has potential for cost-effective and efficient degradation of recalcitrant organic pollutants. Future work should also focus on improving the efficiency of cathode reduction of ferric iron and improving the efficiency of H_2O_2 utilization.

CONCLUSION

In this study, a novel eco-friendly iron cathode electrochemical Fenton (ICEF) system coupled with a pHregulation divided electrolysis cell was developed for PNP degradation. In such a system, 100 mg/L of PNP was not only effectively degraded within 30 min (97%), but also efficiently mineralized with a COD and TOC removal efficiency of 79 and 60%, respectively. The optimal cathode potential exhibited strong inhibition on Fe (tot) production with the concentration of Fe (tot) significantly decreasing from 52 to 21 mg/L, minimizing the ferric sludge generation. And the conductivity increased slightly from 4.35 to 4.37 mS/cm, indicating that the present combined process negligibly affected the salt content of the wastewater. Notably, the system was inexpensive with an energy consumption of 4.92 kWh/kg COD. In general, demonstrated that the present combined system is an effective and environmentally friendly technology for wastewater treatment.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

XW: Conceptualization, Investigation, Writing, and Original Draft preparation. JZ: Investigation and Formal analysis. CS: Formal analysis and Investigation. XS: Validation, Formal analysis, Investigation, and Supervision. PD: Software and Methodology.

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Conflict of Interest: Authors XW, JZ, CS, XS and HD were employed by company Shengli Oilfield Testing and Evaluation Research Co., Ltd., SINOPEC.

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Highly Dispersed CoO Embedded on Graphitized Ordered Mesoporous Carbon as an Effective Catalyst for Selective Fischer–Tropsch Synthesis of C₅₊ Hydrocarbons

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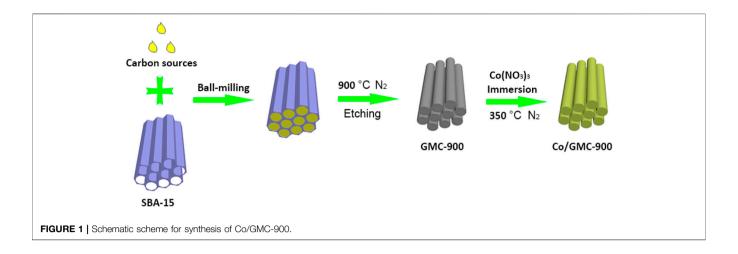
Bai J, Song M, Pang J, Wang L, Zhang J, Jiang X, Ni Z, Wang Z and Zhou Q (2022) Highly Dispersed CoO Embedded on Graphitized Ordered Mesoporous Carbon as an Effective Catalyst for Selective Fischer–Tropsch Synthesis of C₅₊ Hydrocarbons. Front. Chem. 10:849505. doi: 10.3389/fchem.2022.849505 Herein, we report the high Fischer–Tropsch synthesis performance of the Co-based catalysts supported on graphitized ordered mesoporous carbon (GMC-900) by using a facile strategy. Compared with CMK-3 and active carbon (AC), the obtained GMC-900 by using pollution-free soybean oil as a carbon source exhibited enhanced catalytic performance after loading Co species due to its highly crystallized graphitic structure and uniform dispersion of CoO. As a result, Co/GMC-900 was an effective catalyst with the maximum C_{5+} selectivity of 52.6%, which much outperformed Co/CMK-3 and Co/AC. This research provides an approach to produce advanced Co-based catalysts with satisfactory performance for efficient Fischer–Tropsch synthesis.

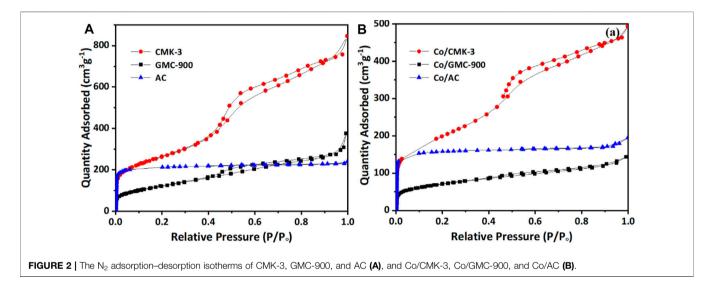
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INTRODUCTION

With the rapid development of human society and economy, it becomes more and more difficult for crude oils to meet people's demands (Guo et al., 2016; Hao et al., 2016; Zhang et al., 2017). Furthermore, the serious problems of air pollution and greenhouse effect caused by the consumption of fossil fuels have impelled the search for more clean alternatives (Qin et al., 2016). Fischer–Tropsch synthesis (FTS) is an alternative route that can transform synthesis gases resulting from gasification of biomass, natural gases, and coals into clean liquid fuels or chemicals without containing nitrogen, sulfur, or aromatics (Liu et al., 2018; Lyu et al., 2018). Traditionally, Ru-based catalysts exhibit high low-temperature selectivity and activity for long-chain hydrocarbons (Guo et al., 2019). However, the large-scale commercial application in industry is severely hampered by some major problems, especially the scarcity in nature and expensive prices (Liu et al., 2018; Guo et al., 2019). In comparison, Co-based catalysts, one of the most optimal choices for FTS due to their low costs, are highly active and selective toward long-chain hydrocarbons, and possess water deactivation stability and low water–gas shift activity during the reaction (Johnson and Bell, 2016; Cheng et al., 2018).

The support of Co-based catalysts greatly influences the catalytic performance during the reaction (Fu and Li, 2015; Qin et al., 2016). Conventionally, various oxide materials such as SiO_2 , Al_2O_3 , and





 ${
m TiO_2}$ are used to support Co-based catalysts. ${
m SiO_2}$ and ${
m Al_2O_3}$ are preferentially used owing to their large surface areas, abrasion resistance, and excellent mechanical properties (Bustamante et al., 2020; Wolf et al., 2020; Xu et al., 2020). However, the relatively strong interaction between cobalt oxide and the support leads to the generation of irreducible substances, such as ${
m CoAl_2O_4}$ or ${
m Co_2SiO_4}$ (Bustamante et al., 2020; Li et al., 2020). As a result, the number of surface active sites on the support decreases, which limits the activity for long-chain hydrocarbons (Wang et al., 2020). Therefore, exploring suitable Co-based catalysts with the low formation of hardly reducible materials is highly desirable.

Carbon materials are also considered as some of the most desirable supports in FTS owing to their unique specific structure and chemistry, such as surface inertness, controllable crystallized graphitic structure, high conductivity, and acid or alkali resistance (Lyu et al., 2019; Dlamini et al., 2020). Reuel and Bartholomew (1984) found that the catalytic performance in CO hydrogenations dropped considerably with the increase of cobalt dispersion degree as follows: $\text{Co/TiO}_2 > \text{Co/SiO}_2 > \text{Co/Al}_2\text{O}_3 > \text{Co/C} > \text{Co/MgO}$. Tavasoli et al. (2008) reported that Co/CNT

catalysts prepared from the impregnation method exhibited much larger activity than $\text{Co/Al}_2\text{O}_3$ on hydrocarbon yield, which can be ascribed to the weak interaction between Co species and CNT. In addition, mesoporous carbon (MC) using mesoporous silica as a precursor has also received much attention on FTS owing to its ordered pore structure and large surface area (Wu et al., 2019). Zhao et al. (2020) prepared Co/MC-1300 (where MC was prepared from pyrolysis of furfuryl alcohol and SBA-16 as the hard template), which showed improved cobalt reducibility and C_{5+} selectivity up to 74%.

The structure of carbon supports, particularly the porous structure, greatly influences the FTS performance (Xiong et al., 2011). Nonetheless, the impact of different carbon sources as the support on the structure and catalysis in FTS is rarely reported. Herein, we report the high Fisher-Tropsch synthesis performance of the Co catalysts supported on graphitized ordered mesoporous carbon (GMC-900) by using pollution-free soybean oil as a carbon source. We also chose the porous CMK-3 prepared and commercial AC from other carbon sources as the supports and controls to evaluate the catalytic performance of GMC-900 in FTS.

TABLE 1 | Physicochemical properties of carbon supports and catalysts.

Sample	Surface area (m ² g ⁻¹)	Pore size (nm)	Pore volume (cm ³ g ⁻¹)
GMC-900	442	5.24	0.58
CMK-3	939	5.57	1.31
AC	657	2.25	0.37
Co/GMC-900	306	3.51	0.26
Co/CMK-3	709	4.30	0.76
Co/AC	492	2.44	0.30

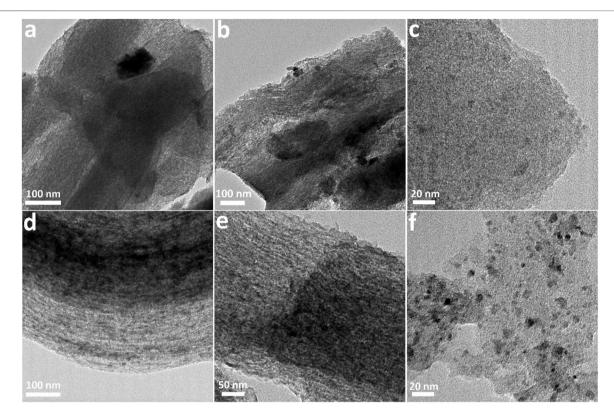


FIGURE 3 | TEM images of CMK-3 (A), GMC-900 (B), AC (C), and the corresponding Co-based catalysts (D-F).

EXPERIMENTAL

Chemicals

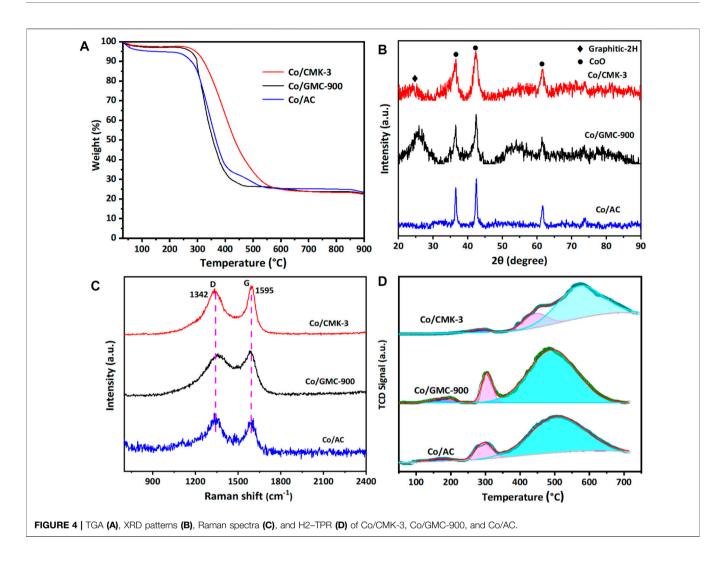
Poly-(ethylene glycol)-block-poly-(propylene glycol)-poly-(ethylene glycol) (P123, average Mn ~5,800) was supplied from Sigma-Aldrich. Ethyl silicate (TEOS, $SiO_2 \ge 28\%$) was purchased from Shanghai Lingfeng Chemical Reagent Co., Ltd., China. Active carbon (AC) was obtained from Huajing Activated Carbon Co., Ltd., China. CMK-3 was supplied Nanjing Xianfeng from Nanomaterials Technology Co. Ltd., and soybean oil was obtained from Jiangsu Junqi Grain and Oil Co., Ltd. Ethanol, glycerol, hydrochloric acid, sodium hydroxide, cobalt nitrate, and dicyandiamide were obtained from Sinopharm Chemical Reagent Co., Ltd. (China). Nitrogen (99.5%), argon (99.999%), hydrogen argon mixed gas $(V_{H2}/V_{Ar} = 5/95)$,

and syngas ($V_{\rm H2}/V_{\rm CO}/V_{\rm Ar}$ = 64:32:4) were purchased from Shanghai Pujiang Gas Co., Ltd. (China). All chemicals were used as received.

Sample Preparation

Synthesis of Mesoporous Molecular Sieve SBA-15

Typically, 6 g of the mixture of P123 and glycerol with the same mass ratio was dispersed into 115 g of hydrochloric acid aqueous solution (M $_{\rm HCl}=1.5$ M) under vigorous stirring at 37°C for 3 h. Then, 6.45 g of ethyl silicate (TEOS) was added dropwise under vigorous stirring. After 5 min, the resulting mixture was kept static for 24 h, and then the obtained mixture was treated with a drying box at 110°C for 12 h. The dried product was gathered by filtering and washing, and dried at 80°C overnight. Finally, SBA-15 was obtained *via* calcination at 550°C for 5 h to get rid of the surfactant.



Synthesis of GMC-900

GMC-900 was prepared by a simple solid–liquid grinding/templating route and calcination using SBA-15 as a hard template and soybean oil as a carbon source. In a typical synthesis, the mixture of SBA-15 and soybean oil with a mass ratio of 1:2 was ground together homogeneously under ball milling (400 rpm min⁻¹) for 5 h; then the mixture obtained was transferred into a quartz boat and calcined at 900°C for 5 h (heating ramp 4°C min⁻¹) in nitrogen gas. Finally, the obtained product was treated by NaOH aqueous solution etching to remove SBA-15, and then filtered and dried to collect GMC-900.

Synthesis of Co/GMC-900, Co/CMK-3, and Co/AC

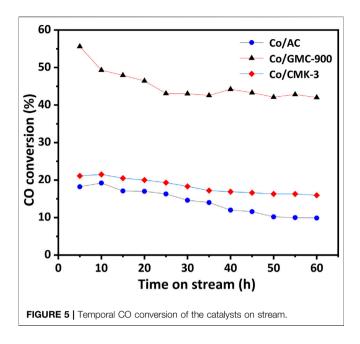
In general, Co/C was prepared using the impregnation method. Briefly, 0.8 g of GMC-900 (or CMK-3 or AC) was added into a cobalt nitrate ethanol solution (0.8719 g, Co (NO₃)₂·6H₂O) under stirring, and stirring was continued for 1 h. Then the cobalt nitrate ethanol solution was evaporated at 35°C in a rotary evaporator. Finally, the obtained mixture was dried at 50°C for 12 h, and then carbonized at 35°C in nitrogen gas. The products were marked as Co/GMC-900, Co/CMK-3, and Co/AC, respectively.

Characterizations

The microstructure of materials was characterized by a JEOL JEM-2010 transmission electron microscope (TEM, 200 kV). The Barrett–Joyner–Halenda (BJH) pore size distributions and Brunauer–Emmett–Teller (BET) specific surface areas were measured by N_2 ad-/desorption isotherms. X-ray diffraction (XRD) was measured on a Rigaku D/Max2rB-II device (Cu Kα radiation, $\lambda = 1.5406 \, \text{Å}$) at a rate of 4°min^{-1} from 20 to 90° . Thermogravimetric analysis (TGA) was carried out by a TGA 8000 analyzer by heating to $900\,^\circ\text{C}$ at a rate of $10^\circ\text{C} \, \text{min}^{-1}$. Raman spectra were observed on a Dilor Labram-1B spectrometer with a 632-nm laser. The behaviors of the samples in H_2 temperature-programmed reduction (TPR) were investigated on a home-made instrument with a thermal conductivity detector (TCD).

Catalysis Measurement

Catalytic performances were assessed using a tubular fix-bed reactor at 270°C, p = 2 MPa, and $H_2/CO = 2$. Briefly, the isothermal zone of the reactor was placed with a catalyst (0.3 g) blended with quartz granules (40–60 meshes, 2.4 g), and its remaining part was filled with the quartz granules. The



 $\mbox{\bf TABLE 2 | FTS catalytic performance of Co/GMC-900, Co/CMK-3, and Co/AC catalysts.} \label{eq:complexity}$

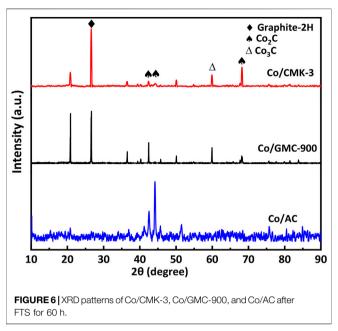
Catalyst	CO conv. (%)	Selectivity (%)			CO ₂ selectivity (%)
		CH₄	C ₂ -C ₄	C ₅₊	
Co/GMC-900	45.2	22.4	25.1	52.6	36.4
Co/CMK-3	18.1	32.1	29.2	24.3	30.7
Co/AC	13.3	43.7	36.0	20.8	88.7

reactor was maintained at 450°C and 0.4 MPa in H_2 atmosphere ($H_2/Ar = 5/95$, v/v) for 16 h. After *in situ* catalyst reduction, the reactor was cooled to 120°C in H_2 atmosphere. Then the syngas $H_2/CO/Ar$ (64:32:4) flowed at a rate of 30 ml min⁻¹ (GHSV = 3.6 L h⁻¹ g⁻¹) through the catalysis bed at 2 MPa and 270°C. Unreacted gases (H_2 , N_2 , and CO) and by-products (CH₄ and CO₂), and hydrocarbons (C_1 – C_{30}) can be detected by TCD and flame ionization detector, respectively.

RESULTS AND DISCUSSION

The procedure for Co/GMC-900 preparation is demonstrated in **Figure 1**. In brief, SBA-15 was synthesized in an acidic environment with ethyl silicate as the silicate source and P123 as the soft template. Subsequently, the obtained SBA-15 was mixed with edible soybean oil through ball-milling to form a homogeneous mixture. Then GMC-900 was collected through carbonizing and etching the above mixture. Finally, Co (NO₃)₃ and GMC-900 were mixed by immersion and heat treatment to form Co/GMC-900.

 N_2 ad-/desorption isotherms used to explore the specific area before and after cobalt loading are displayed in **Figure 2**. Both GMC-900 and CMK-3 correspond to class IV curves with a typical hysteresis loop at relative pressure P/P_0 of 0.4–1.0



(Figure 2A), which suggests the existence of a mesoporous structure (Zhao et al., 2020). The ad-/desorption isotherm of AC is a class I curve, which is characteristic of microporous structures (Asami et al., 2013). After cobalt impregnation, similar ad-/desorption isotherms were found for these catalysts (Figure 2B), suggesting the carbon supports are almost structurally constant (Fu and Li, 2015). The physicochemical properties of carbon supports and catalysts are listed in Table 1. The specific surface areas of CMK-3 and AC (939 and 657 m 2 g $^{-1}$, respectively) greatly surpass that of GMC-900. However, the average pore diameter of AC (2.25 nm) is smaller than those of CMK-3 and GMC-900. Furthermore, the pore volumes and specific surface areas of catalysts decrease after loading Co species on the carbon supports. The reason for these results is that the adsorption of cobalt oxide particles onto mesoporous walls leads to the blockage of small pores (Khodakov et al., 2002). Compared with other catalysts, the pore volume of AC decreases slightly, resulting from the entrance of micropores being more easily blocked than that of mesopores.

As shown in **Figure 3**, the TEM images further reveal the typical mesoporous and morphological structures of mesoporous carbon materials and the corresponding Co-based catalysts. **Figure 3A** exhibits the ordered mesoporous structure of CMK-3. GMC-900 is similar to CMK-3, while the mesoporous structure was damaged slightly due to the high-temperature treatment (**Figure 3B**) (Hanzawa et al., 2002). After Co species loading, the morphological structures of catalysts are very different. As for Co/CMK-3 and Co/GMC-900, CoO was uniformly dispersed in the mesopores (**Figures 3D,E**). However, the ordered meso-structure of Co/GMC-900 was partially damaged, which can be due to both high temperature and Co species loading (Fu and Li, 2015). As for Co/AC, some particles appeared due to the aggregation of CoO after Co species loading (**Figure 3F**).

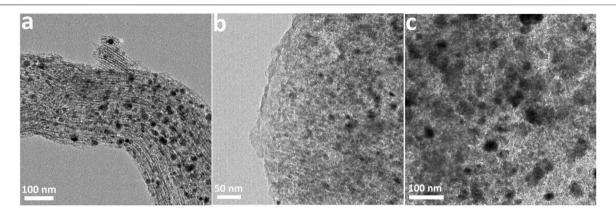


FIGURE 7 | TEM images of Co/CMK-3 (A), Co/GMC-900 (B), and Co/AC (C) after 60 h for FTS.

The thermal stability and amount of CoO in the catalysts were analyzed by TGA in air atmosphere (Figure 4A). All the catalysts experienced mass losses of about 76.3% during calcination. The first mass loss below 200 °C was due to the desorption of physically adsorbed water (Liu et al., 2018). The second remarkable mass loss occurs at 240-600 °C, corresponding to the combustion of graphitic carbon (Qin et al., 2016; Sun et al., 2012). The structural characteristics of Co/CMK-3, Co/GMC-900, and Co/AC were determined by XRD patterns (Figure 4B). The peaks at around 36.4, 42.3, 61.6, 73.9, and 77.8° are indexed to the (111), (200), (220), (311), and (222) reflection for the CoO phase (JCPDS no. 43-1004) (Loewert et al., 2020; Xu et al., 2020). The broad peak at around 26.6° can be attributed to the graphitic carbon (JCPDS no. 41-1487) (Qiu et al., 2014). Compared with Co/CMK-3 and Co/AC, the intensity of this strong graphitic peak for GMC-900 indicates a high degree of graphitization (Torshizi et al., 2020). In addition, the strong peaks of CoO in Co/AC suggest that the particle size of CoO is larger than those of Co/ CMK-3 and Co/GMC-900, which is in accordance with the TEM image (Figure 3F). Calculation shows that the average particle sizes of CoO in Co/CMK-3, Co/GMC-900, and Co/AC are 6.9, 11.6, and 19.2 nm, respectively.

To further check the carbon structures of the obtained materials, we conducted Raman spectra to recognize the changes of carbon species and the defects in the graphite layer. All catalysts display a D band at around 1342 cm⁻¹ and a G band at around 1595 cm⁻¹ (Figure 4C). The D band corresponds to a defect in the lattice of carbon atoms, while the G band reflects the change of sp² hybridized carbon atoms in the graphite layer (Trépanier et al., 2009; Vosoughi et al., 2016; Zeng et al., 2021). Generally, the ratio of relative integrated intensity (I_D/I_G) between these two bands implies the degree of graphitization and the disorder degree of functionalized groups and defects, which was calculated to be 1.98, 1.55, and 2.65 for Co/CMK-3, Co/GMC-900, and Co/AC, respectively. These results indicate that GMC-900 has a high degree of graphitization than Co/CMK-3 and Co/AC, which are in accordance with the above XRD results.

The reducibility of catalysts can be evaluated by H_2 -TPR measurements (**Figure 4D**). Obviously, all the catalysts display

three partially overlapped peaks. The first and second peaks reflect the reduction of $\mathrm{Co_3O_4}$ to CoO , and the reduction of CoO to Co , respectively, and the third reduction peak in the TPR spectra implies the gasification of carbon support (Sun et al., 2012). The third reduction peak around 574°C for $\mathrm{Co/CMK-3}$ is higher than that for $\mathrm{Co/GMC-900}$ and $\mathrm{Co/AC}$, which indicates that it is more irreducible. The absence of the reduction peak above $600^{\circ}\mathrm{C}$ suggests no formation of hardly reducible substances on the catalyst surface because of the much lower interaction of carbon support with Co species than with traditional oxides ($\mathrm{TiO_{2}}$, $\mathrm{Al_2O_{3}}$, or $\mathrm{SiO_{2}}$) (Bai et al., 2012; Cheng et al., 2018).

Catalytic behaviors of all the catalysts were explored by FTS performed at p = 2 MPa, $T = 270^{\circ}\text{C}$, $H_2/\text{CO} = 2$, and GHSV = $3.6 L h^{-1} g^{-1}$. Before reaction, the catalysts were reduced in situ in H2 flow at 450°C for 16 h. Figure 5 exhibits the temporal CO conversion on stream within a time period of 60 h. Among the catalysts, the Co/GMC-900 exhibits relatively higher CO conversion, and even after 60 h, it still has the CO conversion above 40%. As for the Co/CMK-3, the CO conversion is relatively lower than that of Co/GMC-900, while the catalytic activity is more stable (CO conversion decreasing from 21 to 15%). These results can be explained by its ordered pore structure, large specific surface area and pore volume, and open pore structure, benefiting the adsorption and diffusion of syngas in the catalysts (Ahn et al., 2016). By contrast, the Co/AC exhibits lower CO conversion, which can be ascribed to the poor dispersion of CoO (Figure 3C).

Table 2 lists the results of catalysts in FTS, including the catalytic behaviors and production distribution. These data were the mean values over 60 h. Clearly, Co/GMC-900 has a maximum CO conversion rate of 45.2%, resulting from the more reducible of Co/GMC-900 than that of Co/CMK-3 and Co/AC so that it can offer more active sites for FTS. In addition, the highly crystallized graphitic structure of GMC-900 can accelerate the electron transport between CoO and CO, thus facilitating the activation of CO (Reuel and Bartholomew, 1984; Fan et al., 2009). In comparison, despite the high dispersion of CoO on CMK-3, large specific surface area, and the orderly mesoporous structure, Co/CMK-3 only achieved the CO conversion of

18.1%, which can be attributed to the less crystallized graphitic structure of CMK-3. In addition, compared with Co/CMK-3 and Co/AC, Co/GMC-900 was less selective toward CH₄ (22.4%) and C₂–C₄ hydrocarbons (25.1%) (**Table 2**), resulting in the increased C₅₊ selectivity of Co/GMC-900. For Co/CMK-3, the higher CH₄ selectivity can be assigned to smaller CoO particles.

Figure 6 exhibits the XRD patterns of all the catalysts after 60 h for FTS. Three strong diffraction peaks at 42.5, 45.7, and 68.3° in the XRD patterns of these catalysts are assigned to Co₂C (JCPDS 72-1369) (LÜ et al., 2012). The other diffraction peaks at 60 and 75° correspond to Co₃C (JCPDS 89-2866) (Liu et al., 2019). These results suggest the appearance of new species of catalysts during FTS, resulting from the decreased conversion of CO. Compared with unreacted catalysts, the peak at around 26.1° in the XRD patterns of used Co/CMK-3 and Co/GMC-900 is stronger, indicating the slight carbon deposition on the catalyst surface (Qin et al., 2019). The aggregation of Co species in catalysts with different sizes was shown in the TEM images (Figure 7). In comparison, Co/GMC-900 has a slight aggregation, resulting in the CO conversion which is decreased slowly than that of Co/CMK-3 and Co/AC. This result is in accordance with the results of Table 2.

CONCLUSION

In summary, we demonstrate a simple method to prepare Cobased catalysts supported on graphitized ordered mesoporous carbon (GMC-900) for FTS. Compared with other mesoporous carbon (CMK-3 and AC), the obtained GMC-900 by using pollution-free soybean oil as a carbon source exhibited enhanced catalytic performance after loading Co species due to its highly crystallized graphitic structure and uniform dispersion of CoO. FTS results indicate Co/GMC-900 has high catalytic effectiveness with the largest C_{5+} selectivity up to 52.6%, which greatly surpasses those of Co/CMK-3 and Co/AC.

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Therefore, our work provides important information to produce high-performance FTS catalysts through ball-milling of clean soybean oil as a carbon source.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material; further inquiries can be directed to the corresponding authors.

AUTHOR CONTRIBUTIONS

JB contributed to conceptualization, methodology, and writing—original draft. MS contributed to methodology and investigation. JP contributed to investigation. LW contributed to investigation resources. JZ contributed to resources. XJ contributed to resources and funding acquisition. ZN contributed to resources and supervision. ZW contributed to conceptualization and project administration. QZ contributed to resources and funding acquisition. All authors contributed to manuscript revision, and read and approved the submitted version.

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Fabrication and Characterization of the Porous Ti₄O₇ Reactive Electrochemical Membrane

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Preparation of the Magnéli Ti₄O₇ reactive electrochemical membrane (REM) with high purity is of great significance for its application in electrochemical advanced oxidation processes (EAOPs) for wastewater treatment. In this study, the Ti_4O_7 REM with high purity was synthesized by mechanical pressing of TiO₂ powders followed by thermal reduction to Ti₄O₇ using the Ti powder as the reducing reagent, where the TiO₂ monolith and Ti powder were separated from each other with the distance of about 5 cm in the vacuum furnace. When the temperature was elevated to 1333 K, the Magnéli phase Ti₄O₇ REM with the Ti₄O₇ content of 98.5% was obtained after thermal reduction for 4 h. Noticeably, the surface and interior of the obtained REM bulk sample has a homogeneous Ti₄O₇ content. Doping carbon black (0wt%-15wt%) could increase the porosity of the Ti₄O₇ REM (38-59%). Accordingly, the internal resistance of the electrode and electrolyte and the charge-transfer impedance increased slightly with the increasing carbon black content. The optimum electroactive surface area (1.1 m²) was obtained at a carbon black content of 5wt%, which increased by 1.3-fold in comparison with that without carbon black. The asprepared Ti₄O₇ REMs show high oxygen evolution potential, approximately 2.7 V/SHE, indicating their appreciable electrocatalytic activity toward the production of •OH.

Keywords: Ti4O7, reactive electrochemical membrane, Ti, TiO2, thermal reduction

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1 INTRODUCTION

Ceramic porous sub-stoichiometric Ti oxides (${\rm Ti_nO_{2n-1}}$, $4{\le}n \le 10$), known as Magnéli phases, were first synthesized and characterized in the 1950s (Zhou et al., 2018). Among these oxides, ${\rm Ti_4O_7}$ exhibits excellent performance owing to its unique structure, e.g., excellent corrosion resistance and outstanding electrical conductivity with a value of $1000~{\rm S~cm^{-1}}$, which is higher than the 727 S cm⁻¹ of graphitized carbon (Walsh and Wills, 2010). In light of this, the ${\rm Ti_4O_7}$ material has been widely used as a cathodic protection during the electrodeposition process, in batteries as either an electrode material or an additive to the active materials (Zhang et al., 2017). In addition, due to its stability under anodic polarization and high oxygen evolution overpotential, ${\rm Ti_4O_7}$ has been recently utilized as the inert anode material for weekly sorbed ${\bullet}{\rm OH}$ production in the field of electrochemical wastewater treatment, which shows comparable electrocatalytic activity to the boron-doped diamond (BDD) anode for pollutant degradation (Bejan et al., 2009).

Recently, depositing Ti₄O₇ films at the Ti surface has been manufactured successfully by the plasma coating approach, which is a widely spread technology for many types of applications (corrosion protection, abrasion resistance, thermal barriers, etc.) (Ganiyu et al., 2016; Oturan et al.,

Ti₄O₇ Reactive Electrochemical Membrane

2017). This preparation process is mainly proceeded by two steps: 1) reduction of TiO_2 with coke to produce Ti_xO_{2x-1} powder and 2) plasma elaboration of Ti_xO_{2x-1} on the Ti-alloy substrate at 10,000-15,000°C accompanied by conversion of all sub-oxides of Ti to Ti₄O₇ [46]. However, the application of this Ti₄O₇ electrode is greatly limited by mass diffusion since there is a thick stagnant boundary layer (~100 µm) at the plate electrode surface (Liu and Vecitis, 2012; Zaky and Chaplin, 2013). The flow-through mode, which is defined as operating with convective flow perpendicular to the porous electrode surface, allowed for enhanced mass transport rates relative to the traditional parallel flow mode by restricting the diffusional distance of reactants to a length-scale on the order of the pore radius of the electrode (Vecitis et al., 2011; Zaky and Chaplin, 2013; Guo et al., 2016a; Guo et al., 2016b). Thus, significant attention has been recently paid to the integration of membrane filtration electrochemical process, known as the Ti₄O₇ reactive electrochemical membrane (REM), for aqueous contaminant degradation because this operation mode promotes the reaction between the contaminant and •OH produced at the anode surface. As a result, REMs based on electrochemical advanced oxidation processes (EAOPs) are a cutting edge class of electrodes that hold great promise in revolutionizing water/ wastewater treatment (Zaky and Chaplin, 2013).

As for the preparation of the Ti₄O₇ REM, TiO₂ is typically used as the main feedstock due to its abundance and relatively low cost. The mechanical pressing of Ti₄O₇ powders, followed by thermal sintering, has been widely used to fabricate the Ti₄O₇ REMs. There are many conventional approaches available to synthesize the Ti₄O₇ materials under controlled reducing conditions at relatively high temperature using different reducers such as metals (Kitada et al., 2012), carbon (Ganiyu et al., 2016), carbonaceous organic materials (Guo et al., 2019), and reducing atmosphere (H₂ and NH₃) (Li et al., 2010; Zhang et al., 2013; Lin et al., 2018). However, most of the production methods are energy and time-consuming. For example, the Ti₄O₇ REM was synthesized by reduction of commercial TiO2 ultrafiltration membranes at 1333 K for 50 h in the H₂ atmosphere (Guo et al., 2016b). As another example, an ultrafiltration membrane layer composed of Ti₄O₇ and Ti₆O₁₁ was obtained by dip-coating of a TiO₂ layer on the inner surface of a tubular Al₂O₃ membrane, followed by a reduction step under 30% H₂ in the Ar atmosphere at 1308K for 7 h (Geng and Chen, 2016). High processing temperatures over 1000°C and such long time not only inevitably leads to morphology deformation but also results in particle aggregation and dense low surface area materials, which limit its practical applications as electrode materials, where high surface area, a large number of active sites, and a porous structure are all important for the performance (Lin et al., 2018). In addition to the cases under the reducing atmosphere (H₂ and NH₃), the as-prepared Ti₄O₇ REMs did not have high purity since the residual reducing reagents and their derivatives eventually reduce the purity of the obtained Magnéli Ti₄O₇ REM. However, the gaseous reduction process usually brings about high costs and potential danger. The high preparation costs and rigorously controlled fabrication conditions (H2 atmosphere) might limit their commercial development to some extent. Overall, the control of the stoichiometry of Magnéli phases according to the choice of precursors and thermal treatment is an interesting challenge for material science.

In the present study, thermal reduction of ${\rm TiO_2}$ by metal Ti under the vacuum condition was developed to prepare the ${\rm Ti_4O_7}$ REM with high purity. The influences of the preparation temperature and thermal sintering time were optimized for ${\rm Ti_4O_7}$ REM preparation. The ${\rm Ti_4O_7}$ REM was characterized using X-ray diffraction (XRD), scanning electron microscopy (SEM), and mercury intrusion porosimetry. The water filtration performance of these REMs was evaluated based on the pressure-normalized permeate flux. In addition, the electrochemical properties of the REMs were studied by sweep voltammetry (CV) and electrochemical impedance spectroscopy (EIS).

2 MATERIALS AND METHODS

2.1 Reagents

 ${
m TiO_2}$ (99.99%, 25 nm particles) and Ti (99.9%, 10 nm particles) powder were purchased from Beijing Xingyuan Technology Co., Ltd. Carbon black (XC-72R) was bought from Cabot Corporation. Ethanol (EtOH) (99.99%, anhydrous), sodium sulfate (99.9%), potassium ferrocyanide (99.5%), and potassium ferricyanide (99.5%) were obtained from Sigma-Aldrich. All solutions were prepared using deionized water (18.2 ${
m M}\Omega$ cm⁻¹ at 25°C).

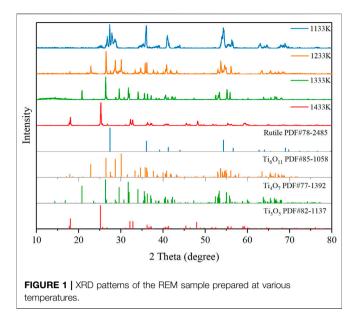
2.2 Ti₄O₇ REM Fabrication

The Ti₄O₇ ceramic microfiltration membrane was prepared by the following route: TiO2 powder and carbon black were first mixed together and then put into a ZrO₂ ball-milling bowl (500 ml in volume, Fritsch, Germany), where the load of carbon black was set to 7.5% of the mass of the TiO₂ powder. A planetary ball-mill (Fritsch, Pulverisette 6, Germany) was utilized to mix the membrane contents, in which the grinding balls were a mixture of Nikkato ZrO₂ balls in the diameters of 1, 2, 5, 10, and 20 mm. The volume of the balls and the material account for 1/3 of the volume of the ball mill tank, respectively. Anhydrous ethanol is used as a ball milling agent. After allowing it to dry at 60°C overnight, 10 g powders were mixed with 2-3wt% of ethanol and transferred to a disc mould and pressed under the pressure of 30 MPa by a hydraulic press (Specac, UK) to form the precursor of the REM. The membrane was first sintered in air for 4 h at 973 K for the removal of carbon black then was reduced in the presence of the Ti powder (about 4 g) in a vacuum ($<8 \times$ 10^{-3} MPa) tube furnace for the preparation of the Ti₄O₇ REM. The precursor of the Ti₄O₇ monolith and Ti powder were separated from each other, and the distance is about 5 cm. The heating/cooling rates were both 4 K min⁻¹.

2.3 Physicochemical and Electrochemical Characterization

XRD analysis was performed to obtain the phase information of the ${\rm Ti_4O_7}$ REM. The Scherrer equation was used to calculate the

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crystallite size. The Ti₄O₇ REM surface morphology was characterized by SEM. Mercury intrusion porosimetry was used to investigate the porous structures of the electrodes. The EIS and CV analyses were conducted with an electrochemical workstation (PGSTAT302N, Metrohm) and used a threeelectrode setup with the Ti₄O₇ electrode as the working electrode, a platinum plate electrode (3 cm × 3 cm) as the counter electrode, and a saturated calomel electrode (SCE) as the reference electrode. EIS analysis was performed at the open circuit potential (OCP, 190 mV/SCE) over a frequency range of 10⁻²-10⁴ Hz in 100 mM Na₂SO₄ supporting electrolyte solution with the presence of 5 mM K₄Fe(CN)₆ and 5 mM K₃Fe(CN)₆ redox couple. CV measurements were recorded at a voltage step of 0.05 V in 100 mM NaClO₄ electrolyte. The electrochemically active surface area was calculated based on CV analysis at a scan rate from 5 to 30 mV s⁻¹ in a potential range of -0.2–0.5 V.

3 RESULTS AND DISCUSSION

3.1 Ti₄O₇ REM Fabrication

The effect of thermal reduction temperature on the purity of the Ti_4O_7 REM was conducted in the range of 1133-1433 K. **Figure 1** shows the XRD patterns of the REM samples prepared at various temperatures. It was observed that the color of the REM sample turned from white to light blue after thermal reduction at the reduction temperature of 1133 K. But the obtained REM sample was mainly rutile. This indicates that this reaction temperature was sufficient for the reduction of Ti^{4+} in anatase- TiO_2 to Ti^{3+} , while it was not high enough to transform anatase- TiO_2 to the Magnéli phase. The phase transformation was observed at a sintering temperature of 1233 K, where the predominant phase was Ti_6O_{11} and Ti_5O_9 was the marginal phase. When the temperature was elevated to 1333 K, the XRD patterns show the characteristic peaks for Ti_4O_7 , and almost no peaks for other Magnéli phases suggests that a high purity Magnéli phase Ti_4O_7

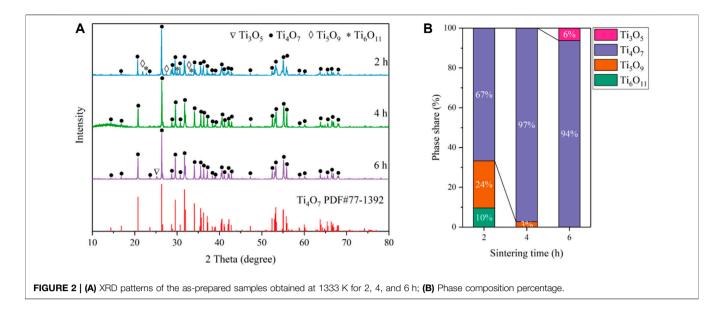
REM was successfully fabricated. At this temperature, the ${\rm Ti_4O_7}$ content of the samples was 98.5%, while the ${\rm Ti_3O_5}$ content was only 1.5%. In contrast, when the reduction temperature was further increased to 1433 K, a single phase of ${\rm Ti_3O_5}$ is formed, indicating that this reaction temperature was too high to synthesize pure ${\rm Ti_4O_7}$.

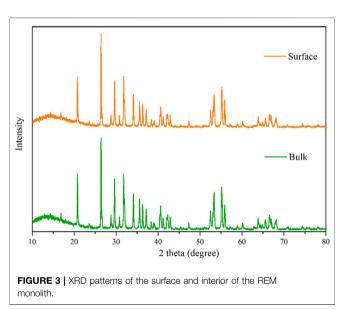
To further find the optimal conditions for the synthesis of Ti₄O₇, the influence of thermal reduction time on the purity of the Ti₄O₇ REM was also studied. The XRD patterns of the asprepared REM samples prepared at 1333K for 2, 4, and 6 h are shown in Figure 2. It is found that the Magnéli phase Ti₄O₇ was the major component at the thermal reduction time of 2–6 h. For 2 h, the as-prepared REM sample contains 24% Ti₅O₉, 10% Ti₆O₁₁, and 66% Ti₄O₇. When the thermal reduction time reached 4 h, XRD patterns show that Ti₅O₉ and Ti₆O₁₁ phases disappeared and Ti₄O₇ to be the main crystalline phase in the material with only <3% Ti₃O₅ left. Extending the reaction time to 6 h, the percentage of Ti₃O₅ phases increased slightly to 6%, and the percentage of Ti₄O₇ exhibited an insignificant change. These results mean that the thermal reduction time of 2 h is insufficient for the complete transformation of TiO₂ to Ti₄O₇. However, as for 6 h, the increase of the miscellaneous peak, especially Ti₃O₅, indicates that the sample proceeded overreduction due to the longer thermal reduction time. These results illustrate the optimum reduction time for preparing the pure Ti₄O₇ REM was 4 h.

The XRD peaks for the reduced phases are relatively sharp (fwhm = 0.117° for 2 h, 0.084° for 4 h and 0.092° for 6 h) for the peaks at 26.4°, respectively. After accounting for instrumental broadening, the estimated crystallite sizes are 67 nm for 2 h, 90 nm for 4 h, and 119 nm for 6 h according to the Sherrer's equation, while the crystallite size of the original TiO₂ is 25 nm, indicating the crystallite growth. For further investigation of the phase composition of the productions, the XRD spectrums of the REM those were not grounded into powder are showed in Figure 3. In addition, the XRD peaks of the REM were perfectly coincident with those grounded into powder, meaning that the component of the REM bulk was homogeneous. It is noteworthy that as for the common carbothermal reduction approach with mixing carbon powder and TiO₂, the surface and interior of the obtained bulk sample show different compositions (Tsumura et al., 2004; Toyoda et al., 2009).

3.2 Pore Properties Modification

The morphology and pore structure of the REM were characterized by SEM Hg porsimetry, respectively. The SEM images in **Figures 4A–D** show the samples prepared at 1333 K with different carbon black contents of 0wt%, 1.5wt%, 5wt%, and 10wt%. The pore size of four samples was almost similar due to the fact that the grain-growth behavior mainly depends on the sintering time and temperature (Guan et al., 2016). The SEM images of the REM exhibit a three-dimensionally assembled structure with macro porosity, and the crystallites were indeed intimately fused or even consolidated to form large single-crystal particles on the micrometer scale. During the high-temperature reduction process, the agglomerates of solid particles and particle





bonding resulted in the formation of the porous structure inside the cavity in the presence of the porosity-producing agent. **Figure 4** shows that the pore size increased with the increasing carbon black content. The size of pores in **Figure 4D** seems to be larger than that in **Figure 4A**, which may be explained by the different carbon contents of these two samples. The detailed pore structure of these membranes was characterized by Hg porosimetry, and the results are presented in the **Figure 5**. It is demonstrated that the REM sample possessed uniform macropores of 0.4– $0.5 \,\mu m$ (**Figure 6**). The almost same macropore diameter and volume indicate that the well-defined macroporous structure of the monolith was retained. These results are consistent with the results of SEM images. Moreover, the REM exhibits a pore size distribution with ~99% of the measured surface area associated with pores

<0.5 µm, and essentially, the entire pore volume attributed to pores with 0.2-0.5 µm diameters. As shown in Figure 5, based on the porosimetry results, the porous surface area for the membrane without carbon black was estimated as 1.477 m² g⁻¹ with the porosity(θ) and median pore diameter of 0.382 and 0.380 μm, respectively. As the content of carbon black was elevated to 1.5wt%, the porous surface area was enhanced to 1.797 m² g⁻¹ with the increase in the porosity by 4.7%, while no difference was observed in the pore size as compared with that without the addition of carbon black. The membrane with 5wt% carbon black has a porous surface area of 2.011 m² g⁻¹, median pore diameter of 0.481 µm, and its porosity is 0.427 which is the same with the former. The porosity for the REM with 15wt% carbon black was determined as 0.594, specific surface area of $2.477 \text{ m}^2 \text{ g}^{-1}$, and median pore diameter of $0.575 \, \mu \text{m}$. As the volume of carbon black increased, the change of pore size is slight, and the porosity has a gap of 21% between the samples without carbon black and with 15% carbon black. Micronsized pores dominated the REM pore volume, which facilitates water transport through the REM at low applied pressures and is expected beneficial for facilitating interfacial mass transfer during the electrochemical reaction. Porosimetry analysis results show that the average pore diameter was closed to the median pore diameter (based on pore volume data) showing symmetrically distribution pore size. The addition of high carbon black content was not recommended since it would cause the crack of the REM monolith during the flow-through operation mode.

A flow-through reactor was used to assess the permeation ability of REMs with ultra-pure water experiments which were carried out with the ${\rm Ti_4O_7}$ REM. A digital gear pump was prepared to control the permeate flux and a pressure gage was used to record the hydraulic pressure. The evolution of the permeate flux with the carbon black content is plotted in **Figure 7**. It is found that the porosity and pore size both exerted the influence on the permeate flux. The REM without carbon black and with 1.5%wt carbon black have the same pore

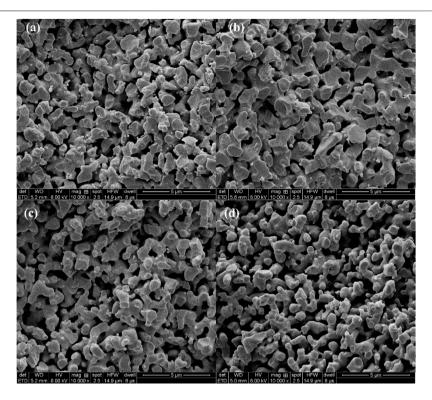


FIGURE 4 | SEM image of the samples obtained at 1333 K with different carbon black contents of 0wt% (A) 1.5wt%, (B) 5wt%, and (C) 10wt% (D).

size of 380 nm but different porosity, e.g., 38 and 42%, respectively. The permeate flux of the latter increased 28% than the former. REMs with 1.5wt% and 5wt% carbon black have the same porosity of 0.42 and different pore size. With the bigger pore size and porosity, the increased extent of the permeate flux was much more evident. The permeate flux for the sample with the pore size of 480 nm increased by 57% than the sample with 380 nm pore size. The results of the REM membrane with 60% porosity and 580 nm pore size showed that the method improved the flux obviously with a 452% increase in the flux from 250 to 1379 L m⁻² h⁻¹ bar⁻¹ than the original REM membrane. This indicates that a high content of carbon black was a crucial factor for the permeation ability of the REM membrane.

The resistance-in-series model was applied to evaluate the characteristics of the membrane flux; according to the Darcy law, the permeation flux (J) takes the following form:

$$J = \frac{\Delta P}{\eta R_m},\tag{1}$$

where J is the permeation flux (L/m² h), ΔP (Pa) is the transmembrane pressure, η is the dynamic viscosity of the permeate, and R_m (m⁻¹) is the intrinsic membrane resistance. **Table 1** made a summary of pressure-normalized permeate fluxes (LMH/bar) and intrinsic membrane resistance (10¹⁰/m) of the four samples. It can be seen that R_m decreased with the increases of the carbon black content. R_m of the original membrane is

~6 times higher than that of the membrane with 15 wt% content of carbon black, which suggest that a lower membrane resistance can be achieved by simply increasing the content of carbon black.

3.3 Electrochemical Characterization

The measurements of the electrochemically active surface area of each electrode were conducted within the potential region between hydrogen and oxygen evolution reaction, i.e., -0.2-0.5 V/SCE, at the sweep rates of 5-30 mV/s. As shown in **Figure 8**, the capacitive current decreases linearly with lowering sweep rates so that the apparent capacitance can be calculated from the slope of the charging current vs sweep rate. The double layer capacitances (C_{dl}) were determined based on the CV test according to **Eq. 2**.

$$\frac{I_{\rm a} - I_{\rm c}}{2} = C_{dl} \nu, \tag{2}$$

where I_a and I_c represent the measured plateau currents at 0.25 V/SCE, and v is the scan rate (V/s). The surface roughness factor and electroactive surface area were calculated according to the previous study with the use of the electrode geometric surface area. Assuming a double layer capacitance of $60 \, \mu \text{F/cm}^2$ for a surface of oxides, the roughness factors "r" can be estimated as follows:

$$r = \frac{C_{dl}}{C_0}. (3)$$

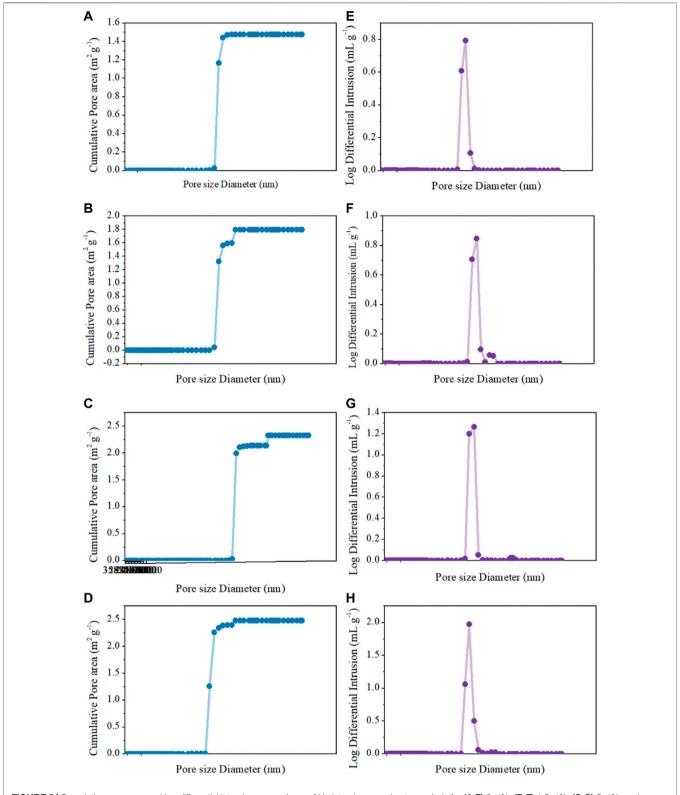
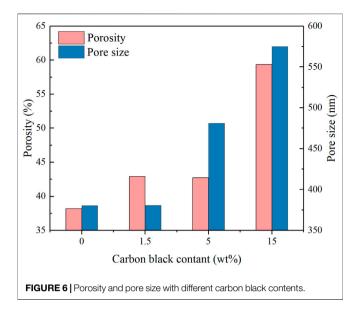


FIGURE 5 | Cumulative pore area and log differential intrusion pore volume of Hg intrusion porosimetry analysis for (A,E) 0wt%, (B,F) 1.5wt%, (C,G) 5wt%, and (D,H) 15wt%.

Ti₄O₇ Reactive Electrochemical Membrane



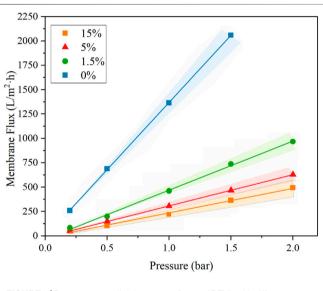


FIGURE 7 | Pressure-normalized permeate fluxes of REMs with different carbon black contents.

Comparative cyclic voltammograms of the four REM membranes with a nominal geometric surface area of $3.38\,\mathrm{cm}^2$ in the potential range of -0.2-0.5 V/SCE are shown in **Figure 8**. It was calculated that the REM samples without doping carbon black and with 1.5% carbon black have the almost same average

roughness (2557–2563). As for 5wt% carbon black, the calculated surface roughness was 3250 and the total electroactive surface area was 1.1 $\rm m^2$, which accounted for approximately 54.6% of the porous surface area measured by Hg porosimetry and increased by 1.3-fold in comparison with that without carbon black. However, the REM membrane obtained with doping 15wt% carbon black has the lowest surface roughness at 1953. In summary, the electrochemically active area (i.e., the roughness factor) of the porous $\rm Ti_4O_7$ electrode is 3 orders of magnitude higher than the apparent surface area of the REM membrane, which was favorable for the electrochemical reaction.

A stepwise increase in potential was implemented by recording the current response to obtain the water oxidation potential in the Na₂SO₄ electrolyte (**Figure 9**). For Ti₄O₇, there was a negligible response of the current when the potential was below 2.7 V/SHE. Further increasing potential resulted in an apparent enhancement of the current, indicating the potential for water oxidation was within the range of 2.5–2.7 V/SHE. This result was higher than that of the oxygen evolution potential of 2.5 V/SHE reported by Smith et al. and reached the highest reported value of 2.7 V/SHE (Miller-Folk et al., 1989; Graves et al., 1991; Kolbrecka and Przyluski, 1994; Grimm et al., 1998). Thus, we can infer that the as-prepared Ti₄O₇ REM exhibits an appreciable electrocatalytic activity toward the production of •OH.

Figure 9B shows the EIS curves of REMs at room temperature. Each of the curves consists of a straight line (at low frequency) and a depressed semicircle (at high frequency), which are related to the ion diffusion in the bulk of the electrode and the charge transfer process at the electrolyte-electrode interface, respectively. The Rs displays the internal resistance of the electrode and electrolyte, and the charge-transfer impedance (R_{ct}) is expressed vividly by the depressed semicircle in the intermediate frequency region. As shown in Figure 9B and **Table 1**, Rs values of Ti_4O_7 were estimated to be 17.1 \pm 0.17, 17.53 \pm 0.18, 18.8 \pm 0.19, and 19.6 \pm 0.20 Ω , respectively, indicating a minimal difference between the conductivity of these REMs. But it can be seen that as the content of carbon black increased, the value of R_s increased, which may be associated with the porosity of the REM membrane samples. The existence of a large number of voids reduced the effective cross-section of current conduction and therefore decreased the conductivity. Notably, the charge transfer resistances (R_{ct}) of these REMs were 3.57 \pm 0.36, 3.68 \pm 0.37, 4.14 \pm 0.41, and 5.19 \pm 0.52Ω , respectively, which were three orders of magnitude smaller than that for the graphite plate electrode (You et al., 2016; Xie et al., 2020), suggesting a much higher charge transfer capacity of Ti₄O₇.

TABLE 1 The effect of carbon black content on the property of REM samples.								
Carbon black contents (wt%)	0	1.5	5	10				
Pressure-normalized permeate fluxes (LMH/bar)	250 ± 10	320 ± 1	503 ± 12	1379 ± 8				
Intrinsic membrane resistance (10 ¹⁰ /m)	9.25	7.3	4.83	1.59				
Determinate coefficient R ²	0.9869	0.9946	0 9979	0 9997				

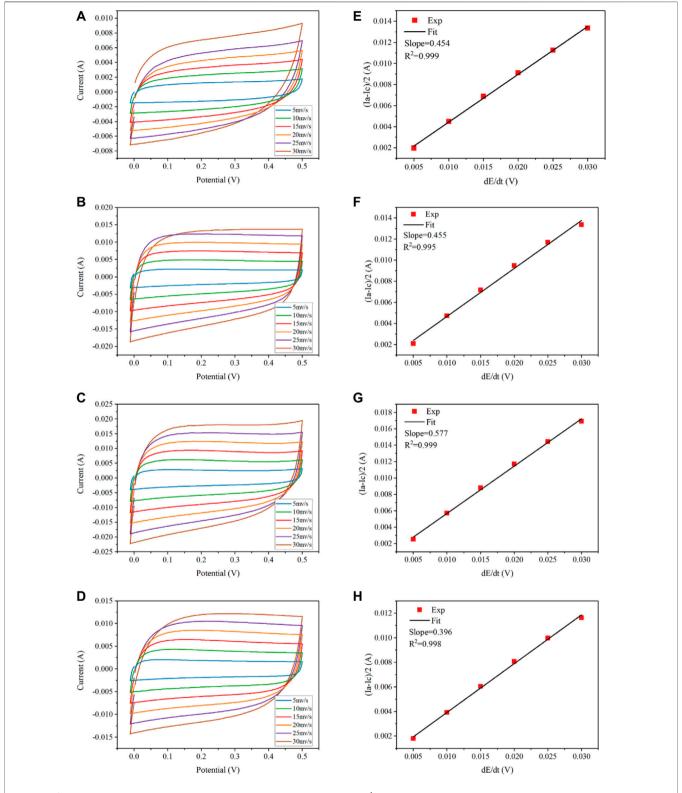
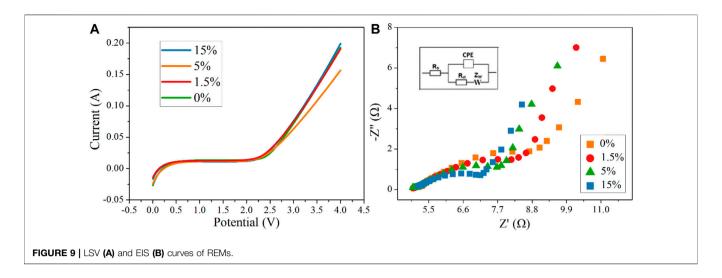


FIGURE 8 | Determination of double-layer capacitance at different scan rates (5–30 mV s $^{-1}$) for REMs using CV in the 100 mM Na₂SO₄ electrolyte solution. CV scans: (A) 0wt%, (B) 1.5wt%, (C) 5wt%, and (D) 15wt%. Corresponding plots of charging currents versus scan rates: (E) 0wt%, (F) 1.5wt%, (G) 5wt%, and (H) 15wt%.



3.4 Thermal Reduction Mechanism

In this study, the ${\rm Ti_4O_7}$ REM fabrication process combined the following two steps: 1) the oxygen atoms in the ${\rm TiO_2}$ monolith reunited to oxygen and then effused into the vacuum environment at the higher reaction temperature and 2) the emanated oxygen is captured by the Ti powder. Thermodynamically, the reaction driving force enables titanium oxidation and ${\rm TiO_2}$ reduction. For step one, the general reaction can be given as

$$2(n-1)\operatorname{Ti_nO}_{2n-1(s)} = 2\operatorname{ni}_{n-1}1O_{2n-3(s)} + O_{2(g)}, \tag{4}$$

where ${\rm Ti_{n-1}O_{2n-3}}$ and ${\rm Ti_nO_{2n-1}}$ are the closest compounds in the Ti–O binary phase diagram. In these reactions, only oxygen is the gas phase, and others are pure solid. Then, the Gibbs free energy could be written as

$$\Delta_{\mathbf{r}}G = \Delta_{\mathbf{r}}G^{\theta} + \frac{1}{2}RT\ln\frac{p_{o_2}}{p^{\theta}},$$
 (5)

where p_{O_2} is the partial pressure of O_2 , p^{θ} is the standard atmospheric pressure, and R is the universal gas constant. Due to the experiment being conducted in a vacuum, the practical pressure of oxygen is smaller than the total pressure of the vacuum chamber and certainly standard atmospheric pressure. This makes the value of $RT \ln \frac{p_{O_2}}{p^{\theta}}$ negative, i.e., the Gibbs free energy change of the reaction at T temperature is minor as compared with the standard Gibbs free energy change, making decomposition of the metal oxide easier to occur. On the other side, the equation shows that the decomposition temperatures of the metal oxide depend on the oxygen pressure. Thus, the vacuum degree was also the critical factor for the successful fabrication of Ti_4O_7 REM samples.

When $\Delta_r G = 0$, i.e., at the equilibrium, the relationship between temperature T and $\ln \frac{p_{O_2}}{p^{\theta}}$ was obtained:

$$\Delta_{\mathbf{r}}G^{\theta} = -\frac{1}{2}RT \ln \frac{p_{O_2}}{p^{\theta}}.$$
 (6)

Based on the data of the Ti-O system, the diagram of this relationship is shown in **Figure 10**, called the Ti-O system phase stable diagram.

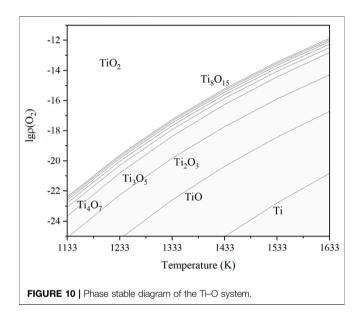
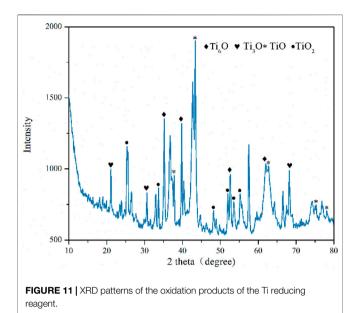


TABLE 2 | Equilibrium oxygen partial pressure of reactions in the Ti–O system at a specified temperature.

Reactions	Sintering temperature T/K, when $\Delta_r G^\theta = 0$	$\lg \frac{p_{O_2}}{p^{\theta}}$
12TiO_2 (s) $=2\text{Ti}_6\text{O}_{11}$ (s)+O ₂ (g)	1233	-19.8
$8TiO_2$ (s) = $2Ti_4O_7$ (s)+ O_2 (g)	1333	-17.9
$6\text{TiO}_2 \text{ (s)} = 2\text{Ti}_3\text{O}_5 \text{ (s)} + \text{O}_2 \text{ (g)}$	1433	-16.3

From Figure 10, Ti_4O_7 could be synthesized from TiO_2 if the oxygen partial pressure and temperature were accurately controlled. If the system oxygen partial pressure is higher than the equilibrium value, the metal will be oxidized, and if it is lower than the equilibrium value, then the oxide will be reduced. The lower the temperature was, the wider the range of the oxygen partial pressure for Ti_4O_7 existed.



When the temperature was adjacent to 1333 K and $\lg \frac{p_{O_2}}{p^{\theta}} < -17.9$, the domain of Ti₄O₇ was expanded.

Table 2 is the equilibrium oxygen partial pressure of reactions in the Ti-O system at the temperature of 1233, 1333, and 1433 K. As the temperature increases by every 100 K, the oxygen partial pressure can increase by several orders of magnitude. It means that raising the temperature could make the reaction occur more easily and more distinguished; thus, the possibility to fabricate a single-phase material is greatly raised. However, it should be noted that the treatment time must be reduced at a high thermal reduction temperature since it probably induced the overreduction of TiO_2 to some Ti_nO_{2n-1} , such as Ti_3O_5 (**Figure 2**).

Excess amount Ti was use to decrease the oxygen pressure and ensure more complete reduction of TiO_2 during the process. It has been shown that the growth of titanium oxide mainly in the form of rutile at and above 10^{-7} MPa and at the temperature below 1573 K. However, at lower pressures and at higher temperatures and after oxygen saturation of the a-phase, all the oxides of titanium (e.g., Ti_2O , TiO, Ti_2O_3 , Ti_3O_5 , and TiO_2) are formed as reaction products depending on the oxygen pressure and elapsed time of reaction. As a matter of

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4 CONCLUSION

In this study, the high purity Ti_4O_7 REM was successfully synthesized by mechanical pressing of TiO_2 powders followed by thermal reduction to Ti_4O_7 using the Ti powder as the reducing reagent. Carbon black was introduced to the monolithic TiO_2 precursor to control the pore size and morphology of the Ti_4O_7 REM. The pore properties modification increased the electroactive surface area by approximately 1.3-fold, which increased the reactivity of the Ti_4O_7 REM toward outer sphere electron transfer reactions. The electrodes had high porosities (38–59%), which showed high permeate fluxes of up to 1379 \pm 8 LMH bar $^{-1}$. These results indicated that the Ti_4O_7 monolithic electrodes could find various electrochemical applications in water treatment and energy storage and conversion.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material; further inquiries can be directed to the corresponding authors.

AUTHOR CONTRIBUTIONS

GQ was responsible for conceptualization, investigation, formal analysis, and writing of the original draft. XW contributed to project administration, resources, validation, and reviewing and editing. JZ and CS carried out investigation and formal analysis. XX helped with software and methodology. YZ, FR, and NZ performed the formal analysis and investigation.

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Dual Effect of Acetic Acid Efficiently Enhances Sludge-Based Biochar to Recover Uranium From Aqueous Solution

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¹University of South China, Hengyang, China, ²Hengyang Key Laboratory of Soil Contamination Control and Remediation, University of South China, Hengyang, China, ³Key Laboratory of Radioactive Waste Treatment and Disposal, University of South China, Hengyang, China, ⁴Decommissioning Engineering Technology Research Center of Hunan Province Uranium Tailings Reservoir, University of South China, Hengyang, China

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Yu S, Wu X, Ye J, Li M, Zhang Q, Zhang X, Lv C, Xie W, Shi K and Liu Y (2022) Dual Effect of Acetic Acid Efficiently Enhances Sludge-Based Biochar to Recover Uranium From Aqueous Solution. Front. Chem. 10:835959. doi: 10.3389/fchem.2022.835959 Excess sludge (ES) treatment and that related to the uranium recovery from uranium-containing wastewater (UCW) are two hot topics in the field of environmental engineering. Sludge-based biochar (SBB) prepared from ES was used to recover uranium from UCW. Excellent effects were achieved when SBB was modified by acetic acid. Compared with SBB, acetic acid-modified SBB (ASBB) has shown three characteristics deserving interest: 1) high sorption efficiency, in which the sorption ratio of U(VI) was increased by as high as 35.0%; 2) fast sorption rate, as the equilibrium could be achieved within 5.0 min; 3) satisfied sorption/desorption behavior; as a matter of fact, the sorption rate of U(VI) could still be maintained at 93.0% during the test cycles. In addition, based on the test conditions and various characterization results, it emerged as a dual effect of acetic acid on the surface of SBB, i.e., to increase the porosity and add (–COOH) groups. It was revealed that U(VI) and –COO– combined in the surface aperture of ASBB via single-dentate coordination. Altogether, a new utilization mode for SBB is here proposed, as a means of efficient uranium sorption from UCW.

Keywords: uranium, uranium-containing wastewater, excess sludge, acetic acid, sludge-based biochar

INTRODUCTION

Uranium-containing wastewater (UCW) contains a certain concentration of nuclide ions, such as uranium ions, radium ions, and thorium ions. In addition, it also contains high concentrations of heavy metal ions, metal ions, and acid ions, such as sulfate ions and nitrate ions. This special industrial wastewater is mainly discharged by uranium mining or uranium hydrometallurgy. Generally, uranium presents in the valence form of U(IV) and U(VI). U(IV) does not dissolve in aqueous solution and usually forms precipitation, while U(VI) generally gives mobile aqueous

Abbreviations: ASBB, acid-modified sludge-based biochar; ASBB-U, Acetic acid-modified sludge-based biochar—uranium; BET, Brunner–Emmet–Teller; EDS, energy-dispersive x-ray spectroscopy; ES, excess sludge; FTIR, Fourier transform infrared spectroscopy; SBB, sludge-based biochar; SEM, scanning electron microscope; SSA, specific surface area; UCW, uranium-containing wastewater; WWTP, wastewater treatment plant; XPS, x-ray photoelectron spectroscopy.

complexes with CO₃²⁻ and OH⁻¹ (Gerber et al., 2016; Abdi et al., 2017). Uranium ions are characterized by radioactivity and chemical toxicity, which could, in turn, cause chronic poisoning, cancer, and immunological diseases (Malenchenko et al., 1978; Baur et al., 1996; Kathren and Burklin, 2008; NaserHumood, 2013). In addition, serious damage might be caused to the surrounding organisms as well as ecosystems once UCW is discharged into the environment by accident. Consequently, it is of great significance to establish rapid and efficient processing methods for UCW treatment aimed at both reducing the hazardous effect of UCW and reusing, as added-value product, uranium recovered by UCW.

At present, the main technologies for uranium recovered from UCW or UCW treatment could be summarized as chemical precipitation, ion exchange, membrane separation, biological treatment, solvent extraction, and sorption (Khani et al., 2008; Wang et al., 2009; Abadi et al., 2011; Gerber et al., 2016; Khawassek et al., 2018; Tan et al., 2018). Among them, sorption is one of the popular technologies because of its advantages, including simple operation, wide range of application, higher removal and recovery rate, etc. (Chen et al., 2020). Generally, the uranium removal rate by sorption is mainly influenced by physical/chemical properties of adsorbents (i.e., pore structure, surface groups), uranium concentration, pH, etc. (Kataria and Garg, 2018) Biochar (Sun et al., 2013; Sun et al., 2017; Kong et al., 2020), graphene (Zhao et al., 2019), calixarene (Fang-Zhu et al., 2019), MOFs (Li et al., 2020), and mesoporous silicon (Jiang et al., 2020) were used as sorption materials. Among them, biochar has been verified as an important sorption material for uranium recovery or removal from aqueous solution (Jin et al., 2018; Li et al., 2019a), due to its simple preparation process, lower price, higher temperature resistance, radiation resistance, higher stability to almost all kinds of acidic and alkali environments, nontoxic, and environmentally friendly nature (Zhao et al., 2017; Pu et al., 2019).

Generally, excess sludge (ES) was applied for biochar preparation (Li et al., 2019b; Hu et al., 2019). ES is mainly generated by wastewater treatment plant (WWTP) with large yield (Ghosh, 2009; Ali et al., 2019). It is difficult to treat ES, and its post-processing cost is relatively high (Hossain et al., 2018). Moreover, secondary pollution might easily happen if ES is not properly treated (Sun et al., 2018). Kanterli reported that sludge-based biochar (SBB) showed high sorption capacity (112.40 mg/g) for Cr(VI) (Ismail Cem and Jale, 2009). SBB prepared from municipal sludge (11.27 mg/g) and papermaking sludge (11.78 mg/g) by hydrothermal treatment had good sorption capacity for Pb(II) removal, too (Alatalo et al., 2013). In addition, SBB and Fe₃O₄modified SBB also showed high uranium ion sorption efficiency (more than 90.0%) (Zeng et al., 2020; Guanhai et al., 2021). What is more, the treatment of UCW by SBB cannot only effectively solve the problem from ES, but also achieve the effect of waste treatment fee and waste resource utilization. However, to make SBB more practical, its sorption capacity for uranium or other heavy metals needs to be further improved.

So far, the most effective method for improving biochar sorption capacity or removal rate of heavy metals is to increase specific surface area or functional groups on its surface. For example, the effect of nitric acid on the surface area enlargement of biochar has been reported (Ioanna et al., 2017; Mishra et al., 2017). In addition, oxygen functional groups (Anirudhan and Deepa, 2015), humus (Zong et al., 2015), amine (Zhao et al., 2015), amine (Deb et al., 2012), dopaminer (Wu et al., 2017), and oximer (Xiong et al., 2017) were considered as corresponding functional groups to improve heavy metal removal rate. –COOH, as a representative of oxygen functional groups, is suitable for the complexation of uranium ions (Park et al., 2019). However, there is still a lack of research on the simultaneous expansion of pores and the addition of groups to recover more uranium ions in SBB.

In order to achieve the above requirements, the removal and recovery efficiency of uranium from UCW was comprehensively studied by involving acetic acid-modified SBB (ASBB) prepared from ES and acetic acid, including 1) differences in uranium recovery efficiency from UCW when SBB or ASBB were used, 2) impacts of variety factors (reaction time, pH, dosage, initial concentration, desorption, and interfering ions) on uranium removal by ASBB, 3) kinetic and thermodynamic analysis of sorption, 4) ASBB uranium removal mechanism based on Brunauer-Emmett-Teller (BET), scanning electron microscopy (SEM), energy-dispersive x-ray spectroscopy (EDS), Fourierinfrared spectroscopy (FTIR), and photoelectron spectroscopy (XPS) techniques. In this paper, acetic acid was used as a modifier to modify SBB and to treat UCW. This modification method could also be used to treat other heavy metal ions in the future.

MATERIALS AND METHODS

Starting Materials

ES was obtained from a WWTP located in Hengyang, China. The reagents used in this study were of analytical grade. Chloroacetic acid (CH2ClCOOH), hydrochloric acid (HCl), ferrous sulfate heptahydrate (FeSO4.7H2O) and sodium hydroxide (NaOH), potassium hydroxide (KOH), and acetic acid (CH3COOH) were purchased from Sinopharm Group Pharmaceutical Co., Ltd. (Shanghai). Arsenio III [(HO)2C10H2(SO3H)2(N=NC6H4AsO3H2)2] and triuranium octoxide (U3O8) were purchased from Tianjin Kemio Chemical Reagent Co., Ltd., and China Academy of Metrology, respectively.

Uranium stock solution (1.0 g/L) was prepared by dissolving $\rm U_3O_8$ in concentrated nitric acid. The specific preparation process was as follows: First, the dried 1.1792 g $\rm U_3O_8$ powder was accurately weighed into a 100-ml beaker. Second, 10.0 ml of hydrochloric acid solution with a density of 1.18 g/cm³, 3.0 ml of 30 wt% hydrogen peroxide, and two drops of 1.0 mg/L of nitric acid solution were sequentially added to the beaker. Then the beaker was covered with a lid for 3 min. After time had elapsed, the solution was stirred by a glass rod for several minutes. After a violent reaction was completed, the beaker was moved a the

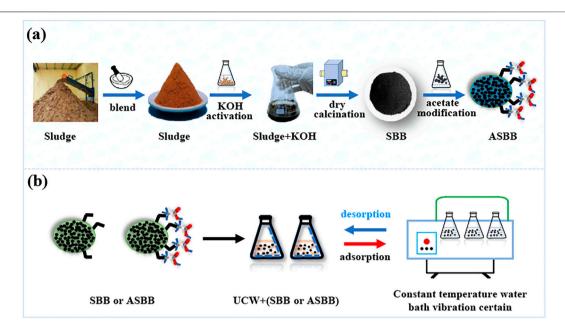


FIGURE 1 | Preparation of sludge-based biochar (SBB) and acid-modified sludge-based biochar (ASBB) and uranium recovery from uranium-containing wastewater (UCW). (A) Preparation of SBB and ASBB. (B) Uranium recovery from UCW by SBB or ASBB.

graphite heating plate for heating and dissolution. When the dissolution was completed, the solution was cooled to room temperature. Finally, the solution was transferred to a 1,000.0-ml volumetric flask, and a nitric acid solution with pH <2 was used for constant volume. More information in detail could be found in cited literature (Lu et al., 2018a). All concentrations of UCW solutions used in the experiment were diluted by $1.0~\rm g/L$ uranium stock solution.

Sludge-Based Biochar and Acetic Acid-Modified SBB Preparation

The preparation process of SBB and ASBB is shown in **Figure 1A**. The dewatered ES was collected from WWTP and then dried at 105° C for 24 h. The dried ES was impregnated with KOH (3.0 mol/L) in proportion to mass and activated for 24 h. The impregnated ES was again dried at 80° C in a constant temperature drying oven. Thereafter, it was pyrolyzed to biochar in a muffle furnace at 350° C- 700° C for 40-50 min under nitrogen atmosphere. Biochar was cooled down to room temperature under nitrogen atmosphere. Then it was washed to neutral by distilled water. The production rate of fresh SBB was $86.0 \pm 10.0\%$. The biochar was immersed in CH₃COOH solution (36.0%-38.0%) for 6 h and then washed with distilled water to neutrality, thus, eventually getting ASBB.

Experimental setup

Orthogonal Experiments

Figure 1B displays the rationale of the experiments of uranium recovered from UCW with different SBB or ASBB dosages. A certain amount of SBB or ASBB was added to 100.0 ml of U(VI) solution. Temperature and stir speed were kept at 25°C and 120 r/

min, respectively. The removal efficiencies of U(VI) by fresh SBB and ASBB were investigated according to orthogonal experiments. They were conducted under different mass ratios of sludge/KOH (MSK), calcination temperature (CTE), calcination time (CTI), and activation time (AT) (**Table 1**). Initial U(VI) concentration in UCW was 10.0 mg/L, pH was 3.03, and the dosage of fresh SBB or ASBB was 0.50 g/L in each investigated case.

Batch Experiment

Several values of reaction time (1.0, 2.0, 3.0, 4.0, 5.0, 10.0, 20.0, and 30.0 min), initial pH (3.0–9.0 with a minimum interval of 1.0), adsorbent dosage (0.05, 0.1, 0.1, 0.3, 0.4, and 0.5 g/L), and initial uranium ion concentration (5.0, 10.0, 20.0, 30.0, 50.0, and 100.0 mg/L) were scrutinized. U(VI) concentration in artificial UCW was kept at 10.0 mg/L except for particular cases. Dosage of SBB or ASBB was 0.30 g/L, and pH was 6.0.

The desorption of ASBB was carried out by utilizing HCl (2.0 mol/L) as a desorption agent. The interference test of the sorption of U(VI) by coexisting ions (cation) in the solution was also carried out. Except for the solution containing 10.0 mg/L of U(VI), the concentration of coexisting ions in each solution was simulated to 10.0 mg/L. The interfering ions involved were Fe³⁺, Na⁺, Mg²⁺, Pb²⁺, and Cr⁶⁺. During the test, two dosages (0.3 and 0.5 g/L) of ASBB were set. HCl (0.01 mol/L) and NaOH (0.01 mol/L) were used for adjusting pH of artificial UCW.

Analysis and Characterization

U(VI) concentration was determined by Arsenazo III spectrophotometer (Ding et al., 2018). The absorbance of UCW was measured at a wavelength of $652\,\mathrm{nm}$ after

TABLE 1 | Effect of biochar on uranium-containing wastewater (UCW) treatment under different preparation conditions

Influencing factors	Sludge: KOH	Calcination temperature (°C)	Calcination time (min)	Activation time (h)		noval e (%)	сар	ption acity g/g)
	MSK	CTE	СТІ	AT	SBB	ASBB	SBB	ASBB
Exp 1	3:1	400	30	3	23.6	42.8	4.72	8.56
Exp 2	2:1	400	40	6	28.1	52.2	5.62	10.44
Exp 3	1:1	400	50	12	39.3	67.3	7.86	13.46
Exp 4	1:2	400	60	24	39.9	68.9	7.98	13.78
Exp 5	1:3	400	70	48	40.8	70.8	8.16	14.16
Exp 6	3:1	450	40	12	30.6	48.6	6.12	9.72
Exp 7	2:1	450	50	24	38.7	58.3	7.74	11.66
Exp 8	1:1	450	60	48	45.2	75.1	9.04	15.02
Exp 9	1:2	450	70	3	46.3	76.2	9.26	15.24
Exp 10	1:3	450	30	6	45.1	77.5	9.02	15.5
Exp 11	3:1	500	50	48	35.1	51.2	7.02	10.24
Exp 12	2:1	500	60	3	43.1	63.1	8.62	12.62
Exp 13	1:1	500	70	6	52.2	83.1	10.44	16.62
Exp 14	1:2	500	30	12	52.5	83.6	10.5	16.72
Exp 15	1:3	500	40	24	53.2	84.1	10.64	16.82
Exp 16	3:1	550	60	6	42.8	55.8	8.56	11.16
Exp 17	2:1	550	70	12	56.2	77.2	11.24	15.44
Exp 18	1:1	550	30	24	57.8	87.1	11.56	17.42
Exp 19	1:2	550	40	48	58.6	87.2	11.72	17.44
Exp 20	1:3	550	50	3	58.9	87.4	11.78	17.48
Exp 21	3:1	600	70	24	45.1	53.1	9.02	10.62
Exp 22	2:1	600	30	48	60.7	83.9	12.14	16.78
Exp 23	1:1	600	40	3	61.2	87.9	12.24	17.58
Exp 24	1:2	600	50	6	61.6	88.1	12.32	17.62
Exp 25	1:3	600	60	12	62.3	87.9	12.46	17.58
F	87.09	9.84	4.34	1.18				
Р	< 0.0001	0.0106	0.0638	0.3034				

Note. The F value represents the significance of the whole fitting equation, and the larger the F implies the more significant the equation, and the better the fitting degree. p-Value is a parameter used to determine the hypothesis test results. The smaller the p-value means the more significant the result. KOH, potassium hydroxide; SBB, sludge-based biochar; ASBB, acid-modified sludge-based biochar; AT, activation time; CTI, calcination time; CTE, calcination temperature; MSK, mass ratio of sludge/KOH.

preheating the spectrophotometer for 30 min. Inductively coupled plasma-mass spectrometry (ICP-MS) was used to double check the values obtained from spectrophotometry. The difference in the results obtained with the two methods was 1.47%-1.53%, indicating that spectrophotometry was a reliable method under these operating conditions.

The uranium equilibrium specific sorption capacity q_e (mg/g) and removal rate η for each sorbent (SBB or ASBB) were calculated according to Eqs. 1 and 2, respectively (Liu et al., 2018):

$$q_e = \frac{\nu(c_0 - c_e)}{m}$$

$$\eta = \frac{c_0 - c_e}{c_e}$$
(2)

$$\eta = \frac{c_0 - c_e}{c_e} \tag{2}$$

where c_0 and c_e are the initial and equilibrium concentrations of uranium in the solution, v is the solution volume, and m is the mass of adsorbent. Langmuir and Freundlich sorption isotherm models were introduced to fit the U(VI) sorption data for ASBB under equilibrium conditions (Eqs 3, 4). The equations read, respectively (Christou et al., 2019):

$$q_e = \frac{q_m K_L Ce}{(1 + K_L Ce)} \tag{3}$$

$$q_e = K_F C e^{\frac{1}{n}} \tag{4}$$

where q_m is the maximum specific sorption capacity, K_L is the Langmuir equilibrium constant (L/mg), while K_F and n are the Freundlich parameters, respectively, representing the sorption capacity and the sorption intensity.

In order to investigate in detail the U(VI) sorption process by ASBB, kinetic data were fitted by pseudo-first-order (Lagergren PFO, Eq. 5) and pseudo-second-order (Ho&McKay PSO, Eq. 6) models. The equations read, respectively (Li et al., 2018):

$$q_t = q_e [1 - \exp(-\kappa_1 t)]$$
 (5)

$$q_t = \frac{\kappa_2 q_e^2 t}{1 + \kappa_2 q_e t} \tag{6}$$

where q_t refers to the specific sorption capacity at t time, κ_1 is the PFO sorption rate constant (min⁻¹), and κ_2 is the PSO sorption rate constant (g/mg·min⁻¹).

To compare the content of acidic functional groups on the surface of SBB, ASBB, and acetic acid-modified sludge-based biochar—uranium (ASBB-U), the contents of -OH, -COO, and -COOH were determined by the Boehm method (Kalijadis et al., 2011). Three samples of 1.0 g of each material were accurately weighed, and the samples were put into 100.0-ml conical flasks.

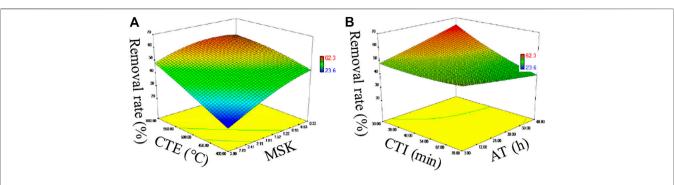


FIGURE 2 | (A) Uranium sorption from SBB and ASBB impacted by calcination temperature (CET) and sludge: KOH (MSK), (B) Uranium sorption from SBB and ASBB impacted by calcination time (CTI) and activation time (AT).

Then three samples of each material were added to 25.0 ml of 0.05 mol/L NaOH, $\rm Na_2CO_3$, and $\rm NaHCO_3$ standard solution, respectively. Nine samples were all stirred for a 24-h reaction and then filtered. During filtration, they were fully washed with distilled water. All the filtrates were collected independently. Methyl red was used as the end indicator of the filtrate. The unreacted alkali in the filtrate was titrated to end by a standard solution of 0.05 mol/L of HCl. The content of –OH, –COO, and –COOH was calculated by the amount of HCl.

The existing forms of uranium in UCW (10.0 mg/L) and $P_{\rm CO2} = 10^{-3.5}$ atm under pH from 3.0 to 9.0 were simulated by Visual MINTEQ 3.1 (Schierz and Zänker, 2009; Zong et al., 2017). The specific surface area of fresh or used SBB and ASBB was determined by BET technique (TriStar II Plus 2.02, Micromeritics, USA). The morphology of fresh or used SBB and ASBB was characterized by SEM (JSM-7500F, JEOL, JPN) coupled with EDS (INCA, Oxford, USA). Functional groups on fresh or used SBB and ASBB were analyzed through FTIR (Nicolet-iS50, Thermo Fisher Scientific, USA). The composition and chemical states of ASBB after UCW sorption were examined by XPS (Escalab 250Xi, Thermo Fisher Scientific, United States) with AlK α radiation. The binding energies were calibrated by using containment carbon (C1s = 284.7 eV). The data analysis was carried out *via* Casa XPS software (Version 2.3.13).

RESULTS AND DISCUSSION

Comparison Between Sludge-Based Biochar and Acetic Acid-Modified Sludge-Based Biochar in Uranium-Containing Wastewater Sorption

The performance of U(VI) removal is presented in **Figure 2**. The removal rate of U(VI) by fresh SBB and ASBB gradually increased with the decrease in MSK and with the increase in CTE (**Figure 2A**), CTI (**Figure 2B**), and AT. The F values of MSK, CTE, CTI, and AT were 87.09, 9.84, 4.34, and 1.18, respectively, (refer to **Table 1**). The p-values were <0.0001, 0.0106, 0.0638, and

0.3034, respectively. These results indicate that the influence ranking of the explored parameters is MSK, CTE, CTI, and AT. In particular, MSK had an extremely significant effect, and CTE showed a similar tendency (Anna et al., 2018). In addition, the removal rate and sorption capacity of ASBB were higher than SBB, indicating that acetic acid modification of the biochar showed excellent effect on U(VI) removal. Altogether, the optimal preparing conditions for fresh SBB and ASBB are suggested as: MSK = 1:1, CTE = 550° C, CTI = 30 min, and AT = 24 h.

U(VI) Removal Efficiencies by Acetic Acid-Modified Sludge-Based Biochar Under Different Conditions

Reaction Time

Figure 3A depicts the removal rate of U(VI) as a function of time for SBB and ASBB. The removal rate of U(VI) by SBB and ASBB increased with time quickly, and the sorption equilibrium was practically achieved within 5.0 min. This phenomenon was mainly due to the high U(VI) concentration, and to the large number of sorption sites made available by SBB and ASBB. U(VI) could rapidly diffuse to the adsorbent particle due to the high concentration gradient, to be then adsorbed on the solid surface-active sites. However, the removal rate and sorption capacity of U(VI) were close to the peak after 5.0 min. Two main reasons could explain this observation. First, the U(VI) concentration in the solution was quite low, and the U(VI) concentration was considered as one main limiting factor for the improvement of U(VI) removal rate. Second, the surface sorption sites decreased as the reaction proceeds. The probability of U(VI) binding to sorption sites was then decreased. As shown in Figure 3A, the U(VI) removal rate by SBB and ASBB was 62.8% and 97.8%, respectively. Meanwhile, the specific sorption capacity of these two adsorbents was 20.9 and 32.6 mg/g, respectively. The sorption capacity of U(VI) by ASBB was 55.8% higher than that of SBB. These results showed that ASBB could adsorb

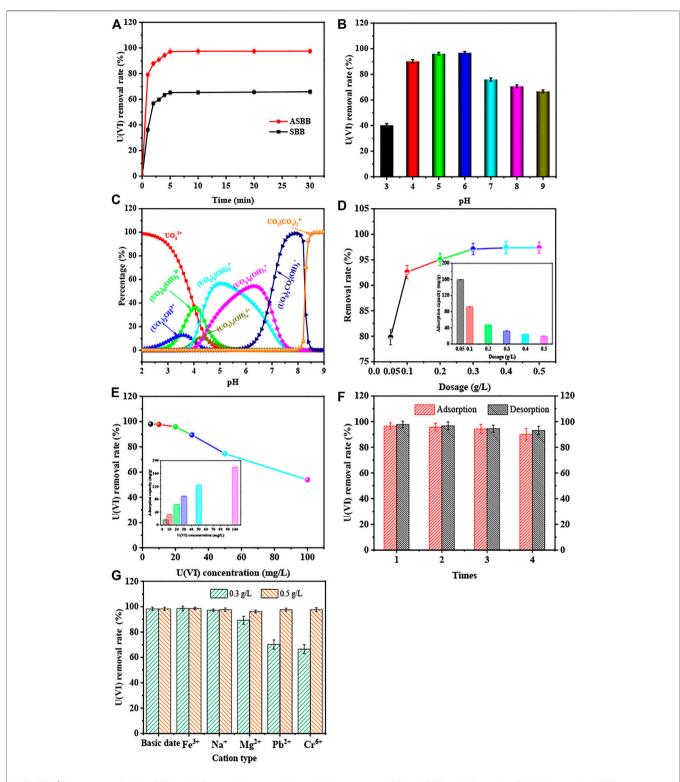


FIGURE 3 | Sorption rate of U(VI) by SBB or ASBB under different conditions. (A) Reaction time of SBB or ASBB for U(VI) sorption, (B) U(VI) sorption by ASBB under difference initial pH of USW, (C) simulation calculation of the existing state of uranium ions under different pH conditions, (D) removal rate of uranium in USW by ASBB under different dosage, (E) the removal rate of uranium ions by ASBB at different initial concentrations of USW, (F) desorption efficiency of uranium ions by ASBB, (G) effect of interfering ions on sorption of uranium ions by ASBB in USW.

U(VI) more rapidly and efficiently, and the sorption equilibrium could be achieved within 5.0 min.

Initial pH of Aqueous Solution

Figures 3B, C illustrate the experimental and simulation results of the influences of the initial pH value of the aqueous solution. Figure 3B shows that sorption of U(VI) from ASBB was greatly influenced by pH. Figure 3C displays that the existing uranium morphology varies under different pH conditions. The main morphologies were UO₂²⁺, $(\text{UO}_2)_2(\text{OH})_2^{2+}$, $(\text{UO}_2)_2\text{OH}^{3+}$, $(\text{UO}_2)_3(\text{OH})_5^+$, $(\text{UO}_2)_3(\text{OH})_4^{-2+}$, $(UO_2)_4(OH)_7^+$, $UO_2(CO_3)_3^{4-}$, and $(UO_2)_2CO_3(OH)_3^-$. The U(VI) removal rate was only 42.4% when pH = 3.0, where uranium mainly exists in the form of UO22+ in UCW. Because the solution pH value was in this case too low, a lot of H^+ competed with UO_2^{2+} sorption. Meanwhile, an H⁺ proton layer on the surface of ASBB could be formed, rather than UO22+. The electrostatic repulsion of ASBB to UO₂²⁺ might increase; thus, the removal rate of uranium was relatively low (Wu et al., 2019). When the pH was between 4.0 and 6.0, the uranium in solution mainly existed in the form of $(UO_2)_2(OH)_2^{2+}$, $(UO_2)_3(OH)_5^{+}$, $(UO_2)_4(OH)_7^{+}$. protonation degree of these forms favored the sorption of uranium by ASBB (Zhu et al., 2018). With the increase in pH, many organic functional groups (such as -OH, -COOH, etc.) might be gradually assembled on the surface of ASBB. H⁺ on these groups then decreased, so the electronegativity of these groups increased. The binding ability and reaction probability between functional groups and uranium increased due to this phenomenon. The uranium removal rate increased under this condition. When pH was 6.0, the U(VI) removal rate peak was 97.2%. When pH was between 7.0 and 9.0, the uranium was mainly in the form of UO₂(CO₃)₃⁴⁻ and (UO₂)₂CO₃(OH)₃. These forms were difficult to be adsorbed by ASBB, and the removal rate of uranium was reduced. Therefore, pH = 6.0 was suggested as the optimal condition for U(VI) sorption from UCW by ASBB.

Dosage of Acetic Acid-Modified Sludge-Based Biochar

Figure 3D shows the effect of different ASBB dosages on U(VI) removal. The initial U(VI) concentration was 10.0 mg/L. The U(VI) removal rate increased from 79.8% to 97.8% when the dosage of ASBB increased from 0.05 to 0.5 g/L. With the increase in the dosing amount, the reaction sites of ASBB in UCW increased as well. The probability of U(VI) to interact with reaction sites, therefore, increased and the U(VI) removal efficiency was improved. In general, 0.30 g/L was determined as the optimal dosage used in further sections also taking into account economic reasons.

Initial U(VI) Concentration

Figure 3E illustrates the sorption capacity of ASBB and uranium removal rate under different initial U(VI) concentrations in the wastewater recovered by ASBB biochar. When the dosage of ASBB was 0.30 g/L, the UCW removal rate result is equal to 98.1% (initial concentration = 5.0 mg/L) and 97.8% (initial concentration = 10.0 mg/L). Namely, with the increase in U(VI) initial concentration, the removal rate of U(VI) by ASBB gradually decreased, while the specific sorption capacity was increased. The latter might be due to the excess U(VI) in the

system, that drives the sorption process. Moreover, when the dosage of ASBB was 3.0 g/L (i.e., one order of magnitude higher), the removal efficiency for 100.0~mg/L of uranium concentration in UCW was 95.7%. These results demonstrated that ASBB was not only suitable for the uranium recovery from UCW with low uranium concentration but also for high concentration values. In addition, **Table 2** shows the results for different adsorbents. The U(VI) sorption capacity of ASBB per unit time was about $10{\text -}1,000$ times that of other materials, indicating that ASBB was a rapid and efficient U(VI) adsorbent, with interesting industrial perspectives.

Desorption From Acetic Acid-Modified Sludge-Based Biochar

The desorption performance of an adsorbent is an important standard to judge whether it can be practically used. Research has shown that adsorbed U(VI) could be replaced by H⁺ through ion exchange (Wen et al., 2016), and then dissolved in acidic solution (Tu et al., 2019). **Figure 3F** displays the results of uranium desorption from ASBB. It could be seen that after sorption and desorption for several cycles, the removal efficiency of uranium by ASBB remained at 90.2%, while the desorption efficiency from ASBB was 93.0%. These results showed that ASBB had good reusability potential, and the recovery of U(VI) could be achieved in practice.

Interfering lons

Figure 3G shows the interference of coexisting ions on ASBB's sorption of U(VI). When the dosage of ASBB was 0.30 g/L, Na⁺ had little effect on the removal of U(VI) by ASBB, while it would be inhibited by Mg²⁺, Pb²⁺, and Cr⁶⁺. In particular, Cr⁶⁺ had the greatest impact on ASBB's sorption of U(VI). The main reason for this phenomenon might be the competitive sorption of these ions and U(VI) on the surface of ASBB. Unlike these ions, Fe³⁺ facilitated the U(VI) removal. The main reason might be that when pH = 6, Fe^{3+} could be hydrolyzed into Fe(OH)3 colloids (Feng et al., 2013), and U(VI) could be combined with Fe(OH)₃ (Bruno et al., 1995). As a result, the efficiency of ASBB's removal of U(VI) was improved. When the dosage of ASBB was increased to 0.50 g/L, U(VI) could still be efficiently adsorbed by ASBB under the interference of various ions. Therefore, when there are interfering ions in the solution, it is recommended to increase the dosage of ASBB or add a certain amount of Fe³⁺ to improve the removal rate of U(VI).

Kinetic and Thermodynamic Analysis of Sorption

Figure 4A and **Table 3** show the results of the PFO and PSO models when they were applied to experimental data. The correlation coefficient R^2 was 0.998 (PFO) and 0.997 (PSO), indicating that both physical and chemical sorption occurred during the sorption of U(VI) by ASBB.

The results of the thermodynamic analysis are illustrated in **Figure 4B** and **Table 4**. The maximum specific sorption capacity was $q_m = 178.194 \text{ mg/g}$ (ASBB adsorbent), a value

TABLE 2 | Comparison of the maximum sorption capacities of different adsorbents toward U(VI).

Adsorbent	U(VI) (mg/L)	Dosage (g/L)	Q _{max} (mg/g)	рН	Time (h)	$q_t/t[(mg/g)/h]$	References
Fe ₃ O ₄ @C@ASA	4.76	0.6	46.20	4.00	24.00	1.91	Li et al. (2018)
HTC-COOH	140.0	0.5	163.00	4.50	24.00	6.79	Cai et al. (2017)
Activated carbon	200.0	2.5	45.24	6.00	5.00	9.05	Morsy and Hussein, (2011)
MAO-chitosan	480.0	1.0	117.65	6.00	5.00	23.53	Zhuang et al. (2018)
P(AO)-g-CTS/BT	100.0	2.0	49.90	8.00	1.00	49.90	Anirudhan et al. (2019)
SDACA	100.0	8.0	105.26	5.00	2.00	52.63	El-MagiedAbd et al. (2017)
PVP/CS	11.9	1.0	167.00	6.00	2.50	66.80	Christou et al. (2019)
AO-MWCNTs	10.0	1.0	67.90	5.00	1.00	67.90	Wu et al. (2018)
PAF	10.0	1.0	115.31	5.00	1.00	115.31	Saleh et al. (2017)
MWCNTs	25.0	0.1	83.40	6.25	0.67	124.45	Ebrahim et al. (2017)
P-Fe-CMK-3	20.0	0.2	150.00	4.00	0.50	300.00	Husnain et al. (2017)
ASBB	10.0	0.3	179.77	6.00	0.08	2,247.13	This work

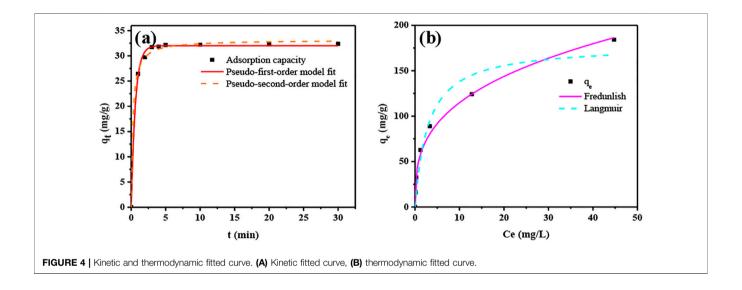


TABLE 3 | Kinetic parameters of U(VI) sorption on ASBB.

U(VI) concentration (mg/L)	Ps	eudo-first-order kinetics	i	Pseudo-second-order kinetics		
	<i>k</i> ₁/min ^{−1}	q_e /(mg/g)	R ²	k ₂ /min ⁻¹	<i>q_e</i> /(mg/g)	R ²
10.0 mg/L	1.716	31.665	0.996	0.126	33.087	0.999

consistent with the laboratory result $q_m = 179.88 \text{ mg/g}$. The correlation coefficient was 0.943 (Langmuir model) and 0.989 (Freundlich model), indicating that the sorption of U(VI) by ASBB was mostly dominated by multilayer sorption.

Characterization and Mechanism Analysis of Uranium Recovered by Acetic Acid-Modified Sludge-Based Biochar

Morphological Characteristics of Sludge-Based Biochar, Acetic Acid-Modified Sudge-Based Biochar, and Acetic Acid-Modified Sludge-Based Biochar—Uranium

The microstructure and surface elements of SBB, ASBB, and ASBB-U (i.e., used ASBB adsorbent after uranium sorption) were characterized

TABLE 4 | Thermodynamic parameters of sludge-based biochar on U(VI) sorption.

Adsorbents	Langmuir			Freundlich		
	<i>q_m</i> /(mg/g)	<i>K_L</i> /(L/mg)	R ²	K _F	q _e /(mg/g)	R ²
	178.194	0.344	0.943	54.584	0.323	0.989

by SEM and EDS (**Figure 5**). As shown in **Figures 5A**, **C**, **E**, the pore size of the SBB surface was quite small, while a more developed pore structure was presented on the surface of ASBB. More reaction sites could be provided by ASBB to adsorb U(VI). When the sorption was completed, the ASBB microstructure changed. The pore structure of ASBB-U obviously decreased, due to the combination of U(VI) with the functional groups on the ASBB surface, or to the direct sorption of

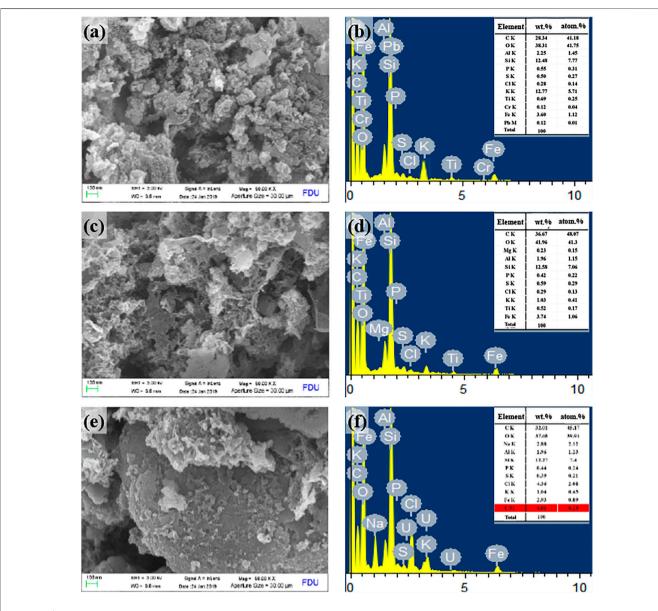


FIGURE 5 | Scanning electron microscope (SEM) and energy-dispersive x-ray spectroscopy (EDS) characterization results of SBB, ASBB, and ASBB-U, (A) SEM of SBB' surface, (B) EDS of SBB' surface, (C) SEM of ASBB' surface, (D) EDS of ASBB' surface, (E) SEM of ASBB-U' surface, (F) EDS of ASBB-U' surface.

U(VI) in the pore network of ASBB. These results were consistent with the results of BET analysis (vide infra).

According to **Figure 5B**, the main surface elements of SBB were C, O, K, and Si in general. **Figure 5D** shows that the fresh ASBB surface mainly consisted of C, O, Al, Si, P, K, and Fe. An amount of U was observed on the ASBB-U surface (**Figure 5F**). The weight percentage was about 4.05 wt%. This indicated that uranium was successfully adsorbed by ASBB.

Brunauer-Emmett-Teller Comparison of Sludge-Based Biochar, Acetic Acid-Modified Sludge-Based Biochar, and Acetic Acid-Modified Sludge-Based Biochar-Uranium

Figure 6A and **Table 5** show the BET results for SBB, ASBB, and ASBB-U. As in **Figure 6A**, the isothermal sorption–desorption curves of SBB, ASBB, and ASBB-U all belonged to the unique I/IV isothermal sorption–desorption path with the H₄ hysteresis curve (Lu et al., 2018b). It means

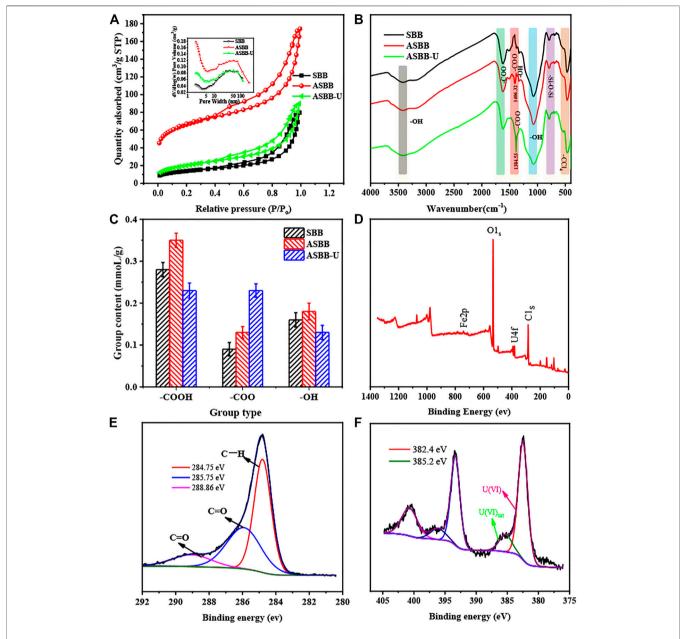


FIGURE 6 | Characteristics of SBB, ASBB, and acetic acid-modified sludge-based biochar—uranium (ASBB-U). (A) Brunner-Emmet-Teller (BET), (B) Fourier transform infrared spectroscopy (FTIR), (C) acidic group content, (D) x-ray photoelectron spectroscopy (XPS) total survey scans of ASBB-U, (E) XPS spectra of C1s, (F) XPS spectra of U4f.

TABLE 5 | Surface aperture analysis.

Sample	SSA (m ² /g)	Average pore width (nm)	Volume (cm ³ /g)
SBB	49.26	10.00	0.12
ASBB	241.42	8.35	0.21
ASBB-U	72.52	7.67	0.14

Note. SSA, specific surface area; ASBB-U, acetic acid modified sludge-based biochar—uranium.

that the porosity network of these materials was structured into micropores, mesopores, and macropores. According to the pore size distribution map (Figure 6A inside), SBB was

mainly mesoporous and macroporous (mean pore size around 50 nm), ASBB was mainly mesoporous (pores of 2 and 20–50 nm), and ASBB-U was mainly mesoporous (2 nm pores) and meso/macroporous (50 nm pores). By comparing the pore size distribution of ASBB before and after uranyl ion sorption, it was found that mesopores decreased after uranium sorption, indicating that the main reaction site was within this pore range. In addition, an inflection point near the monolayer sorption was observed in the isotherm. Multilayer sorption gradually took place with the increase in relative pressure. These phenomena were consistent with the fitting results by the sorption isotherm models above.

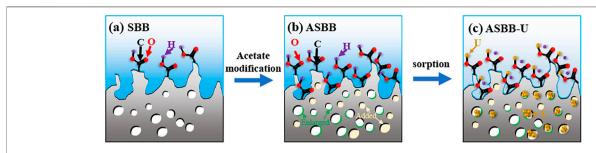


FIGURE 7 | Schematic diagram of SBB modification and uranium adsorbed by ASBB. (A) SBB, (B) ASBB, (C) ASBB-U.

The specific surface area (SSA) of ASBB increased with respect to the untreated biochar. Namely, a pore expansion function of acetic acid was observed. Then SSA for ASBB-U decreased. It indicates that uranyl ion was adsorbed in the pores of the ASBB surface. When the pores were blocked by the absorbed uranyl ion, the SSA of the adsorbent obviously decreased.

Group analysis of Sludge-Based Biochar, Acetic Acid-Modified Sludge-Based biochar, and Acetic Acid-Modified Sludge-Based Biochar-Uranium

FTIR analysis allowed to investigate the functional group modification when SBB was treated by acetic acid to give ASBB and the interaction of these groups with uranium during the sorption of U(VI) on ASBB. Results are illustrated in Figure 6B. According to literature (Gulnaz et al., 2005; Weng, 2010; Meng et al., 2019), -OH (3,427 and 1,070 cm⁻¹), -COO (1,406 and 1,617 cm⁻¹), -Si-O-Si (781 cm⁻¹), and -CCl₄ (476 cm⁻¹) were the main groups retrieved on the surface of SBB, ASBB, and ASBB-U. When the FTIR spectra of SBB, ASBB, and ASBB-U are compared, it is seen that -COO (1,406.32 cm⁻¹) was found on the ASBB surface as a new group with respect to SBB, indicating the modification of SBB by acetic acid. Moreover, when uranium was adsorbed on ASBB, some of the peak's position and intensity changed. The peak of -OH stretching vibration at 1,331.37 cm⁻¹ disappeared, indicating that -OH might react with U(VI) by deprotonation. In addition, the symmetric stretching vibration peak of -COO at 1,406.32 cm⁻¹ moved to 1,384.53 cm⁻¹. Although the peak shape was stable, its intensity was enhanced. The difference of the stretching vibration frequency between -COO antisymmetric stretching vibration peak (1,617.82 cm⁻¹) and -COO symmetric stretching vibration peak (1,384.53 cm⁻¹) was more than 200 cm⁻¹ (233.29 cm⁻¹). This indicates that -COO and U(VI) were combined in monodentate coordination mode (Weng, 2010).

Figure 6C shows the acid group content of SBB, ASBB, and ASBB-U. Compared with SBB, the contents of -COOH and -COO in ASBB had been increased by 0.07 and 0.04 mmol/g, respectively, indicating that SBB had been well loaded with acetic acid, and its loading was about 0.11 mmol/g. After the

ASBB reaction in UCW was completed, the content of –COOH was significantly reduced, while the content of –COO was increased, indicating the sorption of –COOH on U(VI). Combined with FT-IR analysis, U(VI) could be combined with –COO to purify UCW.

Valence state on Acetic Acid-Modified Sludge-Based Biochar—Uranium's Surface

Figure 6D–F present the XPS analysis results for ASBB-U's surface. From **Figure 6D**, it is seen that the main peak around 532 eV belongs to O1s, the peak around 285 eV to C1s, and the peak around 382 and 375 eV to U4f. It could be concluded that the surface of ASBB-U was mainly composed of C and O elements, and a certain amount of U(VI) adsorbed on the surface. In C1s spectrum (**Figure 6E**), the C1s component near 284.75 eV might be associated with C–H (Ding et al., 2018). Besides, the C1s spectrum could show C = O near 285.75 and 288.86 eV (Zhao et al., 2019). Moreover, the blending energy of U4f_{2/5} (382.4 eV, 385.2 eV) corresponded to U(VI) on the surface of ASBB-U (**Figure 6F**) (Husnain et al., 2017; Tan et al., 2018), indicating that no redox reaction happened in uranium sorption process by ASSB.

Mechanism of Modification and Sorption

Following the experimental results, various characterization methods (BET, SEM, EDS, FTIR, XPS), and relevant references (Li et al., 2021; Liu et al., 2021), the mechanism of SBB modification and uranium sorption by ASBB was inferred. A schematic diagram is displayed in Figure 7: 1) The reaction probability of ASBB to uranium was greatly improved, due to the increased pore diameter, specific surface area, and functional group (-COOH) number by acetic acid modification of SBB. 2) The most suitable interaction between uranium ion and adsorbent under suitable reaction conditions might be of van der Waals type (Hussein et al., 2016), as witnessed by the decrease in SSA and pore size after the reaction of ASBB with USW. 3) -COOH had a good uranium sorption behavior (Park et al., 2019). At pH = 5, -H on -COOH could be easily replaced by uranium, which mainly existed in the form of (UO₂)₃(OH)₅⁺ and $(UO_2)_4(OH)_7^+$. They were combined with -COO in monodentate coordination. The specific equation reads (Eq. 7):

$$U + -COH - COU + [H]$$

CONCLUSION

Excess sludge (ES) and acetic acid were utilized to obtain a robust adsorbent starting from sludge-based biochar (SBB), for U(VI) abatement in uranium-containing wastewater Compared with SBB, the removal efficiency and sorption capacity of the acetic acid-modified biochar (ASBB) could be effectively improved. An optimal U(VI) removal rate of 97.8% could be achieved, while initial conditions were pH = 6.0, U(VI) = 10.0 mg/L (initial concentration), adsorbent dosage = 0.30 g/L, and sorption time = 5.0 min. The beneficial effect was attributed to the double action of expanding pores and increasing -COOH functional groups following the acetic acid modification treatment. The process of U(VI) sorption by modified biochar relies on both physical and chemical sorption. The U(VI) removal mechanism by ASBB was of monodentate coordination binding between -COO- and uranium. In addition, ASBB had good reusable performance. Hence, the quick sorption and outstanding efficiency of ASBB offer a meaningful support for the use of biochar in uranium recovery from UCW and for reutilization of ES.

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DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

SY: Resources, Investigation, Writing—Original Draft. XW: Validation, Writing—Review and Editing. JY: Validation. ML: Validation, Visualization. QZ: Investigation. XZ: Validation. CL: Investigation. WX: Investigation. KS: Investigation. YL: Supervision.

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Optimize the Preparation of Novel Pyrite Tailings Based Non-sintered Ceramsite by Plackett-Burman Design Combined With Response Surface Method for Phosphorus Removal

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Chen R, Pan Z, Chu S, Xiao J, Weng R, Ouyang D, Yang Y, Wu X and Huang Z (2022) Optimize the Preparation of Novel Pyrite Tailings Based Nonsintered Ceramsite by Plackett-Burman Design Combined With Response Surface Method for Phosphorus Removal. Front. Chem. 10:850171. doi: 10.3389/fchem.2022.850171 The large amount of untreated pyrite tailings has caused serious environmental problems, and the recycling of pyrite tailings is considered as an attractive strategy. Here, we reported a novel non-sintered ceramsite prepared with pyrite tailings (PTNC) as the main active raw material for phosphorus control, and the dosage effect of ingredients on total phosphorus (TP) removal ability was investigated. The results from Plackett-Burman Design (PBD) suggested the dosages of dehydrated sludge, sodium bicarbonate, and cement were the factors which significantly affect the TP removal ability. The Box-Behnken Design (BBD) based response surface methodology was further employed, and it indicated the interactions between different factors, and the optimized recipe for PTNC was 84.5 g (pyrite tailings), 10 g (cement), 1 g (calcined lime), 1 g (anhydrous gypsum), 3 g (dehydrated sludge), and 0.5 g (sodium bicarbonate). The optimized PTNC was characterized and which presented much higher specific area (7.21 m²/g) than the standard limitation (0.5 m²/g), as well as a lower wear rate (2.08%) rather than 6%. Additionally, the leaching metal concentrations of PTNC were far below the limitation of Chinese National Standard. The adsorption behavior of TP on PTNC was subsequently investigated with batch and dynamic experiments. It was found that the calculated max adsorption amount (q_{max}) was about 7 mg/g, and PTNC was able to offer a stable TP removal ability under different hydraulic retention time (HRT). The adsorption mechanism was discussed by model fitting analysis combined with XRD and SEM characterization, and cobalt phosphide sulfide was observed as the newly formed substance through the adsorption process, which suggested the existing of both physical and chemical adsorption effect. Our research not only offered an economic preparation method of ceramsite, but also broadened the recycling pathway of pyrite tailings.

Keywords: pyrite, solid waste recycling, unburned ceramsite, phosphorus removal, filter material, harmless treatment

1 INTRODUCTION

Pyrite is the most abundant and widespread sulfide mineral which is mainly composed of iron and sulfur, and has been used as the raw material for sulfuric acid production for decades (Chandra and Gerson 2010). However, with the large-scale mining of pyrite, the pyrite tailings have caused serious environmental problems. As sulfide-rich waste materials, pyrite tailings can be oxidized in the presence of air and water (Garcia et al., 2005) spontaneously, which causes acid mine drainage (AMD) consequently (Malmström et al., 2006). AMD is considered as a serious and persistent environmental problem, which leads to the environment acidification and also releasing of significant amounts of various toxic metals into surface and groundwater (Heikkinen and Räisänen, 2009; Wang and Mulligan, 2009; Sahoo et al., 2013; Carvalho et al., 2014). Thus, the control of the pyrite tailings sourced pollution has become an important issue in the past decades, and various methods have been reported (Ouyang et al., 2015; Park et al., 2019; Dong et al., 2020a).

Remediation strategies are effective but unsustainable; thus, recycling of mine tailings is considered as a more economical way for reducing of tailings amount and limiting acid mine drainage formation. Currently, the most popular strategy for tailings recycling is replacing some portion of traditional but expensive construction materials, such as concrete admixture (Guo et al., 2016) and road construction admixture (Oluwasola et al., 2015). However, drawbacks still hindered the application of these strategies, such as higher energy consumption, dust generation increasing, and CO2 emission (Khale and Chaudhary, 2007), and novel effective and environment friendly method towards pyrite tailings recycling should be proposed. One important property of pyrite tailings should not be ignored, that is, large amounts of active reaction sites due to the existing of Fe and S in pyrite tailings, which can be used for removal of various pollutants (Yang et al., 2017). Thus, it is promising to use pyrite tailings as the active material to enhance the wastewater treatment process.

It is well known that the effluents of municipal wastewater treatment plants (WWTPs) contributed highly to these elements' concentrations in surface water, and the abundant nutrition elements (especially phosphorus) in water have caused a serious eutrophication problem in the past decades (Schindler et al., 2016). Thus the resource utilization and advanced treatment of waste water is a very meaningful way for the sustainable development of human beings, and strategies have been proposed (Bashar et al., 2018; Zeng et al., 2021). The biological aerated filter system (BAFS) has gained increasing attention due to smaller footprint and favorable ability for contaminants removal, which presented effective removal effect on COD, NH3-N, and TN (Dong et al., 2020b). BAFS generally takes advantages of a granular media for the formation of microbial biofilms and provides the depth filtration action as well. Certainly, the biomass, bioactivity, and filtration action in BAFS is highly depending on the media character, and it also significantly determines the investment of construction and operating cost. Thus, research has reported focusing on the

investigation of media performance of different materials in BAFS (Qiu et al., 2010; Bao et al., 2016; Bao et al., 2019), and ceramic particle was found as a favorable candidate due to its large specific surface area, high mechanical strength, and biological affinity (Yue et al., 2009; Han et al., 2013; Yang et al., 2015). However, the phosphorus removal by commercial ceramsites was unfavorable as yet (Jiang et al., 2014), and it is significant to propose strategies to improve its phosphorus removal.

Ceramsite was generally prepared with various active materials such as clay (Zhang et al., 2019), activated sludge (Nie et al., 2021) and fly ash (Mi et al., 2021) by high temperature calcination, which not only aim to improve the material properties and safety, but also promote the recovery and utilization of waste resource. However, the calcination is a high energy consumption process, and the crystal structure of raw material would be destroyed leading to the decrease of active adsorption sites. Consequently, non-sintered is considered as a more economic and effective way for preparation of ceramsites. Shao et al. (2019) prepared a non-sintered fly ash ceramsite for ammonia nitrogen adsorption, and which showed favorable adsorption capacity (4.25 mg/g) and standard-compliant leaching toxicity. Li et al. (2015) investigated the performance of non-sintered fly-ash ceramsite in the dual membrane processes for treatment of ethylene chemical plant wastewater, which indicated the biological aerated filter loaded with non-sintered ceramsite was a reasonable and effective method for pretreatment of reverse osmosis process. Besides fly-ash, the raw materials for non-sintered ceramsite preparation can be various, which provides more opportunities for recycling of solid wastes (He and Wang, 2019; Wang et al., 2021). Previous reports have already proved pyrite as a favorable absorbent candidate for wastewater treatment (Xu et al., 2006; Bulut et al., 2014; Ge et al., 2019; Chero-Osorio et al., 2021), and it is attractive to use pyrite tailings as the raw material for preparation of novel effective ceramsite towards phosphorus removal.

To our knowledge, there is no available report about the investigation of pyrite tailings based ceramsite as yet; thus, in this research, we employed pyrite tailings as the major active material aiming to prepare a novel non-sintered ceramsite (PTNC) for phosphorus control in wastewater treatment process. The main objectives are 1) investigate and optimize the recipe of raw materials mass ratio; 2) characterize the optimized PTNC with XRD, BET, SEM, and confirm its security by leaching toxicity metal concentration determination; and 3) investigate the application potential and clarify the removal mechanism of total phosphorus (TP) with batch adsorption experiment and dynamic column experiment.

2 MATERIALS AND METHODS

2.1 Materials and Chemicals

Pyrite tailings were collected from Anyang, Henan Province, and the chemical composition and XRD data of pyrite tailings are shown in **Supplementary Table S1** and **Supplementary Figure S1** respectively. The commercial 425[#] cement was used as

adhesive and stabilizer, and calcium lime (≥60% effective calcium oxide) and anhydrous gypsum (industrial grade) were used as activator. Dehydrated sludge (**Supplementary Table S2**) is obtained from a sewage treatment plant in Wenzhou and used to reduce the product weight. Sodium bicarbonate (analytical grade) was selected as the pore-forming agent.

2.2 Preparation of PTNC

Firstly, 25 ml deionized water was added into a mixture (totally 100 g) containing pyrite tailings, cement, calcium lime, anhydrous gypsum, sodium bicarbonate, and dehydrated sludge with required mass ratio. After pelleting to spherical ceramsite (6–10 mm), it was air-dried for 12 h at room temperature, then the ceramsites were steam cured with an autoclave at 1.2 MPa and 100°C for 10 h. The final PTUC product was obtained by regularly curing with spraying water for 2 days.

2.3 Optimization of the Components Dosage

2.3.1 Single Factor Experiment

Single factor experiments were performed to preliminary define the dosage of raw materials, and the phosphate removal rate as well as porosity were selected as the indicators. For each single experiment, the total mixture weight was fixed as 100 g, and the amount of pyrite tailings varied with the changing of corresponding ingredient amount. The test amounts of each material were shown as follows: cement (10, 20, 30, 40, and 50 g), calcium lime (1, 2, 3, 4, and 5 g), anhydrous gypsum (1, 2, 3, 4, and 5 g), dehydrated sludge (2, 4, 6, 8, and 10 g), and sodium bicarbonate (05, 1, 2, 3, 4, and 5 g).

2.3.2 Plackett-Burman Experiments

In order to obtain the significant influence factors on the phosphate removal capacity and porosity of PTNC, PBD method was used and the design scheme can be found in **Supplementary Table S3**, where five ingredients were coded respectively from code A to E, phosphate removal capacity was set as Y.

2.3.3 Box-Behnken Design Based Response Surface Methodology

Based on the significantly influence factors obtained from PBD experiments, the dosage of dehydrated sludge, sodium bicarbonate, and cement were selected and coded as X_1 , X_2 , and X_3 respectively for Box-Behnken design to optimize the PTNC preparation process. Phosphate removal capacity (Y) was used as the indicators, and the design scheme is shown in **Supplementary Table S4**.

2.4 Batch Adsorption Experiment for TP Removal

A total of 4.5 g PTUC was weighted and added into the conical flask (150 ml) and 50.0 ml solution containing required concentration of potassium dihydrogen phosphate was added,

and the vials were shaken at 100 rpm for 5 h at 25°C. The TP concentration in the filtered liquid was determined by Mo-Sb anti-spectrophotometry method (λ = 700 nm). The effect of pH, PTNC dosage, co-existing anions, and temperature on adsorption were investigated respectively as well as the adsorption kinetic, and all the experiments were performed in triplicate vials. The removal rate of TP was calculated as follow equation:

TP removal rate =
$$\frac{c_1 - c_0}{c_0} \times 100\%$$
 (1)

where c_0 and c_1 were the initial TP and filtered TP concentration in aqueous respectively.

2.5 Dynamic Adsorption of Total Phosphorus by PTNC in Column Experiment

In order to evaluate to the application potential of PTNC in TP control, an organic glass column (50×500 mm) was used to perform the dynamic adsorption experiment. PTNC was prepared according to the optimized results and filled into the column to 400 mm height. Simulated wastewater containing 26 mg/L TP was pumped into the column from the column bottom by a peristaltic pump, and the effect of hydraulic retention time (HRT) on TP removal was investigated in the range of 1–3 h. The diagram of experimental device can be found in **Supplementary Figure S2**.

2.6 Characterization of PTNC

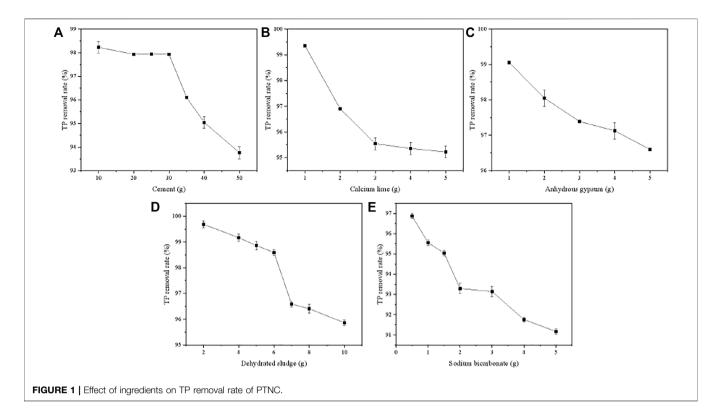
The physicochemical properties such as bulk density, apparent density, crush/wear rate, solubility in hydrochloric acid, voidage, and silt content were tested according to the Chinese standard (CJ/T 299-2008). Water absorption and cylinder compressive strength were tested as Chinese national standard (GB/T 17,431.2-2010). X-ray diffraction (XRD), BET method, and scanning electron microscopy (SEM) were employed to analyze the changes of crystal structure, specific surface area, and morphology after adsorption.

The leaching analysis of heavy metal was performed to evaluate the potential risk of PTNC. Briefly, sulfuric acid and nitric acid were mixed (mass ratio 2:1), and the added to deionized water and the pH was adjusted at 3.2. Then, 100 g PTNC was mixed with 1 L liquid above and shaken at 25°C, 30 rpm, for 20 h. After filtered with 0.45 μm membrane, the concentration of heavy metals was determined by ICP-OES, and the results were compared with the limitation of the standard of Leaching Toxicity Identification of Hazardous Waste (GB5085.3-2007).

3 RESULTS AND DISCUSSION

3.1 Single Factor Experiments

Figure 1 showed the effect of five ingredients on the TP removal capacity of PTNC. In terms of cement, the TP removal rate decreased from 98.23 to 95.04% with the increasing of cement content from 10 to 50 g (**Figure 1A**). It can be found that the removal rate was stable in the dosage range of 10–30 g, which can



attributed to the relative high amount of Ca (over 60%) that react with PO₄³⁻ to form a complex compound. As the dosage of cement was over 30 g, the decreasing of removal rate can be ascribed to the lower porosity of PTNC, which was almost 0 as 50 g cement was added. The TP removal rate decreased from 99.35 to 95.23% with the increasing of calcium lime (Figure 1B). Adding of quicklime can increase the content of Ca in ceramsite to some extent, which is beneficial to the removal of TP. However, the excess using of quicklime will destroy the Si-O bond in the product due to the alkaline environment, which leads to the reduction of the specific surface area. Therefore, the dosage of quicklime was selected as 1 g. With the increasing of gypsum dosage from 1 to 5 g, the TP removal rate decreased from 99.05 to 96.60% (Figure 1C). The main component of gypsum is CaSO₄ which could increase the content of Ca in ceramsite, and was conducive to the removal of TP, but the excessive amount of gypsum leads to a longer digestion time of quicklime due to its high hygroscopicity, which reduces its activity and leads to a decrease in specific surface area and porosity. Therefore, the amount limitation of PTUC gypsum is set as 1 g. In the terms of dehydrated sludge (Figure 1D), the TP removal rate showed decreasing tendency as the dosage increased. It can be ascribed to the high amount of organic matter that inhibited the hydration reaction and hindered the production of gelled substances, which resulted in a decrease in porosity (Figure 1E). A similar tendency can be found in the effect of sodium bicarbonate. Adding sodium bicarbonate can promote the forming of pores structures during steam curing, but too much sodium bicarbonate will release a large amount of CO2 at high temperature, which makes the skeleton structure become

TABLE 1 | Experimental design and response of Plackett-Burman experiment.

Runs	Α	В	С	D	E	Removal rate (%)
1	+1	+1	-1	+1	+1	56.77
2	-1	+1	+1	-1	+1	51.37
3	+1	-1	+1	+1	-1	92.84
4	-1	+1	-1	+1	+1	85.68
5	-1	-1	+1	-1	+1	52.83
6	-1	-1	-1	+1	-1	92.14
7	+1	-1	-1	-1	+1	49.71
8	+1	+1	-1	-1	-1	58.05
9	+1	+1	+1	-1	-1	56.86
10	-1	+1	+1	+1	-1	92.30
11	+1	-1	+1	+1	+1	68.05
12	-1	-1	-1	-1	-1	70.23

loose and difficult to form into pellets. Thus, the sodium bicarbonate dosage is set as 0.5 g here.

3.2 Significant Factors Affecting the TP Removal Rate

Based on the results of a signal factor experiment, a two-level PBD factorial design of 12 runs was employed to unbiasedly screen the variables that significantly affect the TP removal rate by PTNC (Table 1), and Figure 2 showed the analysis results. Five ingredients affected the TP removal rate as the following order: D (Dehydrated sludge) >E (Sodium bicarbonate) >A (Cement) >B (Calcium lime) >C (Anhydrous gypsum), and the dosage of dehydrated sludge affected TP removal rate

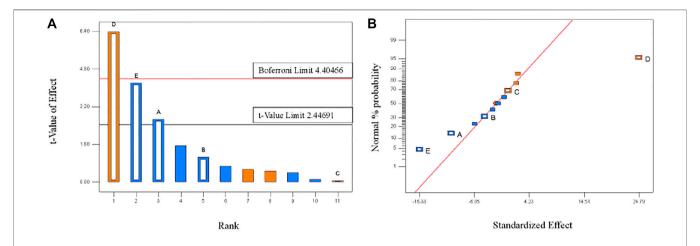


FIGURE 2 | Pareto plot (A) and normal distribution plot (B) of TP removal rates. The hollow square column represents the experimental data, and the solid square column represents the dummy error. The red line in Pareto plot indicates the 99% confidence interval limitation and black line stands for 95% confidence interval limitation

TABLE 2 | Significant test for Plackett-Burman design regression model.

	Factors	Adj SS	DF	Adj MS	F	р
TP removal rate	Model	3,018.45	5	603.69	13.41	0.0033
	Α	323.00	1	323.00	7.18	0.0366
	В	51.07	1	51.07	1.13	0.3278
	С	0.23	1	0.23	0.00518	0.9451
	D	1843.70	1	1843.70	40.96	0.0007
	E	800	1	800.44	17.78	0.0056
	Error	270.05	6	45.01	_	_
	Total	3,288.50	11	_	_	_

Adj SS, Adjusted Sum of Square; Adj MS, Adjusted Mean Square; DF, Degrees of Freedom, (Wang et al., 2014).

most significantly which arrived at the 99% confidence interval. Sodium bicarbonate and cement also showed significant influence effect on TP removal rate, which were observed at 95% confidence interval (**Figure 2A**). It can be also proved by the normal distribution plot (**Figure 2B**), where the points standing for dehydrated sludge, sodium bicarbonate, and cement showed significant dispersion from the fitted line. **Table 2** shows the results of significant inspection of regression, which further proved the factors with significant effect on the TP removal rate were dehydrated sludge, sodium bicarbonate, and cement, and a model **Equation 1** for TP removal rate (%) (Y) was proposed; the p value and p for the model were 0.0366 and 0.9179 which indicated the validity of the model.

$$Y = 68.91 - 5.19A - 2.06B + 0.14C + 12.40D - 8.17E$$
 (2)

3.3 Box-Behnken Design for Preparation Optimization

Based on the PBD results, the significant factors dehydrated sludge (X_1) , sodium bicarbonate (X_2) , and cement (X_3) were considered for further optimization using BBD, and the matrix

TABLE 3 | Experimental design and results of BBD.

Run order	X_1	X_2	X_3	TP removal rate (%)
1	-1	-1	0	60.45
2	1	-1)	0	89.69
3	-1	+1	0	59.74
4	+1	+1	0	81.03
5	-1	0	-1	64.90
6	+1	0	-1	92.00
7	-1	0	+1	38.85
8	+1	0	+1	78.92
9	0	-1	-1	93.34
10	0	+1	-1	80.88
11	0	-1	+1	87.50
12	0	+1	+1	81.47
13	0	0	0	57.32
14	0	0	0	60.15
15	0	0	0	70.93
16	0	0	0	69.66
17	0	0	0	66.45

for BBD along with the experimental results is shown in **Table 3**. By applying multiple regression analysis on the experimental data, the following second order polynomial model was obtained to describe the TP removal rate (2):

$$Y = +64.90 + 14.71X_1 - 3.48X_2 - 5.55X_3 - 1.99X_1X_2 + 3.24X_1X_3$$

+1.61X₃X₂-4.65X₁²+12.48X₂²+8.42X₃² (3)

The adequacy of the model was checked using ANOVA and the results were shown in **Table 4**. The F value of model was 7.54 and the p value (Prob > F) was 0.018, indicating that the model was highly significant, which was also confirmed by the nonsignificant p value of "Lack of fit." It can be also found that the variable X_1 as well as the quadratic terms X_2^2 and X_3^2 showed significant relationship with the TP removal rates. R^2 of the model was 0.9065, suggesting the model has a good agreement for data

TABLE 4 | ANNOVA for BBD.

Source	Adj SS	DF	Adj MS	F-value	p-value
Model	3,197.96	9	355.32	7.54	0.0072
X_1	1731.58	1	1731.58	36.75	0.0005
X_2	97.01	1	97.01	2.06	0.1945
X_3	246.29	1	246.29	5.23	0.0561
X_1X_2	15.80	1	15.80	0.34	0.5806
X_1X_3	42.03	1	42.03	0.89	0.3764
X_2X_3	10.31	1	10.31	0.22	0.6541
X_1^2	91.11	1	91.11	1.93	0.2070
X_2^2	655.62	1	655.62	13.91	0.0074
X_3^2	298.33	1	298.33	6.33	0.0400
Error	329.85	7	47.12	_	_
Lack of fit	188.36	3	62.78	1.78	0.2908
Pure error	141.48	4	35.37	_	_
Total	3,527.81	16	_	_	_

Adj SS, Adjusted Sum of Square; Adj MS, Adjusted Mean Square; DF, Degrees of Freedom, (Wang et al., 2014).

Coefficient of variation - 9.46%; Signal to noise ratio - 9.738; R^2 - 0.9065; R^2_{Adi} - 0.7863.

fitting. The ratio of signal to noise (Adeq Precision) was 9.738 which was over 4, and the coefficient of variation (C.V.) was lower than 10%, indicating the reproducibility of the model. These statistical analysis results showed that the model was reliable and accurate, and can be used for the analysis and prediction of TP removal by PTNC. The statistical model was further validated by experiments with PTNC prepared under different conditions (Supplementary Figure S3). It can be said that the predicted model response for experimental value was close to the predicted value, thus validating the model.

The optimum level of each variable and the effect of their interaction on TP removal rate were investigated by constructing response surface plots and their corresponding contour plots (Figure 3). With the increasing of dehydrated sludge dosage, the TP removal rate of PTUC showed an increasing trend. The response surface showed a steep slope (Figure 3A), which indicated the interaction between factors. The increasing of dehydrated sludge content increased the active adsorption sites for phosphate combination, which improved the TP removal rate reasonably. When the dehydrated sludge content was fixed as 4 g, the TP removal rate of PTUC showed non-significant change with the increment of cement dosage, which was about 80% (Figure 3B). It was reported that the phosphate anion will react with Ca²⁺ and OH⁻ which formed complex precipitates (Qiu et al., 2015). The addition of cement increased the Ca amount in PTNC; however, the increasing of cement dosage would decrease the porosity which hindered mass diffusion, which can be further proved by the high interaction caused by the pore forming substance sodium bicarbonate (Figures 3A,C).

In order to deter the optimum preparation conditions, the primary target value was obtained by calculating the model, and the raw materials dosage was rounded and fitted again with the model for optimal target value. PTNC was prepared consequently, and TP removal rate was tested to calculate the error and determine the fitting result (**Table 5**). The errors between the measured values of TP removal rate and the predicted values of the model fitting were 1.80%, indicating

that the fitting effect was favorable and the model was reliable. Thus the optimal raw material ratio (per 100~g) was 84.5~g (pyrite tailings), 10~g (cement), 1~g (calcined lime), 1~g (Anhydrous gypsum), 3~g (dehydrated sludge), and 0.5~g (sodium bicarbonate).

3.4 Characterization of PTNC Prepared Under Optimized Condition

The surface of PTUC is rough, with low smoothness, dark gray color, and pore structure on the outer surface (Figure 4A), and the apparent morphology observed by SEM showed many grooves on its surface, with uneven interior and abundant pores, indicating its large specific surface area. The determined specific surface area and pore size was consistent with the above conclusion (Supplementary Table S5). It can be said that PTNC was suitable for the attachment and growth of microorganisms. The physical parameters of PTNC meet the requirements of relevant standards favorably (Supplementary Table S6). The high apparent density and water absorption rate ensures the adsorption characteristics of PTNC. And the favorable mechanic strength such as low wear rate and higher cylinder compressive strength ensured the application possibility of PTNC, and the porous nature is a benefit for the attachment of functional microbial community. XRD analysis confirmed the PTNC is mainly composed of FeS2, CaSO4, and SiO2 (Supplementary Figure S4). The peak strength of CaSO₄ crystal is the most obvious, followed by SiO2, indicating the formation of SiO2 during the steam curing process of PTNC, acting as the framework structure of PTNC, which was also consistent with the low wear rate observed. Moreover, the heavy metal ion concentration in the PTNC leachate is much lower than the limitation of Hazardous Waste Identification Standard Leaching Toxicity Identification (GB5085.3-2007) (Supplementary Table S7), which indicate its security to the environment.

3.5 The Adsorption Behavior and Mechanism of TP on PTNC

Simulated wastewater containing 25 mg/L TP was employed to investigate the adsorption kinetic. The adsorption amount showed increased tendency with the increasing of reaction time (Figure 5A). The adsorption equilibrium was observed at 16 h, where the TP concentration decreased to 0.43 mg/L, meeting the V level of "Surface water Environmental Quality Standard" (GB 3838-2002), and the equilibrium adsorption capacity was 0.2864 mg/g. As the mostly using models for description of adsorption kinetic, pseudo first-order and pseudo second-order models (Text S1) were used to fit the experimental data (Supplementary Table S8) (Chen et al., 2019). Although the correlation coefficients of both two kinetic models were similar (>0.9), the predicted adsorption capacity with pseudo first order model is 0.2995 mg/g which is close to the experimental value (0.2864 mg/g). Therefore, the pseudo first-order kinetic model can describe the TP adsorption process on PTNC better. The both two well fitted models indicated that both of chemisorption and physisorptions

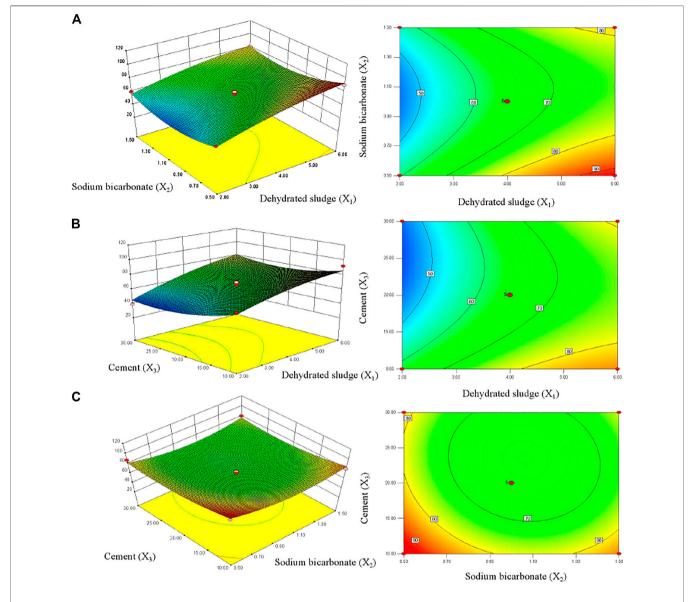


FIGURE 3 | Surface and contour plot showing interactions between variables on TP removal rates by PTNC. (A) stands for interaction between dehydrated sludge and sodium bicarbonate; (B) shows interaction between dehydrated sludge and cement; (C) stands for interaction between sodium bicarbonate and cement.

 $\textbf{TABLE 5} \mid \textbf{The optimization results of regression}.$

	X ₁	X ₂	X ₁	TP removal rate (%)	Degree of fitting
Primary	3.1	0.5	10	89.41	96.3
Optimal	3	0.5	10	88.55	95.5
Actual	3	0.5	10	86.96	_
Error	_	_	_	1.80%	_

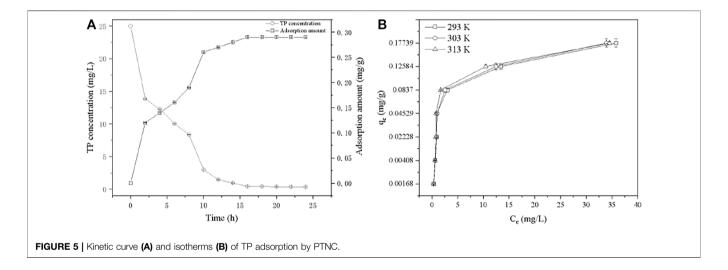
existed in the process of TP removal by PTNC, which were mainly ion exchange effect and precipitation probably (Yang et al., 2017). Generally, adsorption process can be divided into several steps, firstly the adsorbate in aqueous diffuses from

aqueous to the adsorbent surface, then the surface loaded adsorbate diffuses to internal pores (diffusion within particles), and finally the internal adsorption sites are saturated. It can be found that the adsorption rate decreased apparently from 4 to 10 h, which can be attributed to the chemisorption of TP by PTNC leading to the formation of cobalt phosphide sulfide (Supplementary Figure S4) and decreased of the pore size of PTNC (Supplementary Table S5), thus the diffusion of phosphorus to the internal pores can be hindered.

The adsorption thermodynamics was investigated through three isotherms at different temperatures (**Figure 5B**), through the data fitting with Langmuir and Freundlich isotherm models (Text S2) (Chen et al., 2019). It can be found that Langmuir model fitted better with the isotherms, and indicated the mono-



FIGURE 4 | The appearance of PTNC (6-8 mm diameter) (A) and SEM images of PTNC (B).



layer adsorption process (Supplementary Table S9). The thermodynamic parameters were calculated (Text S3), and the negative ΔG suggested the TP removal is a spontaneous process (Supplementary Table S10). Additionally, the obtained negative value of ΔH (-11.69 kJ/mol) and positive value of ΔS (153.09 J/ mol/K) together indicate that the adsorption is an exothermic reaction and is both enthalpy and entropy driven. Generally, the adsorption process is an entropy reduction process; however, are existing adsorption cases that presented entropy-positive with a negative enthalpy change (Wen et al., 2010). For TP removal process by PTNC, it can be ascribed to the releasing of Fe3+, Ca2+, and OH- from PTNC surface which increased the entropy. And these ions would react with phosphate and formed of precipitation on the surface of PTNC which additionally make contribution to the entropy increasing. It can be found that the specific surface of PTNC increased obviously after adsorption (Supplementary Table S5). Moreover, the XRD analysis of the PTNC after adsorption (Supplementary Figure S4), which suggested the newly formation of cobalt phosphide sulfide, and the SEM

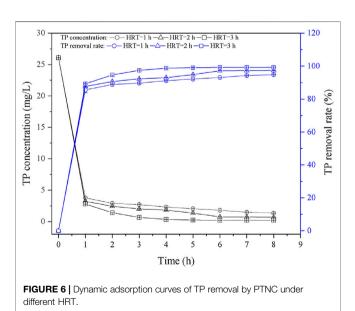


TABLE 6 | Comparison of the TP removal ability of different ceramsites.

Ceramsite	Calcining temperature (°C)	Initial TP concentration (mg/L	Adsorption capacity (mg/g)	Reference
CFA/WS/OS-op	1,050	100	4.51 (calculated)	Cheng et al. (2018)
Slag ceramsite	1,000	10	10.5	Liu et al. (2021)
N&P-adsorbed ceramsite	800	100	0.93	Shao et al. (2022)
DWTS ceramsite	1,050	20	1.43	Chen et al. (2019b)
PTNC	Non	25	6.9978	This work

morphology observation (**Supplementary Figure S5**) of the PTNC after adsorption further confirmed the precipitation formation during the adsorption process. It is consistent with the previous report (Ge et al., 2019).

Figure 6 showed the dynamic TP removal curves under different HRT (1, 2, 3 h). In the initial stage, the TP concentration in effluent decreased rapidly, which is ascribed to the large amount of active adsorption sites in the initial stage (Chu et al., 2014). The TP concentration tended to be stable after running for 8 h, and it was due to the concentration gradient of phosphorus solution decreased gradually. In terms of HRT = 1 h, the TP concentration in the effluent was about 1.35 mg/L, and the TP removal rate was 94.82% after 8 h. As the HRT increased to 2 h, the final TP concentration in the effluent decreased to 0.69 mg/L, and the removal rate further increased to 97.34%. Similar phenomena can be observed when HRT was set as 3 h, where the stable TP concentration in the effluent is about 0.20 mg/L, which is meeting the standard of III class surface water. As expected, the low HRT will lead to the insufficient time for phosphate contact and react with adsorption sites, as well as the released active ions; thus, suitable HRT should be considered in the application. Additionally, it can be found that the performance of PTNC was better than the phosphorus removal effect of the mixture of iron scrap and sand as previous report (88%) (Erickson et al., 2012). Table 6 showed the comparison of the TP removal ability of PTNC with other ceramsite. It can be found that PTNC presented highest TP adsorption capacity besides the Slag ceramsite reported by Liu et al. (2021). But the non-sintered preparation of PTNC is a more economical way. Thus, the prepared PTNC is promising for TP control and waste recycling.

4 CONCLUSION

In this research, a novel non-sintered ceramsite (PTNC) was prepared with pyrite tailings, and the preparation process was optimized by combination of PBD and BBD based response surface methodology, which confirmed the optimized mass ratios of the ingredients was 84.5 g (pyrite tailings), 10 g (cement), 1 g (calcined lime), 1 g (Anhydrous gypsum), 3 g (dehydrated sludge), and 0.5 g (sodium bicarbonate). PTNC presented favorable properties such as high specific surface, low leaching toxicity, and excellent mechanical strength. And the investigation on the adsorption behavior through batch and dynamic experiments showed the favorable adsorption capacity

of PTNC, whose calculated q_{max} was about 7 mg/g, and can offer stable removal ability continuously under different HRT. The analysis of the adsorption mechanism suggested the existing of both physical and chemical adsorption effect. The total results make contribution to the resource of pyrite tailings, which are also benefit to the development of novel effective and economic medium for BAFS in the advanced treatment of wastewater.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/**Supplementary Material**, further inquiries can be directed to the corresponding authors.

AUTHOR CONTRIBUTIONS

All authors contributed to the study conception and design. Material preparation, data collection and analysis were performed by RC, JX and ZP. The first draft of the manuscript was written by RC and all authors commented on previous versions of the manuscript. All authors read and approved the final manuscript.

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Effect of Gallium as an Additive Over Corresponding Ni–Mo/γ-Al₂O₃ Catalysts on the Hydrodesulfurization Performance of 4,6-DMDBT

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Experiments were carried out to research the different contents of Ga₂O₃ modification effects on the hydrodesulfurization (HDS) performance of 4,6-dimethyldibenzothiophene (4,6-DMDBT) catalyzed by the stepwise impregnation method. Characterization techniques such as XRD, BET, HRTEM, NH3-TPD, and Py-FTIR were performed to determine the effects of each modification of the catalyst by Ga on the properties of the prepared supports and catalysts. The catalytic effect of gallium is reflected in the fact that the empty d-orbitals of Ga elements participate in the formation of molecular orbitals in the active center and change their orbital properties, thus generating a direct desulfurization active phase suitable for complex sulfides for endpoint adsorption. The characterization results indicated that the introduction of Ga₂O₃ with appropriate content (2 wt.%) promoted Ni and Mo species to disperse uniformly and doping of more Ni atoms into the MoS₂ crystals, which also increased the average stacking number and the length of MoS₂. As a result, more NiMoS active phases were favored to form in the system. The specific surface area and the amounts of acid sites were increased, facilitating the adsorption of reactant molecules and the HDS reactions. The HDS results also suggested the effects of Ga modification play a very important role in the catalytic performance of the corresponding catalysts. The catalyst Ga-Ni-Mo/Al₂O₃ exhibited the highest conversion rate towards 4,6-DMDBT HDS when the amount of Ga₂O₃ loading was 2 wt.% with an LHSV of 2.5 h⁻¹ at 290°C and Ga modification also can effectively improve the direct desulfurization (DDS) route selectivity in varying degrees.

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INTRODUCTION

With the increase in global environmental pollution and environmental laws and regulations in various countries becoming stricter, exhaust from the combustion of sulfide in automotive diesel has become one of the important sources of pollution (Wang et al., 2017; Liu et al., 2018; Weng et al., 2020; Zeng et al., 2021). The Environmental Protection Agency (EPA) and E.U. stipulate that the sulfur content should not exceed 10 and 15 ppm (Kulkarni and Afonso, 2010; Liu et al., 2020; Guo et al., 2021). Therefore, low sulfurization of diesel fuel and achieving deep desulfurization of diesel fuel have become a key issue in hydrodesulfurization (Humadi et al., 2021). At present, diesel

desulfurization technologies being investigated at home and abroad include adsorptive desulfurization (ADS), oxidative biodesulfurization desulfurization (ODS), (BDS), hydrodesulfurization (HDS). ODS is a technology for oxidizing heavy sulfides by adding one or two oxygen atoms to sulfur using a suitable oxidant at low temperature and pressure; however, the chosen oxidant is not always selective, and the selective solvent for the extraction of sulfur compounds is not necessarily suitable either (Ali et al., 2006). The basic principle of ADS is to use adsorbents to adsorb sulfur compounds in diesel oil so as to remove sulfides from diesel (Selvavathi et al., 2009). However, adsorption desulfurization is difficult to regenerate, and most adsorbents are not highly selective for sulfides such as 4,6-DMDBT, which are difficult to hydrotreat (Jayaraman et al., 2004). BDS is a new technology for the removal of bound sulfur from sulfur-containing heterocyclic compounds in petroleum using aerobic and anaerobic bacteria at atmospheric pressure and temperature, with promising applications (Mohebali and Ball, 2016). Nevertheless, the desulfurization rates of biocatalysts and the ability of organic sulfides limit their large-scale commercialization (Monticello, 2001). Based on the challenges of the abovementioned three technologies, HDS remains the most widely used technology in the world, which is a heterogeneous and conventional hydrogenation reaction (Chandra Srivastava, 2012). Compared with the former three, it has longer catalyst lifetime and stronger catalyst adaptability to the feed and has the advantage of a higher desulfurization rate for HDS (Huang et al., 2018; Weng et al., 2020). However, HDS cannot effectively low-reactive sulfur compounds, dibenzothiophene (DBT) and its derivatives, especially 4,6-DMDBT. In order to effectively remove 4,6-DMDBT, two pathways, desulfurization direct (DDS) hydrodesulfurization (HYD), have been studied by many scholars (Gates and Topsøe, 1997; Li et al., 2019). Studies have shown that unsubstituted 4,6-DMDBT HDS reaction is more dependent on the DDS path, where it not only reacts faster but also results in desulfurization under the premise of ensuring that the aromatic rings do not increase. However, it is limited by its steric hindrance of the substituents (Yin et al., 2013; Wang et al., 2020). In order to design and prepare a highly active hydrodesulfurization catalyst, Okamoto and Kubota (2003) synthesized SiO₂-, TiO₂-, ZrO₂-, and Al₂O₃-supported catalysts using the CVD technique and found that the activity of hydrodesulfurization is positively correlated with the amount of CoMoS phases. Wagenhofer et al. (2020) thought that unsupported Ni-Mo sulfides react more rapidly than Al₂O₃supported catalysts on the rate of hydrodesulfurization. Naboulsi et al. (2017) considered that the DDS route is a mainly hydrodesulfurization route than HYD when dual mesoporous titania is used as a support. Due to the high OH concentration on the surface of the support, an inherent Brönsted acid center is formed that is conducive to direct desulfurization through isomerization and disproportionation reactions. In addition, the exploration of support modification has not stopped, and composite supports such as SiO2-TiO2 (Gallegos-Hernández et al., 2020), SiO₂-Al₂O₃ (Xu et al., 2017), ZrO₂-Al₂O₃ (Baston et al., 2015; Díaz-García et al.,

2017), and MgO₂–Al₂O₃ (Rana et al., 2007; Guevara-Lara et al., 2010; Vázquez–Garrido et al., 2019) are still a hot topic for the majority of scholars. However, due to its low cost, easy industrialization, and high surface area, as well as excellent thermal, mechanical, and chemical stability, γ -Al₂O₃ is still the most widely used carrier for hydrodesulfurization catalysts (Egorova, 2004; Wang et al., 2016).

It has been proposed that most hydrotreating reactions take place at the MoS₂ edge and HDS has been found to occur at the corner sites (Abrams et al., 1996; Eijsbouts, 1997; Kasztelan et al., 1984; Kasztelan, 1990). Schuit and Gates (1973) believed that the S-atom in the upper layer is chemically bonded to the Mo-atom in the immediate lower layer. When the Mo atoms are reduced from Mo⁵⁺ to Mo³⁺, the S atoms move out of the surface, thus forming active sites. The cofactor Ni enters into the surface structure of the alumina carrier and induces the formation of a tetrahedral structure of the secondary Al atoms. Each S atom is bonded to two Mo atoms, and when the S atoms are removed, the S hole formed releases the two Mo atoms and causes one of them to form an adsorption site. The performance of the catalyst is directly related to the number of active sites with high catalytic performance. For the NiMoS active phase, Ni mainly contributes to the associated generation of sulfhydryl (SH) groups and their selective incorporation at the MoS₂ slab edge (Copéret, 2013; Schüth, 2009). When metal elements with suitable electronic structures are introduced into Ni-Mo/Al₂O₃ bimetallic catalysts, the active phase of Ni-Mo-S is affected and the concentration of active centers is increased; thus, the activity of the catalyst for hydrodesulfurization reaction is enhanced (Manoli et al., 2004; Varga et al., 2017). Ferdous et al. (2005) suggested the increased activity is related to the decrease of average slab length and the increase of MoS2 edge along with angular atom dispersion. More importantly, it can promote the formation of more type II NiMoS active phases (Zhou et al., 2017; Zhou et al., 2018; Tanimu and Alhooshani, 2019). It is generally believed that there is a great correlation between the numbers of type II NiMoS active phases and the catalytic activity of the catalyst (Chen et al., 2013). Research shows that the metal-support interaction (MSI) is crucial for electron transfer between the metal and support when the catalysts support multiple metals (Ning et al., 2017). To explore the effect of metal additives on the activity of HDS, a large number of polymetallic catalysts supported on Γ-Al₂O₃ have been investigated, such as Fe (Liu et al., 2021), Zn, Ru, and Ir (Niquillerothlisberger and Prins, 2006), and even noble metal Pt (Liu et al., 2021) and its alloys Pt-Pd (Niquillerothlisberger and Prins, 2006). Pt is favored by scholars over other metals because it has more advantages in providing active hydrogen species, giving the catalyst superior hydrogenation performance. However, the sulfur resistance of Pt-based catalysts is still a major problem that plagues practical applications and needs to be enhanced. In recent years, the addition of Ga as a metal additive for the synthesis of HDS catalysts has started to attract attention due to the advantage of circumventing the high cost of precious metals (Altamirano et al., 2005). Gallium ions not only have a high affinity for tetrahedral sites of alumina but also change the ratio of tetrahedral to octahedral species of Ni (Co) that can

participate in the MoS₂ decoration (Cimino et al., 1975; Jacono et al., 1977). Moreover, people have found that the modification of gallium on the surface will not only change the morphology of the MoS₂ slab promoted by active metal Ni but also enhance the vulcanization of Mo species (Zhou et al., 2017). Altamirano et al. (2005) observed the addition of Ga increased the activity of the NiMo catalyst and affected the reaction rate of the HYD route and DDS route in different degrees. Ga has the outer electron arrangement of 4s²4p¹ and has an outer orbit similar to that of Ni (3d⁸4s²) and Mo (4d⁵5s¹). As a result, the empty orbitals participate in the formation of active center molecular orbitals and modify the morphology of Ni-Mo-S active phases (Altamirano-Sanchez et al., 2008; Zepeda and Pawelec, 2012; Zhou et al., 2018). Nevertheless, for HDS activity, there is no clear and reasonable explanation about the additional amount of metal content and reaction conditions.

Considering that in this context, a series of catalysts with the Ga content ranging from 2 to 6 wt.% were prepared by the stepwise impregnation method. A succession of characterizations (XRD, BET, TEM, NH3-TPD, and Py-FTIR) were carried out to investigate the effect of Ga loading on the physical and chemical properties of the Ni–Mo/ γ -Al₂O₃ catalyst. The hydrodesulfurization reaction was evaluated using 4,6-DMDBT as the probe molecule, and the effects of Ga loading and reaction conditions (temperature and liquid hourly space velocities) on the hydrodesulfurization conversion and DDS selectivity of 4,6-DMDBT were examined.

EXPERIMENTAL

Preparation of the Supports

First, γ -Al₂O₃ was prepared by the strip extrusion method with the following process conditions: pseudo-boehmite (Shandong Aluminum Corporation) and deionized water were mixed thoroughly at a mass ratio of 1:1, and then, 2 wt.% sesbania powder (Shandong Xunda Chemical Group Co., Ltd.) and 5 wt.% nitric acid (HNO₃, Aladdin, 65%) were added. The mixture was extruded by using an extruding machine at 30 MPa pressure, and the extruded strips were shaped into a clover type with a diameter of 1.5 mm. The supports was naturally dried in a place of protection from light and ventilation for 24 h and then dried in a drying oven at 120°C for 12 h, and finally, the required γ -Al₂O₃ supports were obtained in a muffle furnace at a heating rate of 2°C min⁻¹, kept at 500°C for 4.0 h, and naturally cooled to room temperature. The obtained supports were sieved into particles with the size of 20–40 meshes.

Preparation of the Ni–Mo/ γ -Al₂O₃ Catalysts

The incipient wetness co-impregnation method was used to synthesize Ni-Mo/ γ -Al $_2$ O $_3$ catalysts, and the active metal loading was MoO $_3$:16 wt.% and NiO:4 wt.%, respectively. The specific preparation process is as follows: a certain mass of ammonium heptamolybdate tetrahydrate [(NH $_4$) $_6$ Mo $_7$ O $_2$ 4·4H $_2$ O, Aladdin, \geq 99.8%] was added to an appropriate amount of deionized water and ammonia to dissolve it completely, and then, nickel nitrate hexahydrate

 $[\mathrm{Ni}(\mathrm{NO_3})_2\cdot 6\mathrm{H_2O},\ \mathrm{Aladdin},\ \geq 99.8\%]$ solution was added and stirred uniformly to obtain the nickel–molybdenum coimpregnated solution. The prepared Ni–Mo co-impregnation solution was evenly added dropwise to the alumina surface, and the samples were naturally dried at room temperature for 24 h, then dried in an oven for 6 h, and finally, heated to 500°C at a rate of 2°C min⁻¹ in a muffle furnace kept at a constant temperature for 4.0 h.

Preparation of the Ga-Modified Ni–Mo/ γ-Al₂O₃ Series Catalysts

Å series of Ga-modified Ni–Mo/γ-Al $_2$ O $_3$ catalysts were prepared using the stepwise impregnation method, in which the Ga $_2$ O $_3$ loading amount was 2 wt.%, 4 wt.%, and 6 wt.%, respectively, and the specific steps were as follows: gallium nitrate (Ga(NO $_3$) $_3$ ·H $_2$ O, Aladdin, ≥99.5%) was dissolved in the deionized water, and then, the solution was loaded using incipient wetness impregnation on the Ni–Mo/Al $_2$ O $_3$. The sample was dried in air for 24 h and then dried in an oven at 120°C for 4 h. Finally, it was heated to 500°C at 2°C min $^{-1}$ in a muffle furnace, with a constant temperature for 4.0 h. The obtained catalysts were denoted as SCal (2 wt.% Ga $_2$ O $_3$), Scam (4 wt.% Ga $_2$ O $_3$), and SCah (6 wt.% Ga $_2$ O $_3$) depending on Ga $_2$ O $_3$ content from low to high.

Material Characterization

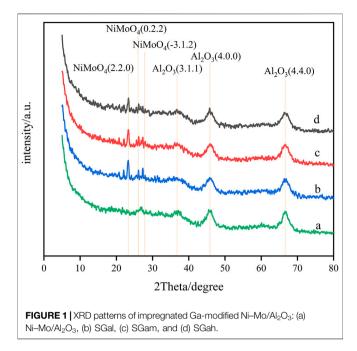
All catalyst samples synthesized were characterized on a PANalytical advanced powder diffractometer using Cu Ka radiation with an accelerating voltage of 40 kV and current of 40 mA in the 20 interval of 5–80 °via a scanning rate of 0.2 °s⁻¹, by which the patterns of X-ray diffraction (XRD) were recorded. The surface areas of the tested samples were carefully calculated by using the Brunauer-Emmett-Teller (BET) equation in the relative pressure (P/P0) range of 0.05-0.30. The pore diameter distributions and pore volumes of all the investigated samples were calculated using the Barrett-Joyner-Halenda (BJH) method from the N₂ adsorption isotherms. The catalysts were sulfided in a JQ-III fixed-bed microreactor with 2 wt.% CS₂ cyclohexane solution at 320°C for 4 h. Afterward, the investigated catalysts were taken on a Philips Tecnai G2 F20 instrument with an acceleration voltage of 200 keV to obtain the images of active phases via a high-resolution transition electron microscope (HRTEM). To analyze the results of the average slab length and average stacking number of MoS₂, no less than 300 MoS₂ slabs were counted using the equations reported elsewhere (Ortega-Domínguez et al., 2015; W. Zhou et al., 2017).

Average slab length
$$\bar{L} = \sum_{i=1}^{n} n_i l_i / \sum_{i=1}^{n} n_i$$
, (1)

Average stacking number
$$\bar{N} = \sum_{i=1}^{n} n_i N_i / \sum_{i=1}^{n} n_i$$
, (2)

where l_i is the length of the slab, n_i is the number of slabs with length l_i , and N_i is the number of layers in slab i.

The acidity of the catalysts was assessed by NH₃ temperature programmed desorption (NH₃-TPD), which was performed on



an Auto Chem II 2920 automatic chemical adsorption instrument. All catalysts were pretreated in an Ar and air mixture (v:v = 3:1) at 773k for 60 min and then cooled to 373 k in Ar flow and adsorbed NH₃ for 40 min. Then, the physically adsorbed NH₃ was removed in a continuous Ar flow for 90 min. The reactor temperature was then programmed to increase with a heating rate of 10°Cmin⁻¹ for 65 min, and the amount of desorbed NH₃ was detected by using a continuous effluent gas monitor with a thermal conductivity detector (TCD). After the IR spectra were recorded on a Magna 560 FT-IR analyzer, pyridine-adsorbed Fourier transform infrared measurements (Py-FTIR) was used to assess the acidity properties of all the samples by using pyridine as a probe molecule. Firstly, the sample was dehydrated for 3 h at 623 K under 10⁻² Pa vacuum. Second, to obtain the saturated adsorption of the Py-FTIR spectrum, pure pyridine vapor was added to the measured samples at room temperature for 30 min. Finally, the adsorbed pyridine was evacuated, respectively, at 523k and 623k for an hour so as to obtain the desorbed Py-FTIR spectra.

Catalyst Assessment

4,6-DMDBT was used as a probe to assess the HDS performances of SCal, Scam, and SCah catalysts. On the fixed-bed reactor whose length was 200 mm and inner diameter was 8 mm, 2.0 g of catalyst was loaded with a particle size of 20–40 meshes. In the first place, the pre-sulfidation of tested catalysts was carried out with 2.2 wt.% CS₂ cyclohexane solution at 330°C and 4 MPa with H_2 /oil (v/v) of 60 for 4 h. Then, the reactor temperature was allowed to drop to the temperature required for the reaction at the previous condition. Stabilization of the 4,6-DMDBT cyclohexane solution at a mass concentration of 1.0% was carried out for 4 h at 4.0 MPa and 270°C, 280, and 290°C, respectively. The H_2 /oil (v/v) was maintained at 120 when all catalysts were evaluated. The collected products of 4,6-DMDBT was determined by the GC–MS technique on an Agilent 4890D gas chromatograph

TABLE 1 | Pore structural properties of impregnated Ga-modified Ni-Mo/Al₂O₃.

Sample	S _{BET} , m ² ·g ⁻¹	V _{total} , cm ³ ⋅g ⁻¹	D, nm
NiMo-Al ₂ O ₃	214	0.51	9.5
SGal	218	0.46	6.8
SGam	227	0.45	7.9
SGah	221	0.41	7.5

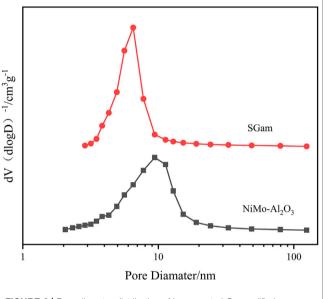


FIGURE 2 | Pore diameter distribution of impregnated Ga-modified Ni-Mo/Al₂O₃.

equipped with a 60 m capillary Rtx-1 column (0.25 mm, RESREK). The column temperature was increased from 50 to 300° C at a rate of 15° C min⁻¹, while the N₂ pressure was maintained at 0.3 MPa and the flow rate was 30 ml min⁻¹. The 4,6-DMDBT conversions and DDS route selectivity (3,3'-DMBP selectivity) were counted using the following equations, respectively:

4, 6 – DMDBT conversions
$$Con = (1 - m_{4,6-DMDBT}) \times 100\%$$
,

(3)

DDS Route selectivity $S_{DDS} = m_{3.3'-DMBP} / (1 - m_{4.6-DMDBT}) \times 100\%$,

DDS Route selectivity
$$S_{DDS} = m_{3,3'-DMBP}/(1 - m_{4,6-DMDBT}) \times 100\%,$$
(4)

where $m_{4,6\text{-}DMDBT}$ is the molar fraction of remaining 4,6-DMDBT and $m_{3,3'\text{-}DMBP}$ is the molar fraction of 3,3'-DMBP tested in the liquid products.

RESULTS AND DISCUSSION

Effect of Ga Modification on Crystalline Structure

The spectra of Ni-Mo/Al₂O₃ modified by the stepwise impregnation method with different Ga loadings determined by powder X-ray diffraction are shown in **Figure 1**. It can be

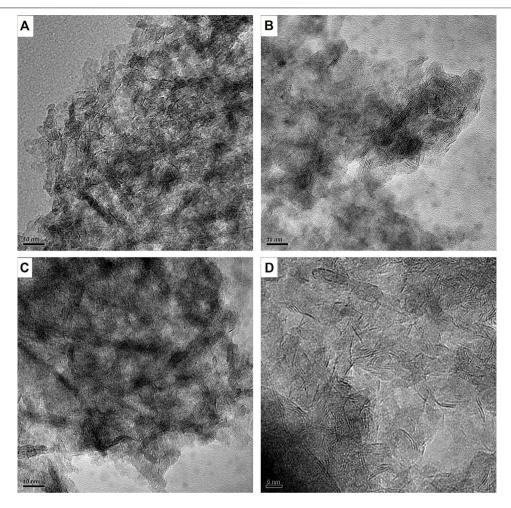


FIGURE 3 | HRTEM of sulfide-impregnated Ga-modified Ni-Mo/Al₂O₃: (A) Ni-Mo/Al₂O₃, (B) SGal, (C) SGam, and (D) SGah.

TABLE 2 | Average length and layer stacks of impregnated Ga-modified Ni–Mo/ Al_2O_3 .

Sample	¯L/nm	_ N	
NiMo-Al ₂ O ₃	2.7	1.1	
SGal	2.4	3.6	
SGam	3.1	3.4	
SGah	3.3	3.3	

seen from the diagrams the characteristic diffraction peaks (4.4.0), (4.0.0), and (3.1.1) of γ -Al₂O₃ are almost unchanged, which shows that the crystal structure of γ -Al₂O₃ is not affected. No characteristic peaks of Ga₂O₃ and other Ga compounds are found in **Figure 1**, which indicates that Ga₂O₃ was highly dispersed on Ni–Mo/Al₂O₃ and loaded well. However, diffraction peaks (0.2.2), (-3.1.2), and (2.2.0) of NiMoO₄ were observed, illustrating that the introduction of Ga₂O₃ brought about the agglomeration of Ni and Mo elements. In addition, the characteristic peak intensity of NiMoO₄ increased with the

increase in the content of Ga_2O_3 , which manifests that the introduction of excessive Ga_2O_3 is not conducive to the dispersion of Ni and Mo elements.

Effect of Ga Modification on Pore Structure

The method of N_2 physical adsorption–desorption was carried out to confirm the size of the specific surface area, average pore diameter, and pore volume of Ni–Mo/Al₂O₃, SGal, SGam, and SGah. The abovementioned textural properties are calculated and displayed about the four synthesized samples in **Table 1**, and the results of pore size distribution for two samples are recorded in **Figure 2**. From the data in **Table 1**, it is clearly found, especially for SGam, that the specific surface area increased from $214 \text{ m}^2 \text{ g}^{-1}$ to $227 \text{ m}^2 \text{ g}^{-1}$ with the addition of Ga_2O_3 in comparison with Ni–Mo/Al₂O₃, indicating that the introduced Ga_2O_3 had a wide distribution in the inner and outer surface of the catalyst; however, the pore volume and pore size decreased to some extent because parts of Ga_2O_3 blocked the pore channel of alumina. It can be seen from **Figure 2** that the pore size distribution curve moved to the direction of small pores, and

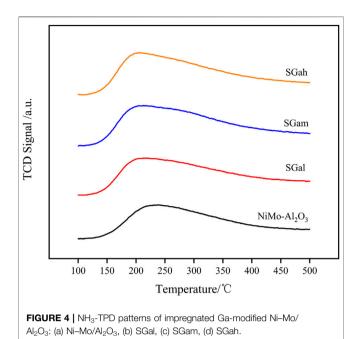


TABLE 3 | NH₃-TPD results of impregnated Ga-modified Ni-Mo/Al₂O₃,

Sample	Peak temperature/°C	Peak area
Ni-Mo/Al ₂ O ₃	237	1.085
SGal	210	1.423
SGam	207	1.386
SGah	205	1.275

TABLE 4 | Acidity properties of impregnated Ga-modified Ni-Mo/Al₂O₃,

Sample	Weak acid sites/µmol·g ⁻¹			Str	ong aci	id sites/µmol⋅g ⁻¹		
	В	L	B/L	B + L	В	L	B/L	B + L
Ni-Mo/Al ₂ O ₃	54	106	50.94	160	10	85	11.76	95
SGal	116	217	53.46	333	0	159	0	159
SGam	35	181	19.34	216	0	137	0	137
SGah	35	224	15.63	259	0	165	0	165

the peak area decreases slightly, which also proved that a large number of pores were blocked or even disappeared with the introduction of gallium.

Effect of Ga Modification on Morphological Characteristics

In order to observe the morphologies, characteristics, and dispersion about the sulfide active phase of Ni–Mo/Al₂O₃ and SGax (x stands for l, m, and h) catalysts, the images obtained by HRTEM characterization are shown in **Figure 3.** At least, 300 MoS₂ slabs of each catalyst were counted to statistically analyze the results of the average slab length and average stacking number of the active-phase slabs in **Table 2.** It can be clearly seen from

Table 2 that the introduction of Ga contributed to an increase in the average stacking number of MoS2 and its change rule kept pace with the increase in Ga loading. Especially, the largest increase of average stacking number for SGal is from 1.1 to 3.6 layers for Ni-Mo/Al₂O₃, which displays that the introduction of Ga weakened the Mo-O-Al bond energy and caused a weaker interaction between MoS₂ and the support, resulting in the formation of more type II Ni-Mo-S reactive phases with high stacking layers. In accordance with the abovementioned regulation, the variation of the average length also has a positive correlation with the Ga₂O₃ content. Also, the degrees of average length increase in the following order: SGal (2.4 nm) < $Ni-Mo/Al_2O_3$ (2.7 nm) <SGam (3.1 nm) <SGal (3.3 nm). The average length slightly increased from 2.7 nm for sample Ni-Mo/ Al₂O₃ to 3.3 nm for sample SGah. This can also be explained by the abovementioned data.

Effect of Ga Modification on Acidity Properties

Acidity plays a crucial role in the formation of the active phase and the HDS reaction, so NH3-TPD characterization of the series samples was carried out and is displayed in Figure 4. The peak temperature and peak area of the NH₃ desorption were calculated for each of the investigated samples and are summarized in Table 3. The NH₃-TPD profiles in Figure 4 reveal the peak temperature of the Ga-Ni-Mo/Al₂O₃ catalyst existed mainly between 150 and 300°C, indicating that the catalyst was mainly the prince of weak acid sites and medium-strong acid sites, which was weaker than that of the Ni-Mo/Al₂O₃ catalyst. It can be seen from Table 3 that the introduction of Ga made the NH₃ desorption peak shift to a lower temperature, manifesting that the weak acid sites of the catalyst mainly increased. According to the comparison of peak area, the number of acid sites of the Ni-Mo/Al₂O₃ catalyst was increased by introducing Ga₂O₃, but it was negatively correlated with introduced Ga₂O₃ content. Thus, the acid sites varied significantly for SGal. That phenomenon explained that the acid sites were covered by Ga₂O₃, leading to reduction in the degree of increase on the number of acid sites.

Effect of Ga Modification on Acid Types and Strength

It is well known that acid types and strength are the key points to decide the performance of the corresponding catalysts. As a consequence, pyridine desorption FTIR analyses were performed at different temperatures, and the results are listed in **Table 4**, where the specific data of weak and strong Brönsted acid sites (BAS) or Lewis acid sites (LAS) were derived from the information of pyridine desorption at 200 and 350°C, respectively. It can be clearly observed from **Table 4** that the introduction of 2 wt.% Ga_2O_3 enhanced the weak B-acid, and the B-acid enhancement facilitates the desulfurization of 4,6-DMDBT through the isomeric desulfurization pathway (ISOM). Moreover, after the isomerization of the methyl group on 4,6-DMDBT, the steric hindrance to sulfur atoms

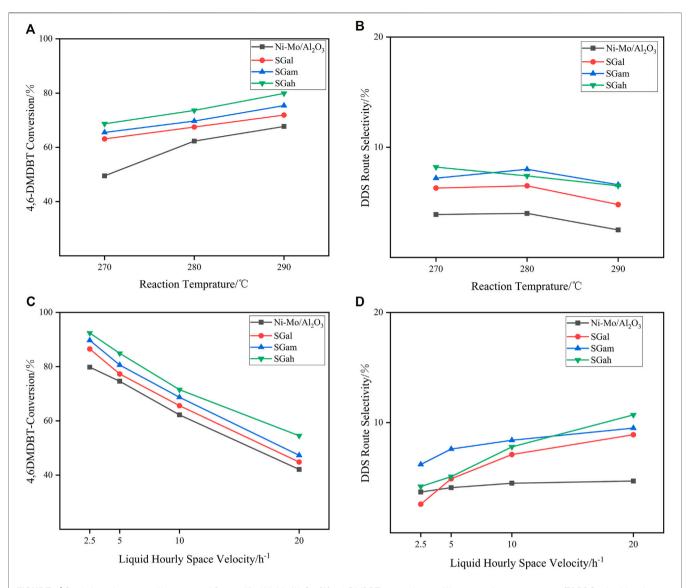


FIGURE 5 | Catalytic performance of impregnated Ga-modified Ni–Mo/Al₂O₃: (A) 4,6-DMDBT conversion on different reaction temperatures, (B) DDS selectivity of 4,6-DMDBT on different reaction temperatures, (C) 4,6-DMDBT conversion on different LHSVs at 280°C, and (D) DDS selectivity of 4,6-DMDBT conversion on different LHSVs at 280°C.

decreased significantly, which provided access to direct desulphurization just by hydrogenolysis of sulfur atoms, and the path to remove sulfur was considered to be very ideal. In addition, the introduction of different contents of Ga increased the Lewis acid, among which the weak Lewis acid increased more and the strong Brönsted acid decreased slightly. This is consistent with the characterization of NH₃-TPD. Except for the enhancement of weak Brönsted acid by SGam, the amount of Ga₂O₃ introduced had little effect on the acid type and amount of Brönsted acid and Lewis acid of Ni–Mo/Al₂O₃, but the amount of Ga₂O₃ introduced increased the total acid amount.

Assessment of Catalytic Activities

As is concretely confirmed, though the appropriate content of Ga₂O₃ modification can effectively improve the physicochemical properties of the catalysts from the characterization results mentioned above, the favorable conditions for conversion and selectivity at different temperatures need to be explored. Thus, 4,6-DMDBT served as the probe molecules in the assessment of the HDS performance of Ni-Mo/Al₂O₃ and SGax series catalysts on a fixed-bed reactor under a total pressure of 4 MPa and the liquid hourly space velocities (LHSVs) of 2.5 h⁻¹ at different reaction temperatures (in the range of 270-290°C). The variation of conversions on 4,6-DMDBT at different temperatures is clearly displayed in Figure 5A, suggesting that the activities of all the investigated catalysts increased with the increase in the reaction temperature. These results also pointed out that there was no significant disparity in the conversion of SGax series catalysts with different Ga₂O₃ loadings, and the highest conversion rate was obtained when the Ga₂O₃ loading was 2 wt.%. In addition, with the increase in reaction temperature, the difference of conversion rate between SGax series catalysts and the Ni-Mo/Al₂O₃ catalyst became smaller, which resulted from the increase in the conversion rate of 4,6-DMDBT at high temperature close to the reaction end point.

Scheme 1 shows the HDY and DDS reaction route over Ga-Ni-Mo/Al₂O₃ catalysts separately. HYD desulfurization is a tedious step to form the products 3,3'dimethylcyclohexanebenzene (3,3'-DMCHB) dimethylbicyclohexyl (3,3'-DMBCH), while DDS pathway desulfurization is achieved with fewer steps and without excess aromatic rings and produces 3,3'-dimethylbiphenyl (3,3'-DMBP). The DDS route selectivity over different catalysts at the same conditions mentioned above was obtained, and the results are shown in Figure 5B. It can be observed from Figure 5B that, with the increase in reaction temperature, the DDS selectivity of the tested catalysts on the DMDBT decreased, owing to that Ni gradually began to be reduced as the reaction temperature exceeded 290°C. Especially, the metal Ni has a strong hydrogenation performance. The reason mentioned above led to the enhancement of the HYD path. In addition, it was also found that if the reaction temperature is higher than 290°C, the high hydrogenation performance of Ni can even convert a small amount of DDS products into HYD products, but it was generally considered that this reaction will not occur, which was the unique characteristic of Ni-containing hydrotreating catalysts. Further increase in temperature would lead to a profound increase in the proportion of hydrogenation

conversion of DDS products to HYD products. In order to properly deal with this situation, the metal promoter can be replaced with the load of Co with low hydrogenation performance, and the amount of the Ni loading or the Ni/Mo atomic ratio ought to be reduced.

The influence of different LHSVs in the investigated series catalysts on the 4,6-DMDBT HDS reaction is shown in **Figure 5C**. As can be clearly noticed from the figure, with the decrease in LHSVs which meant increasing the residence time of raw materials, the conversion rate of 4,6-DMDBT increased gradually and over the tested catalysts was in the order of Ni–Mo/Al $_2$ O $_3$ <SGah < SGam < SGah. When the LHSV decreased gradually, the increasing rate of conversion rates slowed down gradually as the reaction is close to complete conversion. Thus, the conversion rate gap between different Ga $_2$ O $_3$ loading catalysts was bridged.

Figure 5D reveals the transformation about selectivity of DDS route by stepwise impregnation of the Ga-Ni-Mo/Al₂O₃ catalyst with different LHSVs on 4,6-DMDBT at a reaction temperature of 280°C. As it is vividly shown in Figure 5D, the galliummodified catalysts exhibited higher DDS route selectivity than the Ni-Mo/Al₂O₃ catalyst at high LHSV. However, the DDS route selectivity of SGax series catalysts for 4,6-DMDBT exhibited a negative correlation with the variation of LHSV. With the decrease in LHSV, the DDS selectivity of SGax series catalysts for 4,6-DMDBT even decreased to about the corresponding selectivity of the Ni-Mo/Al₂O₃ catalyst. On the one hand, the incorporation of Ga improved the average stacking number of the active-phase slabs and generated more type II NiMoS active phases which weekly interact with the support or do not interact with the support at all, and it is considered to be very active (Nikulshin et al., 2014; van Haandel et al., 2015), so that the HYD route got strengthened. On the other hand, the residence time of raw materials became longer while the LHSV decreased, which is beneficial to the HYD route with longer reaction path and slower reaction rate. In addition, because of the strong hydrogenation ability of the reduced metal Ni, a small part of DDS products was also transformed into HYD products. All mentioned above were identified as the reason for which the variation of LHSV had impact on the DDS route selectivity.

CONCLUSION

The experiments showed that the introduction of Ga_2O_3 with appropriate content (2 wt.%) promoted not only Ni and Mo species to disperse uniformly but also doping of more Ni atoms into the MoS_2 crystals. In addition, the average stacking number and the length of Mo_2S were increased. Those mentioned above resulted in the formation of more NiMoS active phases. The specific surface area and the amount of acid sites were increased, facilitating the adsorption of reactant molecules and the hydrodesulfurization reactions. Last but not the least, the catalyst $Ga-Ni-Mo/Al_2O_3$ exhibited the highest conversion rate towards 4,6-DMDBT HDS when the amount of Ga_2O_3 loading was 2 wt.% with an LHSV of 2.5 h^{-1} at 290°C, and Ga modification also can effectively improve the DDS route selectivity in varying degrees.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/**Supplementary Material**, further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

MH designed experimental plans, performed the main experimental work, analyzed and discussed the results and wrote the manuscript. WH assisted in the design of the scheme and performed the main experimental work. AL participated in manuscript writing. QW proposed the themes, ideas, and content of the research work. YJ, HY, ZY, XW and ZX

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Effect of Borax On Sintering Kinetics, Microstructure and Mechanical Properties of Porous Glass-Ceramics From Coal Fly Ash by Direct Overfiring

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The direct sintering process of coal fly ash for the preparation of glass-ceramics is the liquid-phase sintering process, from non-densification to densification. When the temperature exceeds the densification temperature point, the porosity of glassceramics on the contrary increases and the pore diameter increases. This provides a basis to prepare porous glass-ceramics by direct overfiring. Adding borax to coal fly ash can reduce the temperature of liquid phase formation, reduce the preparing temperature of porous glass-ceramics, achieve the purpose of energy saving. The effects of borax on the structure, properties and sintering kinetics of porous glass-ceramics prepared from coal fly ash by overfiring were investigated. It is found that the introduction of B-O bond can change the network structure of noncrystalline vitreous in coal fly ash, reduce the melting temperature, promote the formation of liquid phase, and thus increase the porosity of porous glassceramics. This paper provides a certain experimental basis for the preparation of porous glass-ceramics by direct overfiring of coal fly ash at low temperature without adding pore-forming agent, and provides a new possibility for the high-value resource utilization of coal fly ash.

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INTRODUCTION

Porous glass-ceramics is a new kind of material which distributes a large number of microcrystalline phases and pores evenly in glass phase based on glass-ceramics. Porous glass-ceramics has been widely used as insulation materials for energy-saving building walls and thermal pipelines due to its large specific surface area, better thermal stability, lower thermal conductivity and higher mechanical strength (Flesoura et al., 2021; Yio et al., 2021). At present, the preparation methods of porous glass-ceramics mainly include crystallization-acid leaching (Wang et al., 2003a; Wang et al., 2003b; Chen et al., 2020), melting sintering with pore-making agent (Ding, et al., 2015; Jiang et al., 2017), direct sintering with pore-making agent (Bernardo and Albertini, 2006; Chen et al., 2016; Hisham et al., 2020; Yio et al., 2021). Among them, the preparation methods of porous glass-ceramic with coal fly ash as raw material are mainly the melting sintering method with adding pore-making agent and the direct sintering method with adding pore-making agent.

The melting sintering method with adding pore-making agent is to add pore-making agent to the basic glass. In the sintering process, pore-making agent through oxidation or release gas to

form pores to prepare porous glass-ceramics. The preparation process is similar to that of preparing glass-ceramics by melting and sintering, which includes batching, melting, water quenching, drying, crushing, sieving, forming, nucleation, crystallization and pore forming (Zhu et al., 2012). As environmental protection is deeply rooted in people's mind, people put forward new requirements for resource utilization (Zeng et al., 2021). In order to save energy consumption and simplify the preparation process, the porous glass-ceramics was prepared by adding poremaking agent in the direct sintering process (Bai et al., 2014; Li et al., 2018; Zhu et al., 2016). No matter which method is used to prepare porous glass ceramics, the type and quantity of pore-forming agent are important indicators affecting the porous glass ceramics (Fernandes et al., 2009; Hou et al., 2017; Wang et al., 2018; Fernandes et al., 2020). The key of pore-making agent selection is that the pore-making temperature should be consistent with the softening temperature of the raw material (Wu et al., 2006). However, the composition and properties of coal fly ash from different producing areas vary greatly. Therefore, it is difficult to select the appropriate type and amount of foaming agent according to its softening temperature point.

Dong et al. found that coal fly ash would self-expansion in the high-temperature sintering process, that is, crystals would be precipitated from the molten liquid to form pores in the high-temperature process (Dong et al., 2008; Dong et al., 2009). Moreover, in the previous experiments, it was found that, the process of sintering is actually the transformation of open pore porosity between particles and particles in the sample into closed pore porosity. In this process, there is an optimal temperature point for densification. Once the temperature point is exceeded, the samples will be overfiring and more molten liquid will be formed. With sufficient viscous flow, small pores will be merged to form large pores, and more crystals will be precipitated from the molten liquid, and the total porosity will gradually increase (Zeng et al., 2020; Zheng et al., 2020). This provides a basis for direct overfiring of porous glass-ceramics. However, preliminary experimental results show that the overfiring temperature of coal fly ash reaches about 1,190°C (Zeng et al., 2019). In order to reduce the temperature of porous glass ceramics prepared by overfiring, a fluxing agent must be added. Borax is widely used as a flux in the preparation of porous glass ceramics, it can reduce the temperature of liquid phase formation (Chen et al., 2013; Guo et al., 2014; Yio et al., 2021). In this experiment, borax was added to reduce the temperature of preparing porous glass-ceramics prepared by overfiring method, so as to achieve the purpose of energy saving and consumption reduction.

The purpose of this paper is to discuss the effect of borax on the morphology, performance and sintering kinetics of the coal fly ash porous glass-ceramics prepared by overfiring, so as to achieve the purpose of preparing porous glass-ceramics without adding pore-making agent at low temperature, and to provide a new way for the high-value utilization of coal fly ash.

EXPERIMENTAL PROCEDURE

Raw Materials and Experimental Equipment

Raw materials, the coal fly ash used in the experiment came from a coal-fired power plant in Jiangyou, Sichuan, the pure polyvinyl alcohol (PVA) and borax were purchased from Chengdu Kelon Chemical Co., LTD. The chemical composition analysis and phase composition of coal fly ash are shown in **Table 1** and **Figure 1** respectively. The main constituents of coal fly ash are alumina and silicon oxide, accompanied by a small amount of calcium oxide and iron oxide. The phase composition is mainly the amorphous silicate vitreous represented by the uplift steamed bread peak, crystalline mullite (PDF#00-002-0430,3Al₂O₃.2SiO₂), quartz (PDF#00-033-1161, SiO₂) and hematite (PDF#00-024-0072,Fe₂O₃) (Lin et al., 2015).

Experimental equipment, 769YP-24B infrared powder tablet press (Xi 'an minsks testing equipment Co. Ltd., China), KSY-25-16-8X2-20-13 box type resistance furnace (Shanghai shiyan electric furnace, Co. Ltd., China), 305F-2 microcomputer control electronic pressure testing machine (Shenzhen wance testing machine Co. Ltd., China), WT5003GHS hydrostatic balance (Changzhou Wantai Balance Instrument Co. LTD.), XPM- Φ 100 \times 4 planetary four-cylinder grinding machine (Wuhan prospecting machinery Factory).

Preparation of Porous Glass-Ceramics

The specific process of preparing porous glass-ceramics by direct overfiring with borax is shown below. Borax ($Na_2B_4O_7$ $10H_2O$) and coal fly ash were mixed evenly according to mass ratios of 10: 90, 15:85, 20:80, 25:75 and 30:70 (denoted as 10B-90F, 15B-85F, 20B-80F, 25B-75F, 30B-70F) for 5 min by ball grinding. PVA was used as the binder for granulation. The samples were sintered in a box type resistance furnace at different temperatures (800-1100°C) for 60 min after tablet forming. After cooling down, the samples were taken out for phase, morphology and corresponding performance test and characterization. The sample was labeled as 10B-90F, 15B-85F, 20B-80F, 25B-75F, 30B-70F sintering temperature.

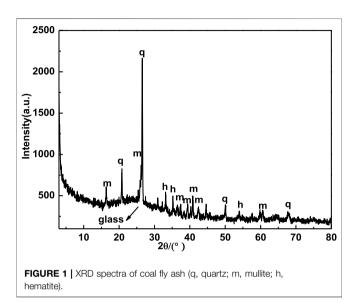
Characterization

The phase composition of the raw material and the samples were analyzed by the X-ray diffractometer (XRD) of PANalytical B.V. (20 range 3–80°, step 0.03°). The chemical composition of raw materials was analyzed by X-ray fluorescence (XRF) of PANalytical B.V. (Rh target, maximum power 2.4 kW). The morphology of porous glass-ceramics was characterized by DV230E3FL optical microscope and the pore size distribution was measured by "Nano Measurer" size statistics software. The three-point bending strength of $5 \times 10 \times 60 \text{ mm}^3$ samples was tested at the speed of 0.05 mm min⁻¹, and the average value was taken three times for each test. The true density (ρ_t) and bulk density (ρ_b) were measured by the gas (A_r) pycnometer and Archimedes method, respectively. The porosity (P) can be calculated by Eq. 1 (Bai et al., 2014).

$$P = \left(1 - \frac{\rho_b}{\rho_t}\right) \times 100\% \tag{1}$$

TABLE 1 | Chemical compositions of coal fly ash powder.

Composition	SiO ₂	Al ₂ O ₃	CaO	Fe ₂ O ₃	K ₂ O	SO ₃	TiO ₂	Na ₂ O
wt%	53.31	26.55	5.88	4.41	2.42	1.42	1.06	0.60
Composition wt%	MgO 0.52	P ₂ O ₅ 0.47	BaO 0.10	MnO 0.03	ZrO ₂ 0.03	ZnO 0.02	Other 0.16	LOI 3.02



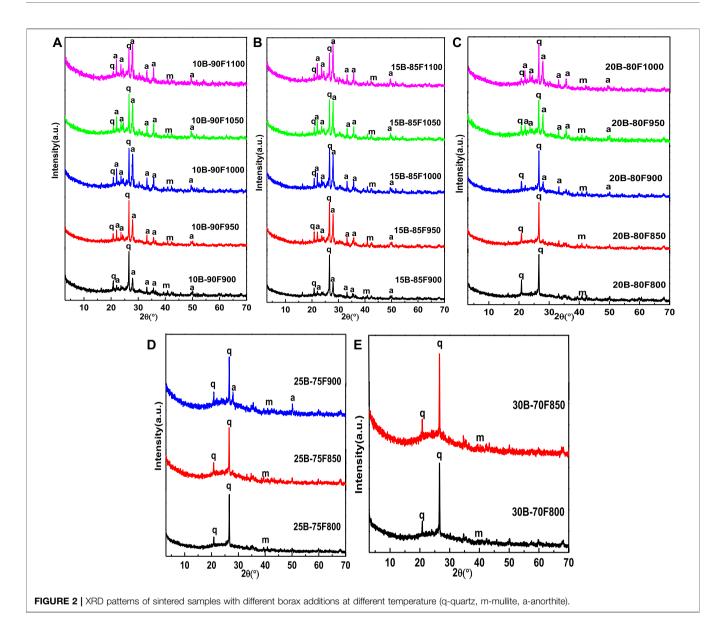
RESULTS AND DISCUSSION

Phase and Microstructural Evolution

Figure 2 shows the XRD patterns of samples sintered at different temperatures with different borax additions. It can be seen from the figure that the addition amount of borax has a great influence on the phase of porous glass-ceramics. When the amount of borax is small (10B-90F, 15B-85F), the phase of the porous glassceramics are the same as the glass-ceramics prepared without borax, they all composed of anorthite, quartz and mullite (Zeng et al., 2019). Without borax, anorthite is precipitated from molten quartz and amorphous vitreous at a temperature of 1,000°C (Zeng et al., 2019). When the amount of borax is 10% and 15%, the temperature of anorthite precipitated reduced to 900°C. Indicating that borax will react with the oxides in coal fly ash to reduce the melting temperature of quartz and amorphous vitreous in coal fly ash, so that the molten liquid phase is formed at a lower temperature, and anorthite precipitated (Chen et al., 2013). By comparing the peak strength ratio of anorthite (I_{204}) and quartz (I₁₀₁) between 10B-90F1000 and 15B-85F1000 at 1,000°C, it is found that the ratio increases from 0.87 of 10B-90F1000 to 0.91 of 15B-85F1000. Meaning that borax can reduce the melting temperature of quartz and amorphous vitreous, and increase the amount of anorthite precipitated from the molten liquid. By comparing the critical temperature point of collapse of porous structure of porous glass-ceramics (10B-90F is 1,100°C, 15B-85F is 1,100°C, 20B-80F is 1,000°C, 25B-75F is 900°C), it is found that with the increase of borax addition, the critical temperature point of collapse of porous structure decreases

gradually. In addition, by comparing the peak strength ratio of anorthite (I_{204}) and quartz (I_{101}) at the critical temperature point, it was found that the ratio increased from 1.12 in 10B-90F1100 to 1.32 in 15B-85F1100, and then decreased to 0.68 in 20B-80F1000 and 0.47 in 25B-75F900. The reason may be that, at the low amount of borax (10B-90F, 15B-85F), due to the higher critical temperature point of porous structure collapse (1,100, 1,100°C), the addition of borax can simultaneously reduce the melting temperature point of quartz and amorphous vitreous in coal fly ash to form liquid phase, precipitation of more anorthite. With the addition of borax (20B-80F, 25B-75F), the collapse temperature of porous structure reduced (1,000, 900°C). At this temperature, the addition of borax can only reduce the melting temperature of non-crystalline vitreous body in coal fly ash, cannot promote the melting of quartz in coal fly ash. Therefore, the content of precipitated anorthite is lower than that of 10B-90F and 15B-85F. Continue to increase the amount of borax (30B-70F), no anorthite was observed before the pore structure of porous glass-ceramics collapsed (850°C), meaning the glass liquid phase is formed by the melting of borax. This is also the reason why borax is not detected in XRD (Chen et al., 2012). Under the proper temperature, the B-O bond with low binding energy in borax can changes the network structure of quartz and amorphous vitreous in coal fly ash to form liquid phase (Chen et al., 2012). Therefore, the sintering temperature also plays an important role in the liquid phase formation of porous glass-ceramics.

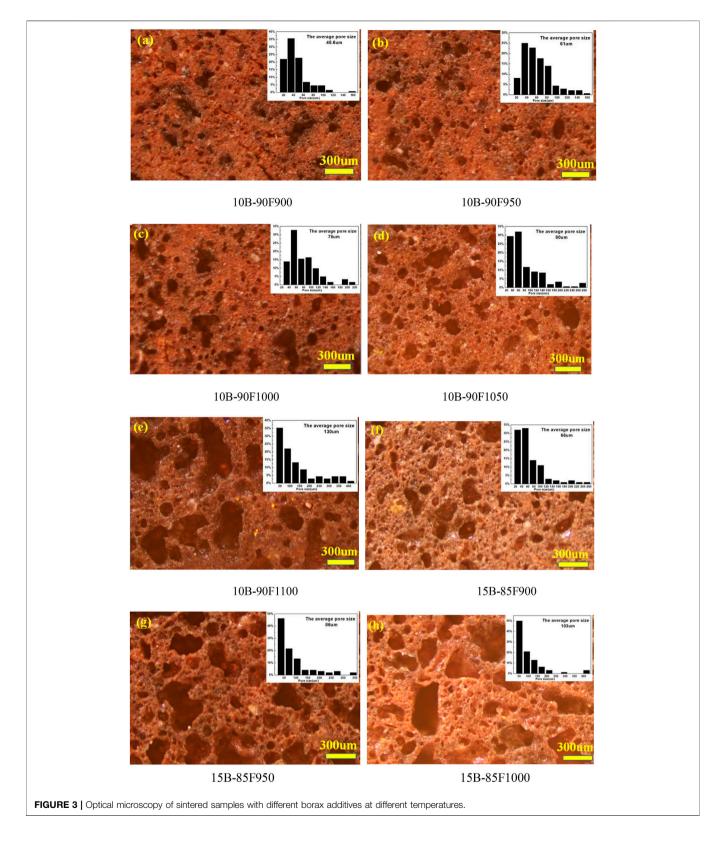
Figure 3 shows the influence of sintering temperature on the morphology and pore size distribution of porous glass-ceramics under different borax additions. Figures 3A-E shows the change of the morphology of the sample with temperature when borax is added at 10%. The average pore size increased from 46 µm in 10B-90F900 to 130 µm in 10B-90F1100, and the distribution of pore size increased from 20–160 μm in 10B-90F900 to 20–430 μm in 10B-90F1100. Figures 3F-J is the morphology and pore diameter distribution of the samples at 900-1,100°C when the addition amount of borax is 15%. By comparing Figures 3A-J, the average pore diameter and pore diameter range of the samples increase with the addition of borax at the same temperature. For example, the average aperture of 10B-90F1000 is 78 µm, the aperture range is 20-220 µm, the average aperture of 15B-85F1000 increases to 103 μm, and the aperture range is 20-400 μm. On one hand, the increase of borax provides more molten liquid, which reduces the viscosity, promotes the formation of pores and the merging of small pores. On the other hand, the introduction of borax destroyed the quartz and amorphous glass structure of coal fly ash (Zeng et al., 2019), reduced its melting temperature, and formed more liquid phase to promote the formation of pores. The anorthite



precipitated from the molten liquid phase. Therefore, the results are consistent with **Figures 2A,B**, at the same temperature, the amount of anorthite in the sample with the borax additive amount of 15% was higher than that of 10%.

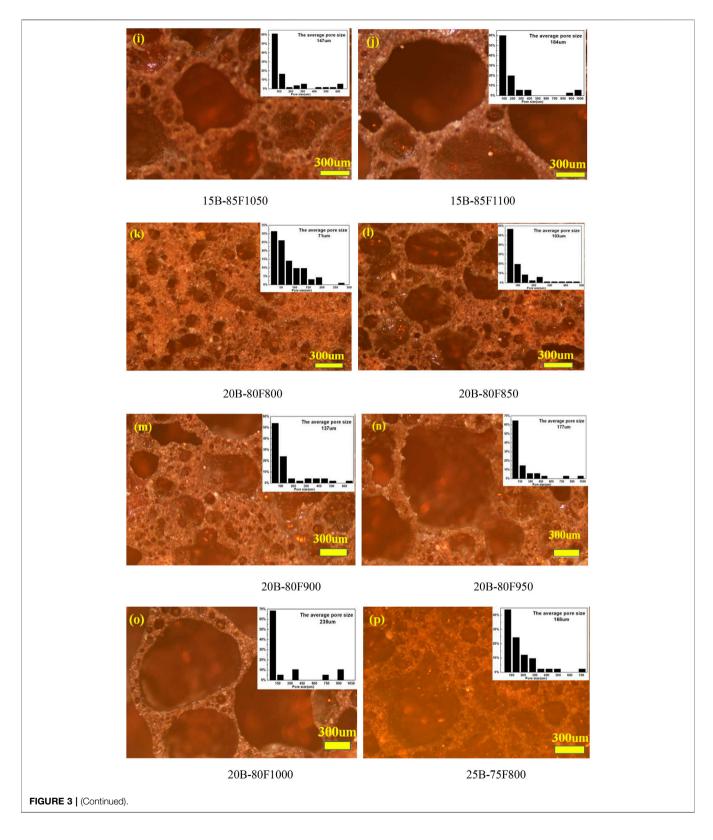
The micromorphology and pore size distribution of the porous samples were shown in **Figures 3K–R**, when the addition amount of borax was 20% and 25%, respectively. It can be seen from the figure that no matter how much borax is added, the average diameter and diameter distribution of the samples increase with the increase of temperature. For example, the average particle size of 20B-80F800 is 71 μ m, and the particle size distribution range is 20–280 μ m. When the temperature increases to 900°C, the average particle size of 20B-80F900 is 137 μ m, and the particle size distribution range is 20–600 μ m. As another example, the average particle size of 25B-80F800 is 168 μ m, the particle size distribution range is 20-700 μ m. The average particle size of 25B-80F850 is 224 μ m and the particle size distribution range is

20-800 μm when the temperature increases to 850°C. Interestingly, the average aperture of the 20B-80F1000 is 238 µm and the aperture range is 50-1,000 µm, while the average aperture of the 25B-75F900 is 240 µm and the aperture range is $50-1000 \, \mu m$. It means that the two have the same liquid phase and the same viscosity at different temperatures and different borax addition. By comparing Figures 2C,D, the content of anorthite in 20B-80F1000 is higher than in 25B-75F900, indicating that more liquid phase is provided by coal fly ash in 20B-80F1000, so more anorthite is precipitated out. More liquid phase is provided by borax in 25B-75F900, means increase the amount of borax can decrease the sintering temperature of porous glass-ceramics. So, to obtain porous samples with the same pore size and pore size distribution, borax can be added or sintering temperature can be increased. Figures 3S,T show the micromorphology and pore diameter distribution of 30B-70F800 and 30B-70F850. In combination



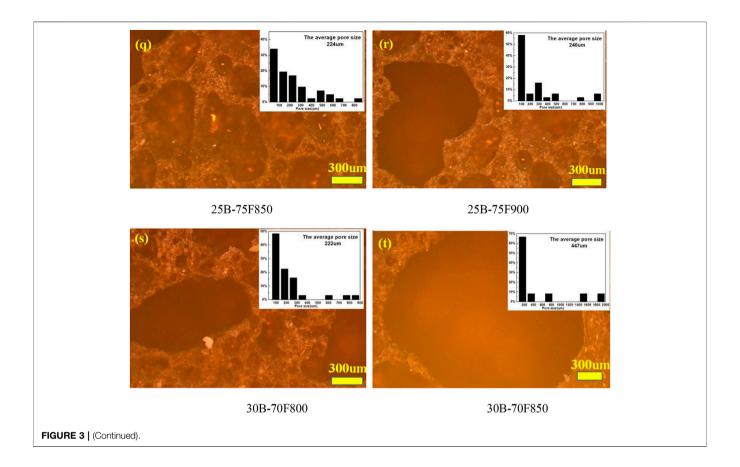
with **Figure 2E**, no anorthite was observed in the sample when the borax addition amount was 30%. Due to the addition amount of borax is large, borax has been completely melted and form a

liquid phase to promote the formation of pores before destroy the quartz and amorphous glass structure in coal fly ash. The average pore size of the sample at 850°C has reached $447\,\mu\text{m}.$ In



conclusion, the addition of borax can increase the high temperature liquid phase, reduce the viscosity and promote the formation of pores. At the same time, it can increase the

average pore size and pore size distribution range of porous glass-ceramics, reduce the sintering temperature of porous glass-ceramics, reduce energy consumption.

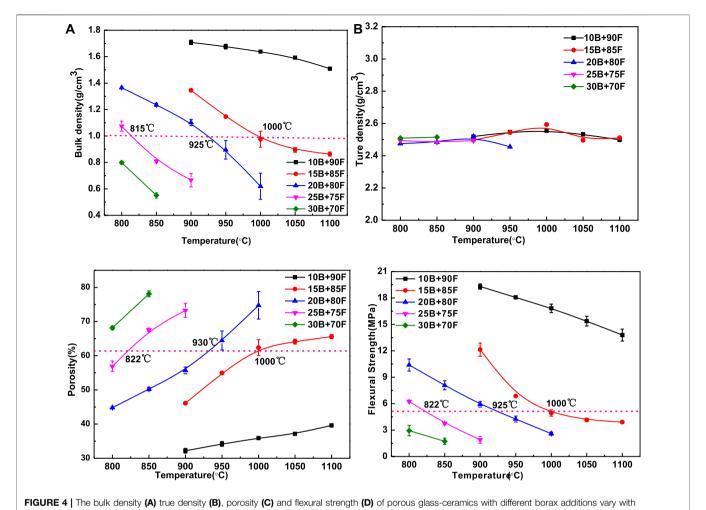


Properties

Figure 4 shows the effect of borax addition amount on the performance of porous glass-ceramics, in which 4(1) is bulk density, 2) is true density, 3) is porosity, and 4) is flexural strength. Obviously, the amount of borax has great influence on the bulk density, porosity and flexural strength of porous glassceramics, but has little effect on its true density. The main reason is that the true density is not affected by the porosity, but related to the phase. As can be seen from Figure 2, although the phases contained in porous glass-ceramics are different, the difference in true density between phases is small, so the addition of borax amount has little impact on the true density of porous glass-ceramics (Figure 4B). The bulk density and porosity of porous glass-ceramics are closely related to the viscosity of vitreous. With the increase of borax addition and temperature, the viscosity of vitreous decreases gradually, porosity increases gradually, and bulk density decreases gradually (Figures 4A,C). The similar average particle size and the same particle size distribution of 20B-80F1000 and 25B-75F900 in Figures 3O-R, meaning that the viscosity of the two high-temperature liquid phases is basically the same. It can be seen that the addition amount of borax and sintering temperature have a great influence on the viscosity of high temperature liquid phase in the preparation process of porous glass-ceramics. Similarly, using the bulk density of 1.0 g/cm³ as the ordinate plot in Figure 4A, showing that in order to get the bulk density of 1.0 g/cm³

porous glass-ceramics, relatively low sintering temperature of 815°C but high borax content 25% can be used, or a moderate sintering temperature of 925°C and moderate borax content 20% can be selected, or a relatively high temperature of 1,000°C and relative lower borax content 15% can be used. The same trend can be seen in **Figure 4C**. The porosity of porous glass-ceramics sintered at 1,000°C and with borax addition of 15% is the same as that sintered at 925°C and with borax addition of 20%, sintered at 815°C and with borax addition of 25%. It means that the sintering temperature and the amount of borax can adjust the viscosity of the high temperature liquid phase, which has a great influence on the bulk density and porosity of porous glass-ceramics.

The flexural strength of porous glass-ceramics depends on its bulk density and porosity. The larger the bulk density is, the greater the flexural strength is, and the greater the porosity is, the smaller the flexural strength is (Bernardo et al., 2010). It can be seen from **Figure 4D** that, on the whole, with the increase of temperature and borax addition, the flexural strength decreases. As can be seen from the dotted line in **Figure 4D**, when the sintering temperature is 822, 925 and 1,000°C, the amount of borax added is 25%, 20% and 15%, the porous glass-ceramics has the same flexural strength. It means that the flexural strength of porous glass-ceramics is actually affected by the viscosity of high-temperature liquid. Therefore, in the practical application process, the viscosity of high temperature liquid can be adjusted by adjusting the



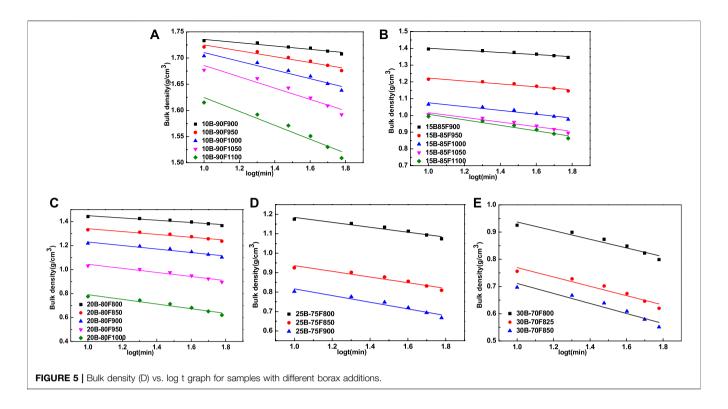
temperature.

TABLE 2 | Comparison of properties of porous materials prepared from coal fly ash.

Samples	Raw material	Porosity (%)	Flexural strength (MPa)	Bulk density (g/cm³)	Compressive strength (MPa)	References
Foam glass ceramic	30% HAFA, 50% Waste glass, 15% clay and 5% Feldspar (2% CaSO ₄)	_	-	0.98	9.84	Wang et al., 2018
Porous glass- ceramics	55% solid (fly ash:glass-1:1), 27% water glass, 18% dolapix CE 64 (Using polyurethane foam as pore creators)	70	4.5	_	_	Bossert et al., 2004
Foam glass	14.75% fly ash and 84.75% waste glass (0.5% SiC)	81.55	-	0.2672	0.9829	Bai et al. (2014)
Foam glass	50-70% fly ash, 5% Na_2HPO_4 , 22.5-37.5% $Na_2B_4O_7$ and 7.5-12.5% $CaCO_3$	52-66.1	1.95-2.59	0.591- 0.876	2.09-3.95	Chen et al
Foam glass	20% fly ash and 80% glass (1-5% carbonates)	_	_	0.36-0.41	2.40-2.80	Femandes et al., 2009
Foam ceramics	26.25–40% fly ash, 40–50% red mud, 15–20% sodium borate and 5% sodium silicate	64.14- 74.15	2.31-8.52	0.51-0.64	4.04-10.63	Chen et al., 2013
Porous glass- ceramics	70-90% coal fly ash and 10-30% borax	32.2-78.1	1.72-19.29	0.55-1.71	_	This paper

sintering temperature or borax addition, so as to adjust the bulk density, porosity and flexural strength of porous glass-ceramics.

Table 2 compares the properties of porous materials prepared from coal fly ash. After comparison, the amount of coal fly ash used in this experiment is relatively high, ranging from 70% to



90%, with a wide range of porosity, bulk density and flexural strength. The porous materials prepared in this experiment can be adjusted according to their properties of porosity, bulk density and flexural strength. More importantly, the porous materials prepared in this experiment without the pore forming agent, and there was no problem in choosing the amount of the type of pore forming agent.

Sintering Kinetics

According to Kingery's liquid-phase sintering theory, liquidphase sintering can be divided into three stages: with the increase of sintering temperature, a large number of liquid phase appeared, and the solid particles precipitated from the liquid phase moved and rearranged under the action of capillary force; further rearrangement of grain creep; through liquid phase mass transfer, the grain size and grain shape change constantly, and the rearrangement achieves densification (Luo et al., 2019). In previous experiment, it was found that rise temperature after the sample was densified, the small pores originally existing in the sintered sample would be merged into large pores to form porous structure due to the effect of mass transfer in liquid phase (Zeng et al., 2020). The formation temperature of porous glass-ceramics is between overfiring and softening of the sample, so the sintering activation energy cannot be calculated by the shrinkage rate of the sample with temperature. With the progress of sintering, the porosity of the sample increases and the bulk density decreases. The dynamic empirical formula of ceramic sintering can be used to calculate the activation energy of porous glass-ceramics (Eq 2, 3).

$$D = Klogt + C \tag{2}$$

$$K = Aexp\left(-\frac{Q}{RT}\right) \tag{3}$$

Where, D is the bulk density, C is the characteristic constant of powder, K is the reaction rate constant, T is the sintering time, Q is the sintering activation energy, R is the gas constant, T is the absolute temperature, and A is the constant (Demirkiran et al., 2008; Yürüyen and Toplan, 2009).

Figure 5 is the curve of the logarithm of the bulk density and sintering time of porous glass-ceramics prepared with different borax additions. The bulk density of porous glass-ceramics is linearly correlated with the logarithm of sintering time, which conforms to the dynamic empirical formula of ceramic sintering (2). The relationship between ln (-k) and 1/T was plotted using the reaction rate constant K and sintering temperature T, as shown in Figure 6. According to Arrhenius formula, the sintering activation energy of porous glass-ceramics prepared by different borax additives was calculated, as shown in Table 3. As can be seen from the correlation factor in Table 3, the correlation factor is close to 1, indicating that ln (-k) has a good correlation with 1/T, and Arrhenius formula can be used to calculate the sintering activation energy. The sintering activation energy of porous glass-ceramics decreases with the increase of borax content, from 95.30 kJ/mol to 29.49 kJ/mol. Obviously, more borax is added, lower sintering activation energy is. On the one hand, the addition of borax provides more liquid phase to facilitate liquid phase sintering. On the other hand, the addition of borax provides B-O bond to change the network structure of non-crystalline vitreous of coal fly ash, to reduce its melting temperature, and promote liquid phase sintering.

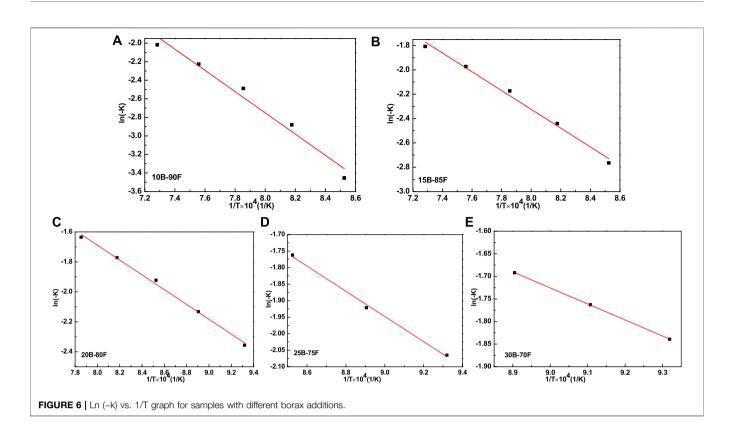


TABLE 3 | Activation energy of sintering samples with different borax additions.

Samples	Borax content (%)	Correlation factor (r)	-Q/R	Activation energy Q (kJ/mol)
10B-10F	10	0.98	11,462.50	95.30
15B-85F	15	0.99	7,715.40	64.15
20B-80F	20	0.99	4,944.10	41.11
25B-75F	25	0.99	3,809.70	31.67
30B-70F	30	0.99	3,547.00	29.49

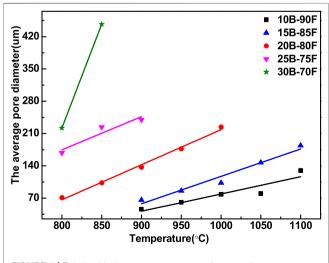


FIGURE 7 | Relationship between average pore diameter of porous galss-ceramics with different borax additions and temperature.

Figure 7 shows the relationship between the average pore diameter and temperature of porous glass-ceramics prepared with different borax additions. With the increase of temperature and borax, the average pore size of porous glass-ceramics increased gradually. It can be seen from the figure that the average aperture has a good linear correlation with the temperature. With the increase of borax addition, the slope of the related line gradually increases. The more borax is added, the more B-O bonds are provided, the more liquid phase is provided, the easier sintering is, and the greater change of average pore diameter is. In other words, with the increase of borax addition, the mass transfer in liquid phase is more obvious, and the process of forming large pores is more affected by temperature. The sintering process of porous glass-ceramics by overfiring can be regarded as the fourth stage after the third stage of glass-ceramics, which is caused by mass transfer in liquid phase and the formation of large pores.

CONCLUSION

In this experiment, the porous glass-ceramics was directly overfired from coal fly ash and borax at low temperature without pore-forming agent. It provides a new possibility for preparing porous glass-ceramics with low energy consumption and high utilization of coal fly ash. The addition of borax has great influence on the phase, morphology and properties of porous glass-ceramics. B-O bond in borax can destroy the structure of quartz and amorphous vitreous body in coal fly ash, reduce its melting temperature and increase the high-temperature liquid phase, thus increasing the content of anorthite. With the increase of borax content from 10% to 15%, the anorthite content in porous glass-ceramics also increases gradually. When the amount of borax increases to 15% and the sintering temperature is 1,100°C (15B-85F1100), the content of anorthite reaches the maximum. Then, with the increase of borax addition, the content of anorthite further decreased. When borax addition was 30% and sintering temperature was 850°C (30B-70F850), the content of anorthite decreased to zero. It shows that although borax can destroy the structure of quartz and amorphous vitreous in coal fly ash to precipitate anorthite, the role of sintering temperature in the preparation of porous glass-ceramics cannot be ignored. The larger the borax addition is, the larger average pore size and porosity of porous glass-ceramics are, the smaller the bulk density and the flexural strength are. The properties of porous glass ceramic can be adjusted by adjusting the sintering temperature or the amount of borax.

The dynamic process of direct overfiring for the preparation of porous glass-ceramics extends to the fourth stage after the

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three-stage theory of liquid phase sintering. That is, with the increase of temperature, the small pores remaining in the compact stage are merged into large pores due to the mass transfer effect of liquid phase. With the increase of borax, the sintering activation energy of porous glass ceramics decreased obviously. On the one hand, the addition of borax provides more liquid phase to facilitate liquid phase sintering. On the other hand, the addition of borax provides B-O bond to change the network structure of non-crystalline vitreous of fly ash, to reduce its melting temperature and promote liquid phase sintering.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

HS designed the research. LZ conceived the experiments and analysed the results with the help of HS and TP. LZ drafted the manuscript.

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Roles of Surfactants in Oriented Immobilization of Cellulase on Nanocarriers and Multiphase Hydrolysis System

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Surfactants, especially non-ionic surfactants, play an important role in the preparation of nanocarriers and can also promote the enzymatic hydrolysis of lignocellulose. A broad overview of the current status of surfactants on the immobilization of cellulase is provided in this review. In addition, the restricting factors in cellulase immobilization in the complex multiphase hydrolysis system are discussed, including the carrier structure characteristics, solid-solid contact obstacles, external diffusion resistance, limited recycling frequency, and nonproductive combination of enzyme active centers. Furthermore, promising prospects of cellulase-oriented immobilization are proposed, including the hydrophilic-hydrophobic interaction of surfactants and cellulase in the oil-water reaction system, the reversed micelle system of surfactants, and the possible oriented immobilization mechanism.

Keywords: cellulase, surfactants, nanocarriers, reversed micelle system, oriented immobilization

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INTRODUCTION

Bioethanol, as a renewable, economically affordable, and environmentally safe energy material, will gradually become a substitute for fossil fuels. It has far-reaching research significance and application value for the development of a sustainable energy strategy (Karimi et al., 2021; Zeng et al., 2021; Ziaei-Rad et al., 2021; Suhartini et al., 2022). Due to competition with food supply in the first generation of bioethanol production, lignocellulose, a non-starch material, has become an important raw material for bioethanol production (Alonso et al., 2019; Maia et al., 2020; Winarni et al., 2020). Adsorption of cellulases onto lignin has been considered as the major factor in retarding enzymatic cellulose degradation of lignocellulosic biomass (Djajadi et al., 2018). Hydrophobic interaction, electrostatic interaction and hydrogen bonding have been regarded as the cause of the nonproductive binding of cellulases to lignin (Djajadi et al., 2018; Li et al., 2020; Song et al., 2020). A natural "biodegradable barrier" of lignin cell walls which are connected in a strong, yet resilient network under the action of covalent and non-covalent bonds render the cellulose inaccessible (Mnich et al., 2020; Chu et al., 2021). Therefore, to reduce the recalcitrance of lignocellulosic biomass to biochemical degradation, pretreatment methods have been developed to break down the lignin-hemicellulose-cellulose matrix and increase the enzyme accessibility of the cellulose scaffold (Jiang et al., 2017a; Jia et al., 2018; Rocha-Martin et al., 2018).

TABLE 1 | The characteristics of various immobilization method of enzymes.

Methods Adsorption Physical		Mechanisms	Characteristics	References	
		Adsorbed on the carriers	Active center of the enzyme is not easy to be destroyed, and not obvious structure change occurs	Gao et al. (2009)	
	Ionic	Combined with water-insoluble carrier containing ion- exchange group by electrostatic force	Structure and amino acids of the active center rarely change, and the higher activity immobilized enzyme can be obtained	Sui et al. (2015)	
Encapsulatio	on	Mixed with polymer monomer and further embedded in the polymer	It is not necessary to combine with amino acid residues of enzyme protein, and rarely change the spatial conformation of enzyme	Singh et al. (2020)	
Covalent bin	iding	Covalently bonded to the water-insoluble carrier	Enzyme molecules are firmly connected with the carrier, the structure of the enzyme protein is often changed, resulting in the damage of the active center of the enzyme	Ghasemi et al. (2021)	
Cross-linking	9	Bifunctional reagent or multifunctional reagent is used to form covalent bond between enzyme molecules	Combined with adsorption or encapsulation method, the activity of immobilized enzyme can be increased and the reinforcement effect can be achieved	Ouyang et al. (2020)	
Cross-linked aggregates (,	Covalently bound by cross-linking agent to keep the supramolecular structure and activity	Carrier free immobilization, good stability, low cost, large activity per unit volume, and high space efficiency	Xu et al. (2020)	
Co-immobiliz	zation	Different enzymes are immobilized in the same carrier at the same time	Several kinds of enzymes and cells with different functions work together in the same system	Qiu et al. (2021)	
Oriented Specific site of enzyme connects with carrier and the action immobilization site faces outsid		Specific site of enzyme connects with carrier and the active site faces outsid It is beneficial for the substrates to enter into the active site of the enzyme and can significantly improve the activity of the immobilized enzyme		Zhou et al. (2021)	

In general, lignin-derived inhibition is the major physical obstacle restricting the enzymatic hydrolysis of cell wall polysaccharides (Leonidas et al., 2019; Zheng et al., 2021). More importantly, the non-specific binding of free cellulase on lignocellulosic substrates may account for the low rate of hydrolysis at the action mechanism level during enzymatic hydrolysis. Some enzymes remain free after the enzymatic hydrolysis of lignocellulosic substrates, while non-specific binding to the residual substrates also prevents the efficient recycling of cellulase (Rahikainen et al., 2011; Kellock et al., 2017; Bhawna et al., 2020). Moreover, the utility of cellulases has been limited due to their low operational stability, high costs, and poor reutilization when used in the native form (Yang et al., 2017).

To overcome these barriers, immobilization is usually used to improve enzyme stability and even activity or selectivity when properly designed, which can also facilitate the reuse of enzymes and effective cost of catalytic processes (Mita and Eldin, 2014; Li et al., 2016; Mehta et al., 2016; Xu et al., 2016; Zhang et al., 2016). The characteristics of various immobilization methods of enzymes is summarized in Table 1. Cellulases represent a large group of enzymes from various organism and with different substrate specificity, biophysical properties, etc. The immobilization behavior is different depending on the enzyme or enzyme mixture investigated. During the immobilization process of cellulase, the structure and properties of carrier materials have significant effects on the performance of the immobilized enzyme (Kalantari et al., 2013; Li et al., 2018). The size of the carriers plays an important role in determining the activity of the immobilized enzyme owing to the inverse relationship between the carrier size and enzyme loading. Thus, large carrier size decreases enzyme activity in general (Valencia et al., 2010), and a reduction in the size of the carriers results in a higher surface area for enzyme binding (Malar et al., 2018; Malar

et al., 2020). For the immobilization of cellulase, the smaller size of the surface pore should be kept lower than that of the cellulase macromolecule (6–20 nm), which can further reduce the internal and external diffusion resistance in the heterogeneous system (DiCosimo et al., 2013; Santos et al., 2015). Therefore, nanocarriers are widely used in the immobilization of enzymes because of their unique properties, such as large specific surface area to volume ratio (Cao et al., 2016; Roth et al., 2016; Malar et al., 2020).

Moreover, the immobilization of cellulase has been achieved based on physical adsorption, covalent binding, or affinity interactions (Zang et al., 2014; Hosseini et al., 2018; Zhang and Hay, 2019), including carrier-binding, microemulsionorgano-gels (MBGs), ultrasonic encapsulation, crosslinking, entrapment, glutathione-labeling, and chelation (Mroczkiewicz et al., 2012; Nicoletti et al., 2015). However, enzymes often display drastically lower activity in organic solvents than in water, and the water layer on the molecular surface of enzymes determines their activity in organic media (Zhang et al., 2012). Therefore, among several approaches to resolve the challenges, one of the most effective methods is immobilization of the enzymes within an microenvironment in the organic solvents. Microemulsions formed by amphiphilic surfactants have been widely reviewed as effective media for the immobilization of enzymes in hydrophobic solvents (Itabaiana et al., 2014; Rajnish et al., 2021; Savic et al., 2021). The MBGs method based on microemulsions has been used to form matrices for enzyme immobilization to achieve enzymatic catalysis nonconventional medium as they appear to be rigid and stable for a long time, even within the reaction solution (Zhang et al., 2012). Therefore, the MBGs method has unique advantages of improving the chemical stability of immobilized enzymes and maintaining high catalytic activity (Pavlidis et al., 2010; Itabaiana

TABLE 2 | Applications of surfactants in preparing nanomaterials.

Applications	Types	Characteristics	References
Nanomaterials	Metallic nanoparticles Semiconductor nanoparticles	It is usually prepared in the reversed micelles and microemulsions system It is prepared in the reversed microemulsions system, including the oxides, sulfides, and selenides etc.	Kawasaki, (2013) Anjum et al. (2019)
	Organic nanoparticles	It includes organic drug nanoparticles and polymer nanoparticles, which can be prepared in microemulsions system	(Li, Kawakami, and Hiramatsu, 2003)
	Nanowires	It can be prepared by the templates from micelles, liquid crystals, vesicles formed by the surfactants	Xu et al. (2010)
	Porous nano-materials Nano-films Nanocomposites	Surfactants can be the structure directing agent of mesoporous materials It mainly includes Langrnuir-Blodgett (LB) film and Molecular-Deposition (MD) film Organic polymer was encapsulated on inorganic nanoparticles in inverse microemulsion system	Carrillo et al. (2011) Shil et al. (2017); Lai et al. (2020) Al-Shemmari et al. (2014)
Methods	Template-directed synthesis	The electrostatic attraction, hydrogen bond and Van der Waals force between surfactant molecules and nano materials are used for the formation of special micelle structures, which can further used as the synthesis templates of nano materials	Xu et al. (2010); Kayhomayun et al. (2020)
	Microemlusion method	When the amount of surfactant and polar organic matter is large, the microemulsion can be obtained, which can be used as a microreactor for synthesizing nanomaterials	Anjum et al. (2019); Cui et al. (2019)
	Hydrothermal synthesis Sol-gel method	Surfactants are mainly used as auxiliary materials The transparent sol is formed by hydrolysis and condensation reaction, and gradually gelatinization. After drying and heat treatment, nanomaterials can be obtained	Cui et al. (2019) Hassanzadeh-Tabrizi et al. (2016)
Surface modification	Physical and chemical properties	Surface adsorption and chemical reactivity of surfactants can modify the surface of nanoparticles	Chaudhary et al. (2014)
	Interfacial modification of nanofilms	Hydrophilicity or lipophilicity of surfactants can be used to modify the interface of nanofilms	Kovalchuk, (2015)
Effects	Dispersion of nanoparticles in media	Prevent particle agglomeration	Fiorati et al. (2021)
	Functional effects on nanoparticles	Improve the compatibility and affinity between polymer materials and inorganic materials	You et al. (2019)

et al., 2014). It is clearly that the surfactants play an important role in the preparation of nanomaterials (Lou et al., 2017; Bao et al., 2019; Ortiz-Martínez et al., 2019; Alexander et al., 2020).

The surfactants have been widely used for the preparation of nanocarriers as shown in Table 2, forming the nano-template by micelles and emulsions of surfactants is a common method that can greatly reduce the surface tension of the solvent and change the interface composition and structure (Carter and Puig-Sellart, 2016; Bao et al., 2019). Desirable nanostructured materials can be produced because of the special nanoreactors formed by surfactant micelles and the oriented alignment characteristics of surfactants in solution, such as the Langmuir-Blodgett (LB) membranes and liposomes (Lok Kumar et al., 2014; Gutierrez et al., 2016). Furthermore, the non-ionic surfactants can significantly enhance cellulose hydrolysis, thus reducing enzyme loading (Lou et al., 2017; Bao et al., 2019). However, inhibitory effects have been observed with the addition of amphoteric, anionic, and cationic surfactants (Lou et al., 2017; Bao et al., 2019). Moreover, the loss of enzyme activity during immobilization is a notable problem; the structural distortion caused by the strong enzyme-support interactions may produce steric hindrances and catalytic cleft blockage (Carlsson et al., 2014; Suárez et al., 2018). Although a large dose of original cellulase is added for a higher load of immobilized enzyme to improve the activities of the immobilized enzyme, no significant improvement in enzymatic activity has been observed due to the

random and inhomogeneous combination of the nanocarriers and cellulase molecules (Nakayama et al., 2009). Oriented immobilization, as a specific binding method, can effectively prevent the nonproductive combination of enzymes and nanocarriers, which further improves the immobilization and hydrolysis efficiency. The reversed micelles formed by surfactants have been successfully used in the preparation of orientedimmobilized lipase when their concentration exceeds the critical micelle concentration (CMC) (Fan et al., 2016). To date, few studies have reported the oriented immobilization of cellulase. Therefore, this review mainly focuses on the important roles of surfactants in the immobilization of cellulase, mainly including the preparation of nanocarriers and cellulase hydrolysis. Moreover, a novel insight into the oriented immobilization of cellulase in a surfactant reversed micelle (SRM) system was discussed and found to have promising prospects.

EFFECTS OF SURFACTANTS ON NANOCARRIERS

Preparation of Nanocarriers Based on Surfactants

The basic physical and chemical properties of surfactants, such as micelle formation, dispersing, emulsifying, and solubilizing, have

made them widely useful in the field of nanotechnology (Yang et al., 2017). Several ordered aggregations formed by the surfactants are used as nano-templates for the preparation of nanocarriers, such as micelles and reversed micelles. The process can greatly reduce the surface tension of the solvent and change the interface composition and structure (Bao et al., 2019). For the preparation of nanocarriers, surfactant micelles are the microreactors of nanocarriers during the preparation process, and the morphology of microreactors is controllable because of the amphiphilic characteristics of surfactants, which have been used for the preparation of desirable nanostructured carriers (Yiamsawas et al., 2017). For instance, hydrophilic surfactants are often used for the preparation of spherical nanocarriers because of their dispersibility in water (Luan and Ramos, 2010). Similarly, the reversed micelles of surfactants can effectively define the particle size and microenvironment in the water, providing a nanoscale reaction space. It has been widely used because the aggregates self-assembled by surfactant molecules can be used to synthesize ordered mesoporous materials with a simpler operation and more uniform channel distribution (Bao et al., 2017; Bao et al., 2019).

Surface Modification of Nanocarriers in the Surfactant System

Surfactants can also change the surface properties of nanocarriers, such as their morphology, magnetic properties, dispersion, and catalytic performances (Asghar et al., 2016; Wei et al., 2018; Lopes et al., 2019; Alexander et al., 2020). This modification may result in a new structure with new surface activity due to the combination of hydrophilic groups of surfactants and surface groups of nanocarriers. For example, of surfactants of decylamine the cetyltrimethylammonium bromide can provide an easy and effective way to change the functionality of cellulose nanocrystals with a hydrophobic polylactic acid matrix and to evaluate the effects of surface chemistry on the reinforcement mechanisms (Orellana et al., 2018). Meanwhile, the presence of surfactants can make nanocarriers more difficult to reagglomerate by reducing the surface energy and form a steric hindrance effect (Wang M. et al., 2013; Tan et al., 2019), the surfactants are coated on the surface of the nanocarriers to form a space barrier layer, the hydrophilic group faces outward and the hydrophobic group faces inward, so that the agglomeration of the particles is avoided.

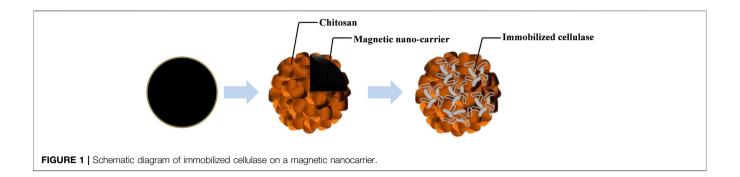
EFFECTS OF NANOCARRIERS ON IMMOBILIZATION OF CELLULASE

The structure and properties of carrier materials have great influence on the properties of immobilized cellulase, such as internal geometry (e.g., flat surfaces or thin fibers), specific surface area, superficial activation degree, mechanical resistance, and pore diameter (Santos et al., 2015; Begum et al., 2019; Malar et al., 2020). Meanwhile, partitioning and mass transport limitations may yield spatial variations in local

reaction rates in porous materials (Neira and Herr, 2017). Therefore, to improve the stability and catalytic activity of immobilized cellulase, various materials, such as chitin, chitosan, nylon, and polyvinyl alcohol, have been widely used as carriers (Cherian et al., 2015; Priydarshani et al., 2018).

The physical effects of nanocarriers on immobilized cellulase are as follows: 1) The pore size and effective surface area of the nanocarriers. Not all porous carriers can be used for immobilization of cellulase due to the limitation of pore size, which should be larger than or equal to that of the cellulase to reduce steric hindrance. The effective surface area occupied by the enzyme determines the maximum load of the immobilized cellulase (Santos et al., 2015). When a stable surface area is maintained, the amount of immobilized or absorbed cellulases is related to the pore size because the pore diameter determines the size of the protein that can be immobilized on that carrier (Teresa et al., 2009; Webster et al., 2015); 2) the number of carrier-bound active groups (CAGs) is another key factor controlling the enzyme-carrier multi-interaction (Cristina et al., 2011; Santos et al., 2015); 3) the size of carriers plays a very important role in the preparation of immobilized cellulase, in that a smaller carrier size with larger specific surface area will be better for the cellulase immobilization load, and the higher surface porosity of the carriers providing numerous binding sites for cellulase is one of the most important factors influencing the activity of immobilized cellulase (Chen et al., 2010; Santos et al., 2015; Malar et al., 2020); 4) the mechanical properties of the carriers need to be controlled considering the final configuration of the reactor. If the reactor is a fixed-bed reactor, such as inorganic supports like porous glass, silicates, it should possess very high rigidity to withstand high pressures without pressure problems, but the situation is different if a stirred-tank reactor is used (Cristina et al., 2011; Santos et al., 2015); 5) after the cellulase penetrates the carriers, the internal morphology of carriers will determine the possibility of obtaining a very intense or very limited enzyme-carrier interaction (Santos et al., 2015). When the diameter of the carriers is smaller than that of the enzyme, it is difficult to obtain an intense enzyme-carrier interaction (Cristina et al., 2011), but if the carriers have sufficiently large internal surfaces, it is possible to get an intense interaction with a similar flat surface (e.g., agarose beads, porous glass, or silicates) (Malar et al., 2018).

In particular, the special superparamagnetism of magnetic nanocarriers has attracted increasing interest as they allow easy recycling and separation of catalysts and biomolecules from high-viscosity liqueurs and high-solid-content broths. This unique characteristic has been well-applied to immobilization of cellulase, and a better hydrolysis efficiency and recycling feasibility have been observed (Alftrén et al., 2014; Cao et al., 2016; Cipolatti et al., 2014; Xing et al., 2015). During immobilization of cellulase, magnetic chitosan microspheres (C-MNPs) are frequently used as carriers because of their significant biological (i.e., biodegradable, biocompatible, bioactive) and chemical properties (polycationic, hydrogel, contains reactive groups, such as -OH and -NH₂). Moreover, the hydrophilic properties of the C-MNPs play an important role in the preparation of oriented-immobilized cellulase based on the



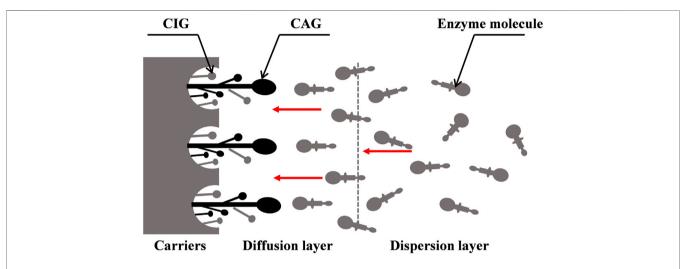


FIGURE 2 | Binding schematic diagram of enzyme and carrier caused by the chemistry properties during the immobilization process. CIGs means the carrier-bound inert groups and CAGs means the carrier-bound active groups; The larger end of enzyme molecule stands for the catalytic domain and the other end stands for the adsorption domain.

SRM system. The conventional immobilization of cellulase molecules on a single magnetic nanocarrier is simple, the chitosan was usually first coated on the magnetic nanocarriers for further combination with cellulase (**Figure 1**). Subsequently, the combined material based on Fe_3O_4 nanocarriers have received extensive attention in cellulase immobilization to improve enzyme activity, loading, and stability because of their low toxicity, biocompatibility, and easy synthesis (Jordan et al., 2011). Magnetite nanocarriers coated with silica and modified by organic-silanes, biocompatible, and with hydrophilic properties, are promising for cellulase immobilization.

The binding sites of enzymes on the surfaces of carriers depend on the chemical properties of the carriers. For non-covalent immobilization, the chemical structure of the skeleton and surface determines the applicability of carriers. The functional groups play a key role in the activity, stability, and selectivity of the enzyme, and the size, charge, polarity, and hydrophilicity/hydrophobicity of groups can affect their binding functions (Watanabe et al., 2010). Different properties of the ionic groups on the surfaces of carriers may result in different enzyme activities and further determine the structure of immobilized cellulase (Santos et al., 2015; Berlin et al., 2016;

Frančič et al., 2016; Hui et al., 2016; Zhou et al., 2018). The chemistry properties of enzyme and carrier cause the oriented distribution of catalytic domain of enzyme from dispersion layer to diffusion layer during the immobilization process is shown in Figure 2. In this process, the CAGs directly participate in binding with enzyme molecules, but the carrier-bound inert groups (CIGs) are not directly involved. This interaction inevitably disturbs the maintenance of the natural conformation of the enzyme, leading to structural and functional changes in the enzyme molecules. No obvious stability change has been observed when the newly formed conformation is similar to that of the natural enzyme.

The covalent binding between carriers and catalytic cleft of the enzyme not only causes pore plugging of the surface, but also leads to the drag increment of in-diffusion. Although an initial high dosage of cellulase is added, the inhomogeneous distribution of the carrier surface structure results in the uncontrollable immobilization sites, and ineffective immobilization may lead to a significant loss of enzymatic activity and reduce the accessibility of the substrate to the functional sites. Moreover, the partition and mass transport limitations of nanocarriers may cause spatial variation in local reaction rates and further affect

enzymatic hydrolysis (Du et al., 2017; Zeng et al., 2019). The chitosan molecules are mostly used because of the large number of -OH and amino groups (-NH3), which are easier to coprecipitate with cellulase (Bindhu and Abraham, 2010; Urrutia et al., 2018; Saha et al., 2019; Mo et al., 2020). Moreover, surface modification is an important strategy for tuning the properties of nanocarriers. Surface modification can either alter the existing property or introduce new properties onto nanoparticles using various siloxane, agents, such as organ dimethylaminopropyl)-N'-ethylcarbodiimide hydrochloride (EDC), and carbodiimide, as well as amino silanes, such as 3aminopropyltriethoxysilane, aminoethyl aminopropyl polydimethylsiloxane, and silica (Chang et al., 2011; Gokhale et al., 2013; Riedel et al., 2017; Malar et al., 2018; Malar et al., 2020).

ROLES OF SURFACTANTS ON CELLULASE HYDROLYSIS

In most reports about hydrophobic ionic liquids, the enzymes are not dissolved but merely in a dispersed state and therefore regarded as a heterogeneous catalyst. Some hydrophilic ionic liquids can accelerate the dissolution of enzyme molecules, but cause the destruction of the protein secondary structure, leading to the inactivation of the enzyme (Fujita and Ohno, 2010; Moniruzzaman et al., 2010). In pure hydrophilic ionic liquids the enzymes can be dispersed at the monomolecular level. The hydrophilic proteins in almost anhydrous nonpolar solvents form suspensions, whereas proteins with extended hydrophobic surface segments form microemulsions in the same media, greatly reducing the catalytic efficiency of the enzyme (Zuev et al., 2003; Predvoditelev et al., 2010). Nonpolar hydrophobic solvents, such as heptane, octane, and benzene, do not cause the dehydration of biocatalysts. Therefore, the enzyme can maintain its catalytic activity (Muginova et al., 2010). Similarly, the catalytic activity of enzymes can be retained in the surfactant micelle system due to the water-oil amphiphilicity of surfactants (Muginova et al., 2010). Non-ionic surfactants can significantly accelerate the enzymatic hydrolysis of lignocellulose (Qing et al., 2010; Seo et al., 2011b; Eckard et al., 2012; Yiamsawas et al., 2017). For instance, Tween-20 can enhance the specific adsorption of cellulase, and the conversion efficiency of cellulose increased from 9 to 21% within 72 h when a high lignocellulosic substrate was added (Seo et al., 2011a). The prevention of non-productive enzyme adsorption onto lignin is the most widely investigated mechanism for this enhancement (Sipos et al., 2010; Lou et al., 2017). Recently, Djajadi et al. (2018) has proved that the adsorption of cellulases onto lignin substrates is reversible by nature, the reversible adsorption-desorption is existing in the process. But the nonproductive adsorption caused by the ineffective combination will occupy large number of catalytic clefts of enzyme molecule which greatly hinder the enzymatic hydrolysis. Non-ionic surfactants can render lignin surfaces more hydrophilic by increasing their polar surface energy component, which can reduce the non-productive adsorption of cellulases onto

lignocellulosic substrates caused by the ineffective combination between catalytic clefts of enzymes and lignin substrates (Jiang et al., 2017b), thereby promoting the enzymatic hydrolysis of lignocellulose. However, for the anionic surfactant-cellulase system, the adsorbed surfactants on the surface of cellulase cause a lower negative charge area, which further leads to negative catalytic activity due to the presence of sulfonic acid groups with a higher ionization degree (Yu and Zhang, 2016).

Furthermore, the effect of surfactants on cellulase hydrolysis is related to the concentration of surfactants (Zhou et al., 2015). In the enzymatic hydrolysis process, cellulose molecules are specifically adsorbed by the cellulose-binding domain (carbohydrate-binding module, CBM) and exert a driving force on the enzyme during the hydrolysis of cellulose (Liu et al., 2011; Tomme et al., 2015; Arslan et al., 2016). The adsorption of CBM can increase the cellulase concentration of the substrate surface by promoting the association of enzymes and substrates, but the noncovalent interactions (e.g., hydrogen bonds, electrostatic, and hydrophobic interactions) may lead to a nonproductive combination, because the random combination will occupy the active center of enzyme, resulting in the loss of catalytic activity. Ineffective adsorption can be reduced in the presence of surfactants due to the hydrophobic structure of surfactants, which can interact with the hydrophobic lignocellulosic substrates and form a coating (Kumar and Wyman, 2010; Li et al., 2012). However, contrasting results were obtained when different concentrations of surfactants were added to the enzymatic hydrolysis system. Some studies have suggested that a high concentration of surfactants can inhibit cellulase activity because strong hydrophobic interaction between the surfactant and cellulase can further reduce the effective adsorption of enzymes on cellulose (Wang Z. et al., 2013; Bao et al., 2019). However, the promotion effect of surfactant in enzymatic saccharification was observed in low concentration of lignosulfonate with low molecular weight and good sulfonation, which can be explained that the lignosulfonate can prevent the nonproductive binding of cellulase to lignin substrate, and the formed lignosulfonatecellulase aggregate can also stabilize and enhance the binding of cellulase to lignin substrate (Lou et al., 2014).

THE ORIENTED IMMOBILIZATION OF CELLULASE IN THE SRM SYSTEM

The oriented immobilization of proteins on a solid support can effectively avoid its denaturation and keep its catalytic clefts fully exposed to solution, thus maximally preserving the bioaffinity or bioactivity. Liu and Yu (2016) has summarized the recent advances in oriented immobilization of proteins with a particular focus on antibodies and enzymes. However, the orientated immobilization of enzymes at the solvent interface is never involved. Thereby, the follow-up content will propose a novel method to achieve the oriented immobilization of cellulase in the SRM system.

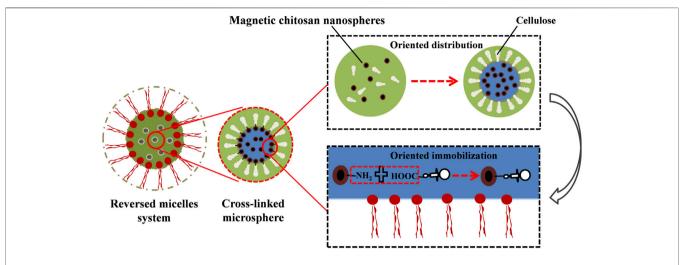


FIGURE 3 | The oriented immobilization diagrammatic sketch of single-layer cellulase in the surfactant reversed micelles system, the "green" represents the internal "pool" of SRM system, "black" represents the magnetic chitosan microspheres (C-MNPs), "brown" represents the cross-linked microsphere.

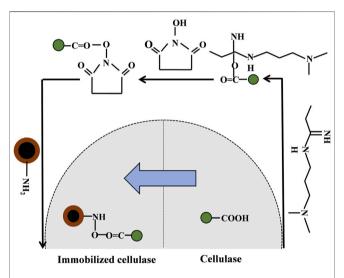


FIGURE 4 | The oriented immobilization process of cellulase on magnetic nanoparticles.

Construction of the SRM System

The SRM system has been widely used in the preparation of immobilized enzymes (Dong et al., 2010; Marhuendaegea et al., 2015). The special structure of surfactant molecules caused a water-oil amphipathy with a hydrophobic nonpolar hydrocarbon chain (alkyl) and a hydrophilic polar group (such as -OH, -COOH, -NH₂, and -SO₃H) distributed at different ends. In the water-oil (W/O) system, the surfactants are dissolved in the nonpolar organic solvent when a trace of water is provided, and the reversed micelles are formed when the concentration exceeds the CMC (Takagi et al., 2019; Chi et al., 2018). In reversed micelles, the nonpolar groups of the surfactants are exposed to the nonpolar organic solvents, while the polar groups are arranged inside. Therefore, a polar core with the ability

to dissolve polar substances in the microreactors is formed. The SRMs are nanoscale aggregates that are formed spontaneously, and the W/O microemulsion with low water content provides a stable thermodynamic system (Tao et al., 2013). According to the hydrophilic-hydrophobic interaction of surfactants and cellulase in the oil-water reaction system, the large number of oil-water interfaces in the system provides a good environment for the catalytic reaction of enzyme molecules (Brady and Jordaan, 2009).

Mechanism of Oriented-Immobilized Cellulase in the SRM System

Multipoint covalent attachment is likely the most effective strategy for immobilization, but it is difficult to allow the immobilization of enzymes at a well-defined position since the proteins are usually attached to the solid surface by uncontrolled chemical bonds (Barbosa et al., 2015; Hernandez and Fernandez-Lafuente, 2011; Li et al., 2016). The uncontrolled conformational changes were caused by random immobilization, which may lead to a significant loss of enzyme activity, and the disordered enzyme orientation may also reduce the accessibility of the substrate to functional sites (Orellana et al., 2018; Steen Redeker et al., 2013; Yu et al., 2012). However, the hydrophilic cellulase will be dissolved in the SRM system due to the existence of surfactants, which can maintain the activity of the enzyme and prevent the toxic effects of organic solvents (Tao et al., 2013). The active centers of cellulase molecules are usually clefts, which provide a different microenvironment (Zhang et al., 2015) because the structures of cellulase active centers are mainly composed of eight kinds of amino acids (tryptophan, tyrosine, histidine, phenylalanine, aspartic acid, glutamic acid, and arginine). Aromatic amino acids and some polar amino acids appeared more frequently, such as tryptophan, tyrosine, histidine, aspartate, asparagine and arginine, most of which are hydrophobic tryptophan and phenylalanine residues, especially

the tryptophan which has the highest content and plays an important role in the recognition and binding of enzyme molecules and substrate (Zhang et al., 2015). Hydrophobic active centers are conducive to the combination of catalyzed groups of cellulase and substrates. When the specific substrate is close to the active centers, a change in the conformation of the cellulase molecule can be induced so that the reaction groups of the enzyme active centers and substrate are aligned correctly. Meanwhile, the molecular orbitals between the reaction groups of the active centers are strictly located in the right direction for easier enzymatic reactions. Therefore, cellulase is distributed in the W/O interface, and the catalytic active center is toward the organic solvent and the other side toward the "pool". Moreover, the addition of surfactants can enhance the aggregation effect of cellulase on the W/O interface, and the existence of a crosslinking agent promotes the covalent crosslinking of enzyme molecules. The catalytic activity centers of the cross-linked microspheres are distributed uniformly and toward the outside, which solves the challenge of the uncontrollable attachment sites of the cellulase molecules in the immobilization process (Li et al., 2016; Steen Redeker et al., 2013; Yu et al., 2012). In the SRM system, the hydrophobic active molecules are exposed to the outside, which is beneficial for the further combination of immobilized cellulase and lignocellulosic substrates. However, the immobilized sites of cellulase molecules remain stochastic and heterogeneous, which may lead to covalent binding between the carriers and the active center of the enzyme and further cause ineffective immobilization and enzymatic reactions (Li et al., 2016). Therefore, to achieve oriented immobilization and improve the recycling times of cellulase, C-MNPs can be used as carriers as shown in Figure 3. This method can effectively prevent the ineffectiveness of cellulase immobilization. In this process, glutaraldehyde is used as the crosslinking agent, and EDC and N-hydroxysuccinimide are the coupling agents (Figure 4). In the W/O system, the free carboxyl group (-COOH) in the adsorption zone of the cellulase molecules can realize covalent binding with a large number of amino terminal catalytic residues of chitosan molecules (Fan et al., 2016). The process cannot destroy the catalytic center of cellulase, and the exposed catalytic clefts increase the effective attachment of immobilized cellulase to solid substrates, which further promotes enzymatic hydrolysis. Therefore, the oriented immobilization of enzymes is obtained in the SRM system, which can prevent

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CONCLUSION

Cellulase plays an important role in the production of fuel ethanol by the enzymatic hydrolysis of lignocellulose, and the immobilization of cellulase on the nanocarriers is an effective way to improve hydrolysis efficiency. However, the nanocarrier structure characteristics, solid-solid contact obstacles, external diffusion resistance, limited recycling frequency of nanocarriers, and nonproductive combination of enzyme active centers restricted the further improvement of hydrolysis efficiency in the complex multiphase system. Surfactants can promote the enzymatic hydrolysis of lignocellulose and play an important role in the preparation of nanocarriers. The special SRM system caused by the amphiphilicity in the oil-water reaction system can provide effective protection to obtain the immobilization of single-layer cellulase, which can effectively prevent the immobilization of cellulase and increase the effective attachment of immobilized cellulase and solid substrates.

AUTHOR CONTRIBUTIONS

ZW: conceptualization, investigation, methodology, and writing (original draft preparation). CF: methodology and article revision. XZ: data collection and writing (review and editing). ZJ: methodology and investigation. KB: formal analysis and investigation. MZ: data collection, article revision and funding acquisition. HK: methodology, writing (review and editing) and supervision.

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Preparation of Templated Materials and Their Application to Typical Pollutants in Wastewater: A Review

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As the pollution and destruction of global water resources become more and more severe, the treatment of wastewater has attracted significant attention. The template method is a synthetic method in which the template is the main configuration to control, influence, and modify the morphology as well as control the dimensions of the material, thus achieving the properties that determine the material. It is simple, highly reproducible, and predictable, and more importantly, it can effectively control the pore structure, size, and morphology of the material, providing a novel platform for the preparation of adsorbent materials with excellent adsorption properties. This review focuses on the classification of the templates according to their properties and spatial domain-limiting capabilities, reviews the types of hard and soft template materials and their synthetic routes, and further discusses the modulation of the morphological structure of the materials by the introduction of templates. In addition, the application and adsorption mechanisms of heavy metal ions and dyes are reviewed based on the regulatory behavior of the template method.

Keywords: template method, moderating behavior, heavy metals, dyes, adsorption mechanism

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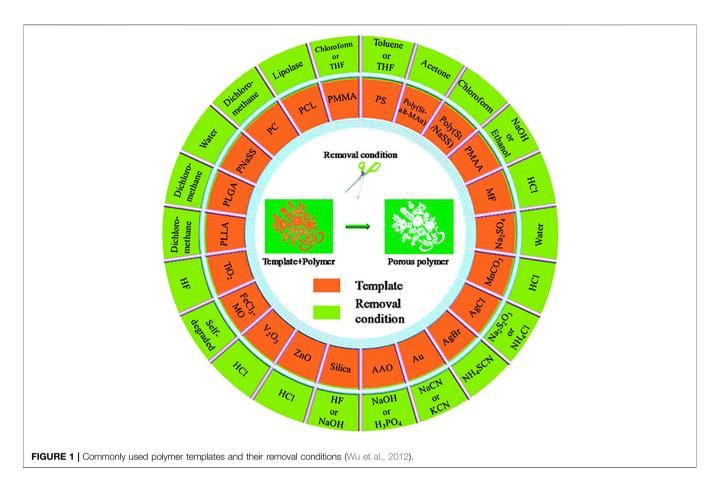
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1 INTRODUCTION

Pollution (Yang et al., 2019; Zhang et al., 2019; Zhao et al., 2019), especially water pollution, has been a global problem that needs to be addressed immediately , with the rapid development of industrial economy. Human production and living activities result in a considerable discharge of pollutant into the water resources, particularly organic dyes and heavy metals, which can pose a serious threat to people's living environment if not properly treated. Dyes are extremely harmful to ecosystems due to their toxicity and the reduction of dissolved oxygen in water, while heavy metals can cause pernicious health effects on humans and other organisms (Zare et al., 2018). Therefore, there is an urgent need to develop remediation strategies that effectively mitigate organic dyes and heavy metal pollution.

Nowadays, several techniques have been successfully used for the purification of heavy metal ions and organic dyes in wastewater, such as chemical precipitation, ion exchange, and adsorption. Among them, adsorption has become one of the most influential and promising methods (Zhou et al., 2018) due to its simplicity, low cost, mature process, and low energy consumption (Liu J. et al., 2016; Yu et al., 2018). At present, various adsorbents such as activated carbon (Ekinci et al., 2002; Zhou et al., 2015; Kuroki et al., 2019), zeolites (Briao et al., 2017; Zanin et al., 2017), nanomaterials (Sarma et al., 2019; Madima et al., 2020; Yu et al., 2021), biochar (Wang et al., 2019a; Wang et al., 2019b; Wang L. et al., 2020; Wang et al., 2021; Wei et al., 2022), and metal organic framework polymers (Huang et al., 2018; Pi et al., 2018), have been developed and widely used for the adsorption of wastewater. However, most adsorbents still have some problems, such as uneven pore size



distribution and difficulty in achieving effective control of pore size, which directly affect the adsorption capacity of the adsorbent. The template method, which has been developed in recent years, is simple, highly reproducible, and predictable (Liu et al., 2019; Ma et al., 2019). More importantly, the template method enables effective control of the pore structure, dimensions, and morphology of the composite material (Marrakchi et al., 2017), which is expected to be a solution to these problems and achieve efficient adsorption of adsorbents.

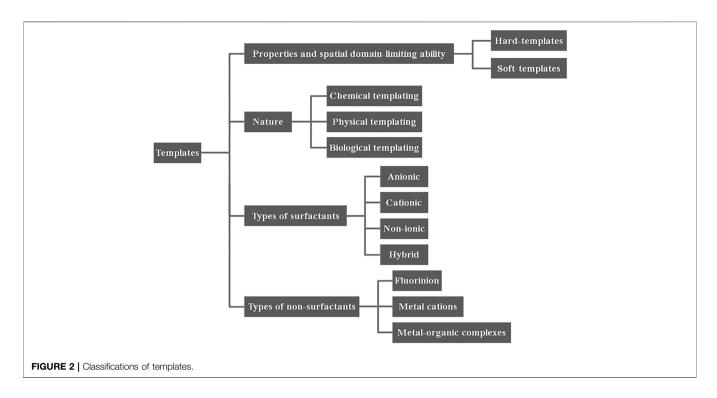
The template method, essentially a forming or casting technique, which is different from the conventional methods, in that it needs to introduce a template agent in advance. Whether the reaction takes place in the liquid or solid phase, the template method can effectively modulate the size, morphology, structure, and even the arrangement of the sample. The morphology of the product varies depending on the template chosen, so it is important to select the right template (Liu et al., 2013). The template method is now widely used in water treatment [such as photocatalysis (Ahmad et al., 2017; Yang et al., 2021), adsorption (Libbrecht et al., 2017; Zhao et al., 2020a), and electrochemistry, as well as biology and medicine (Miao et al., 2010; Wu and Xu, 2010; Li et al., 2013)]. This study outlines the classification of the template method, focuses on the hard and soft template methods, discusses the modulating behavior of the template method on the morphological structure of materials, and further

discusses the current status of the application of the template method for heavy metal ions and organic dyes in water treatment.

2 PREPARATION AND CLASSIFICATION OF THE TEMPLATE METHOD

The template method is based on the morphological characteristics of the synthetic material, introducing its self-assembly or organic molecular system as a template, and effectively regulating and modifying the morphology, structure, and dimensions of the material through forces like hydrogen bonding and Van der Waals forces. It is essentially a forming or casting technique (Thomas et al., 2008), generally speaking, synthesis of the template method includes three main steps (Knezevic et al., 2018): 1) preparation of templates; 2) synthesis of target materials using the templates; and 3) removal of templates.

In general, there are four requirements for the preparation of template method: 1) in order to achieve successful replication of the template, the surface properties of the template used should be consistent with the raw material; 2) the template should have a well-defined structure, such as an easily adjustable morphology; 3) the template should be easy to remove. **Figure 1** summarizes the commonly used polymer templates and their removal



conditions (Wu et al., 2012), such as silica templates, as one of the most commonly used templates, are usually removed using hydrofluoric acid or sodium hydroxide; 4) the polymer template should be robust enough to prevent deformation of the pores after template removal.

At present, there are various classifications of template agents; the specific classification is shown in **Figure 2**. One kind of classification can be divided into hard templates (porous silica, silica) and soft templates (biomolecules, surfactants) according to the templates' own properties and spatial domain-limiting ability (Bao et al., 2016). Depending on the nature of template, it can be subdivided into physical templates, chemical templates, and biological templates (Liu et al., 2013; Zhao et al., 2020b). In addition, some scholars classify it according to surfactants and non-surfactants. The former includes anionic template agents, cationic template agents, non-ionic template agents, and hybrid template agents; while the latter includes metal cations, organic molecules, metal–organic complexes, etc. (**Figure 2**).

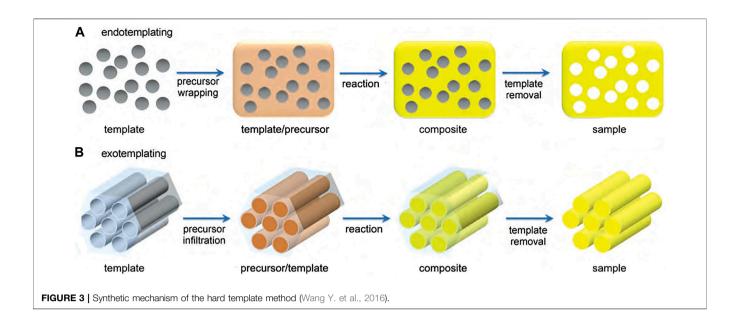
Currently, based on different compositions and characteristics of templates, the most common way to classify them is to divide into hard and soft templates, both of which provide a tunable reaction space for the adsorbent. Among them, hard template is mainly selected from material that is prepared already, such as mesoporous carbon (Libbrecht et al., 2015), mesoporous silica (Marciniak et al., 2019), metal oxides (MO) (El-Hankari et al., 2016), etc. During the preparation process, the raw material is adsorbed or permeated on the surface or internal lattice of the template, and the template is removed after the reaction (Petkovich and Stein, 2013). Materials prepared by the hard template method can be precisely regulated in terms of size and structure, but the removal of the template can easily cause structural damage to the raw material (Liu D. et al., 2016). In

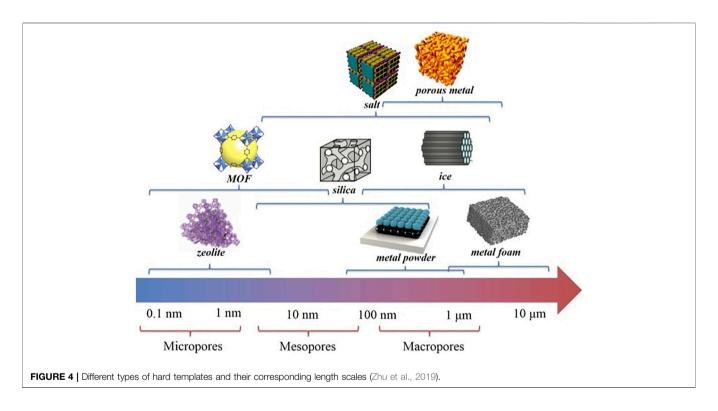
contrast, soft template is formed during the reaction, that is, a phase interface is formed between the soft template [such as polymers (Liu D. et al., 2016), biological macromolecules (Zhao et al., 2017), and surfactants (Cao et al., 2014)]; the target product by micelles and a certain spatial structure is established by the internal polymerization of the molecules. In comparison, soft template is easier to remove and the production condition is mild and simple, which is a current trend in the preparation of materials by the template method (Xie et al., 2016). The detailed characteristics and preparation of each of the two template methods are described below.

2.1 Hard Template

Hard templates are usually connected by covalent bonds, and the reaction cavity is in dynamic equilibrium, with substances diffusing in and out through the cavity walls, such as molecular sieves, metals (Wang H. et al., 2016), and carbons (Xie et al., 2018). Generally, the preparation process for materials prepared using hard templates is to wrap or infiltrate the selected template with a precursor, transforming the precursors into solid material by chemical or thermal treatment, and then removing the template by chemical etching or high temperature calcination (Petkovich and Stein, 2013).

Depending on the inclusion relationship between the hard template and the precursor, the hard template method can be divided into exotemplating and endotemplating methods (Schuth, 2003). As shown in **Figure 3A** (Wang Y. et al., 2016), endotemplate is the precursor wrapping template. Template molecules enter the precursor and create pore channels, and after the removal of the template, a pore system is formed in the precursor. Exotemplating is the opposite, as shown in **Figure 3B**, where the precursor penetrates the template.





Exotemplate can be materials with structural pores, and the precursor infiltrates into the pore channel. Depending on the connectivity of the template, a porous or finely split material remains after the template removal.

Compared to soft templates, hard templates have better domain limitation and higher stability, so they can achieve a strict regulation of material size and morphology. And different template agents can be selected according to the requirements of the target product to achieve precise regulation of different specific surface areas, pore sizes, morphology, and other characteristics. As shown in **Figure 4**, Zhu et al. (Zhu et al., 2019) classified various hard templates according to the pore sizes of different templates and corresponding composites. It can be seen that different pore sizes correspond to different template materials, therefore, based on the performance requirements of the target product, selecting the most suitable template material, which is one of the key factors for the successful synthesis of template

materials. However, hard templates are difficult to be removed; the majority of these templates act as supports, which limits the application of hard template method to a certain extent (Liu D. et al., 2016).

In practice, hard template method has excellent results in the treatment of industrial wastewater, such as the adsorption of heavy metal ions. Currently, numerous types of hard templates have been investigated, such as silica (Fuertes et al., 2005), metal–organic frameworks (MOF) (Amali et al., 2014), mesoporous carbon (Libbrecht et al., 2015), poly (methyl methacrylate) (PMMA) (Liu et al., 2018), etc., and the specific materials are described below.

2.1.1 Mesoporous Silica Templates

Mesoporous silica has a high specific surface area and good hydrophobicity. When used as a hard template for wastewater adsorption treatment, it can improve the morphology and pore structure of the material very well, and is commonly used as a hard template for the synthesis of mesoporous carbon materials in practical applications. Mesoporous silica has a three-dimensional interconnected pore structure, which offers the possibility of introducing carbon precursors. On the other hand, the three-dimensional interconnected pore structure of mesoporous silica also ensures the successful synthesis of mesoporous carbon, rather than obtaining carbon materials with nanowire or rod-like structures.

The preparation process usually starts by immersing the carbon precursor into the pore channel of the template agent to cause polymerization, and then removing the mesoporous silica template with hydrofluoric acid or sodium hydroxide solution after carbonization. The ordered mesoporous carbon CMK-1 was successfully prepared using mesoporous silicas MCM-48 as templates and sucrose as carbon precursors, heated to 1173 K and carbonized, and removed the silicon template using dissolution in sodium hydroxide solution. Moreover, they obtained samples Cn-CMK-1 by controlling the pore size of the template, and the specific surface area and pore size of the samples were 1700 m²/g, 1.24 cm³/g (C16-CMK-1), $1800 \text{ m}^2/\text{g}$, $1.21 \text{ cm}^3/\text{g}$ (C18-CMK-1), and $1710 \text{ m}^2/\text{g}$, 1.23 cm³/g (C20-CMK-1), respectively (Kruk et al., 2000). Similarly, Jun et al. (Jun et al., 2000) used ordered mesoporous silica SBA-15 as a template agent and sucrose as the carbon source, carbonized the mixture at 1173 K, and finally the ordered mesoporous carbon CMK-3 was obtained by removing the mesoporous silica template using sodium hydroxide or by washing with hydrofluoric acid. The specific surface area of CMK-3 was 1520 m²/g, and the total pore volume was $1.3 \text{ cm}^3/\text{g}.$

Kim et al. (2005) used mesoporous silica SBA-16 as a template agent; and sucrose, furfuryl alcohol, and acenaphthene as carbon precursors to synthesize cubic mesoporous carbon, respectively. The reactions were all carbonized at 1173 K, and the mesoporous silica templates were removed with hydrofluoric acid. The experimental results showed that the furfuryl alcohol-based mesoporous carbon has a high specific surface area and total pore volume (2050 m²/g, 2.33 cm³/g), which is higher than that of sucrose-based mesoporous carbon (1370 m²/g, 1.20 cm³/g) and

acenaphthene-based mesoporous carbon ($1260 \text{ m}^2/\text{g}$, $1.68 \text{ cm}^3/\text{g}$). It further shows that the selection of suitable silicon templates and carbon precursors can effectively control the mesoporous structure of the materials.

2.1.2 Carbon Templates

Carbon materials, such as mesoporous carbon and carbon nanotubes, are also used as template agents. Among them, mesoporous carbon is stable and has an ordered pore structure, so it is often used as a template agent to synthesize ordered mesoporous materials such as nanoscale zeolite molecular sieves and mesoporous metal oxides. The process of synthesizing mesoporous carbon into a mesoporous material usually involves replicating the pore channels of the mesoporous carbon into the new mesoporous material and removing the mesoporous carbon template under certain conditions. Roggenbuck et al. (2006) chose mesoporous carbon CMK-3 as a hard template, infiltrated the carbon matrix with Mg(NO₃)₂, removed the template by heating, and later obtained mesoporous MgO. The specific surface area and total pore volume of mesoporous MgO were 280 m²/g and 0.52 cm³/g.

Carbon nanotubes can greatly improve the reactivity of the material due to their characteristic pentagonal defect structure. Liu et al. (2015) prepared MWCNTs@carbon nanocables by a hydrothermal synthetic method using multi-walled carbon nanotubes (MWCNTs) as a template agent and glucose as a carbon source, and used anhydrous ethanol for washing to remove the template during the preparation.

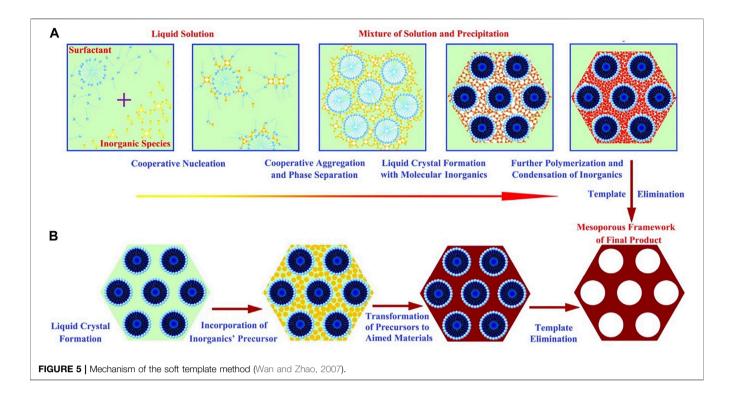
2.1.3 Metal-Organic Framework Polymer Templates

Metal–organic frameworks (MOFs) are a new class of materials with a three-dimensional pore structure, in which specific surface areas are significantly high (in the range of $1000-10000~\text{m}^2/\text{g}$), even higher than that of zeolites ($3500~\text{m}^2/\text{g}$). Also, based on the inherent instability of the MOFs, it is easy to remove when they were used as template agents (Zhao et al., 2021).

ZIF-8, as one of the typical MOF materials, has excellent chemical and thermal stability and is an ideal template for the preparation of the material. The ZnS nanocages were prepared using ZIF-8 as template agents and thioacetamide as the sulfur precursor, and the ethanol solution was chosen to remove the template during the preparation process (Jiang et al., 2012). Zhang et al. (2018) prepared PDA/PEG@ZIF-8 composite nanoparticles by grafting polyethylene glycol (PEG) polymers by the template method using ZIF-8 as a hard template. The ZIF-8 template was further removed by etching with dilute hydrochloric acid adjusting the pH to 7 to obtain PDA/PEG composite nanocapsules.

2.1.4 Other Hard Templates

Nanoporous anodic alumina, palygorskite (Pal) and spherical particles (PMMA microspheres, CaMg(CO₃)₂ microspheres) are also widely used as hard templates for wastewater adsorption. Mohajeri et al. (2017) used nanoporous anodic alumina as a template agent, ethylene as a carbon precursor, and argon as a carrier gas to synthesize ordered carbon nanotube arrays by chemical vapor deposition (CVD), and the template was



removed by pyrolysis during the preparation. Zhong et al. (2019) used modified palygorskite (Pal) as a hard template and glucose as a carbon source to synthesize carbon-coated palygorskite (Pal@ C) by impregnation and carbonization, with further final acid-base treatment to remove the Pal template to obtain amorphous carbon nanotubes (ACNT).

Spherical particles were also successfully applied as hard templates for the synthesis of adsorbents, such as poly (methyl methacrylate) (PMMA) microspheres. Using PMMA colloidal microspheres as template agents can synthesize three-dimensional hierarchical porous graphene-Fe₃O₄ (3D-HPGF) nanocomposites, and the PMMA templates were removed by calcination at 873 K under nitrogen atmosphere (Liu et al., 2018). Similarly, by using CaMg(CO₃)₂ microspheres as a template agent and Al(NO₃)·9H₂O as an aluminium source, Al₂O₃ hollow microspheres can be successfully synthesized with further calcinations, and the CaMg(CO₃)₂ microsphere template was also removed by calcination during the preparation process (Tian et al., 2016).

2.2 Soft Template

Soft templates mainly rely on intermolecular interaction forces to maintain the stability of the structure, and the material diffuses through the cavity walls into the interior of the static pore. Wan and Zhao (2007)schematically summarized the two mechanisms for the synthesis of soft templates (**Figure 5**), including the cooperative self-assembly and liquid-crystal templating processes. As shown in **Figure 5A**, cooperative self-assembly is based on inorganic–organic interactions between inorganic and surfactants. In this pathway, inorganic species and surfactants cooperate to nucleate as well as form liquid crystals with

molecular inorganics, removing the template after further polymerization and condensation of inorganics. As shown in **Figure 5B**, the "true" liquid crystal templating process is that the liquid crystal mesophases are involved in the templating assembly to synthesize aimed materials, which means the liquid crystals are incorporated directly with precursors, and the template is removed after the transformation of the precursor to target product by reaction.

The advantages of the soft template method typically include simple construction, relatively mild experimental conditions, and its capacity to synthesize different materials with various morphologies. However, it has low structural stability compared to the hard template method, which results in it being a less efficient template. Typically, organic molecules are used as soft templates, such as micelles (Zhao et al., 2006; Gao et al., 2015), emulsified droplets (Bourret and Lennox, 2010; Wang B. et al., 2011; Pang M. et al., 2013), biological molecular assemblies (Yan et al., 2017; Zhao et al., 2017; Wang Y. et al., 2020), gas bubbles (Fan et al., 2004; Yan and Xue, 2007), etc., and the specific materials are described below.

2.2.1 Micelle Templates

Micelles, refer to the aggregates by the mutual attraction of hydrophobic parts of surfactants after they are dissolved in water, which have excellent solubilization effects, are extremely common and highly versatile soft template materials. However, during the preparation process, a single aggregated micellar template tends to be very sensitive to the solvent, resulting in it being unstable in the reaction. In the recent years, it has been found that the introduction of surfactants in the preparation process can effectively improve this phenomenon. For example,

Zhao et al. (2006) prepared SnO₂ hollow spheres using micelles composed of terephthalic acid and sodium dodecylbenzene sulfonate (SDBS) as templates, and successfully constructed hollow structures for the materials. Gao et al. (2015) used worm-like micelles as soft templates to prepare Au and Aubased alloy nanowire networks with adjustable composition ratios. The worm-like micelles were obtained by mixing HAuCl₄ and 3-(N,N-dimethylpalmitylammonio) propanesulfonate (PAPS) in an aqueous solution, and the AuAg and AuPt alloy nanowire networks were synthesized by a stepwise reduction method using NaBH₄-PAPS and ascorbic acid (AA)-PAPS mixtures as reductants.

2.2.2 Emulsion-Based Templates

Emulsified droplets, a non-homogeneous system formed within a mixture of two and more incompatible liquids, are an important class of soft templates. During the preparation process, emulsion droplets usually obtain materials with hollow structures through sol-gel coating, interfacial precipitation, and hydrothermal reactions. Pang M. et al. (2013) chose polyoxyethylene and sorbitan trioleate to form emulsified droplets, and used them as templates to synthesize Fe-soc-MOF cubes *via* solvothermal method. After removing the droplets, Fe-soc-MOF cubic hollow colloids with different sizes and arrangements with a specific surface area of 1100 m²/g, and a total pore volume of 0.49 cm³/g were obtained.

Oil-in-water (O/W) microemulsions and water-in-oil (W/O) microemulsions are two important types of emulsified droplets. Wang B. et al. (2011) used glycerol/water as emulsion templates and Fe₂O₃ nanoparticles as raw materials to synthesize α-Fe₂O₃ hollow spheres with lamellar substituents under hydrothermal conditions. The prepared templated material has a large cavity space and well-defined shell layer, and has a specific surface area of 103.3 m²/g and a wide pore size distribution. Similarly, the W/O microemulsion templates have been widely applied at present. For example, Bourret et al. (Bourret and Lennox, 2010) used CH₂Cl₂ solution as the aqueous phase of the microemulsion and obtained copper hydroxide nanofibers (NF) by interfacial reaction in a two-phase system (H₂O/ CH₂Cl₂). As the reaction proceeds, porous microspheres with shell-like structures were finally synthesized, and the prepared CuS nanohollow spheres have a diameter of about 200 nm and a wall thickness of about 30 nm.

2.2.3 Biological Templates

Biological templates, such as biopolymers, cellular tissues, bacteria, and DNA, are some of the most common soft templates, because of their wide source, non-toxicity, non-contamination, and low cost, they have a great potential in the development of template agents. Zhao et al. (2017) treated rape pollen grains with anhydrous ethanol and 8 M hydrochloric acid, respectively, and dried at room temperature to obtain two types of pollen templates. These two pollen templates were used to synthesize ZrO₂ hollow microspheres with scale-like outer walls (S-1) and porous hollow ZrO₂ microspheres (S-2) via the same experimental method, that is, treated by microwave solvothermal method at 110°C, washed with distilled water

and absolute ethanol, dried, and calcined at 580°C. The specific surface areas of S-1 and S-2 are 27.99°m²/g and 40.92°m²/g, respectively, while the average pore diameters are 14.57 and 10.19°nm, respectively.

In addition, cotton is one of the most common biological templates. The dried cotton templates were dipped into the solution for hydrolysis treatment, followed by the reaction in the reactor under nitrogen atmosphere and washed with anhydrous ethanol and deionized water, and dried to obtain the corresponding cotton templated materials. For example, Yan et al. (2017) prepared fibrous magnesium oxide by template-directed synthesis using cotton as a template agent and hydrolyzed in cetyltrimethylammonium bromide solution. Wang Y. et al. (2020) used cotton as a template agent and hydrolyzed it in sulfuric acid solution to synthesize mesoporous carbon lanthanum-doped films (MC-La).

2.2.4 Other Soft Templates

In addition to the template materials mentioned above, bubbles, vesicles, and amphiphilic polymers are also excellent materials for soft templates. The preparation process of bubble templates in the liquid phase usually consists of the following two steps: preparation of the template (generation of bubble emulsion), deposition/ adsorption of particles on the template surface, and further growth/aggregation of particles (Fan et al., 2004). In addition, Yan and Xue (2007) used the CO₂ bubbles generated during the reaction as a template agent to obtain ZnO hollow microspheres by pyrolysis.

Vesicles, as one of the most important microreactors for controlled growth, are important materials for soft templates. Zheng et al. (2002) obtained anionic sodium dodecyl sulfate (SDS) vesicles by ultrasonic irradiation and used them as soft templates. The cadmium ions were adsorbed on the surface of the templates by electrostatic interaction, and after washing with distilled water and anhydrous ethanol to remove the templates, CdSe hollow nanoparticles with the size of 100–200 nm were obtained.

Amphiphilic polymers can also be used as soft templates to synthesize hollow structural materials, and different morphologies of materials can be obtained by adjusting the size and composition of the template. For example, Lin et al. (Pang X. et al., 2013) used a star-shaped PS-b-PAA-b-PS triblock copolymer as soft templates to synthesize hollow gold nanoparticles.

3 MODERATING THE BEHAVIOR OF MATERIALS BY THE TEMPLATE METHOD

3.1 Pore Structure Tuning

The size and nature of different template agents vary, and their introduction into the same material or different materials will result in different specific surface areas, pore sizes, and pore volumes; the pore sizes and volumes will show a certain variation with the concentration of the template agent. In general, smaller sized and more concentrated template

TABLE 1 | Structural parameters of the samples synthesized with different templates.

Sample	Template agent	Specific surface area (m²/g)	Pore volume (cm ³ /g)	Average pore size (nm)	References
Al ₂ O ₃ (CTAB)	Cetyltrimethylammonium bromide (CATB)	335.7	0.66	6.1	Bo and Jing
Al ₂ O ₃ (CA)	Sodium laurate (CA)	312.0	0.44	4.1	(2007)
Al ₂ O ₃ (P123)	PPO-PEO-PPO (P123)	318.8	1.00	9.8	
Aluminosilicate materials (CTAB)	Cetyltrimethylammonium bromide (CTAB)	211.5	0.31	4.4	Ma et al. (2020)
Aluminosilicate materials (DETA)	Diethylenetriamine (DETA)	75.2	0.12	4.8	
Aluminosilicate materials (CMC)	Sodium carboxymethylcellulose (CMC)	161.5	0.37	6.2	
Aluminosilicate materials (SDS)	Sodium dodecyl sulfate (SDS)	144.3	0.27	5.4	
Aluminosilicate materials (F68)	PEO ₈₀ -PPO ₃₀ -PEO ₈₀ (F68)	277.6	0.24	6.0	
Aluminosilicate materials (F108)	PEO ₁₃₃ -PPO ₅₀ -PEO ₁₃₃ (F108)	289.7	0.24	6.5	
S7	F127 (EO ₁₀₆ PO ₇₀ EO ₁₀₆)	1022	1.35	5.3	Yang et al. (2006)
S14	F127 + PEG	1145	0.82	2.9	
Mesoporous Titania (TS-0.1)	Cetyltrimethylammonium chloride (CTAC)	83.8	0.17	9.0	Yusuf et al. (2003)
Mesoporous Titania (TP-0.1)	Polyethylene glycol (PEG)	57.1	0.094	8.4	
Mesoporous Titania (TPS-0.01)	CTAC + PEG	39.6	0.076	6.2	
Nano ferric oxides (C-Fe ₂ O ₃)	Cetyltrimethylammonium bromide (CTAB)	24.8	0.11	11.9	Lei et al. (2018)
Nano ferric oxides (G-Fe ₂ O ₃)	Glycerine (GI)	23.6	0.091	10.2	
Nano ferric oxides (T-Fe ₂ O ₃)	Tartaric acid (TA)	40.8	0.092	4.8	
ZSM-5 Zeolite (NZ)	Tetrapropylammonium hydroxide (TPAOH)	364.0	0.39	_	Zhang et al. (2015)
ZSM-5 Zeolite (MZ)	Cetyltrimethylammonium bromide (CTAB)	374.0	0.45	_	- '
ZSM-5 Zeolite (NSZ)	N-octadecyl-N'-hexyl-tetramethyl-1,6-hexanediaminium $(C_{18\cdot 6\cdot 6}Br_2)$	505.0	0.63	_	

agents are more favorable for the preparation of templated materials.

3.1.1 Effect of Template Agent Type on Pore Structure

The specific surface area, pore volume, and pore size of the synthesized materials varied considerably depending on the template agent (**Table 1**). The pore size of the materials depends on the size of the template agent used. When the radius of the template agent is smaller than the pore size of the precursor, it can be easily incorporated into the precursor, thus limiting the pore shrinkage of the material during the reaction process. After the reaction, when the radius of the template agent is still smaller than the pore size of the synthetic material, the pore structure will remain after the template agent is removed, resulting in larger pore size of the material and further increasing its specific surface area and pore volume. Therefore, the template with a smaller pore diameter than the material should be selected.

Using different sizes of template agents will produce materials with different structures. Some synthetic materials have many mesopores, as well as slit pores formed by the accumulation of particles, which all can lead to an uneven distribution of pore sizes in the synthesized material and thus affect the structural parameters of the material. Therefore, the specific surface area, pore diameter, and pore volume of the same material synthesized with different templates are different. For instance, mesoporous alumina was prepared using cetyltrimethylammonium bromide (CATB), sodium laurate (CA), and poly (propylene oxide)-Poly (ethylene

oxide)-Poly (propylene oxide) (PPO-PEO-PPO, P123) as template agents, respectively (Bo and Jing, 2007); aluminosilicate mesoporous materials were synthesized using cetyltrimethylammonium bromide (CTAB), diethylenetriamine (DETA), sodium carboxymethylcellulose (CMC), sodium dodecyl sulfate (SDS), and polyethylene glycol-polypropylene glycol-polyethylene glycol (PEO₈₀-PPO₃₀-PEO₈₀, F68 and PEO₁₃₃-PPO₅₀-PEO₁₃₃, F108) as template agents correspondingly (Ma et al., 2020); and silica spheres were prepared using pluronic triblock copolymer (EO₁₀₆PO₇₀EO₁₀₆, F127), F127, and PEG respectively as template agents (Yang et al., 2006).

3.1.2 Effect of Template Agent Concentration on Pore Structure

The concentration of the template agent also has a large effect on the specific surface area, pore volume, and pore size of the synthetic material. As the concentration of the template agent increases, the average pore size of the material gradually increases, and the pore capacity also increases accordingly. Nevertheless, the change in specific surface area is related to the porosity of the synthetic material, so for different synthetic materials, the specific surface area has a different change pattern of the change in mass concentration.

For example, the use of polyethylene glycol (PEG) and/or cetyltrimethylammonium chloride (CTAC) as templates enables the preparation of mesoporous titanium dioxide (**Table 2**). It was shown that with the increase of CTAC and PEG concentration, the specific surface area, average pore size,

TABLE 2 | Structural parameters of the samples synthesized with different concentrations of templates.

Template agent	Concentrations (g/ml)	Specific surface area (m²/g)	Pore volume (cm ³ /g)	Average pore size (nm)	References
PEO ₁₃₃ -PPO ₅₀ -PEO ₁₃₃ (F108)	0.01	297.6	0.23	6.0	Ma et al. (2020)
	0.02	269.8	0.25	6.4	
	0.03	237.6	0.26	7.2	
	0.04	204.6	0.27	11.7	
Cetyltrimethylammonium chloride (CATC)	0	38.6	0.063	5.2	Yusuf et al. (2003)
	0.001	54.2	0.078	4.6	
	0.01	56.6	0.088	5.0	
	0.05	72.8	0.13	7.6	
	0.1	83.8	0.17	9.0	
Polyethylene glycol (PEG)	0.01	27.8	0.041	4.8	
	0.05	47.3	0.067	4.6	
	0.1	57.1	0.094	8.4	

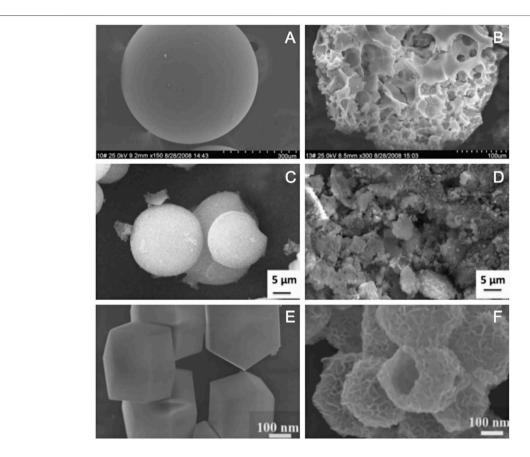


FIGURE 6 | SEM images of D311 resin (A) and PCTOM (B) (Zhang et al., 2011); SiO₂ (C) and Fe₂O₃/SiO₂ composite monoliths (D) (Singh et al., 2018); ZIF-67 (E) and NiCo-LDH (F) (Hu et al., 2019).

and pore volume of the gel increased. These structural parameters of gels prepared from CTAC solution (TS-0.1), gels prepared from PEG solution (TP-0.1), and dry gels prepared from CTAC and PEG were higher than those without additives (TiO₂-0), and the specific surface area and pore size of TS-0.1 were even about twice as large than those of

 ${
m TiO_2}$ -0 (Yusuf et al., 2003). The average pore size and pore volume of the silica-aluminate mesoporous material synthesized using F108 as a template agent gradually increased with increasing mass concentration of F108, but the specific surface area gradually decreased (Ma et al., 2020).

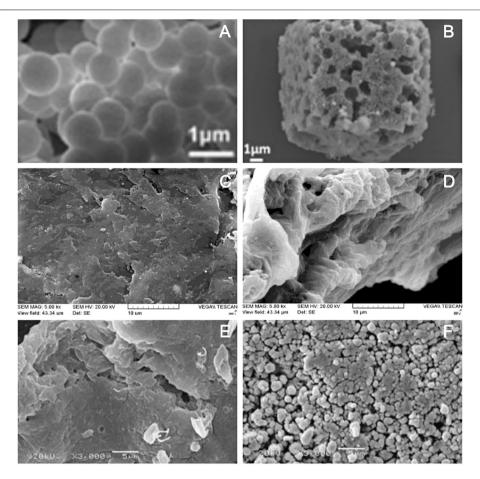


FIGURE 7 | SEM images of carbon sphere (A) and DP Mn₂O₃-carbon-PVP cubes (B) (Shao et al., 2017); CTS (C) and TCCTS (D) (Dai et al., 2012); NSC (E) and crosslinked NSC resin (F) (Sun et al., 2007).

3.2 Morphology Tuning

The introduction of template will change the microstructure of materials. Different template agents will get different structures, such as porous structure, worm-like structure, core-shell structure, etc. As the mass transfer of contaminants within an adsorbent is largely dependent on the pore structure of the material, this section will focus on porous materials, which are subdivided into disordered and ordered pore structures.

3.2.1 Disordered Porous Structure

The template method is mainly used to make the porous structure on the surface of materials or to make the surface rough. In some cases, the porous structure is disordered. Considering the template to be the skeleton, the material with pore structure can be obtained by solution etching, for example, using D311 resin as the template skeleton to synthesize porous nano-calcium titanate microspheres (PCTOM). The D311 resin is a sphere with a smooth surface (**Figure 6A**); the surface of the synthesized material became rough and disordered porous structure was obtained (**Figure 6B**; Zhang et al., 2011). SiO₂ is a spherical particle with smooth surface (**Figure 6C**). Considering it to be the template skeleton and introducing the precursor Fe_2O_3 , the

Fe₂O₃/SiO₂ composite monoliths with rough surface and pore structure can be obtained (**Figure 6D**; Singh et al., 2018). Zeolitic imidazolate framework-67 (ZIF-67) is a dodecahedral structure with a smooth surface (**Figure 6E**), which is used as a template skeleton to synthesize hierarchical porous Ni/Co-layered double hydroxide (NiCo-LDH), and the NiCo-LDH is a hollow dodecahedron with porous structure (**Figure 6F**; Hu et al., 2019).

The disordered porous material with rough surface can also be obtained by using porous material as the precursor, meanwhile, taking it as skeleton and introducing template into its pores. The carbon spheres are smooth spheres (**Figure 7A**) and when used as templates for the synthesis of double porous Mn₂O₃ (DP Mn₂O₃-carbon-PVP) cube, the carbon spheres embedded the precursor well and the final material with rough surface and porous structure was obtained (**Figure 7B**; Shao et al., 2017). The surface of the chitosan (CTS) is relatively smooth and the structure is compact (**Figure 7C**). After introducing the template Fe(III), the surface of the thiourea cross-linked chitosan (TCCTS) obtained is rough and the structure is incompact and reticular with disordered pore structure (**Figure 7D**; Dai et al., 2012). Crosslinked NSC resin was

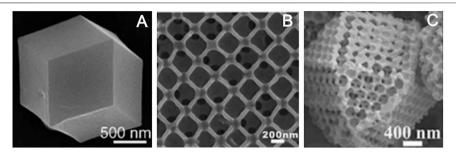


FIGURE 8 | SEM images of ZIF-8 (A) (Salunkhe et al., 2016); HKUST-1 (B) (Wu et al., 2011); and SOM-ZIF-8 (C) (Shen et al., 2018).

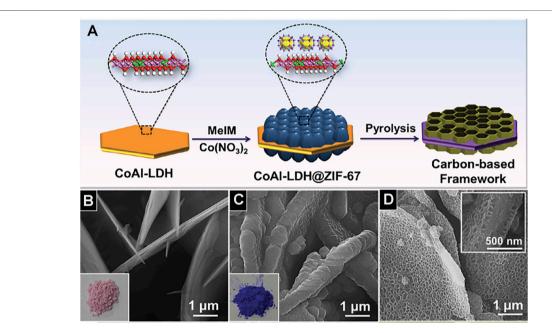


FIGURE 9 (A) Schematic illustration for the synthesis of porous carbon-based framework. SEM images of CoAl-LDH (B), CoAl-LDH@ZIF-67 (C), and LDH@ZIF-67-800 (D) (Li et al., 2016).

synthesized with N-succinyl-chitosan (NSC) as the precursor skeleton and Cu (II) as a template agent. After the introduction of template, the surface structure of crosslinked NSC resin was denser than that of NSC and has a porous structure (**Figures 7E,F**; Sun et al., 2007).

3.2.2 Ordered Porous Structure

Template method can also construct the ordered porous structure. Metal-organic framework polymer is one of the most typical examples, although different templates will get different structural materials, they almost have ordered pore structure. For instance, metal-organic frameworks (MOFs) ZIF-8 synthesized by the template-free method has a dodecahedral shape, but without porous structure (**Figure 8A**; Salunkhe et al., 2016). Using polystyrene (PS) as a template agent, MOFs precursor solution was introduced to infiltrate the template. After removing the template, HKUST-1 crystal was

obtained. HKUST-1 has three-dimensionally ordered and interconnected macropores (**Figure 8B**; Wu et al., 2011). PS has adjustable and stable morphology in methanol solution (MeOH). After the precursor infiltrates the template PS, it exposed the precursor@PS to NH₃/MeOH solution and SOM-ZIF-8 with three-dimensionally ordered macropores can be obtained (**Figure 8C**; Shen et al., 2018). Using CoAl-layered double hydroxide (CoAl-LDH) as a template skeleton, and introducing ZIF-67 to synthesize CoAl-LDH@ZIF-67, the final material LDH@ZIF-67-800 was obtained after the removal of the template by pyrolysis and the synthetic path is shown in **Figure 9A**. LDH@ZIF-67-800 is a surface ordered porous structure (**Figure 9C**; Li et al., 2016).

In addition to MOF materials, ordered porous structures can also be obtained for some other templated materials. For example, using nanoporous anodic alumina (NPAA) as the template skeleton, the synthesized carbon nanotube arrays have a highly

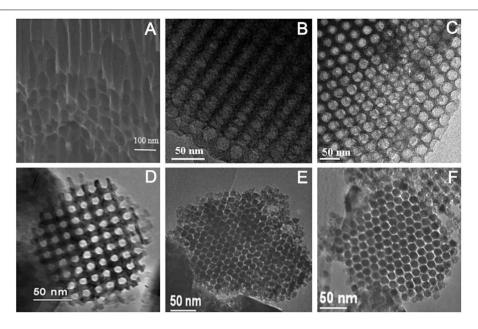


FIGURE 10 | SEM images of S of CNTs arrays/NPAA composite membrane (A) (Mohajeri et al., 2017); TEM images of C-FDU-18-800 (B) and Si-FDU-18-HC (C) (Deng et al., 2007); Cr_2O_3 (D), (Jiao et al., 2005), Ir_2O_3 (E), and Co_3O_4 (F) (Yue and Zhou, 2007).

ordered pore structure (Mohajeri et al., 2017; **Figure 10A**). The mesoporous carbon (C-FDU-18-800) and mesoporous silica (Si-FDU-18-HC), synthesized using poly (ethylene oxide)-b-polystyrene (PEO-b-PS) diblock copolymers as templates, have highly ordered mesoporous structures (**Figures 10B,C**; Deng et al., 2007). Similarly, metal oxides such as Cr_2O_3 (**Figure 10D**; Jiao et al., 2005), In_2O_3 (**Figure 10E**), and Co_3O_4 (**Figure 10F**; Yue and Zhou, 2007), synthesized with mesoporous silica as the template skeleton, all have regular mesoporous structures.

4 APPLICATION TO TYPICAL POLLUTANTS IN WASTEWATER

Current research on templated materials as adsorbents is focused on two types of pollutants, namely dyes and heavy metals. As mentioned above, the template method can effectively modulate the morphological and structural parameters such as pore size, pore volume, and specific surface area of materials, which are the direct factors affecting the adsorption performance. In addition to enormous specific surface area and rich pore structure, the introduction of templates to modulate the surface functional groups and charges can achieve significant improvements in the adsorption performance of the target pollutants.

4.1 Heavy Metals

Heavy metals in water, even at very low concentrations, are extremely harmful to humans and the ecology. Currently, templated materials have been widely used for the adsorption of heavy metal ions in water like Ni(II), Co(II), Cu(II), Cr(III), Pb(II), etc., and have exhibited relatively outstanding adsorption

capacities (Table 3). For example, using attapulgite (ATP) as a template agent, a novel polyaniline/attapulgite (PANI/ATP) material can be obtained by oxidative composite polymerization. The PANI/ATP exhibited an excellent adsorption capacity for Hg(II) (824 mg/g) (Cui et al., 2012), which was much higher than those of PANI (600 mg/g) (Wang et al., 2009)- amine resins (156-556 mg/g) (Zhu and Alexandratos, 2005; Alexandratos, 2007), aniline-msulfophenylenediamine copolymer (PANSP) (498 mg/g) (Lü et al., 2007), chitosan beads (323 mg/g) (Li et al., 2005), and mercaptopropyl mesoporous adsorbent (461 mg/g) (Brown et al., 2000). Using SiO₂ monoliths as a template agent to synthesize metal oxide monoliths (Fe₂O₃/SiO₂), the Fe₂O₃/SiO₂ demonstrated high adsorption capacities for Pb(II) (850 mg/g) and Cr(III) (770 mg/g) (Singh et al., 2018), which were much higher than those of Fe₂O₃ monoliths (166 mg/g) (Singh et al., 2018), carbon coated monoliths (72 mg/g) (Teoh et al., 2013), and mesoporous silica (184 mg/g) (Awual and Hasan, 2014) for Pb(II), and those of Fe₂O₃ monoliths (125 mg/g) (Singh et al., 2018), modified lignin (68 mg/g) (Demirbaş, 2005), and borax sludge (16 mg/g) (Senberber et al., 2017) for Cr(III).

4.1.1 Factors Affecting the Adsorption of Heavy Metals by Templated Materials

Like conventional adsorbents, adsorbents prepared by the template method are also mainly influenced by factors such as pH and temperature.

Solution pH is one of the most critical factors affecting the adsorption of heavy metal ions by templated materials. Normally, as the pH increases, the proton concentration decreases and the adsorption of heavy metal ions increases accordingly. Nevertheless, when the solution is in an alkaline environment,

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TABLE 3 | Properties of various template materials and their ability to adsorb heavy metals.

Samples	Template agent	Surface area (m²/g)	Adsorbate	Adsorption capacity (mg/g)	Equilibrium time (min)	рН	Kinetics	Thermodynamics	Isotherms	Cycle numbers	References
C _{KIT-6}	KIT-6	821	Ni(II) Co(II)	145 148	_ _	5	Pseudo second order	Spontaneous and endothermic	Langmuir	_	Marciniak et al. (2019)
Fe ₂ O ₃ / SiO ₂	SiO ₂	562	Cd(II) Cr(III) Pb(II)	690 770 850	120	6	Pseudo second order	Spontaneous and exothermic	Freundlich and Langmuir	_	Singh et al. (2018)
CF-S-N	SiO ₂	-	Cu(II) Mn(II) Cd(II) Pb(II)	197 195 187 183	200	7	Pseudo second order	Spontaneous and endothermic	Langmuir	_	Ren et al. (2017)
PANI/ATP	ATP	95	Hg(II)	824	200	6	Pseudo second order	Spontaneous and endothermic	Langmuir	5	Cui et al. (2012)
MCMs	SiO ₂	682	U(VI)	294	120	4	Pseudo second order	Spontaneous and endothermic	Langmuir	5	Zhang et al. (2017)
NSHS	CaCO ₃	_	Pb(II)	267	-	_	Pseudo second order	Spontaneous and endothermic	Langmuir	-	Manyangadze et al. (2020)
MP-Silica	Citric acid	504	Ag(I)	115	30	1–7	Pseudo second order	_	Langmuir	_	Pongkitdachoti and Unob (2018)
C _{ST}	F127	426	Ni(II) Co(II)	126 135	_ _	5	Pseudo second order	Spontaneous and endothermic	Langmuir	_	Marciniak et al. (2019)
PCTOM	D311 resin	_	Pb(II) Cd(II) Zn(II)	30 30 15	142 18 24	6	Pseudo second order	Spontaneous and endothermic	Langmuir	_	Zhang et al. (2011)
TP- CMCBs	CaCO ₃	53	Cu(II) Mn(II) Ni(II)	342 262 243	30 30 30	6	Pseudo second order	_	Langmuir	5	Liu et al. (2021)
MSC	CTMAB- MA	239	Ni(II) Cu(II) Zn(II) Pb(II) Mn(II) Cd(II)	278 390 402 452 201 438	80 30 80 40 110 60	5–7.5	Pseudo second order	Spontaneous and endothermic	Langmuir	2	Liu et al. (2020)
TCCTS	Fe(III)	_	Fe(II) Fe(III)	48 72	60	5	Pseudo second order	_	Langmuir	-	Dai et al. (2012)
NiCo-LDH	Ni(NO ₃) ₂	267	Cr(VI)	100	50	_	Pseudo second order	_	Langmuir	5	Hu et al. (2019)
MSNs	CTAB	675	Fe(III)	21	50	_	Pseudo second order	-	Langmuir	4	Meng et al. (2018)

hydroxyl ions form precipitates of hydroxides with metal ions, resulting in a decrease in the adsorption capacity of the adsorbent. For example, as the pH value of the solution is increased from 1 to 5, the adsorption capacity of both Fe(II) and Fe(III) by the thiourea crosslinked-chitosan (TCCTS) synthesized with iron (III) as a template agent gradually increased, and thereby reaching a maximum at pH = 5. In the higher pH range, the adsorption capacity of TCCTS decreases sharply (Dai et al., 2012).

Temperature is also one of the important factors affecting the adsorption of heavy metal ions in solution, as it mainly affects mobility and chain flexibility of metal ions, resulting in an increase in the adsorption capacity of the adsorbent with increasing temperature. For example, as temperature was increased from 25 to 55°C, the adsorption capacity of Cu(II) by the templated material CF-S-N increased from 196 mg/g to 199 mg/g. The adsorption of Cu(II) by polyacrylamide/functionalized multi-walled carbon nanotube PAAm/FMWCNTs) composites (Abo-Zahra et al., 2021) and the adsorption of Ni(II) and Co(II) by ordered mesoporous carbon (Marciniak et al., 2019) show this trend.

Furthermore, the adsorption kinetics of the adsorbent synthesized by template method fit the pseudo-second-order kinetic model, indicating that chemisorption primarily promotes the adsorption of heavy metal ions. The relevant thermodynamic parameters were calculated to confirm that the adsorption process is spontaneous and endothermic for most of the adsorbents. And the adsorbents all fit more closely to the Langmuir adsorption model, therefore the adsorption of heavy metal ions onto the synthesized adsorbents can be considered as a monolayer adsorption process.

4.1.2 Mechanisms of Heavy Metal Adsorption

As mentioned in the previous section, the introduction of a template agent can effectively regulate the specific surface area, pore diameter, and pore volume of materials and change the microscopic morphology of materials, all of which provide the possibility to improve the adsorption performance of the material. On the one hand, the pore structure constructed by the template method can provide wider diffusion channels and lower mass transfer resistance, which facilitates the rapid diffusion of heavy metal ions in the internal structure of the adsorbent. On the other hand, the large specific surface area and pore size distribution formed by the template method provide more active sites for the adsorbent. For instance, mesoporous carbon (MCMs), synthesized using ordered mesoporous silica as a template agent, has a specific surface area of 682 m²/g (Zhang et al., 2017), which is higher than other carbon-based nanomaterials such as graphene oxide supported polyaniline (141 m²/g) (Sun et al., 2013) and carbonaceous nanofibers (264 m²/g) (Sun et al., 2016). Correspondingly, MCMs have a good adsorption property for U(VI) of 294 mg/g, which is also higher than that of graphene oxide-supported polyaniline (245 mg/g) and carbonaceous nanofibers (125 mg/g) (Table 3).

For templated materials, in addition to the pore adsorption mechanism, ion exchange, electrostatic interaction, and surface complexation are also the predominant adsorption mechanisms of heavy metals. The introduction of templates can alter the surface chemistry of the materials, providing favorable ions and functional groups for adsorption, as well as altering the surface charge properties of the material, all of which contribute to the adsorption performance of the material. For instance, templated material mesoporous carbons (MCMs) containing a large number of oxygenated functional groups such as -OH and -COOH have good adsorption properties for cationic heavy metals such as U(VI) (Zhang et al., 2017). For materials with an intrinsic surface charge that is less conducive for the adsorption of ions, for example, natural attapulgite (ATP), which has negatively charged functional groups on its surface and does not have electrophoretic mobility equal to zero, was used as a template agent to polymerize aniline, the obtained polyaniline/attapulgite (PANI/ATP) exhibits a point of zero charge and achieved a maximum adsorption capacity of Hg(II) over 800 mg/g (Cui et al., 2012). After the introduction of the template, the positively charged hierarchical porous Ni/Colayered double hydroxide (NiCo-LDH) hollow dodecahedra exhibiting excellent adsorption properties for the negatively charged Cr(VI) ions in aqueous solution, and the NO- 3 ions which initially on the surface of the NiCo-LDH were replaced by Cr(VI) ions after adsorption (Hu et al., 2019; Table 3).

4.2 Dyes

Wastewater discharged from the printing, electroplating, textile, and leather industries contains large amounts of toxic and nonbiodegradable dyes that have an irreversible effect on humans and the environment. The use of templated materials for the adsorption of dyes such as bisphenol A, rhodamine B, and methylene blue in wastewater exhibit better adsorption properties than the most conventional adsorbents. For example, Al₂O₃ hollow microspheres (AHS) adsorbed as much as 690 mg/g of Congo Red (Tian et al., 2016). Its adsorption performance outperformed many other metal oxide adsorbents such as Co₃O₄-Fe₃O₄ hollow spheres (123 mg/g) (Wang X. et al., 2011), NiO nanospheres (440 mg/g) (Zhu et al., 2012), and MgO-MgFe₂O₄ composite (498 mg/g) (Han et al., 2014). The new hollow polydopamine microcapsules (H-PDA-MCs) showed a capacity of 179 mg/g for methylene blue (Feng et al., 2021), exceeding that of PDA microspheres (91 mg/g) (Fu et al., 2015), palm kernel fibres (95 mg/g) (El-Sayed, 2011), and magnetic γ- Fe₂O₃/SiO₂ (116 mg/g) (Chen et al., 2016).

4.2.1 Factors Affecting the Adsorption of Dyes by Templated Materials

The solution pH value is regarded as one of the most important factors affecting the adsorption of organic dyes. In general, the adsorption of anionic dyes increases with decreasing pH, while the opposite is true for cationic dyes. For anionic dyes, competition between OH⁻ and anionic dyes for adsorption is intense in the high pH range, while at low pH, the hydroxyl and carboxyl groups will be protonated to form -OH+ 2 groups, strengthening the electrostatic gravitational force between the adsorption site and the anionic dyes. For example, poly (acrylamide-acrylic acid-dimethylaminoethyl methacrylate) P(AAm-AA-DMAEMA) resin is effective for the adsorption of indigo carmine and eriochrome black-T anionic dyes, and the

TABLE 4 | Properties of various template materials and their ability to adsorb organic pollutant.

Sample	Template agent	Surface area (m²/g)	Adsorbate	Adsorption capacity (mg/g)	Equilibrium time (min)	рН	Kinetics	Isotherms	Cycle numbers	References
DP Mn ₂ O ₃ -carbon-PVP	Carbon spheres	37	Congo Red	126	20	-	Pseudo second order	Langmuir	4	Shao et al. (2017)
AHS	CaMg(CO ₃) ₂	318	Congo Red	690	120	5–6	Pseudo second order	Langmuir	_	Tian et al. (2016)
MWCNTs@ carbon	MWCNTs	_	Methylene Blue Crystal Violet	298 228	120	8–9	Pseudo second order	Langmuir	_	Liu et al. (2015)
CNTs	Pal	887	Congo Red Methyl Orange	468 253	30	1–13	Pseudo second order	Langmuir	_	Zhong et al. (2019)
CMK-3	CMK	1420	Bisphenol-A	474	20	6	Pseudo second order	Freundlich	_	Libbrecht et al. (2015)
TNC	MCM-22	660	Amoxicillin Ethinylestradiol	69 61	_	-	_	Langmuir	_	Barrera et al. (2014)
NMCS	SiO ₂	789	Methyl Orange	352	200	2	Pseudo second order	Langmuir	5	Jiao et al. (2017)
3D-HPGF	PMMA	486	Methylene Blue	70	25	_	Pseudo second order	Langmuir	5	Liu et al. (2018)
P (AAm-AA- DMAEMA)	PAAm	_	Indigo Carmine Eriochrome Black-T		120	2.5	Pseudo second order	Freundlich	_	Abdel-Aziz and Siyam, (2011)
SMC	SMC	476	Bisphenol-A	154	60	1–7	Pseudo second order	Freundlich	_	Libbrecht et al. (2015)
S-2	Rape pollen	41	Congo Red	97	120	_	Pseudo second order	Langmuir	_	Zhao et al. (2017)
OMCs	F127	424	Rhodamine B	_	240	5	Pseudo second order	_	-	Cao et al. (2014)
C-V-50-T- 50-600	PEO- PBO-PEO	810	Lysozyme	446	-	-	-	Langmuir	-	Wickramaratne and Jaroniec (2013)
NiCo-LDH	Ni(NO ₃) ₂	267	Congo red	909	80	-	Pseudo second order	Langmuir	5	Hu et al. (2019)

property of adsorption decreases with increasing pH (Abdel-Aziz and Siyam, 2011). The adsorption of methylene blue and crystalline violet by the MWCNTs@carbon with negative surface charge was low in acidic solutions and increased significantly with increasing pH (Liu et al., 2015).

However, unlike the templated materials for the adsorption of heavy metal ions, the templated materials for the adsorption of dyes are either endothermic or exothermic processes, resulting in different trends in their temperature dependence. For example, as the temperature increases, the adsorption of amorphous carbon nanotubes (ACNTs) increases (Zhong et al., 2019) while the

adsorption of P(AAm-AA-DMAEMA) resin decreases (Abdel-Aziz and Siyam, 2011).

As can be seen from **Table 4**, the organic dye molecules almost always conform to the quasi-secondary kinetic model on the template materials. Unlike the adsorption of heavy metal ions, while the adsorption isotherms of most of the template materials conform to the Langmuir model, a few conform to the Freundlich model, indicating that for the adsorption of dyes, in addition to monolayer adsorption, multilayer adsorption can occur within the pore channels of a small number of template materials.

4.2.2 Mechanisms of Dye Adsorption

The excellent performance of the templated materials for dyes is partly attributed to the porous structure and high specific surface area. The porous structure and high specific surface area facilitate the exposure of more active sites, thus promoting the diffusion of dye molecules, that is, the efficient adsorption of dyes through adsorption and the filling of pore channels. Dual-porous Mn₂O₃ (DP Mn₂O₃-carbon-PVP) cubes have a specific surface area of 37 m²/g and the mesopore size of 24 nm, higher than that of the Mn₂O₃-Ncarbon prepared without polyvinylpyrrolidone (PVP) (22 m²/g, 23 nm) and without carbon sphere templates (15 m²/g, 4 nm). Comparing their sorption rates to Congo Red, DP Mn₂O₃carbon-PVP had a sorption capacity of 126 mg/g, but 64 mg/g and 112 mg/g for Mn₂O₃-Ncarbon and Mn₂O₃-carbon (Shao et al., 2017). ACNTs have a high specific surface area of 877.09 m²/g, which is much higher than that of raw Pal $(181.14 \text{ m}^2/\text{g})$, H-Pal $(157.50 \text{ m}^2/\text{g})$, Pal@C $(103.41 \text{ m}^2/\text{g})$. The maximum adsorption of Congo Red by ACNTs (358 mg/g) was more than 20-fold times that of raw Pal, and nearly 14-fold higher than that of H-Pal and Pal@C (Zhong et al., 2019; Table 4).

In addition to the structure of the material, electrostatic interactions and π - π electron coupling interactions are also important mechanisms for the adsorption of dyes. For instance, the adsorption processes of nitrogen-doped mesoporous carbon spheres (NMCS) on methyl orange (Jiao et al., 2017) and ACTNs on Congo red (Zhong et al., 2019) are electrostatic attraction and π - π electron coupling, respectively, while the adsorption processes of hollow polydopamine microcapsules (H-PDAMCs) on methyl blue involve both electrostatic interaction and π - π stacking mechanisms (Feng et al., 2021). However, for materials with an intrinsic charge, the adsorption performance can be unsatisfactory due to electrostatic repulsion between the functional group of the dye and the functional group of the material. The introduction of template to adjust its surface charge can effectively improve this problem. For example, the large number of oxygen-containing functional groups such as -OH and -COOH generated on the surface of MWCNTs@carbon nanocables provides an abundance of active sites for positively charged dyes compared to the original MWCNTs (Zhang et al., 2017). The zero charge of Al₂O₃ is close to 9, using it as a template agent, the obtained alumina hollow microspheres (AHS) still have a high adsorption capacity for Congo Red when the initial solution pH is beyond 10 (Tian et al., 2016; **Table 4**).

5 CONCLUSIONS AND PERSPECTIVES

Based on the properties and spatial domain-limiting capability of templates, this study introduces the types of templates and their synthetic routes, and the regulation behavior of materials by template method and its application in the adsorption of typical pollutants in wastewater has been reviewed. In comparison, hard templates are more stable and allow for precise regulation of material size and structure, but hard

templates are often difficult to remove and can easily cause structural damage to the raw material after removal, while soft templates are easy to construct and have relatively mild experimental conditions and allow for the synthesis of different materials with different morphologies, but soft templates are less stable and less efficient. The behavior of the template method in modulating the morphological structure of the materials was further discussed and it was found that the adsorbents prepared by the template method had a high specific surface area and abundant pores and were able to successfully construct pore channel structures. The type and concentration of the template agent are found to be the most crucial factors affecting the morphology of the final product. Therefore, in practice, the most suitable template should be selected according to the performance requirements of the target product and the reaction conditions.

The large specific surface area and porous structure of the templated materials offer the possibility of efficient adsorption of heavy metal ions and dyes. The adsorption mechanism for heavy metal ions includes ion exchange, electrostatic interaction, and complexation, while electrostatic interaction, π - π electron stacking, and hydrogen bonding are possible for dyes. The application of templated materials as effective adsorbents in wastewater and their adsorption mechanisms are still at the research stage. Moreover, during the preparation process of templated materials, the removal of the template may lead to the collapse of the pore structure. Optimization of the textural properties and attention to the removal conditions are desired to ensure the effective diffusion of pollutants within the adsorbent.

Templated materials have good application prospects in removing pollution in wastewater. However, templated materials have been less studied for contaminants such as nutrients, biomolecules, and complex pollutants, and further research into the regeneration and desorption properties of adsorbents is required to achieve large-scale commercial use of templated materials.

AUTHOR CONTRIBUTIONS

HL summarized and wrote the article under the guidance of LW. All authors contributed to the conceptualization and editing of the article and commenting on and reviewing the manuscript.

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Ultrasonic-Assisted Synthesis of CdS/Microcrystalline Cellulose Nanocomposites With Enhanced Visible-Light-Driven Photocatalytic Degradation of MB and the Corresponding Mechanism Study

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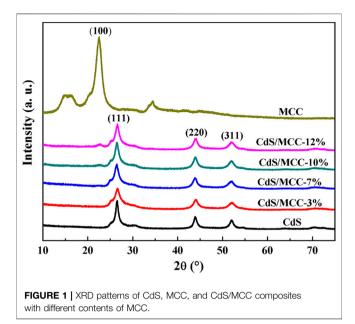
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A simple and efficient ultrasonic-assisted approach was designed to synthesize CdS/microcrystalline cellulose (MCC) nanocomposite photocatalyst. The obtained products have been characterized by XRD, FE-SEM, TEM, UV-Vis DRS, and nitrogen adsorption isotherms. The results showed that the intimate contact of MCC and CdS is beneficial for enhancing the photocatalytic performance because heterojunction formation can efficiently promote the separation of photogenerated electrons and holes of the nanocomposite photocatalyst. By using 10% MCC coupled CdS, the decoloration rate of methylene blue (MB) in the solution under visible-light was increased nearly 50%. In addition, the reuse experiments confirmed that the CdS/MCC nanocomposite photocatalyst had outstanding cycle performance and durability. Mechanism study demonstrated that hydroxyl radicals, photogenerated holes and superoxide radicals were the active species in the photocatalytic oxidization degradation of MB.

Keywords: cds, microcrystalline cellulose, visible-light photocatalysis, MB decolorization, charge separation

INTRODUCTION

Since TiO_2 as a photocatalytic material for water decomposition in 1972, photocatalysis has attracted great interest and is recognized as a promising strategy for treating pollutants because it is highly effective, low cost and environmentally friendly (Liu et al., 2021; Mohua Li et al., 2020b; Ren et al., 2022; Fang Li et al., 2020). In view of the drawbacks of TiO_2 (especially it can only utilize ultravioletlight from the Sun) (Sheng et al., 2020; Ni et al., 2021; Jiang et al., 2020), narrow bandgap visible-light-active semiconductors such as BiOBr, BiOI, SnS₂, CdS, g-C₃N₄, etc. have been increasingly studied as photocatalysts and their photocatalytic mechanisms have been explored in numerous published works (Yang et al., 2018; Wei et al., 2017; Silva-Gaspar et al., 2022; Liu et al., 2020; Beyhaqi et al., 2021). For developing efficient visible-light-active photocatalyst, CdS is one of the extensively studied semiconductor materials because its bandgap matches well with the spectrum of visible light



(Cheng et al., 2018; Liu et al., 2021). However, the photocatalytic efficiency of CdS is fairly poor by reason of the fast recombination of photo-generated holes and electrons (Gurugubelli et al., 2022). Additionally, CdS nanoparticles are prone to encounter photocorrosion, namely, the surface sulfide ions can be oxidized to sulfur by photogenerated holes under the irradiation (Ning and Lu, 2020). In consideration of that photocatalytic reactions occur on the surface of CdS, necessary modifications are needed to stabilize the surface sulfide ions and to transfer the photogenerated holes out from the surface in order to suppress photocorrosion (Jiang et al., 2021). Many measures have been devoted to improving the photocatalytic efficiency and inhibiting the photocorrosion of CdS, like changing the surface structure of CdS nanoparticles by controlling morphology (Liu et al., 2021), doping with noble metal (Nawrot et al., 2020), combining with other semiconductors or organic polymers (Kiani et al., 2020). Among all the modification measures, combining with organic substances (especially conjugated polymers) shows great advantages owing to their excellent characteristics (Zhang et al., 2020). Polymers can provide a suitable cyberspace so as to limit the continuous growth of crystalline grain and prevent the particle aggregation. Moreover, the high stability, simple synthesis and good environmental compatibility of polymers are helpful for practical application (Chen et al., 2020; Zeng et al., 2021). Besides, the CdS/conjugated polymer nanocomposites possess better machinability and optical performance (Lee and Chang, 2019; Melinte et al., 2019).

Cellulose, as one of renewable resources on the Earth and the most abundant natural polymers (Tian Li et al., 2021), has been widely investigated as a modifier for semiconductors because of its distinctive properties, including biocompatibility, biodegradation, mechanical strength, and chemical stability (Jiang et al., 2019). Microcrystalline cellulose (MCC) is a kind of common organic conjugated polymers, which was obtained by

purifying and depolymerizing cellulose. It possesses a lot of properties that eligible for modifying semiconductors, such as large surface area for interaction with water, water insolubility, high water absorption and retention capacity, good blinding nature, remarkable ability to prevent phase separation (Zhou et al., 2019; Amaly et al., 2022). Because of the above advantages, MCC has been considered as a promising material to modify semiconductor photocatalysts for enhanced water purification performance.

In this work, a simple and efficient ultrasound approach was designed to synthesize CdS/MCC nanocomposites. The photocatalytic activity of the products was tested based on the decoloration of MB aqueous solution under visible-light. The degradation mechanism of MB over CdS/MCC nanocomposite was also explored.

MATERIALS AND METHODS

Materials

Microcrystalline cellulose (MCC), $Cd(CH_3CH_2O)_2 \cdot 2H_2O$, thioacetamide (TAA), PVP (MW = 40,000 g/mol), methylene blue (MB), 1, 4-benzoquinone (BQ), triethanolamine (TEOA), and isopropanol (IPA), coumarin (COU) nitroblue tetrazolium (NBT), and ethanol were bought from Sinopharm Chemical Reagent Co., Ltd. The reactants and solvents were analytical grade and used with no further purification. Ultrapure water (resistivity 18.2 M Ω cm) was used in this study.

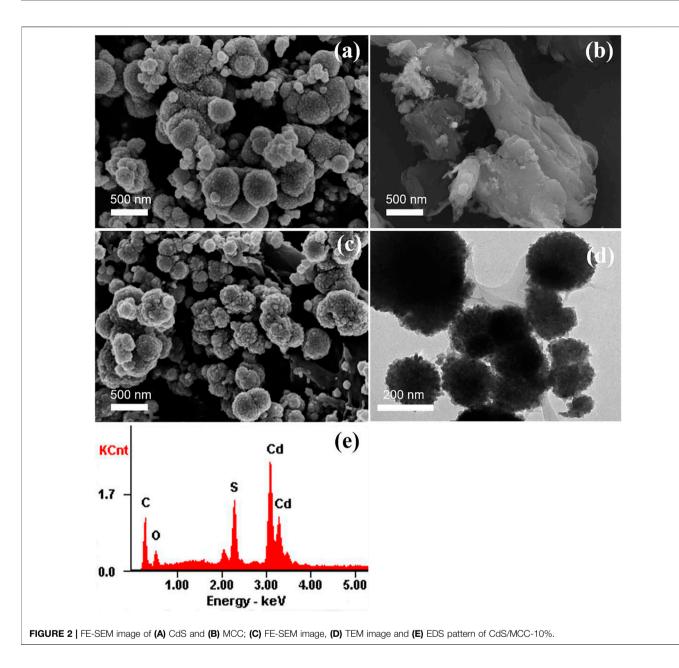
Preparation of CdS/MCC Nanocomposites

The synthesis was conducted in SK3210HP 53 kHz Ultrasonic Cleaner (Shanghai KUDOS Ultrasonic Instrument Co., Ltd.). 0.2 g PVP and 0.1–0.5 g MCC were dissolved into 20 ml ethanol by sonication (18 W/cm²) for 30 min. Next 100 ml 0.28 mol/L Cd(CH₃CH₂O)₂·2H₂O aqueous solution was added and further ultrasonically treated for 30 min, subsequently 100 ml 0.2 mol/L TAA aqueous solution was introduced. Keep ultrasonic treatment for 3 h. The formed solid product was washed with ultrapure water and ethanol, then dried at 60°C for 12 h. Depending on the different MCC contents, the CdS/MCC composites were marked as CdS/MCC-3%, CdS/MCC-7%, CdS/MCC-10% and CdS/MCC-12%.

For comparison, CdS nanoparticles were synthesized according to the aforementioned procedures but in the absence of MCC.

Characterization of the Prepared Photocatalyst

The compositions and microstructures of the CdS/MCC nanoparticles were analyzed by X-ray diffractometer (XRD, D8, Germany Bruker), field emission scanning electron microscopy (FE–SEM, S4800, Japan Hitachiltd, accelerating voltage 15 kV), and transmission electron microscopy (TEM, JEM–2100UHR, Japanese electronics, accelerating voltage 200 kV). Compositional analysis was carried out by energy-dispersive X-ray analysis (EDS). Nitrogen sorption



measurements were performed with N_2 at 77 K after degassing the samples at 300°C under vacuum for 3 h using a Quantachrome Quadra orb SI-MP porosimeter. The specific surface area was obtained by using the Brunauer–Emmett–Teller (BET) model to analyze the N_2 adsorption equilibrium data. UV–Vis diffuse reflectance spectra (UV–Vis DRS) was performed by a UV–Vis spectrophotometer (UV–2600, Shimadzu Corporation).

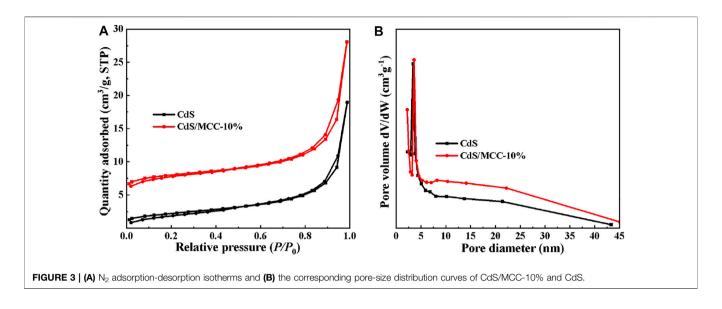
Photocatalytic Performance Tests

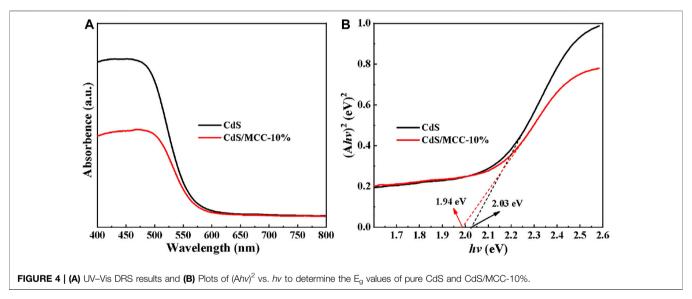
The photocatalytic performance of CdS/MCC nanocomposites synthesized were tested based on the degradation of MB in aqueous solution. 0.05 g CdS/MCC composites and 50 ml 10 mg/L MB solution were mixed by magnetic stirring for 30 min under dark condition to realize an adsorption/desorption equilibrium between

the organic dye and photocatalyst. The photoreactor comprises a Xe arc lamp (1000 W) with a 400 nm optical filter, a cold trap to prevent the temperature rise of the reaction solution, and a set of 80 ml capacity cylindrical quartz reactors (Beijing Precise Technology Co., Ltd., PL-02). At the given intervals of irradiation time, 4 ml solution was fetched and filtered through a 0.45 μm filter to get rid of the photocatalyst, then the absorbance of the supernatant was measured at the wavelength of 664 nm using a Shanghai Lengguang Technology Co., Ltd. GS54T UV–Vis spectrophotometer. The degradation efficiency (η) of MB was calculated using the following :

$$\eta = \frac{A_0 - A}{A_0} \times 100\% = \frac{C_0 - C}{C_0} \times 100\% \tag{1}$$

Where η = the decolorization efficiency, C = the MB concentration at a certain irradiation time, and C₀ = the MB





concentration at the dark environment adsorption-desorption equilibrium.

RESULTS AND DISCUSSION

Crystal Phase and Morphology Analysis

Figure 1 displays the XRD patterns of the synthesized CdS/MCC composites with different contents of MCC, CdS and MCC. Compared with the standard XRD peaks of cubic phase CdS (JCPDS file No. 800–0019) and hexagonal phase CdS (JCPDS file No. 800–0006), the synthesized CdS comprised a mixture of major cubic phase and minor hexagonal phase. The peaks at 2θ values of 26.5°, 44.0°, and 52.1° were in turn assigned to the (111), (220), and (311) planes of cubic phase CdS. The weaker peaks at 2θ values of 26.7° and 28.3° corresponded to the (111) and (101) planes of hexagonal phase CdS (Kong et al., 2022), respectively.

The XRD pattern of MCC showed sharp and high peaks, which revealed that the MCC itself has excellent crystallization. As for the various CdS/MCC composites, they display similar XRD spectra to mere CdS. Apparently, the XRD peaks of MCC did not appear in the XRD spectra of the CdS/MCC-3% and CdS/MCC-7% samples, which may be because that the minor amounts of MCC cannot be detected by the XRD equipment. When the MCC content is more than 10%, the significant (100) peak of MCC at a 2θ value of 22.5° begins to appear in the CdS/MCC composites. This confirmed that the MCC was successfully introduced to CdS and had formed CdS/MCC composites. Nevertheless, the introduction of MCC caused not shift of the XRD peak positions of CdS in the CdS/MCC composites, which suggested that MCC is not doped into the lattice of CdS nanocrystals.

The morphology, size and elemental compositions of the products were investigated using FE-SEM, TEM, and EDS. The

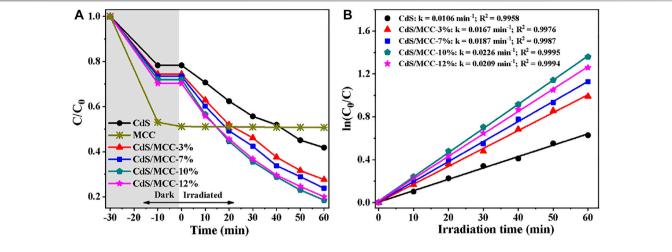
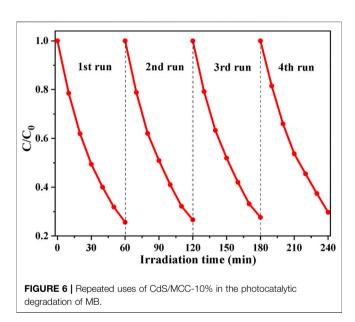
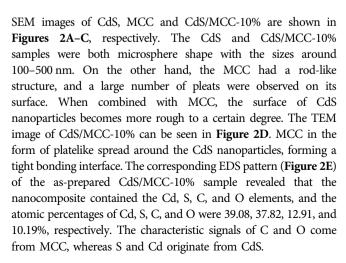


FIGURE 5 | (A) Adsorption and photocatalytic decolorization of MB over prepared photocatalysts; (B) Corresponding kinetics plots for the photocatalytic MB decolorization reactions in (A).





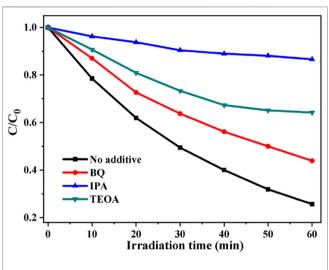


FIGURE 7 | Photocatalytic MB degradation by CdS/MCC-10% with the addition of different scavengers.

Nitrogen Adsorption Analysis

Nitrogen adsorption tests at 77 K were performed to examine the porosity of the samples of pure CdS and CdS/MCC-10%. The BET specific surface areas of pure CdS and CdS/MCC-10% were 7.89 and $10.26 \text{ m}^2/\text{g}$. **Figures 3A,B** show respectively the nitrogen adsorption-desorption isotherms and the corresponding pore-size distribution curves of the prepared products. The isotherms of the CdS/MCC-10% and CdS show similar hysteresis loops ranging at $P/P_0 = 0.8-1.0$ and 0.9-1.0, respectively, which match the type IV on the basis of the IUPAC classification (You et al., 2021). The pore-size distribution curves of both products show some disorder with the pore-size distribution from 3 to 30 nm.

UV-Vis DRS Spectra Analysis

The UV-Vis DRS results of our prepared pure CdS and CdS/MCC samples were used to analyze their optical absorption

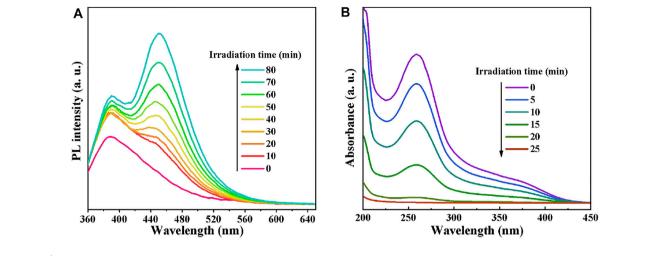
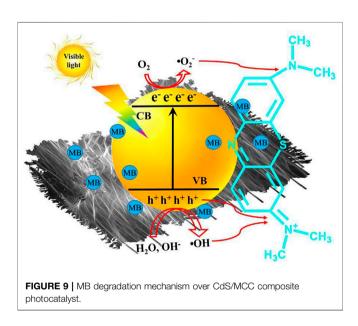


FIGURE 8 (A) PL intensities emitted by the mixture of CdS/MCC-10% and COU solution at different visible-light irradiation times; (B) The time-varying absorption spectra of NBT in the presence of CdS/MCC-10% and visible-light.



properties and bandgap energies. **Figure 4A** illuminates that both samples exhibit obvious absorption of 400–550 nm visible-light. The bandgaps of the two samples are procured according to the Tauc's plots in **Figure 4B** (Shkir et al., 2021). The determined $E_{\rm g}$ values of CdS and CdS/MCC are 1.94 and 2.03 eV, respectively. Compared with pure CdS, the narrower bandgap value of CdS/MCC-10% indicates that it can absorb a wider range of visible-light, which can be favorable for photocatalytic reactions (Zhao et al., 2021).

Assessment of Photocatalytic Activity of CdS/MCC Composites

The photocatalytic activities of all the products were assessed for MB degradation under visible-light ($\lambda > 400 \text{ nm}$)

irradiation for 60 min. Figure 5A and Figure 5B displays the degradation of MB photocatalyzed by pure CdS, MCC and CdS/MCC composites under visible-light. From tte figures, MCC has strong adsorption capacity for MB, but almost no photocatalytic effect. The photocatalytic performance of CdS/MCC composites (especially the CdS/ MCC-10% sample) improved significantly compared with CdS. When irradiated for 60 min, the CdS/MCC-10% sample has degraded 81.5% of the initial MB aqueous solution while the pure CdS degraded about 58.8%. When the MCC contents in the CdS/MCC composites were 3, 7, and 12%, the photodegradation rates of MB were lower than that over the CdS/MCC-10% sample. This suggests that MCC/CdS-10% had the highest visible-light photocatalytic activity compared with other CdS/MCC composites. Hence, there is an optimum MCC content for CdS/MCC composite to reach the most efficient visible-light photocatalysis. When the combined MCC was excess, the MCC sites may also function as photogenerated charge recombination centers. Accordingly, the excessive MCC sites can significantly reduce the amount of photogenerated charges and decrease the visible-light photocatalytic efficiency of CdS/MCC composites. Nevertheless, too less MCC content in the CdS/ MCC composites resulted in less active sites, which also decreased the photocatalytic efficiency. Besides, the MB adsorption by CdS/MCC nanocomposites improved compared with pure CdS, which is consistent with the result of Nitrogen adsorption analysis.

Photocatalytic Stability of Samples

For practical application, it is also important for the photocatalyst to have high photocatalytic stability (Ping Li et al., 2021). The photocatalytic stability of CdS/MCC-10% was further assessed in the MB decoloration reactions. The same photocatalytic process as above-mentioned was repeated for several times, but used 200 ml of MB and 200 mg of

photocatalyst. After every cycle of reactions, the photocatalyst was collected, washed and used again, meanwhile the initial concentration of MB was maintained by injecting the stock solution of MB. As **Figure 6** shows, the photocatalytic activity of CdS/MCC-10% had little decrease after the fourth run tests, which indicate that the CdS/MCC-10% photocatalyst is reusable for the environmental purification application.

MB Degradation Mechanism Over CdS/ MCC Composite Photocatalyst

To investigate the photocatalytic MB degradation mechanism by the CdS/MCC composite, the major reactive oxygen species involved in the degradation of MB were determined by free radical trapping experiments. The experimental procedure was the same as the photocatalytic activity test, but 50 ml of mixture of MB solution and scavenger, instead of 50 ml of MB solution was used. BQ (0.001 mol/L), TEOA (0.01 mol/L), and IPA (0.02 mol/L), were introduced into the reaction system as the scavengers for $\bullet O_2^-$, h^+ , and $\bullet OH$ (Zhu et al., 2016; Gao et al., 2021), respectively. As can be clearly seen from Figure 7, the presence of TEOA, IPA and BQ all remarkably reduces the photocatalytic decolorization efficiency of MB under the same condition, which suggests that all $\bullet O_2^-$, h^+ , and $\bullet OH$ participated in the decolorization reactions of MB. However, the photocatalytic degradation rate of MB after the addition of IPA is the slowest, indicating that •OH played a major role in the photocatalytic degradation of MB by CdS/MCC composite.

To verify the above experiment results, the generated •OH and •O₂ species in the photocatalytic process were inspected by COU photoluminescence probing and NBT transformation techniques, respectively. As •OH can react with COU to generate strongly fluorescent substance (7hydroxycoumarin), the generation of •OH in the lightirradiated CdS/MCC-10% aqueous suspension was detected using fluorescent probe technique. In this experiment, a 50 ml COU solution (0.1 g/L) replaced the 50 ml MB solution. The supernatant was monitored directly using a fluorescence spectrophotometer (the excitation wavelength is 340 nm). The PL intensities emitted by the mixture of CdS/MCC-10% and COU solution at different visible-light irradiation times are shown in Figure 8A. Clearly, the PL intensity of the generated 7-hydroxycoumarin at about 453 nm became stronger as the irradiation time increased. These results indicated that the •OH radicals were produced and they might act as the predominant active oxygen species during the photocatalytic process (Wang et al., 2020). The •O₂ radicals in the mixture of 50 mg CdS/MCC-10% and 50 ml 0.01 mmol/L NBT solution under light irradiation were determined employing NBT (Shi et al., 2020; Du et al., 2021; Feng et al., 2021). The time-varying absorption spectra of NBT in the presence of CdS/MCC-10% and visible-light are shown in Figure 8B. The maximum absorbance of NBT at 260 nm decreased fastly as the irradiation time increased, indicating the formation of •O₂ in the CdS/MCC-10% system under visible-light.

Based on the above analysis, the photodegradation processes of MB over the CdS/MCC composite photocatalyst are interpreted in Figure 9. The photogenerated electrons and the photogenerated holes are produced respectively in the conduction band (CB) and valence band (VB) of CdS/MCC by excitation with visible-light (Eq. 2). Meanwhile a portion of the photogenerated charges would recombine. When MB molecules were adsorbed on the surface of CdS/MCC composite and excited, they would deliver electrons to the CB of CdS/MCC composites. The VB holes of CdS/MCC can oxidize MB (Eq. 3), or react with the surface bound OH (or by H₂O) to generate •OH (Eqs 4, 5) (Liu et al., 2022). The •OH can attack the chromophoric structure and the diethylamino groups effectively, causing the cycloreversion of MB molecules (Eq. 6) (Sun et al., 2021) as well as final mineralization into CO₂, H₂O, and other inorganic substances. Besides, the highly reducing electrons in the CB of CdS/MCC can reduce O_2 to $\bullet O_2^-$ (Yao et al., 2020), which are also able to oxidize MB (Eqs 7, 8). The MCC can transfer electrons from its excited energy level to the CB of CdS, increasing the reactive oxygen species (•O₂⁻) and reducing electron-hole recombination (Hasanpour et al., 2021). Moreover, the heterojunction formed between the two components of the synthesized CdS/MCC nanocomposite (Figure 2C) also favors the charge separation.

$$CdS + hv \rightarrow h^{+} + e^{-}$$
 (2)

$$MB + h^+ \rightarrow oxide product$$
 (3)

$$h^+ + OH^- \rightarrow \bullet OH$$
 (4)

$$h^{+} + H_{2}O \rightarrow \bullet OH + H^{+}$$
 (5)

•OH + MB
$$\rightarrow$$
 oxide product (6)

$$e^- + O_2 \rightarrow \bullet O_2^- \tag{7}$$

$$\bullet O_2^- + MB \rightarrow oxide product$$
 (8)

CONCLUSION

CdS/MCC nanocomposite photocatalyst has been successfully prepared by a mild and simple sonochemical method. In addition, the photocatalytic performance of the prepared products was also assessed. The results indicated that the synthesized CdS/MCC nanocomposite exhibited excellent photocatalytic activity, and the optimum content of MCC in the CdS/MCC nanocomposite was found to be 10%. When irradiated by visible-light for 60 min, CdS/MCC-10% can catalyze the degradation of 81.5% of MB, much higher than pure CdS. The boosted photocatalytic efficiency of CdS/MCC-10% was likely resulted from the tight junction between CdS and MCC and the larger surface area. Furthermore, the radicals capture experiments, NBT transformation and coumarin photoluminescence probing suggested that •OH was the dominant active oxygen species in the photocatalytic degradation of MB by CdS/MCC-10%. Our research provides evidence that the modification with MCC can efficiently improve the photocatalytic activity of semiconductors (such as CdS).

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding authors.

AUTHOR CONTRIBUTIONS

Conceptualization, CZ and YZ; methodology, CZ; investigation, CZ, XZ and YJ; resources, CZ and JL; data curation, CZ and YL; writing—original draft preparation, CZ; writing—review and editing, YZ and JL; visualization,

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Hydroisomerization of n-Hexadecane Over Nickel-Modified SAPO-11 Molecular Sieve-Supported NiWS Catalysts: Effects of Modification Methods

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The complexation-excessive impregnation modification method, which was original in this study, and the ion-exchange method and the in situ modification method were used to synthesize Ni-modified SAPO-11 molecular sieves. With the Ni-modified SAPO-11 samples as support, the corresponding NiWS-supported catalysts for the hydroisomerization of n-hexadecane were prepared. The effects of Ni-modification on SAPO-11 characteristics and the active phase were studied. The structure, morphology, and acidity of SAPO-11, as well as the interaction between active metals and support, the morphology, dispersibility, and stacking number of the active phase, were all changed by Ni-modification methods. The complexation-excessive impregnation modification method deleted a portion of AI from SAPO-11 molecular sieves while simultaneously integrating Ni into the skeletal structure of the surface layer of SAPO-11 molecular sieves, considerably enhancing the acidity of SAPO-11 molecular sieves. Furthermore, during dealumination, ethylenediaminetetraacetic acid generated more mesoporous structures and increased the mesoporous volume of SAPO-11 molecular sieves. Because the complexationexcessive impregnation modification method increased the amount of Ni in the surface framework of the SAPO-11 molecular sieve, it has weakened the interaction between the active phase and the support, improved the properties of the active phase, and greatly improved the hydroisomerization performance of NiW/NiSAPO-11. The yield of i-hexadecane of NiW/NiSAPO-11 increased by 39.3% when compared to NiW/ NiSAPO-11. It presented a realistic approach for increasing the acidity of SAPO-11, reducing the interaction between active metals and support, and improving the active phase stacking problem.

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INTRODUCTION

The presence of long-chain n-alkanes is thought to be the cause of the high freezing point of diesel and the poor low-temperature fluidity of lubricating base oil (Tao et al., 2017). The formation of branched isomers by hydroisomerization of long-chain n-alkanes can effectively lower the freezing point of diesel and increase the low-temperature fluidity of lubricating base oil (Du et al., 2018). The

bifunctional catalyst for the hydroisomerization of n-alkanes contains an acid site for the skeletal isomerization of olefin intermediates and a metal site for de/hydrogenation (Wei et al., 2017). Acidic supports, such as zeolites, usually supply acid sites, whereas noble metals or other transition metals give metal sites (Yang et al., 2017a). Because of their one-dimensional porosity and low acidity, SAPO-11 molecular sieves are commonly employed as a support for n-alkane hydroisomerization catalysts (Guo et al., 2012). Noble metals like platinum and palladium have strong de/hydrogenation activities, whereas nonnoble metals like nickel are also used as metal components in hydroisomerization catalysts (Zhao et al., 2014; Wang et al., 2018).

Although SAPO-11 molecular sieves have been used in industry and have shown to be a solid support for hydroisomerization catalysts, increasing their performance in hydroisomerization is still a concern worth investigating (Blasco et al., 2006). The active sites for catalyzing isomerization of the alkane molecular skeleton are thought to be Brnsted (B) acid sites in the SAPO-11 molecular sieve, particularly the medium strength B acid sites (Guo et al., 2013). As a result, improving the isomerization performance of SAPO-11 requires a better understanding of enhancing the proportion of medium and strong B acid sites. Lyu et al. (2019a) used in situ synthesis to introduce varying amounts of Ni into SAPO-11 to investigate the effects of metal-acid balance on n-hexane hydroisomerization and the acidity of SAPO-11. However, up to now, no one has studied the effects of modification methods in the process of Ni modification on the physicochemical properties (such as textural and acidity) of SAPO-11 molecular sieves. Furthermore, despite the remarkable catalytic activity of noble metals as metal components of hydroisomerization catalysts, there are two issues. On the one hand, the high cost of noble metals restricts their use in industry (Tian and Chen., 2014). Noble metals, on the other hand, are poisoned and inactivated due to their sensitivity to sulfur-containing compounds in raw materials (Yang et al., 2017b; Lyu et al., 2020). Although some researchers have reported employing Ni as a metal component instead of noble metals, hydroisomerization results revealed that Ni has a high hydrogenolysis activity, resulting in lower isomer selectivity and yield than noble metal-supported catalysts (Karthikeyan et al., 2016; Yang et al., 2017c). Transition metal sulfides have a good de/hydroisomerization performance and are widely used as the active phase of catalysts for hydrodesulfurization (Díaz de León et al., 2017), hydrodenitrogenation, and hydrocracking (Cui et al., 2019), such as NiMoS (Zhou et al., 2017) and NiWS (Minaev et al., 2019). In the past, there have been many reports on the application of noble metal (Pt, Pd) or Nisupported catalysts in alkane hydroisomerization (Lyu et al., 2017; Hongloi et al., 2021), but there have been few on the application of transition metal sulfide catalysts in alkane hydroisomerization and the effects of the properties of the transition metal sulfide active phase hydroisomerization (Shi et al., 2009; Tan et al., 2021).

In this study, the ion-exchange method, the *in situ* modification method, and the complexation-excessive

impregnation modification method were used to modify SAPO-11 molecular sieves with Ni in this study. The hydroisomerization of n-hexadecane was carried out using the Ni-modified SAPO-11 molecular sieves, which were supported by NiWS. The impact of various modification methods on the physicochemical properties of SAPO-11, the active phase properties, and the hydroisomerization performance of several catalysts were studied.

EXPERIMENTAL

Materials

Phosphoric acid (H₃PO₄, 85wt%; Aladdin), pseudo-boehmite (Al₂O₃, 70wt%; Macklin), acid silica sol (SiO₂, 30wt%; Dezhou Jinghuo technology Glass Co., Ltd.), di-n-propylamine (DPA, 99wt%; Aladdin), diisopropylamine (DIPA, 99wt%; Aladdin), dodecyltrimethylammonium bromide (DTAB, 99wt%; Aladdin), ammonium chloride (NH₄Cl, 99.5wt%; Macklin), nickel nitrate hexahydrate(Ni(NO₃)₂·6H₂O, 98wt%; Aladdin), ammonium metatungstate hydrate ((NH₄)₆H₂W₁₂O₄₀·xH₂O, 99.5wt%; Macklin), ethylenediaminetetraacetic acid (EDTA, 98wt%; Aladdin), and deionized water.

Synthesis and Modification of SAPO-11 Molecular Sieves

Deionized water and phosphoric acid were mixed in a normal synthesis procedure, then pseudo-boehmite was added to the solution and agitated for 2 h. DPA and DIPA were added and mixed continuously for 2 h. Drop by drop, acid silica sol was added to the system and aggressively agitated for 2 h. Finally, DTAB was added and agitated for 1 h, resulting in an initial gel with the following molar composition: 1.0 Al₂O₃: 0.75 P₂O₅: 0.45 SiO₂: 0.5 DPA: 0.5 DIPA: 0.05 DTAB: 45 H₂O. The gel was precrystallized at 90°C for 12 h before being crystallized at 190°C for 24 h. The SAPO-11 molecular sieves were obtained by washing the solid products collected by filtration to neutrality with deionized water, drying them at 110°C overnight, and calcining them at 600°C for 6 h.

For the ion-exchange procedure, 10.0 g of SAPO-11 was mixed with 100 g of 0.3 mol/L nickel nitrate solution, which was then exchanged at 90°C for 4 h, filtered, dried at 110°C overnight, and calcined at 500°C for 4 h. Ni@SAPO-11 was the name given to the dried and calcined sample. The operation procedures for the in situ modification method were similar to the above-mentioned SAPO-11 synthesis steps, with the exception that 3% nickel was added during the initial gel formation process (the molar ratio of Ni/Al₂O₃ was 3%). The products were filtered before being dried at 110°C overnight and calcined for 4 h at 500°C. Ni-SAPO-11 was the name given to the dried and calcined sample. 0.1 mol EDTA was added to 50 ml of 0.3 mol/L nickel nitrate solution for complexation-excessive impregnation modification procedure, and then 10 g of SAPO-11 molecular sieve particles with 20-40 mesh were impregnated with the resulting solution. SAPO-11 molecular sieve particles after complexation-excessive

impregnation were obtained by filtration, dried, and calcined, and designated NiSAPO-11 after soaking for 4 h.

Preparation of NiW-Supported Catalysts

The SAPO-11, Ni@SAPO-11, and Ni-SAPO-11 particles were pressed, crushed, and sieved to a size of 20–40 mesh. The NiW-supported catalysts were made using the incipient-wetness impregnation method with an aqueous solution of nickel nitrate hexahydrate and ammonium metatungstate hydrate, then dried at 110°C for 6 h and calcined at 500°C for 4 h after being evaporated at room temperature overnight. The loading concentration of NiO was 5% and the loading concentration of WO₃ was 15% for each catalyst. NiW/SAPO-11, NiW/Ni@SAPO-11, NiW/Ni-SAPO-11, and NiW/NiSAPO-11 were the names given to the resulting catalysts.

Characterization

The SAPO-11 samples were characterized by X-ray diffraction (XRD) on a Bruker AXS D8 Advance X-ray diffractometer using Cu K α radiation at 40 kV and 40 mA, and 2 θ varied from 5 to 90° at a scanning speed of 5°/min. On a field-emission environmental scanning electron microscope, images of the SAPO-11 samples were taken using scanning electron microscopy (SEM) (FEI Quanta 200F). After degassing the materials at 350°C under vacuum for 15 h, N₂ adsorption-desorption measurements were performed on a Micromeritics ASAP 2020 analyzer at -196°C. The Brunauer-Emmett-Teller (BET) and de Boer t-plot methods were used to compute the specific surface area and micropore volume, respectively, while the Barrett-Joyner-Halenda technique was used to calculate the mesopore volume. A Micromeritics auto-chem 2920 device was used to analyze temperature-programmed desorption of ammonia (NH₃-TPD). The sample was heated to 600°C in an Ar flow for 30 min, then switched to an ammonia flow for another 30 min before being cooled to 70°C. The sample was purged with Ar for 2 h to eliminate the physically adsorbed ammonia, and the TPD signal was recorded using a thermal conductivity detector with a heating rate of 10°C/min from 70 to 600°C. A Nicolet 5700 spectrometer was used to record Pyridine adsorbed infrared (Py-IR) spectra. At 200 and 350°C, the pyridine samples were evacuated. On a Quantachrome Autosorb-iQ-C chemical system, temperature-programmed reduction (H₂-TPR) measurements were taken. The samples were heated at a rate of 10°C/min in an H₂-Ar flow containing 5% H₂ from room temperature to 1,050°C. The presulfurized catalysts were analyzed using X-ray photoelectron spectroscopy (XPS) on a Thermo spectrometer using Al Kα radiation as the excitation light source. To calibrate the binding energy scale, all spectra used the Al 2p peak with a binding energy of 74.6 eV. The presulfurized catalysts' XPS spectra were decomposed using XPS PEAK, and the deconvolution was achieved using Gaussian-Lorentzian band shapes. A JEM 2100 LaB₆ transmission electron microscope was used to obtain high-resolution transmission electron microscope (HRTEM) images of the presulfurized catalysts. The average length and average stacking number of WS₂ slabs were determined using methods described in the literature (Yu et al., 2012):

Average slab length
$$\bar{L} = \frac{\sum\limits_{i=1}^{n} n_i l_i}{\sum\limits_{i=1}^{n} n_i}$$
 (1)

Average stacking number
$$\bar{N} = \frac{\sum\limits_{i=1}^{n} n_i N_i}{\sum\limits_{i=1}^{n} n_i}$$
 (2)

where l_i denotes the WS₂ slab length, n_i denotes the number of slabs of length l_i , and N_i is the number of layers in a WS₂ slab. The dispersion degree of the WS₂ active phase, f_W , was derived using the following equation, assuming that the WS₂ slabs are presented as perfect hexagons (Tao et al., 2014):

$$f_W = \frac{W_{edge}}{W_{total}} = \frac{\sum_{i=1}^{t} 6(n_i - 1)}{\sum_{i=1}^{t} (3n_i^2 - 3n_i + 1)}$$
(3)

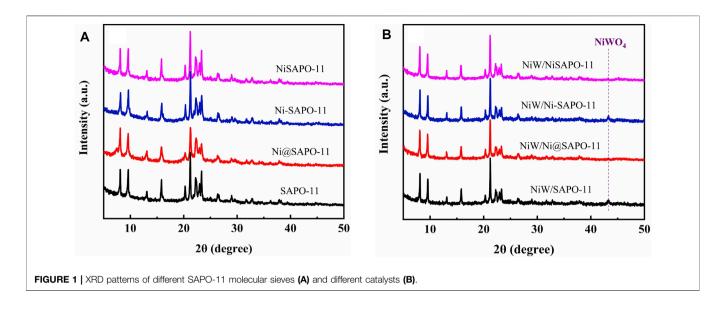
where W_{edge} denotes the W atoms on the edges of WS₂ slabs, W_{total} denotes the total number of W atoms, n_i denotes the number of W atoms along one side of a WS₂ slab determined by its length [L = 3.2 (2ni—1) Å], and t denotes the total number of slabs determined by at least 500 WS₂ slabs obtained from HRTEM images of various catalysts.

Catalytic Performance Assessment

fixed-bed hydrogenation micro-reactor, hydroisomerization of n-hexadecane (n-C₁₆) was carried out. In a typical reaction, the tubular furnace held 9.0 ml of catalyst and 22 ml of silica sand. The catalyst was presulfurized using a CS2 cyclohexane solution containing 2% CS₂ at 320°C and 4 MPa for 5 h with a liquid hourly space velocity (LHSV) of 7 h⁻¹ and an H₂/oil ratio of 100 (v/v) before the reaction. After presulfurization, the catalytic performance of the catalyst was examined at 2 MPa, 1.5 h⁻¹ LHSV, $600 \text{ (v/v) H}_2/\text{oil}$, and $320-400^{\circ}\text{C}$ reaction temperature. When the temperature was reduced to the reaction temperature, a syringe pump was used to feed the reactant n-hexadecane into the reactor. The products were analyzed using a Shimadzu GC-2014 gas chromatograph with a capillary HP-PONA column and GC-MS for qualitative analysis. The TOF (turnover frequency, which is used to evaluate the catalytic activity of a catalyst) of each active site was calculated using the following equation based on the number of all available active sites and the conversion of n-C₁₆ of each catalyst at 340°C (Wen et al., 2020):

$$TOF = \frac{V_{feed} \cdot x}{n_W \cdot f_W} \tag{4}$$

where V_{feed} is the feed rate of the reactant n-C₁₆ in mol/h, x is the conversion of n-C₁₆ at 340°C, n_w is the amount of W atom in the catalyst in mol, and f_W is the dispersion degree of W species. The following equation was used to compute the hydroisomerization reaction rate constant (Pimerzin et al., 2019):



$$k_{iso} = \frac{V_{feed}}{m} \ln(1 - x) \tag{5}$$

where k_{iso} , V_{feed} , m and x are the quasi-first-order reaction rate constant of n-C₁₆ hydroisomerization on different catalysts, the feed flow rate of the reactant n-C₁₆ in mol/h, the mass of catalyst and the conversion of n-C₁₆, respectively.

RESULTS AND DISCUSSION

Phase Structure

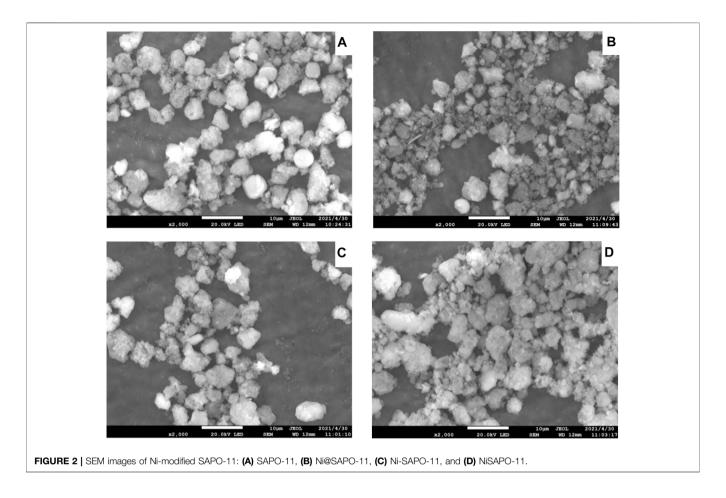
The XRD patterns of Ni-modified SAPO-11 molecular sieves generated by various ways are shown in Figure 1A. All samples exhibited diffraction peaks in the 2θ range of 5-50° that were assigned to the normal AEL structure, demonstrating that SAPO-11 samples retained full structural units after Ni alteration by various methods (Lyu et al., 2019b). The prominent characteristic diffraction peaks of Ni-SAPO-11 indicate that it has a high crystallinity (Song et al., 2017). Because Ni species replaced a portion of Al species in the SAPO-11 framework, crystalline Ni species resulted. The strength of the distinctive diffraction peaks of Ni@SAPO-11 reduced slightly when compared to SAPO-11, which could be attributable to a decrease in crystallinity during the ammonium-exchange and nickel ion-exchange processes (rehydration) (Yang et al., 2017c). Furthermore, the intensity of the characteristic diffraction peaks of NiSAPO-11 did not significantly decrease, indicating that EDTA could remove some Al species but not the crystal structure of SAPO-11. A weak characteristic diffraction peak attributed to NiO appeared at 2θ = 37.2° of XRD patterns of all the samples, which indicates that there were a small number of NiO species in all the samples, and the distribution of NiO species in SAPO-11 molecular sieves was relatively uniform. Figure 1B shows the XRD spectra of the different catalysts. It can be seen that the different catalysts still retained the characteristic diffraction peaks attributed to AEL structure, indicating that the loading of metal components did not cause the crystal structure of SAPO-11 molecular sieves to be destroyed. In addition, all the catalysts showed a weak characteristic diffraction peak attributed to NiWO₄ species around $2\theta=43.2^{\circ}$, which indicates that NiWO₄ species existed in all samples and dispersed relatively evenly.

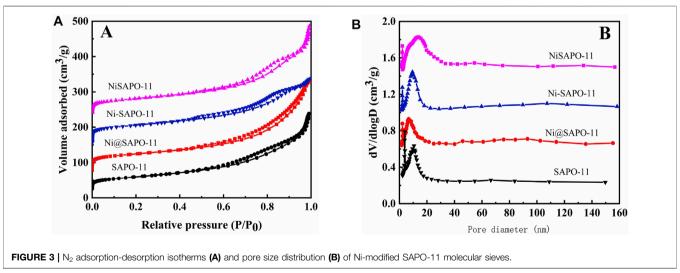
Morphology

SEM images of Ni-modified SAPO-11 molecular sieves generated by various procedures are shown in **Figure 2**. SAPO-11 had pseudospherical particles with a particle size of roughly 5 μ m and a fairly uniform particle size distribution. The particle shape of Ni@SAPO-11 was not as regular as that of SAPO-11, and the discrepancy could be due to its particle form being destroyed when it was exchanged in aqueous solution twice. While Ni-SAPO-11 was basically the same as SAPO-11 in particle shape and size. As for NiSAPO-11, a small number of small particles similar to amorphous substances appear in its SEM image, which may be the smaller particles formed by the decomposition of SAPO-11 molecular sieve particles in the process of removing Al species by EDTA.

Textural Properties

Figure 3 shows the N_2 adsorption-desorption isotherms (**Figure 3A**) and pore size distribution (**Figure 3B**) of the Nimodified SAPO-11 molecular sieves. Isotherms with typical H4-type hysteresis loops were seen in all samples (Chen et al., 2017). At low relative pressure $(10^{-5} \le P/P_0 \le 10^{-2})$, the amount of N_2 adsorption in all samples rose dramatically, which was attributable to N_2 filling the micropores (Du et al., 2019). Within the relative pressure P/P_0 range of 0.4–0.9, all samples showed clear hysteresis loops, showing that these samples have a lot of mesopores (Wen et al., 2019). The hysteresis loop of NiSAPO-11 is clearly larger than that of other samples, indicating that NiSAPO-11 has a more mesoporous structure than other samples. This is because, when eliminating Al species, EDTA dissolved and etched in the crystals of SAPO-11 molecular sieves, forming many new mesoporous structures. **Figure 3B**





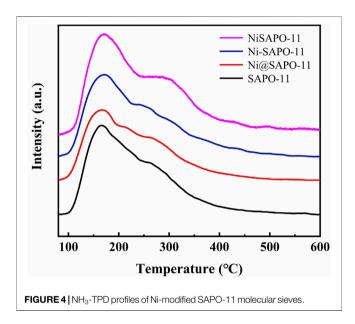
shows the pore size distribution of all samples, with the pore size of SAPO-11, Ni@SAPO-11, and Ni-SAPO-11 primarily dispersed around 12 nm. The foregoing findings show that these samples include hierarchical micro-mesoporous structures. However, the mesoporous size of NiSAPO-11 is centered at 18 nm, which is

larger than that of other samples, implying that EDTA does have a pore-expansion role.

The BET surface area ($S_{\rm BET}$), exterior surface area ($S_{\rm ext}$), and pore volume of the Ni-modified SAPO-11 are shown in **Table 1**. The $S_{\rm BET}$ and pore volume of Ni@SAPO-11 were reduced to some

TABLE 1 | Textural properties of Ni-modified SAPO-11.

Sample	S _{BET} , m ² /g	S _{ext} , m ² /g	V _{micro} , cm ³ /g	V _{meso} , cm ³ /g	V _{total} , cm ³ /g
NiSAPO-11	188	96	0.11	0.36	0.47
Ni-SAPO-11	174	94	0.08	0.30	0.38
Ni@SAPO-11	158	88	0.07	0.20	0.27
SAPO-11	166	91	0.09	0.26	0.35



extent when compared to SAPO-11. One probable explanation is that Ni species enter the pores, blocking certain micropores and occupying a portion of the mesopore volume (V_{meso}) in the ionexchange process. Another possibility is that during the ionexchange process, a portion of the crystal structure collapses, causing the pore channels to fill. The S_{BET} and V_{meso} of Ni-SAPO-11 have increased, indicating that the addition of Ni in situ helps to improve the $S_{\rm BET}$ and $V_{\rm meso}$ of SAPO-11 (Liu et al., 2013). The micropore volume (V_{micro}) of Ni-SAPO-11 decreased, implying that some Ni species remain in the micropores and occupy the micropore volume. The S_{BET} , V_{micro} , and V_{meso} of NiSAPO-11 all increased, with V_{meso} increasing by a substantial margin, confirming the prior conclusion that EDTA has the ability to ream and manufacture new mesopores. The S_{BET} and V_{meso} of the different SAPO-11 samples increased in the order of Ni@SAPO-11 < SAPO-11 < Ni-SAPO-11 < NiSAPO-11, indicating that the textural properties of SAPO-11 molecular sieves can be improved most obviously by the complexation-excessive impregnation modification method.

Acidity Properties

The NH₃-TPD measurements were used to determine the acid amounts and acid strength distribution of the Ni-modified SAPO-11 molecular sieves manufactured using various procedures. **Figure 4** shows the NH₃-TPD profiles of the several Ni-modified SAPO-11 samples. Each NH₃-TPD profile revealed two NH₃ desorption peaks about 180 and 310°C,

corresponding to NH3 adsorbed on weak acid sites, medium and strong acid sites, respectively (Yang et al., 2019). The intensity of the desorption peak represents the acid amount (Li and Wu, 2020). The acid amount of Ni@SAPO-11 was much lower than that of SAPO-11, which was attributable to the fact that part of the acid sites were covered and sheltered by Ni species during Ni ion exchange. The strength of the NH3 desorption peak corresponding to weak acid sites reduced somewhat in Ni-SAPO-11, indicating that the weak acid amount of Ni-SAPO-11 fell slightly (Yang et al., 2017c). This is due to the fact that the acid sites in SAPO-11 are thought to be formed by Si-OH, Al-OH, P-OH, and Si-OH-Al, respectively (Tiuliukova et al., 2018). Some Al precursors were substituted with Ni precursors, resulting in a reduction in acid sites. The intensities of the NH3 desorption peaks corresponding to medium and strong acid sites increased, indicating that the concentrations of medium and strong acid increased as well. It can be explained by the fact that Ni has a greater average electronegativity (1.91) than Al (1.71), and Ni has a higher covalency than Al. As a result, the Brnsted protons and Lewis caverns generated by Ni substituting part of Al in SAPO-11 have a higher acid density, resulting in more medium and strong acid sites in Ni-SAPO-11. The amount of weak acid, medium and strong acid in NiSAPO-11 were all improved. The increase in weak acid amonut is due to EDTA dredging some blocked channels and establishing new ones, exposing and detecting more acid sites to a large extent. The rise in medium and strong acid amounts in NiSAPO-11 can be attributed to two factors. On the one hand, the exposure of acid sites is caused by an increase in pore volume. In the process of eliminating Al species, EDTA can integrate Ni species into the surface framework of SAPO-11 molecular sieves to generate Ni-OH-Si species, which helps to enhance the density of medium and strong acid in SAPO-11. The results show that the amounts of the weak acid in Nimodified SAPO-11 decreased in the order of NiSAPO-11 > SAPO-11 > Ni@SAPO-11 > Ni-SAPO-11, while the amounts of medium and strong acid decreased in the order of NiSAPO-11 > Ni-SAPO-11 > SAPO-11 > Ni@SAPO-11.

Py-IR was used to analyze the variations in Brønsted (B) acid sites and Lewis (L) acid sites in the Ni-modified SAPO-11 molecular sieves to determine the acidity of the different SAPO-11 samples (Jin et al., 2018). **Figure 5** shows the Py-IR spectra of the Ni-modified SAPO-11 samples generated using various procedures. Py-IR spectra obtained after pyridine molecules desorbed at 200°C were used to compute the amount of weak acid, whereas Py-IR spectra formed after pyridine molecules desorbed at 350°C were used to calculate the amounts of medium and strong acid. **Table 2** shows the

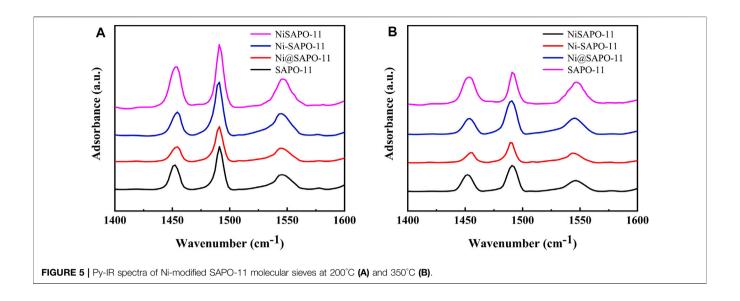
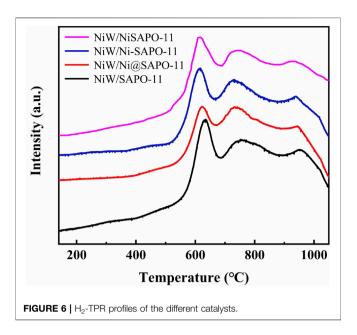


TABLE 2 | Acidity properties of Ni-modified SAPO-11 determined by Py-IR.

Sample			Acidity ((µmol/g)		
		Weak acid sites (200°C	()	Mediur	n and strong acid sites	(350°C)
	В	L	B + L	В	L	B + L
SAPO-11	91.87	29.32	121.19	30.62	20.97	51.59
Ni@SAPO-11	53.09	24.25	77.34	23.51	15.11	38.62
Ni-SAPO-11	69.91	35.84	105.75	48.21	18.16	66.37
NiSAPO-11	82.21	56.88	139.09	58.35	24.66	83.01

results of calculating the number of B acid sites and L acid sites and the accompanying findings. All samples had three peaks in the range of 1,400-1,600 cm⁻¹, as illustrated in Figure 5. The peaks at 1,455 cm⁻¹ and 1,545 cm⁻¹ are assigned to pyridine molecules desorbed on L acid sites and B acid sites, respectively (Wen et al., 2020), whereas the peak at 1,490 cm⁻¹ is attributed to a combined line of B acid sites and L acid sites (Zhang et al., 2018). The amounts of weak L acid in Ni-modified SAPO-11 molecular sieves decreased in the following order: NiSAPO-11(56.88 µmol/ g) > Ni-SAPO-11 (35.84 μ mol/g) > SAPO-11 (29.32 μ mol/g) > Ni@SAPO-11 (24.25 μmol/g), while the amounts of medium and strong L acid decreased in the following order: NiSAPO-11 $(24.66 \, \mu mol/g) > SAPO-11 (20.97 \, \mu mol/g) > Ni-SAPO-11$ $(18.16 \,\mu\text{mol/g}) > \text{Ni@SAPO-11} \ (15.11 \,\mu\text{mol/g})$. This can be explained by the fact that during the ion-exchange and in situ modifications, certain NiO species covered several strong L acid sites. However, some additional weak L acid sites were generated in Ni species in the surface framework of NiSAPO-11, resulting in an increase in the amount of weak L acid and the amount of medium and strong Lacid in NiSAPO-11. The amounts of weak B acid in Ni-modified SAPO-11 molecular sieves decreased in the order of SAPO-11 (91.87 μmol/g) > NiSAPO-11 (82.21 μmol/g) > Ni-SAPO-11 (69.91 $\mu mol/g$) > Ni@SAPO-11 (53.09 $\mu mol/g$), while the amounts of medium and strong B acid decreased in the order of NiSAPO-11 (58.35 μ mol/g) > Ni-SAPO-11 $(48.21 \mu mol/g) > SAPO-11 (30.62 \mu mol/g) > Ni@SAPO-11$

(23.51 µmol/g). In the process of Ni ion exchange (part of H⁺ being swapped by Ni²⁺), Ni species covered some weak B acid sites and medium and strong B acid sites, resulting in a decrease in both the amount of weak B acid and the amount of medium and strong B acid (MSB) in Ni@SAPO-11. Some Ni species would undoubtedly cover the acid sites during Ni in situ alteration, resulting in a reduction in the number of weak B acid sites in Ni-SAPO-11. Meanwhile, Ni species entered the skeleton structure of SAPO-11 and substituted Al species by mechanism (1) and mechanism (2). Whether it is $(NiO_{4/2})^{2-}(PO_{4/2})^{+}$ species produced by mechanism (1) substitution or (HONiO_{4/2}) ²⁻(PO_{4/2})⁺ species produced by mechanism (2) substitution, it is beneficial to form more medium and strong B acid sites, which well explains that Ni-SAPO-11 has more medium and strong B acid sites. However, in the process of in situ modification, Ni species uniformly enter the bulk and surface framework of SAPO-11 molecular sieves, which is limited to the increase of B acid amount. EDTA only integrates Ni species into the surface framework of SAPO-11 molecular sieves during the complexation-excessive impregnation process, and more Ni species are distributed in the surface framework of SAPO-11 molecular sieves, resulting in a significant improvement of the surface acidity of SAPO-11 molecular sieves, which is the reason why the weak B acid amount, medium and strong B acid amount of NiSAPO-11 reach their maximum. Ni-SAPO-11 modified by Ni by the complexation-excessive impregnation method initiated



in this study has the largest amount of medium and strong B acid, which is beneficial to improve the catalytic performance of the catalyst.

Mechanism

(1):
$$(AlO_{4/2}) - (PO_{4/2}) + \rightarrow (NiO_{4/2})^{2-} (PO_{4/2})^{+} + H^{+}$$

(2):
$$(HOAlO_{3/2}) - (PO_{4/2})^+ \rightarrow (HONiO_{4/2})^{2-} (PO_{4/2})^+ + H^+$$

Active Phase Characterization

On bifunctional catalysts, the reducibility of active metals can effectively reflect the interaction between active metals and supports (Yang Z et al., 2019). As a result, H₂-TPR characterization was used to investigate the reducibility of the active metals on the catalysts. Figure 6 depicts the H2-TPR profiles of all catalysts. In the range of 0-1,050°C, all samples revealed three hydrogen consumption peaks. The lowtemperature reduction peak at 610-635°C is attributed to the reduction of highly dispersed octahedrally coordinated polymeric tungsten species and mostly NiO species, while the moderatetemperature reduction peak at 710-765°C is attributed to the reduction of NiWO₄ species, and the high-temperature reduction peak at 930-955°C is attributed to the reduction of refractory tungsten species in the form of W-O-Al (Cui et al., 2013). The results revealed that the low-temperature reduction peaks, moderate-temperature reduction peaks, and high-temperature reduction peaks of the catalysts all migrated to lower temperatures after Ni alteration. The reduction temperatures of low-temperature reduction peaks decreased in the order of NiW/SAPO-11 (634°C) > NiW/Ni@SAPO-11 (624°C) > NiW/ Ni-SAPO-11 (611°C) > NiW/NiSAPO-11 (608°C), and the reduction temperatures of moderate-temperature reduction peaks decreased in the order of NiW/SAPO-11 (760°C) > NiW/Ni@SAPO-11 (737°C) > NiW/Ni-SAPO-11 (726°C) > NiW/NiSAPO-11 (723°C), while the reduction temperatures of high-temperature reduction peaks decreased in the order of NiW/SAPO-11 (957°C) > NiW/Ni@SAPO-11 (944°C) > NiW/Ni-SAPO-11 (936°C) > NiW/NiSAPO-11 (922°C), indicating that the reducibility of active metal NiW on NiW/SAPO-11 catalysts can be improved by introducing Ni into SAPO-11 through the ion-exchange method or the *in situ* modification method.

The sulfided catalysts were studied by HRTEM to visualize the morphologies of the NiWS active phase on the catalysts and compare the dispersibility of sulfided metals on the various Nimodified SAPO-11 supports. Figure 7 shows sample HRTEM images of the different supported NiW sulfided catalysts. The WS₂ slab structure is represented by the black line-like layers in the images (Yu et al., 2012). The average length and average stacking number of WS2 slabs on different catalysts were calculated using statistical analysis (Eqs 1, 2) of at least 500 slabs from different regions of each sulfide catalyst, and the findings are reported in Table 3. The results showed that Ni alteration altered the morphologies of the active phase. The average length of WS2 slabs dropped in the sequence NiW/ SAPO-11 (4.62 nm) > NiW/Ni@SAPO-11 (3.95 nm) > NiW/Ni-SAPO-11 (2.98 nm) > NiW/NiSAPO-11 (2.63 nm), whereas the average stacking number rose in the order NiW/SAPO-11 (1.33) < NiW/Ni@SAPO-11 (2.64) < NiW/Ni-SAPO-11 (3.23) < NiW.NiSAPO-11 (3.27). The length of WS₂ slabs on NiW/SAPO-11 ranged from 1 to 7 nm, with the majority falling within the 3-6 nm range. The length of WS₂ slabs on NiW/Ni@SAPO-11 ranged from 1 to 5 nm, with the majority falling between 2 and 5 nm. The length distribution of WS₂ slabs on NiW/Ni-SAPO-11 was 1-4 nm, with the majority in the 2-4 nm region. The length of WS₂ slbs of NiW/NiSAPO-11 ranges between 1-4 nm, but is mainly in the 2-3 nm range. It is often assumed that the dispersibility of the active phase is proportional to its length. The larger the dispersion degree, the shorter the active phase slabs are (Zhou et al., 2018). As a result, the degree of metal dispersion on the catalysts decreased in the following order: NiW/NiSAPO-11 > NiW/Ni-SAPO-11 > NiW/Ni@SAPO-11 > NiW/SAPO-11, which was consistent with the f_W values in **Table 3**. However, in addition to the length of WS2 slabs, the number of WS2 slabs stacked can have an impact on the properties of the active phase. The interaction between active metal and support is adequately reflected by the stacking number of WS₂ slabs (Zhou et al., 2017). The average stacking number of WS2 slabs for NiW/SAPO-11 was only 1.33. There were about half of the monolayer WS₂ slabs, which were classified as the "type I active phase" with low de/ hydrogenation activity. This can be explained by the fact that when tungsten species are loaded on SAPO-11, they form strong W-O-Al bonds with the support, and the interaction is too strong. The average stacking number of WS₂ slabs for NiW/Ni@SAPO-11 was 2.64, with around 33% of WS₂ slabs having stacking numbers ranging from 3 to 4. This could be due to a decrease in the L acid sites of Ni@SAPO-11, resulting in a weaker interaction between active phase and support. The average stacking number of WS2 slabs in NiW/Ni-SAPO-11 was 3.23, with over 70% of WS₂ slabs having stacking numbers ranging from 3 to 4. Because of their moderate dispersibility and stacking number, NiW/ NiSAPO-11 slabs had an average stacking number of 3.27, and around 85% of WS2 slabs had 3-4 stacking layers, which are

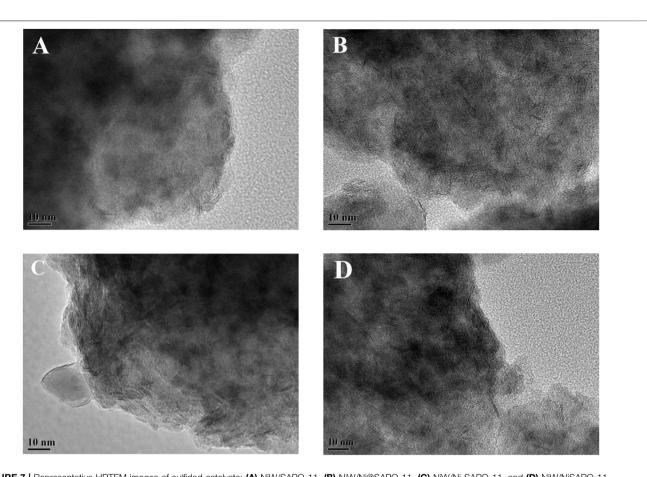


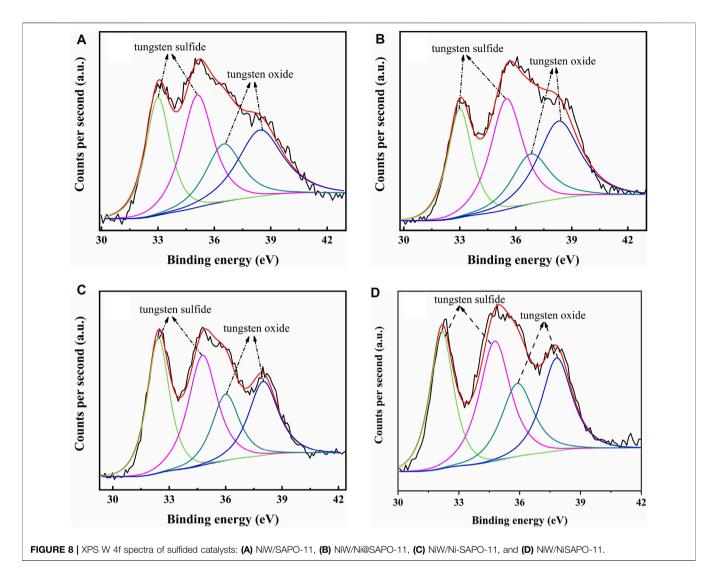
FIGURE 7 | Representative HRTEM images of sulfided catalysts: (A) NiW/SAPO-11, (B) NiW/Ni@SAPO-11, (C) NiW/Ni-SAPO-11, and (D) NiW/NiSAPO-11.

TABLE 3 Average lengths, layer numbers, and f_W values of WS₂ of all catalysts.

Sample	Ē (nm)	$ar{\mathbf{N}}$	f _W
NiW/SAPO-11	4.62	1.33	0.28
NiW/Ni@SAPO-11	3.95	2.64	0.29
NiW/Ni-SAPO-11	2.98	3.23	0.31
NiW/NiSAPO-11	2.63	3.27	0.32

designated the "type II active phase" with good de/hydrogenation activity. This can be explained by the fact that when tungsten species are loaded on Ni-SAPO-11 and NiSAPO-11, they form W-O-Ni bonds with the support, and W-O-Ni bonds are weaker than W-O-Al bonds. Additional Ni species were coupled to the surface framework of SAPO-11 molecular sieves rather than the bulk phase during the complexation-excessive impregnation modification, resulting in the formation of more W-O-Ni species. EDTA can similarly "anchor" Ni species, allowing them to be evenly "anchored" in a specific place and hence uniformly integrated into the surface framework of the SAPO-11 molecular sieve. "Delumination and nickel supplementation" is the term for this phenomenon. Overall, among the Ni-modified SAPO-11-supported NiW catalysts, NiW/NiSAPO-11 had the best metal dispersibility and reducibility, as well as the highest hydrogenation activity.

The catalysts were studied using XPS to determine the covalent states of nickel and tungsten surface species on the sulfided catalysts. The W 4f XPS spectra and Ni 2p XPS spectra of the sulfided catalysts are shown in Figures 8, 9, respectively, and the binding energies (BE) and Sulfidation degree of tungsten and nickel species on the sulfided catalysts are provided in **Tables 4**, 5, respectively. The W 4f XPS spectra were decomposed into four peaks, each of which consisted of two overlapping W⁴⁺ and W⁶⁺ peaks. The W 4f_{7/2} and W 4f_{5/2} levels of W⁴⁺ (WS₂) have binding energies of around 32.70 \pm 0.50 eV and 35.40 \pm 0.50 eV, respectively, while the W 4f_{7/2} and W 4f_{5/2} levels of W⁶⁺ (WO_3) have binding energies of about 36.50 \pm 0.50 eV and $38.30 \pm 0.50 \,\mathrm{eV}$, respectively (Cui et al., 2012). The easy metals are to sulfide, the weaker the connection between the metal and the support, and the more metal layers there are. The percentage of $W^{\bar{4}\bar{+}}$ species $[W^{4+}/(W^{4+}+W^{6+})]$ has a significant impact on the catalytic performance of hydrotreating catalysts, hence the sulfidation degree of tungsten species on sulfided catalysts was estimated (Cui et al., 2013). The degree of sulfidation of tungsten species on different sulfided catalysts decreased in the order NiW/NiSAPO-11 (62.07%) > NiW/ N-SAPO-11 (60.93%) > NiW/Ni@SAPO-11 (56.96%) > NiW/ SAPO-11 (56.96%) > NiW/SAPO-11 (56.96%) > NiW/SAPO-11 (56.96%) > NiW/SAPO (54.29%). The decrease in interaction



between active metals and support causes the increase in sulfidation degree of tungsten species on NiW/NiSAPO-11, NiW/Ni-SAPO-11, and NiW/Ni@SAPO-11 as compared to NiW/SAPO-11. To some extent, BE value can reflect the interaction between metal species and support. Table 4 shows that the BE values of tungsten species on the three catalysts, whether oxidic or sulfided, decrease in the order of NiW/SAPO-11 > NiW/Ni@SAPO-11 > NiW/Ni-SAPO-11 > NiW/NiSAPO-11. The results show that the interaction between tungsten species and support decreases in the order of NiW/SAPO-11 > NiW/Ni@ SAPO-11 > NiW/Ni-SAPO-11 > NiW/NiSAPO-11, which is completely consistent with the results reflected by H2-TPR and HRTEM. The Ni 2p XPS spectra were separated into five peaks, including two overlapping nickel oxide and nickel sulfide peaks. The Ni $2p_{3/2}$ and Ni $2p_{1/2}$ levels of nickel oxide (NiO) have binding energies of around 862.50 ± 0.50 eV and 880.50 ± 0.50 eV, respectively, while the Ni 2p_{3/2} and Ni 2p_{1/2} levels of nickel sulfide (NiS_x) have binding energies of about 856.50 ± 0.50 eV and $874.20 \pm 0.50 \text{ eV}$, respectively (Yu et al., 2012). The sulfidation degree of nickel species was defined as the percentage

of nickel sulfide species $[NiS_x/(NiO + NiS_x)]$ (Cui et al., 2013). The sulfidation degree of nickel species on different sulfided catalysts decreased in the order of NiW/NiSAPO-11 (52.23%) > NiW/Ni-SAPO-11 (49.13%) > NiW/Ni@SAPO-11 (48.35%) > NiW/SAPO-11 (45.41%), and the explanation for this change order is the same as that of tungsten species explained above.

Catalytic Performance

The catalyst was sulfurized ahead of time, and the reaction pressure was set to 2.0 MPa, LHSV was set at $1.5\,h^{-1}$, and $H_2/$ oil was $600\,(v/v)$ in a typical reaction. In the reaction temperature range of 300– $400\,^{\circ}$ C, the catalytic performance of the catalyst was studied. **Figure 10A** depicts n-C₁₆ conversion on several catalysts at various reaction temperatures. The conversion on all catalysts increased with the increase in reaction temperature, as shown in **Figure 10A**. The catalytic activity of NiW/NiSAPO-11 was much higher than that of other catalysts. The catalytic activity of all the catalysts increased in the order of NiW/Ni@SAPO-11 < NiW/SAPO-11 < NiW/NiSAPO-11. The selectivity of all catalysts to i-hexadecane (i-C₁₆) reduced as

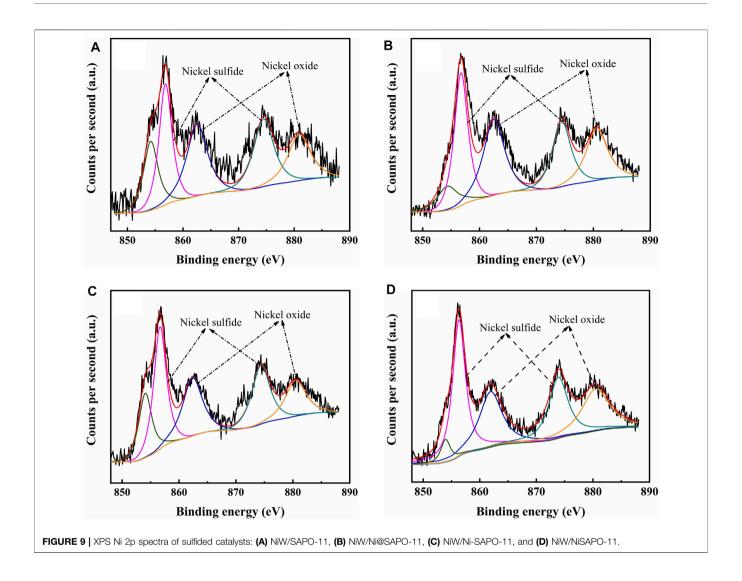


TABLE 4 | Binding energy and sulfidation degree of W on different catalysts.

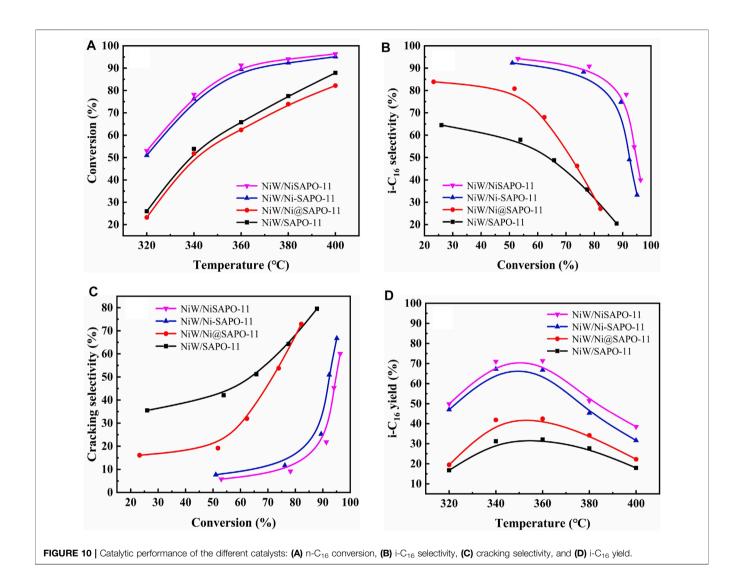
Sample	NiW/SAPO-11	NiW/Ni@SAPO-11	NiW/Ni-SAPO-11	NiW/NiSAPO-11
Oxidic	Binding energy (eV)			
W 4f ₇	36.70	36.50	36.10	35.82
W 4f ₅	38.43	38.30	38.00	37.78
Sulfided	Binding energy (eV)			
W 4f ₇	33.00	32.90	32.42	32.14
W 4f ₅	35.35	35.25	34.77	34.62
Sulfidation degree of W (%)	54.29	56.96	60.93	62.07

reaction temperature climbed, showing that the rate of cracking side reactions increased as reaction temperature increased **Figure 10C**. The selectivity of NiW/NiSAPO-11 to i-C₁₆ was clearly higher than that of NiW/SAPO-11, NiW/Ni@SAPO-11, and NiW/Ni-SAPO-11 within the reaction temperature range of catalytic performance evaluation (**Figure 10B**). This can be explained by the fact that NiSAPO-11 has the most medium and strong B acid sites, which are universally recognized as active sites for the isomerization of olefin intermediate skeletons (Yu

et al., 2021). Furthermore, on NiW/Ni-SAPO-11, the interaction between active metals and support is weak, and the dispersibility and stacking number of the so-called NiWS active phase are moderate, resulting in good hydrogenation activity for isomeric olefin intermediates that diffuse from the acid to the metal sites. The interaction between the active metals and the support in NiW/SAPO-11 is strong, making it difficult to diminish the active metals and resulting in lower i- C_{16} selectivity than NiW/Ni-SAPO-11. NiW/Ni@SAPO-11

TABLE 5 | Binding energy and sulfidation degree of Ni on different catalysts.

Sample	NiW/SAPO-11	NiW/Ni@SAPO-11	NiW/Ni-SAPO-11	NiW/NiSAPO-11
Oxidic	Binding energy (eV)			
Ni 2p ₃	862.71	862.50	862.15	861.89
Ni 2p ₁	880.90	880.57	880.26	880.11
Sulfided	Binding energy (eV)			
Ni 2p ₃	856.84	856.74	856.65	856.35
Ni 2p ₁	874.51	874.42	874.31	873.88
Sulfidation degree of Ni (%)	45.41	48.35	49.13	52.23



has the fewest medium and strong B acid sites, but its active phase dispersion degree and stacking number are higher than those of NiW/SAPO-11, resulting in lesser n- C_{16} conversion and higher isomer selectivity than NiW/SAPO-11. **Figure 10D** shows the yield of i- C_{16} for various catalysts, and the yield of i- C_{16} for NiW/NiSAPO-11 is clearly higher than the other three catalysts. The maximum yield of i- C_{16} of different catalysts increased in the order of NiW/SAPO-11

(32.10%) > NiW/Ni@SAPO-11 (42.41%) > NiW/Ni-SAPO-11 (66.82%) > NiW/NiSAPO-11 (71.40%). These results indicate that the complexation-excessive impregnation-modified SAPO-11-supported NiWS catalyst has a better catalytic performance than that of ion-exchange modified SAPO-11 support NiWS catalyst, unmodified SAPO-11-supported NiWS catalyst, and *in situ* Ni-modified SAPO-11 support NiWS catalyst for n-hexadecane hydroisomerization.

TABLE 6 | Isomer distributions, TOF values, and k_{iso} values of n-C₁₆ hydroisomerization over the different catalysts at 340 °C.

Products		Selectivity (%)								
	NiW/SAPO-11	NiW/Ni@SAPO-11	NiW/Ni-SAPO-11	NiW/NiSAPO-11						
Selectivity of C ₁₆ (%)	57.92	80.81	88.30	90.81						
TOF (h^{-1})	26.29	26.72	30.41	31.22						
k_{iso} (mol g^{-1} h^{-1})	7.26×10^{-3}	5.80×10^{-3}	1.16×10^{-2}	1.21×10^{-2}						
2-MC ₁₅	13.57	16.99	17.87	19.77						
3-MC ₁₅	13.65	19.07	20.43	18.25						
4-MC ₁₅	7.17	12.74	13.27	16.31						
5-MC ₁₅	7.18	8.81	10.01	8.78						
6-MC ₁₅	4.54	5.41	5.95	6.17						
2,4-DMC ₁₄	3.10	4.18	5.72	5.69						
2,5-DMC ₁₄	2.92	4.23	4.91	4.42						
2,6-DMC ₁₄	1.98	3.31	3.35	3.87						
3,6-DMC ₁₄	1.13	1.88	2.37	3.03						
3,7-DMC ₁₄	0.77	1.21	1.38	1.77						
3-EC ₁₄	0.43	0.73	0.76	1.13						
5-EC ₁₄	0.38	0.78	0.83	0.97						
6-EC ₁₄	0.32	0.55	0.48	0.55						
5,8-DEC ₁₂	0.28	0.44	0.25	0.45						
Others	0.50	0.48	0.72	0.65						

The isomer product distributions, TOF values and kiso values of different catalysts at 340°C are presented in **Table 6**. The reaction rate constants of different catalysts increased in the order of NiW/Ni@SAPO-11 $(5.80 \times 10^{-3} \text{ mol g}^{-1} \text{ h}^{-1}) < \text{NiW/SAPO-11}$ $(7.26 \times 10^{-3} \text{ mol g}^{-1} \text{ h}^{-1}) < \text{NiW/Ni-SAPO-11} (1.16 \times 10^{-3} \text{ mol g}^{-1} \text{ h}^{-1})$ $10^{-2} \text{ mol g}^{-1} \text{ h}^{-1}$) < NiW/NiSAPO-11 (1.21 × $10^{-2} \text{ mol g}^{-1} \text{ h}^{-1}$), which is due to the difference between the amount of medium and strong B acid in the three supports. While the TOF values of the three catalysts decreased in the order of NiW/NiSAPO-11 $(31.22 \text{ h}^{-1}) > \text{NiW/Ni-SAPO-11} (30.41 \text{ h}^{-1}) > \text{NiW/Ni@SAPO-11} (26.72 \text{ h}^{-1}) > \text{NiW/SAPO-11} (26.29 \text{ h}^{-1})$, and the calculated TOF values well verified the catalytic activity of the catalysts. This result can be explained by the fact that the weakening of the interaction between the active phase and the support promoted more active phases to form "type II active phase", which increased the desorption rate of carbocation on the active phase. The isomer products of different catalysts were mainly mono-branched isomer products, and monomethyl branched isomer products were the main mono-branched isomer products.

CONCLUSION

The ion-exchange method, in situ synthesis method, and complexation-excessive impregnation modification method successfully prepared Ni-modified SAPO-11 molecular sieves, and the corresponding NiW-supported catalysts were successfully prepared by the incipient-wetness impregnation method, and then used for hydroisomerization of n-hexadecane. The effects of several Ni-modification procedures on the properties of SAPO-11, particularly the active phase properties on the related catalysts, were studied. The results showed that the crystal structure of Ni@SAPO-11 prepared by the ion-exchange method collapsed partially, and nickel species occupied a

portion of the pore volume and covered a portion of the acid sites, resulting in a drop in specific surface area, pore volume, and acid sites amount. Ni-SAPO-11 produced in situ had a larger specific surface area, pore volume, and medium and strong Brønsted acid sites. However, during dealumination, EDTA had the effect of dredging channels and reaming holes, resulting in a larger BET specific surface area and pore volume of NiSAPO-11. Furthermore, EDTA made it simple to incorporate Ni species into the surface framework of the SAPO-11 molecular sieve rather than the bulk phase, resulting in NiSAPO-11 with better acidity. The support of NiW/NiSAPO-11 had the most Brønsted acid sites, the weakest interaction between active metals and support, and the highest dispersibility and stacking number of active phase, all of which were helpful to n-hexadecane hydroisomerization. NiW/NiSAPO-11 had much greater n-C₁₆ conversion, i-C₁₆ selectivity, and i-C₁₆ yield than the other catalysts. It is expected to provide theoretical guidance for the design of high-activity non-noble metal catalysts for the hydroisomerization of alkanes.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

XD designed experimental plans, performed main experimental work, analyzed and discussed results, and wrote the manuscript. YC assisted in the design of the scheme, performed the main experimental work and assisted in literature review and manuscript sorting. MS

participated in the manuscript writing. QW proposed the themes, ideas, and content of the manuscript research work, assisted in literature review and manuscript sorting. YZ guided experimental work and manuscript revision.

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Enhanced Heterogeneous Fenton Degradation of Organic Pollutants by CRC/Fe₃O₄ Catalyst at Neutral pH

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Fe₃O₄-based heterogeneous Fenton catalysts have been widely employed for degrading organic pollutants, however it is challenging to use them in highly efficient and recyclable application in wastewater treatment. In this work, carboxylate-rich carbon (CRC)-modified Fe₃O₄ magnetic particles are prepared by the sol-gel self-combustion method, where CRC is obtained from the carbonization of sodium gluconate. The CRC/Fe₃O₄ catalyst exhibits high heterogeneous Fenton degradation performance. The complete 10 mg L⁻¹ methylene blue (MB) removal is achieved in 180 min under conditions of 10 mM H₂O₂ and 1.00 g of L⁻¹ CRC/Fe₃O₄ at neutral pH. After five cycles, the structure and morphology of CRC/Fe₃O₄ composites remained unchanged and the catalytic activity also remained unaltered. Moreover, phenol, benzoic acid (BA), sulfamethazine (SMT), and tetracycline (TC) were also degraded in the heterogeneous Fenton reaction using CRC/Fe₃O₄ as a catalyst. The strong coordinating ability of -COOH/ -COO⁻ functionalities of CRC formed strong bonds with Fe(II/III) ions on the surfaces of Fe₃O₄ particles, which was conducive to adsorption of organic matter on the surface of the catalyst and promoted the occurrence of heterogeneous Fenton reactions. It was found that CRC/Fe₃O₄ had higher removal rates for the adsorptive exclusions of pollutants, such as TC and MB, whereas there were lower removal rates for phenol, BA, and SMT. This work brings potential insights for development of a novel adsorption-enhanced heterogeneous Fenton reaction for wastewater treatment.

Keywords: heterogeneous fenton, CRC@Fe3O4 catalyst, degradation, methylene blue, adsorption

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1 INTRODUCTION

Fenton oxidation technology is the most representative advanced oxidation process (AOP). The Fenton process has gained widespread acceptance for efficient degradation of recalcitrant organic contaminants (Pignatello et al., 2006; Wang and Wang, 2020; Coha et al., 2021; Zeng et al., 2021). However, the requirement of low pH and generation of huge amounts of iron sludge hinder widespread application. In order to avoid the drawbacks of the traditional Fenton reaction, iron oxide heterogeneous Fenton-like technology has been developed recently, in which iron oxide-catalyzed decomposition of H_2O_2 occurs to generate OH (He et al., 2016; Thomas et al., 2021). In fact, heterogeneous Fenton oxidation possesses inherent advantages, such as a wide pH application range, lower peroxide consumption, and recyclability *via* catalyst regeneration, over homogeneous Fenton oxidation (Lai et al., 2021; Xiea et al., 2021). The principal objectives behind developing heterogeneous Fenton oxidation technology are to prepare highly efficient, cheap, and easy to separate solid-phase catalysts.

Fe₃O₄ has been widely studied for its excellent magnetic separation performance (Wu et al., 2015; Xu et al., 2018; Adewunmi et al., 2020). Its magnetic properties allow for easy, fast, and inexpensive separation from the reaction medium. In addition, the potential of Fe₃O₄ derives from the higher ability for degradation of recalcitrant pollutants compared to the conventional iron-supported catalysts due to the presence of both Fe(II) and Fe(III) species (Munoz et al., 2015). However, Fe₃O₄ magnetic nanoparticles agglomerate easily because of their highly specific surface energy, resulting in uneven particle size (Liu et al., 2020). Therefore, the exposed Fe₃O₄ is easily oxidized, resulting in the reduction of magnetic properties (Yan et al., 2009). Again, at low pH, Fe₃O₄ magnetic nanoparticles are easily etched, affecting their morphology and properties, whereas Fe₃O₄ Fenton catalytic performance is inhibited when the pH of solution is weakly alkaline.

In order to overcome the above drawbacks, functionalization of nanoparticles is expected to be an effective alternative method (Zhu et al., 2018). Wrapping of inorganic materials, organic functional groups, such as -COOH, -NH₂, and -SH, and biological macromolecules on the particle surface or superficial modification improve stability and functionalities of particles (Wulandari et al., 2018; Khatamian et al., 2019; Wang et al., 2021). The as-obtained multifunctional magnetic nanoparticles possess broader application prospects.

For synthesizing Fenton catalysis, Fe_3O_4 is first modified by humic acid (HA) to impart elevated photosensitivity, followed by modification with organic chelating agents to enhance the iron cycle and superficial compounding of the polymer to improve dispersion and stability. Klamerth et al. (Klamerth et al., 2011) pointed out that HA is a good choice for the improved optical Fenton system with a pH value of 6.5. Hua et al. (Hua et al., 2021) reported that the coating of catechol polymer on Fe_3O_4 enhanced the iron cycle and promoted the Fenton reaction. Again, Xue et al. (Xue et al., 2019) used electrospinning technology to prepare porous polycaprolactone composite nano Fe_3O_4 membrane synergy of the porous surface and embedded Fe_3O_4 nanoparticles to degrade methylene blue in the Fenton reaction. The surface modification of Fe_3O_4 improved its stability and catalytic efficiency, which is a potential research direction of Fenton heterogeneous catalysis.

Hence, in this work, CRC/Fe_3O_4 magnetic composites were synthesized by the sol-gel self-combustion method (Qu et al., 2016). The CRC/Fe_3O_4 samples were characterized and applied in the Fenton process to degrade MB. The effects of H_2O_2 and catalyst dosage, initial MB concentration, and pH value on the catalytic activity were investigated. The stability and recyclability of catalysts were also evaluated. The adsorption and heterogeneous Fenton degradation of phenol, benzoic acid (BA), sulfamethazine (SMT), tetracycline (TC), and MB were discussed to propose a possible adsorption/catalytic mechanism.

2 EXPERIMENTAL

2.1 Chemicals

All chemicals were of analytical grade and used without further purification. Ferric chloride (FeCl₃·6H₂O), sodium gluconate (C₆H₁₁NaO₇), hydrogen peroxide (H₂O₂, 30 wt.%), methylene

blue ($C_{16}H_{18}ClN_3S$), tetracycline ($C_{22}H_{24}N_2O_8$), sulfamethazine ($C_{12}H_{14}N_4O_2S$), phenol (C_6H_6O), and benzoic acid (C_6H_5COOH) were purchased from Sigma-Aldrich (China). All solutions and suspensions were prepared by using deionized water.

2.2 Preparation and Characterization of Catalysts

Preparation of CRC/Fe $_3$ O $_4$ magnetic composites by sol-gel self-combustion: A certain mass of sodium gluconate and FeCl $_3$ ·6H $_2$ O were dissolved in 20 ml of distilled water, followed by the addition of 1.0 mol L $^{-1}$ of NaOH solution to adjust the pH to 7. The as-obtained solution was stirred continuously at room temperature for 30 min, followed by solvent evaporation on a petri dish at 80°C for 1–2 h to obtain the gel. The as-obtained gel was then transferred to the crucible, covered, heated in a muffle furnace at 350°C for 2 h, and neutrally cooled to room temperature. Thereafter, the synthetic composite was ground and crushed, washed several times with distilled water and ethanol, separated by magnet, and dried at 60°C for 2 h.

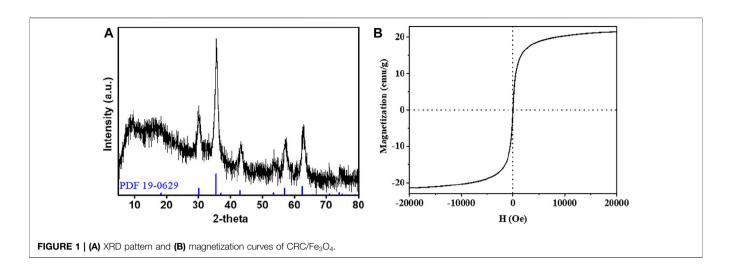
The morphology and size distribution of CRC/Fe₃O₄ were observed by a scanning electron microscope (SEM, Pheonom ProX, Netherlands). The phase structures were determined by X-ray diffraction (XRD, PANalytical-PW3040/60, Netherlands). To verify the formation of CRC, surface chemistry was analyzed using a Fourier transform infrared (FTIR) spectrometer (Bruker TENSOR II Hyperion 2000, Germany). Thermal stabilities of CRC/Fe₃O₄ were assessed by a thermogravimetric analyzer (TGA, TGA/DSC PerkinElmer- TGA4000, US). The zeta potentials of the catalyst suspensions at different pH values were determined by an analyzer (Zetasizer, Malvern 3000).

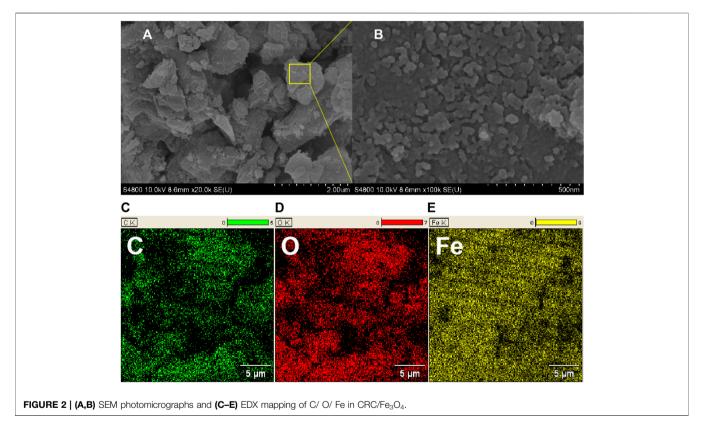
2.3 Degradation Procedures

The degradation procedures were carried out in a 100 ml beaker shaken at a speed of 200 rpm. In a typical reaction, 50 ml of MB solution of a certain concentration was prepared by adding the specified amount of CRC/Fe₃O₄. The pH of reaction solution was adjusted to the required value by using 1.0 mol L⁻¹ of H₂SO₄ or 1.0 mol L⁻¹ of NaOH solutions. Degradation reactions were initiated by adding H₂O₂ to the suspension after attainment of the adsorption equilibrium. At pre-determined time intervals, 0.5 ml of sample suspension was withdrawn and the on-going reaction was quenched immediately by adding 30 μ L of pure methanol. The solid particles were separated from the solution using an external magnet. The supernatant liquid was collected for analysis. Each experiment was run in triplicate and the arithmetic mean of the three measured values was used in the reported data.

2.4 Analytical Methods

The concentration of MB was measured by UV-vis spectroscopy at the fixed wavelength of 660 nm, which is the maximum absorption wavelength of MB. The concentration of other organic matters (Phenol, BA, SMT, TC) were determined by liquid chromatography-mass spectrometry (H-class/ QDA, waters, United States). The total leached iron was measured using the orthophenantroline complexometric method (λ = 510 nm).





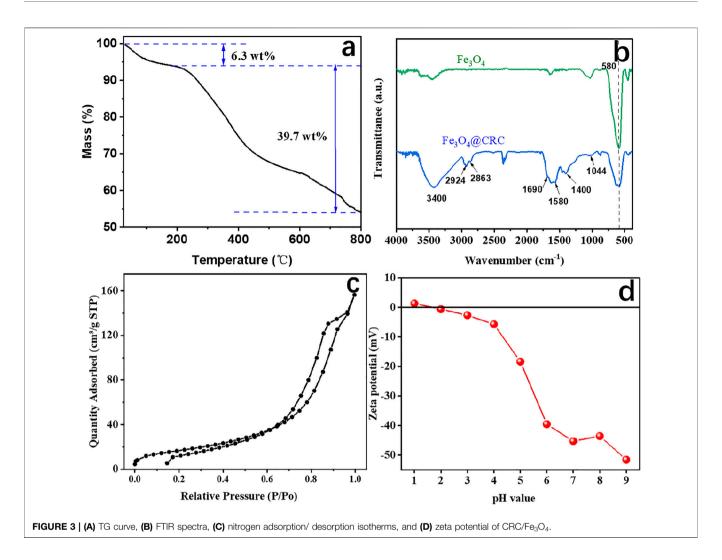
3 RESULTS AND DISCUSSION

3.1 Formation of CRC/Fe₃O₄

The XRD patterns of CRC/Fe₃O₄ contained sharp crystalline peaks at $2\theta = 30.3$, 35.6, 43.3, 53.7, 57.2, and 62.7° (**Figure 1A**), attributed to (220), (311), (400), (422), (511), and (440) planes of the cubic spinel structure of Fe₃O₄ (JCPDS 19–0629), respectively. In CRC/ Fe₃O₄, the absence of the characteristic peaks of carbon either individually or overlapped with the strong peaks of Fe₃O₄ inferred the presence of amorphous carbon. The magnetic properties of

 CRC/Fe_3O_4 were studied using a superconducting quantum interference device (SQUID) magnetometer at room temperature. The hysteresis loop of CRC/Fe_3O_4 (**Figure 1B**) indicated the magnetic saturation (Ms) of CRC/Fe_3O_4 was approximately 21.4 emu g⁻¹.

From the SEM photomicrograph of CRC/ Fe_3O_4 (**Figure 2**), particles of uniform sizes and shapes were observed. The particle size distribution of cubic Fe_3O_4 was within 30–40 nm. Meanwhile, the energy dispersive X-ray (EDX) spectroscopy study verified the existence and even distribution of Fe, O, and C in CRC/ Fe_3O_4 .



The carbon content in CRC/Fe $_3$ O $_4$ was determined by TG analysis performed under air (**Figure 3A**). The 6.3 wt% mass loss in CRC/Fe $_3$ O $_4$ up to 190 °C was attributed to the loss of loosely adhered water and structural water molecules. However, major degradation took place within 190–800°C because of the combustion of carbon giving rise to a large weight loss of about 39.7 wt%. While considering that Fe $_3$ O $_4$ would be converted to Fe $_2$ O $_3$ when heated in air, the actual carbon content in CRC/ Fe $_3$ O $_4$ could be estimated to be lower.

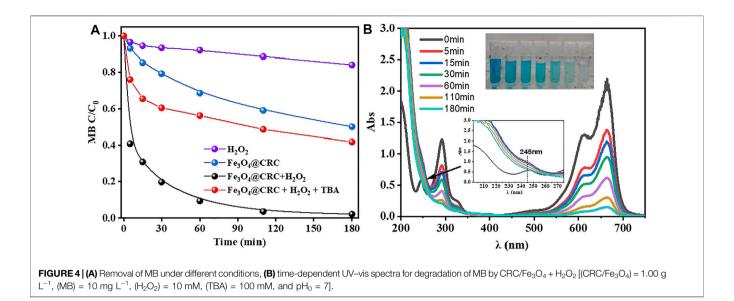
Figure 3B displays the FTIR spectra of the as-prepared samples. In Fe₃O₄, the presence of Fe–O was identified by the peaks around 580 cm⁻¹ (Leng et al., 2013). In CRC/Fe₃O₄, the incorporation of CRC was envisaged from the prevalent CRC-specific functionalities, such as C–O, C–C, C=O, C–H, and O–H. For instance, the small peaks at 1,044 and 1,580 cm⁻¹ indicated C–O *str.* and C–C *str.* of the aromatic ring, respectively (Qu et al., 2013). Again, peaks at 1,690 and 1,400 cm⁻¹ were assigned to C=O *str.*, which envisaged the abundance of carboxylate functionalities in the carbon shell. The absorption peaks of H–C–H *str.* were detected at 2,924 and 2,863 cm⁻¹ (Le et al., 2021). The peaks at 3400 cm⁻¹ indicated the presence of large numbers of hydroxyl groups in CRC/ Fe₃O₄ (Kong et al., 2002).

Surface area, pore volume, and pore size distribution of CRC/ ${\rm Fe_3O_4}$ were analyzed by nitrogen adsorption-desorption techniques. According to **Figure 3C**, the type-IV isotherm pattern of CRC/ ${\rm Fe_3O_4}$ was characteristic of mesoporous materials. However, in CRC/ ${\rm Fe_3O_4}$, the prevalent narrower hysteresis loop and steep increase in adsorption at P/P₀ close to 0.7 indicated the presence of macropores. The BET surface area and total pore volume were measured to be 42.44 m² g⁻¹ and 0.0125 cm³ g⁻¹, respectively. Because of the significant population of carboxylate functionalities in CRC, the zero point charge of CRC/ ${\rm Fe_3O_4}$ was found to be approximately 1.7 (**Figure 3D**). Moreover, zeta potentials of CRC/ ${\rm Fe_3O_4}$ became more negative with the increasing suspension pH. Abundant numbers of negative charges on the surface of CRC/ ${\rm Fe_3O_4}$ benefited the sorption of positively charged metal ions, such as Fe(II) ions.

3.2 Heterogeneous Fenton Catalytic Activity of CRC/Fe₃O₄

3.2.1 CRC/ Fe₃O₄ Catalytic Activity

The catalytic activity of CRC/Fe_3O_4 was evaluated by MB degradation experiments through the Fenton reaction. As



indicated in **Figure 4A**, after 180 min of reaction, MB was removed almost completely, whereas in absence of the catalyst, the degradation of MB in the $\rm H_2O_2$ system was kinetically slower to ensure only 16% removal at 180 min. Again, in the absence of $\rm H_2O_2$, 50% of MB was adsorbed onto CRC/Fe₃O₄. Interestingly, in **Figure 4B**, absorption peaks at 660/ 290 and 245 nm decreased significantly and disappeared, respectively, after initiation of the reaction. At the same time, the UV absorption within 200–270 nm increased significantly, indicating degradation of MB and the simultaneous formation of some small molecular organics.

TBA was added into the CRC/Fe $_3O_4$ -H $_2O_2$ system to capture ·OH, as shown in **Figure 4A**. Herein, after TBA was added, the removal rate of MB dropped to 59% at 180 min, confirming that ·OH is the most important active oxygen species in the system. At neutral conditions, there were few iron ions dissolved in the bulk solution, and the reaction mainly occurred on the surface of the catalyst. The CRC/Fe $_3O_4$ catalytic degradation of MB can be attributed to the synergistic effects of catalyst adsorption and degradation. Since the surface of the sodium gluconate-modified Fe $_3O_4$ catalyst possessed a highly developed pore structure and plenty of functionalities, the porous CRC/Fe $_3O_4$ structure provided a larger specific surface area to adsorb a higher amount of MB, thereby increasing the relative concentration of pollutants. At the same time, H $_2O_2$ also reacted on the surface of the catalyst to form ·OH and reacted with MB. Adsorption is a controlled step of MB degradation.

3.2.2 Effects of Degradation Conditions

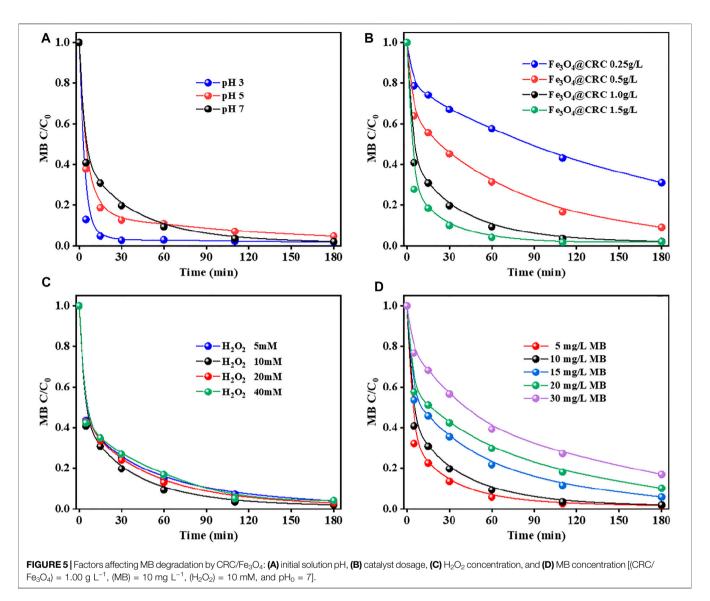
In the study of conventional Fenton treatment, the best result can be obtained at pH 3. Under neutral or alkaline conditions, it is not conducive to treat MB wastewater because of the restricted degradation treatment and research of MB. Herein, the catalytic activities of CRC/Fe $_3$ O $_4$ were studied at different pH values. As can be seen from **Figure 5A**, MB could be completely degraded within 180 min within pH 3-7, indicating that CRC/ Fe $_3$ O $_4$ has good applicability in a wide pH range. In fact, the fastest degradation rate at pH 3 was mainly caused by the dissolution of iron ions (\sim 0.16 mmol/L), replicating the homogeneous Fenton reaction.

However, no significant difference in the reaction rates were observed for pH=5 and 7 because of the poor iron ion concentration (<0.01 mmol/L). The heterogeneous Fenton catalytic degradation reaction occurred after adsorption of MB on the catalyst.

Figure 5B shows the degradation of MB by CRC/Fe₃O₄ under different catalyst dosages. Results showed that when the dose of CRC/Fe₃O₄ increased from 0.25 to 1.00 g L⁻¹, the removal efficiency of MB improved gradually, while the removal efficiency exhibited negligible change when the dose of CRC/Fe₃O₄ increased beyond 1.50 g L⁻¹. This was because with the increase in the amount of catalyst, the surface area and active sites, responsible for the acceleration of H₂O₂ decomposition, also increased. However, with the further increment in the amount of catalyst, agglomeration of catalyst particles and excessive iron accumulation removed ·OH, which inhibited the increment of the removal efficiency of MB (Phan et al., 2018; Qin et al., 2018; Xiao et al., 2018). When the amount of catalyst was varied within 1.00–1.50 g L⁻¹, no significant effect on the final removal rate of MB was observed.

The concentration of H_2O_2 plays an important role in the heterogeneous Fenton process because it is directly related to the amount of \cdot OH produced. Generally, the amount of \cdot OH produced is directly proportional to the concentration of H_2O_2 , that is, the higher the concentration of H_2O_2 , the more \cdot OH produced, and the more degradation of pollutants. However, when the concentration of H_2O_2 exceeds the critical value, the degradation rate may be limited because of the reaction of \cdot OH with excess H_2O_2 and the conversion into a hydrogen peroxide radical (Liu et al., 2019). As shown in **Figure 5C**, with an increase in the initial H_2O_2 concentration from 5 to 20 mM, the removal rate of MB did not improve significantly. This observation inferred that a lower concentration of H_2O_2 is sufficient for the degradation of MB, and CRC/Fe₃O₄ as a catalyst has a good utilization rate of peroxide.

The initial concentration of MB affects the adsorption and degradation of the catalyst. As seen in **Figure 5C**, with the increase in MB concentration, the degradation efficiency was found to decrease gradually. When the initial MB concentration was 5 mg $\rm L^{-1}$, 90% MB removal could be achieved after 30 min. The



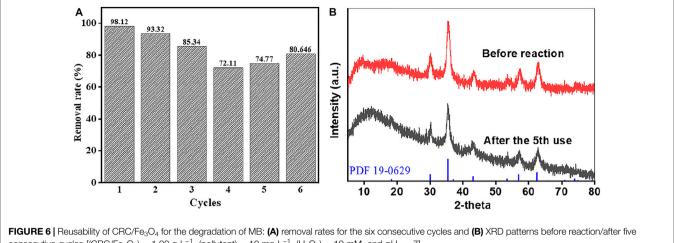
degradation of 10 mg L^{-1} MB was similar to that of 5 mg L^{-1} . However, the degradation rates of MB at 15, 20, and 30 mg L^{-1} were 46.41, 42.47, and 23.30%, respectively. However, the degradation rates of MB at 15, 20, and 30 mg L^{-1} were 46.41, 42.47, and 23.30%, respectively (**Figure 5D**). The higher the MB concentration, the longer the duration of the degradation process. This was because the amount of \cdot OH produced in the reaction system became constant when the dose of the CRC/Fe₃O₄ catalyst and H₂O₂ were constant. For the lower dye concentration, the \cdot OH in the solution would be relatively excessive. However, with the increase in dye concentration, the \cdot OH produced in the solution should be relatively insufficient. Therefore, it became necessary to prolong the reaction time to remove the higher concentration of the MB solution.

3.2.3 CRC/Fe₃O₄ Stability and Reusability

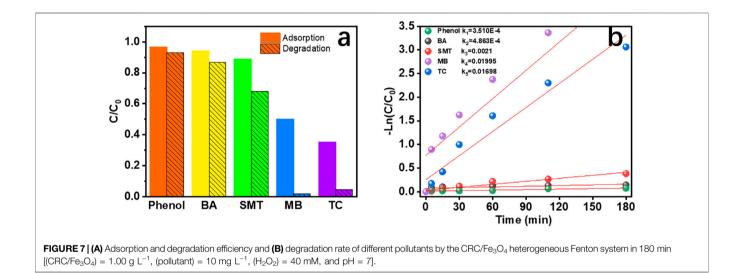
Stability and reusability of materials are extremely important for an effective catalyst. In this study, MB was continuously degraded by the heterogeneous Fenton reaction with CRC/Fe₃O₄ under the same conditions, and its stability was evaluated. As shown in **Figure 6A**, the

catalytic performance of CRC/Fe $_3$ O $_4$ declined in six consecutive cycles, because of the possible loss of active sites and adsorption of by-products during MB degradation (Doan et al., 2019). Importantly, after five continuous uses, the CRC/Fe $_3$ O $_4$ composite still maintained high degradation efficiency. Additionally, at pH = 7, the total dissolved concentration of leached iron was lower than that of the detection limit. As demonstrated in **Figure 6B**, there was no obvious change in XRD pattern after five consecutive cycles.

Figure 7A shows the adsorption and degradation efficiency of CRC/Fe_3O_4 for phenol, BA, SMT, MB, and TC, of which adsorption and degradation of phenol and BA were poor. The adsorption/removal rates of SMT, MB, and TC were 12/20%, 50/98%, and 65/95%, respectively. The degradation trend of organic pollutants was similar to the adsorption trend on the surface of the CRC/Fe_3O_4 catalyst, since adsorption of contaminants promotes their catalytic degradation. The same trend is also reflected in the degradation rate in **Figure 7B**. The synergistic effects of adsorption and catalytic degradation significantly improved the removal effect of organic matter.



consecutive cycles [(CRC/Fe₃O₄) = 1.00 g L⁻¹, (pollutant) = 10 mg L⁻¹, (H₂O₂) = 10 mM, and pH₀ = 7].



4 CONCLUSION

This study reports the spontaneous synthesis of CRC/Fe₃O₄ magnetic particles by the sol-gel combustion method and their catalytic properties and related mechanisms. CRC is conducive towards adsorption of organic matter on the surface of the catalyst and promotes the occurrence of heterogeneous Fenton reactions. Under neutral conditions, the CRC/Fe₃O₄ heterogeneous Fenton reaction predominantly occurs on the surface of the catalyst. Therefore, adsorption of pollutants on the surface of the catalyst is closely related to the CRC/Fe₃O₄ heterogeneous Fenton degradation effect, and the larger the adsorption amount, the higher the degradation removal rate. Experimental results infer that CRC/Fe₃O₄ is negatively charged and therefore possesses better adsorption and degradation of positively charged substances. Further modification of materials is expected to enable selective removal of specific contaminants.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding authors.

AUTHOR CONTRIBUTIONS

CW: Conceptualization, methodology, and writing-original Investigation and formal analysis. Conceptualization, Writing-Reviewing and Editing. PW: Resources and Supervision.

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Synergistic Fluoride Adsorption by Composite Adsorbents Synthesized From Different Types of Materials—A Review

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Wei Y, Wang L, Li H, Yan W and Feng J (2022) Synergistic Fluoride Adsorption by Composite Adsorbents Synthesized From Different Types of Materials—A Review. Front. Chem. 10:900660. doi: 10.3389/fchem.2022.900660 The reduction of fluoride concentrations in water is one of many concerns. Adsorption is the most widely used technology for fluoride removal and the center to development of adsorption technology is the improvement of adsorbents. This review classifies the typical fluoride removal adsorbents into four types: metal oxides/hydroxides, biopolymers, carbon-based, and other adsorbents. The exploitation of new materials and the synthesis of composite materials are two ways of developing new adsorbents. In comparison to the discovery of novel adsorbents for fluoride adsorption, research into the composite synthesis of different types of conventional adsorbents has proliferated in recent years. The traditional adsorbents used the earliest, metal oxides, can act as active centers in a wide range of applications for modifying and compounding with other types of adsorbents. This study emphasizes reviewing the research on fluoride removal by composite adsorbents synthesized from different types of metal-modified materials. Seven factors were compared in terms of material characterization, initial fluoride concentration, adsorbent dose, pH, temperature, reaction time, and maximum adsorption capacity. The modification of composite adsorbents is facile and the synergistic effect of the different types of adsorbents significantly improves fluoride adsorption capacity. Metal composite adsorbents are synthesized by facile coprecipitation, hydrothermal, or impregnation modification methods. The adsorption mechanisms involve electrostatic attraction, ion exchange, complexation, and hydrogen bonding. The fluoride adsorption capacity of composite adsorbents has generally improved, indicating that most modifications are successful and have application prospects. However, to achieve significant breakthroughs in practical applications, numerous issues such as cost, separation/regeneration performance, and safety still need to be considered.

Keywords: fluoride adsorption, metal oxides/hydroxides, carbon-based adsorbents, biopolymer, modification

1 INTRODUCTION

Fluoride ions in water have a strong affinity with positively charged elements such as calcium (Bhatnagar et al., 2011), which is a major component of human bone and tooth structure (Rehman et al., 2015). Low concentrations of fluoride in drinking water (0.5-1.5 mg/L) (Chen et al., 2017) can strengthen bones and prevent dental caries, while excessive concentrations of fluoride (4-10 mg/L) can cause diseases such as fluorosis, osteoporosis, brittle bones, brain damage, and several thyroid disorders (Kumar et al., 2020). Excessive fluoride concentrations in water have become a public health concern in developing countries. High concentration (>10 mg/L) fluorinated wastewater is easier to treat and can be removed or reduced by coagulation, precipitation, electrochemistry, and other methods. The treatment of low concentration (2–10 mg/L) fluorinated wastewater is relatively difficult and is also a current research hotspot. The treatment methods include adsorption (Lin et al., 2016), membrane separation, ion exchange (Xu et al., 2017), nanofiltration (Wang A. et al., 2018), reverse osmosis (Ye et al., 2019), and electrodialysis (Fan et al., 2019). Among them, the adsorption method has the advantages of low cost, high flexibility, simple operation, and high efficiency (Sarkar et al., 2019). It is the most widely used and the treatment effect is more satisfactory.

The treatment effectiveness of the adsorption method is influenced by a number of factors, including adsorbent properties, fluoride ion selectivity, compatibility, solution pH, temperature, co-existing ions, and contact time (Pigatto et al., 2020). It mainly depends on the adsorbent properties such as particle size, pore size structure, zero charge point (pH_{PZC}), and specific surface area (S_{BET}) (Biswas et al., 2017). High specific surface area (developed pore structure) and ideal chemical surface (abundant functional groups) are two essentials for effective removal of fluoride by adsorbents. Although not systematically categorized, this review found that the main traditional sorbents frequently used for fluoride removal are metal oxides/hydroxides (Dhillon et al., 2017), low-cost carbon materials (Zhang X. et al., 2021), biomolecular materials (Jia et al., 2018), and others such as clay, hydroxyapatite, and graphite. This review classifies the more researched fluoride removal adsorbents into four categories: metal oxide/hydroxide adsorbents, biopolymer adsorbents, carbon-based adsorbents, and other adsorbents (industrial waste, minerals, etc.).

For the development of new adsorbents, the discovery of novel adsorbents that have never been used before and the composite material synthesis by combining traditional adsorbents are the two main approaches to improve adsorption capacity. In comparison to the discovery of novel adsorbents that have never been used before, research into the composite synthesis of different types of conventional adsorbents for fluoride adsorption has proliferated in recent years. The emphasis of this study is placed on the fluoride adsorption effect of this adsorbent compounded from different types of conventional adsorbents. The study of other types of metal-modified adsorbents accounts for a major part. A total of seven factors were compared in terms of material characterization, initial fluoride concentration, adsorbent

dose, pH, temperature, reaction time, and maximum adsorption capacity.

2 CONVENTIONAL TYPES OF ADSORBENTS

2.1 Metal Oxide/Hydroxide Adsorbents

Metal oxide/hydroxide nanoparticles were reported to show an affinity for fluoride and high performance in fluoride removal. The high reactivity (Lanas et al., 2016), specificity, specific surface area (Rathore and Mondal 2017), stability, and self-assembly potential have attracted attention in fluoride removal studies. Nanoscale dimensions with desirable physicochemical properties, such as high density of hydroxyl ions on the high specific surface area, will further enhance the fluoride adsorption capacity.

2.1.1 Aluminum Oxide/Hydroxide

Aluminum oxide/hydroxide was the earliest studied and used adsorbents for fluoride removal (Chinnakoti et al., 2016a). Typically, aluminum hydroxide is first prepared by electrolysis or pyrolysis and then partially converted to aluminum oxide by calcination. One of the advantages of aluminum oxide/hydroxide adsorbents is the large specific surface area (Hafshejani et al., 2017), as shown in **Table 1**, and in general, $S_{BET} > 200 \,\mathrm{m}^2/\mathrm{g}$. Generally, high pH_{PZC} allows its surface to appear positively charged in water (Dhawane et al., 2018). Several studies have reported that the mechanism of fluoride adsorption by alumina mainly consists of electrostatic attraction and ion exchange (Rathore and Mondal 2017), as shown in Figure 1A; the monodentate complex Al-F is the major formation after adsorption (Kang et al., 2018; Lin et al., 2020). Kang et al. (2018) synthesized an amorphous alumina microsphere using solvothermal reaction and calcination, with $S_{BET} = 400 \text{ m}^2/\text{g}$ and a maximum adsorption capacity of 129.4 mg/g; they proposed that the adsorption mechanism involves chemical reaction and pore filling in addition to ion exchange and electrostatic attraction. However, aluminum is easily leached out in aqueous solutions, especially under acidic conditions (Lin et al., 2020), leading to high concentration of aluminum residues in drinking water, which is also a major threat to human health.

2.1.2 Rare Earth Metal Compounds

Compared to aluminum, the rare earth metals (cerium, titanium, lanthanum, etc.) have further affinity for fluoride due to the ability to stabilize in the +3 or +4 valence state with a few numbers of outermost electrons; therefore, sufficient empty orbitals are available for fluoride ions (Zhang K. et al., 2016). The solubility of rare earth metals is relatively limited over a wide pH range (Dhillon et al., 2016), so rare earth oxides/hydroxides have been increasingly investigated as substitution for aluminum in recent years. Among these, CeO₂ readily forms oxygen vacancies and, therefore, has particularly high oxygen storage/release capacity with high adsorption capacity (Kullgren et al., 2014; Wu and Gong 2016; Kang et al., 2017). Kang et al. (2017) compared the physicochemical characteristics and adsorption performance of different

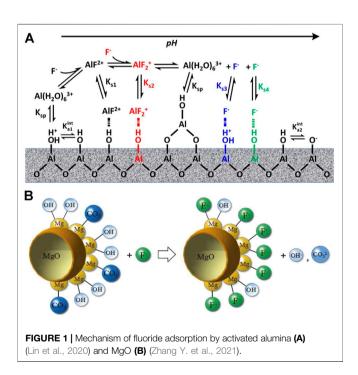
TABLE 1 | Summary of the preparation methods, characteristics, and adsorption mechanisms of four traditional adsorbents.

Adsorbents	Preparation method	Dimension	S _{BET} (m²/G)	Aperture (nm)	pH _{PZC}	Adsorption mechanism	Ref
Cactus-like amorphous alumina oxide microspheres	Solvothermal method without templates	40 µm	419.6	5.3	6.6	Chemical coordination, electrostatic attraction, and ion exchange	Kang et al. (2018)
Nano γ-alumina	Surfactant-assisted combustion	_	221	_	6.5	_	Chinnakoti et al. (2016a)
Mesoporous micro alumina	γ-AlOOH calcined at 873 K	0.9 mm	254.1	12.96	9.0	Electrostatic attraction	Lanas et al. (2016)
Al ₂ O ₃ nanoparticles	Flame spray pyrolysis (FSP)	9.8 nm	213	93	_	Electrostatic attraction	Hafshejani et al. (2017)
Porous-layered Al ₂ O ₃	Roasting of AlFu MOFs	_	329.3	3.8	_	Ion exchange, complexation	Yang et al. (2020)
Activated alumina	Al ₂ O ₃ cauterized at 673 K	1–3 mm	185.6	5.1	8.5	Lewis acid and base	Dhawane et al. (2018
Aluminum oxide/hydroxide	Electrolysis, calcination at 973 K	1.5 mm	253.2	4.7	7.52	Electrostatic attraction	Rathore and Monda (2017)
Cubical ceria nano-adsorbent	Coprecipitation, calcination at 473 K	4.5 nm	98	2.62	6	Ligand exchange, complexation	Dhillon et al. (2016)
CeO ₂ nanorods	Hydrothermal at 373 K	20*200 nm	111.4	8.65	_	Ce ³⁺ -O defect, ion exchange,	_
Pore filling	Kang et al. (2017)	_	_	_	_	_	_
CeO ₂ octahedron	Hydrothermal at 453 K	14 nm	160.2	9.66	_	_	_
CeO ₂ nanocubes	Hydrothermal at 473 K	25 nm	55.8	15.1	_	_	_
CeCO ₃ OH nanosphere	Hydrothermal	250 nm	10.6	15.5	_	Electrostatic attraction, ion exchange	Zhang et al. (2016b
Porous MgO nanoplates	Solvothermal, calcination	_	47.4	3.3	_	Ligand exchange	Jin et al. (2016)
Hollow MgO spheres	Hydrothermal, calcination at 773 K	2 µm	_	_	10	Ligand exchange	Zhang et al. (2021b
/licrosphere-like MgO	Hydrothermal, calcination at 773 K	46 µm	120.7	5.12	-	lon exchange	Lee et al. (2017)
Pillar-like MgO	Hydrothermal, calcination at 773 K	2*20 μm	99.44	6.26	-	lon exchange	Lee et al. (2017)
-Fe ₂ O ₃ nanoparticles	Precipitation	5–20 nm	_	_	8.13	Complexation	Jayarathna et al. (2015)
Trititanate nanotubes	Hydrothermal at 403 K, 1 h	8–12 nm	282	-	2.5	lon exchange, electrostatic attraction	Chinnakoti et al. (2016b)
ΓiO ₂	Solvothermal method	1 µm	31.9	_	6.5	Complexation	Zhou et al. (2019b)
anthanum alginate bead Biopolymer pectinandalginate	LaCl ₃ cross-linking Glutaraldehyde cross-	1 mm	2.618	1.441	_	lon exchange	Huo et al. (2011) Raghav et al. (2019
	linking mixture	_	_	_			
Porous zirconium alginate	CaCl ₂ cross-linking SA, Zr(NO ₃) ₄ immersion	2 mm	3	_	_	Electrostatic attraction, ion exchange	Qiusheng et al. (2015)
Shell biochar	Calcination at 1073 K	0.5 mm	4	413	6	Complexation	Lee et al. (2021)
Nanoscale rice husk biochar	Calcination at 873 K, ball milling	_	_	_	_	lon exchange	Goswami and Kuma (2018)
Mustard ash biochar	Carbonization at 873 K	_	_	_	_	_	Jadhav and Jadhav (2021)
Peanut shell biochar	Pyrolysis at 673 K, 1 h	_	98	7.05	_	_	Kumar et al. (2020)
Rhodophyta biochar	Calcined in muffle for 2 h	75 µm	320	1.28	5.4	Complexation	Naga Babu et al. (2020)
Rice husk biochar	Pyrolysis at 698 K in tube furnace	_	3	13.29	5.9	lon exchange	Yadav and Jagadevan (2020)
Activated sugarcane ash	Burning at 773 K in muffle furnace	150 µm	64	_	_	lon exchange	Mondal et al. (2016)
KOH-treated jamun seed	KOH activation, pyrolysis at 1173 K	_	748	2.19	4.9	Ligand exchange	Araga et al. (2017)
KOH-treated activated carbon	Carbonization with solid KOH at 873 K	_	1,006	1.95	6.11	Protonation, ion exchange	Bhomick et al. (2019
Activated carbon	Surfactant modification	_	_	_	6.86	Electrostatic attraction	Chen et al. (2019)
Coconut-shell carbon	Carbonization at 1173 K in tube furnace	500 nm	358	_	_	Electrostatic attraction	Araga et al. (2019)
Chicken bone biochar	Burning at 873 K in muffle furnace	159 µm	126	_	_	Ion exchange	Herath et al. (2018)
Bone char	_	0.8 mm	104	11.4	8.4	Electrostatic attraction	Medellin-Castillo et al. (2014)

(Continued on following page)

TABLE 1 (Continued) Summary of the preparation methods, characteristics, and adsorption mechanisms of four traditional adsorbents.

Adsorbents	Preparation method	Dimension	S _{BET} (m²/G)	Aperture (nm)	pH _{PZC}	Adsorption mechanism	Ref
Bovine bone biochar	Burning at 773 K in muffle furnace	-	115	3.823	2.2	lon exchange	Zhou et al. (2019a)
Kaolinite	Alkali-hydrothermal	_	18	4	5	Ion exchange	Wang et al. (2017b)
Activated clay	Sulfuric acid activation	_	167	4.9	_	_	Guiza et al. (2019)
Fly ash-paper mill lime mud	Mixing, calcination	60 µm	58.9	_	_	Ligand exchange, complexation	Ye et al. (2019)
Natural clay	_	-	-	_	8	_	Nabbou et al. (2019)
Natural pumice	_	200 µm	9.5	_	3	_	Dehghani et al. (2016)
Natural zeolite	NaOH activation	_	_	_	_	Ion exchange, H-bonding	Cheng et al. (2018)
Clay	Heat treatment at 573 K	_	44.29	_	6	_	Zhang et al. (2016c)
Scoria	HCl immersion for 24 h	_	_	_	_	Ion exchange, complexation	Asadi et al. (2018)
Porous nanohydroxyapatite	Organic template coprecipitation	25 nm	41.3	-	6.8	Lattice substitution, precipitation	Wimalasiri et al. (2021)
Hierarchical hydroxyapatite	Ca and phosphate hydrothermal at 393 K	2 µm	83.17	11.52	7.73	Electrostatic attraction, ion exchange	Gao et al. (2019)
NaP-hydroxyapatite	Hydrothermal with zeolite gel at 373 K	2 µm	45	13.7	_	Ion exchange	Zendehdel et al. (2017)
Hydroxyapatite	Aqueous double decomposition	_	_	_	_	Ion exchange	Mourabet et al. (2015)



morphologies of CeO_2 (nanorods, octahedrons, and nanocubes) prepared under different hydrothermal conditions. The different morphologies of CeO_2 were found to expose distinct crystalline surfaces and proportions of oxygen defects, leading to significant differences in fluoride adsorption capacity, with CeO_2 nanorods having the largest $Q_{\rm max}$ (71.5 mg/g). However, rare earth metal oxides are costly, prone to agglomeration, and high leaching concentrations can be toxic to water (Yu et al., 2015).

2.1.3 Magnesium Oxide

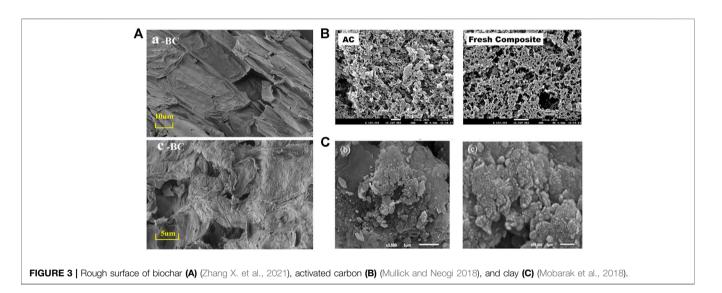
MgO is less dissolved, nontoxic, abundant in reserves compared to other metals, and has an affinity for fluoride (Jin et al., 2016), giving it an opportunity to be used. It has been reported that MgO has a high isoelectric point and relies on electrostatic attraction to adsorb fluoride (Suzuki et al., 2013). Y. Zhang et al. tested the zeta potential of hollow MgO spheres of $pH_{PZC}=10$, which is the highest value reported. In order to improve the morphology, Z. Jin et al. used a typical solvothermal method followed by calcination to form porous MgO nanoplates with an increased maximum adsorption capacity from 115.5 mg/g to 185.5 mg/g. They suggested that the mechanism of adsorption mainly consists of ligand exchange between fluoride and hydroxyl groups and carbonates on the surface of MgO (**Figure 1B**). Thus, the presence of carbonate in the solution can affect the fluoride adsorption capacity of MgO.

The most significant problem concerning metal oxide/hydroxide nanoparticles is low structural stability and the tendency to leach in water causing secondary contamination (Lin et al., 2020).

2.2 Biopolymer Adsorbents

Biopolymers are the natural macromolecular materials derived from cellular or extracellular substances with properties such as biodegradability, nontoxicity, low waste generation, low leaching, biocompatibility, and hydrophilicity. The most researched fluoride removal biopolymer adsorbents in recent years include sodium alginate (SA), pectin, chitosan (CS), and carboxymethyl cellulose (CMC) (Araga and Sharma 2019). Hydrogels formed by chemical or physical cross-linking of biopolymers have hydrophobic, three-dimensional network structures, which are easier to separate compared to the

FIGURE 2 | Ionic cross-linking procedure of sodium alginate (A) (Sharma et al., 2019) and fluoride adsorption mechanism of pectin (B) (Raghav and Kumar 2019).



powder state, making them an environment-friendly adsorbent.

2.2.1 Sodium Alginate

Sodium alginate (SA) and pectin are both natural polysaccharides in colloidal form. Sodium alginate contains large numbers of -OH and -COOH groups on the main chain. The -COOH in the M unit is more bound by the surrounding electron cloud, while the -COOH in the G unit is arranged in the corner of the peak consisting of two adjacent carbon atoms; thus, G unit is more reactive (Wu T. et al., 2017). In the ionic cross-linking process (**Figure 2A**), when the dissolved colloidal sodium alginate is dropped into the solution of high-valent metal cations (Ca²⁺, Ce³⁺, Fe³⁺, Al³⁺, La³⁺, etc.), the high-valent cations in the solution will rapidly replace Na⁺ (Wu et al., 2016a). The embedded high-valent cations form ligand chelate crosslinks with the oxygen atoms in the carboxyl and hydroxyl groups of the G-units, which form irreversible hydrogel-like microbeads (Qiusheng et al., 2015). The thermal stability and acid resistance of sodium

alginate are further improved after the formation of the gel, while some of the carboxyl functional groups are occupied by high-valent metal cations, so the active sites with an affinity for fluoride ions are increased. Huo et al. (2011) used ionic crosslinking to prepare lanthanum alginate with stable skeletal junctions. SEM showed cracks in the dense surface structure after adsorption, with $Q_{\rm max}=197.2$ mg/g.

2.2.2 Pectin

Pectin is also rich in -COOH and -COOCH₃ groups. The active sites of sodium alginate and pectin are essentially identical, the only difference being the presence of -COOCH₃ in pectin (Sharma et al., 2019), whereas sodium alginate contains only -COOH. The ester group chelates better with metals through its lone pair of electron contribution. The carboxyl group is present in a dimeric form due to the conjugation effect, with the lone pair participating in the conjugation. Therefore, the ester group has a nucleophilic reaction to F⁻ (Figure 2B), providing more active sites, and the pectin should have a higher fluoride removal

TABLE 2 | Adsorption conditions and performance of fluoride by four conventional adsorbents.

Adsorbents	-		Adsorption c	ondition		Isotherm	Regeneration	Q _{max}	Ref	
	Initial C _F ⁻ (mg/L)	Adsorbent dose (g/L)	Reaction pH	Temperature (K)	Equilibrium time (min)	model	performance	(mg/g)		
Cactus-like amorphous alumina oxide	50	1	5–8	298	300	Langmuir	80% at 5th cycle	129.40	Kang et al. (2018)	
microspheres Nano γ-alumina	8	1	4	303	120	Freundlich	80% at 5th cycle	32.00	Chinnakoti et al. (2016a)	
Mesoporous micro alumina	80	0.5	5.5	298	60	Langmuir	_	26.00	Lanas et al. (2016)	
Al ₂ O ₃ nanoparticles	10	0.5	4–6	298	60	Langmuir	_	13.70	Hafshejani et al. (2017)	
Amorphous porous- layered Al ₂ O ₃	120	5	2–5	313	150	Langmuir	_	12.05	Yang et al. (2020)	
Activated alumina	10	2	6–8	318	120	Freundlich	_	4.31	Dhawane et al. (2018)	
Aluminum oxide/ hydroxide	10	8	4–7	298	300	Langmuir	_	2.00	Rathore and Mondal (2017)	
Cubical ceria nano- adsorbent	20	1	7	298	120	Langmuir	_	80.64	Dhillon et al. (2016)	
CeO ₂ nanorods	50	0.5	3.5	298	1,500	Langmuir	_	71.50	Kang et al. (2017)	
CeO ₂ octahedron	10	1	3–10	293	400	Langmuir	_	40.13	Zhang et al. (2016b)	
CeO ₂ nanocubes	50	0.5	3.5	298	1,500	Langmuir	_	28.30	Kang et al. (2017)	
CeCO ₃ OH nanosphere	50	0.5	3.5	298	1,500	Langmuir	_	7.00	Kang et al. (2017)	
Porous MgO nanoplates	20	1	2-11	298	180	Freundlich	_	185.50	Jin et al. (2016)	
Hollow MgO spheres	10	1	3–11	298	250	Freundlich	_	182.40	Zhang et al. (2021b)	
Microsphere-like MgO	100	1	3–9	298	300	Langmuir	40% at second cycle	166.70	Lee et al. (2017)	
Pillar-like MgO	100	1	3–9	298	300	Langmuir	40% at second cycle	151.50	Lee et al. (2017)	
γ-Fe ₂ O ₃ nanoparticles	100	10	4.5	298	15	-	_	3.65	Jayarathna et al. (2015)	
Trititanate nanotubes	10	0.5	2	298	10	Langmuir	_	58.60	Chinnakoti et al. (2016b)	
TiO ₂	5	0.5	7	298	30	Langmuir	_	5.00	Zhou et al. (2019b)	
Lanthanum alginate bead Biopolymer pectin and alginate	10 60	1 0.1	4 7	298 298	1,440 35	Langmuir Langmuir		197.20 50.00	Huo et al. (2011) Raghav et al. (2019)	
Porous zirconium alginate	20	1	2	303	1,200	Langmuir	_	27.95	Qiusheng et al. (2015)	
Shell biochar	300	3.33	7	298	1,440	Langmuir	60% at third cycle	82.93	Lee et al. (2021)	
Nanoscale rice husk biochar	5	1	7	303	60	Freundlich	_	21.70	Goswami and Kumar (2018)	
Mustard ash biochar	5	2	2	298	150	Langmuir	30% at third cycle	4.42	Jadhav and Jadhav (2021)	
Peanut shell biochar	10	8	7	298	120	Langmuir	_	3.66	Kumar et al. (2020)	
Rhodophyta biochar	15	0.6	6	303	90	Freundlich	80% at fifth cycle	2.10	Naga Babu et al. (2020)	
Rice husk biochar	4	5	6	303	360	Langmuir	-	1.86	Yadav and Jagadevan (2020)	
Activated sugarcane ash	5	2	2	303	100	Langmuir	-	10.99	Mondal et al. (2016)	
KOH-treated jamun seed	10	0.4	2.5	298	120	D-R	-	3.65	Araga et al. (2017)	
KOH-treated activated carbon	5	3	4	303	100	Langmuir	-	2.52	Bhomick et al. (2019)	
Activated carbon	380	2	3	298	_	_	50% at fifth cycle	1.15	Chen et al. (2019)	
Coconut-shell carbon	4.4	10	2	323	180	Langmuir	_	0.36	Araga et al. (2019)	
Chicken bone biochar	10	_	_	298	1,440	Langmuir	_	11.20 (Continued	Herath et al. (2018) on following page)	

TABLE 2 | (Continued) Adsorption conditions and performance of fluoride by four conventional adsorbents.

Adsorbents			Adsorption of	ondition	Isotherm	Regeneration	Q_{max}	Ref	
	Initial C_F^- (mg/L)	Adsorbent dose (g/L)	Reaction pH	Temperature (K)	Equilibrium time (min)	model	performance	(mg/g)	
Bone char	10	1	7	298	1,440	Langmuir	_	5.40	Medellin-Castillo et al. (2014)
Bovine bone biochar	20	5	8	298	_	Langmuir	50% at fourth cycle	5.05	Zhou et al. (2019a
Kaolinite	100	1	7	298	150	Langmuir	_	125.00	Wang et al. (2017b)
Activated clay	30	1	5	298	80	Langmuir	_	75.76	Guiza et al. (2019)
Fly ash-paper mill lime mud	15	1.5	5	298	120	Langmuir	_	7.37	Ye et al. (2019)
Natural clay	5	1	6	301	120	Langmuir	_	3.74	Nabbou et al. (2019)
Natural pumice	3	0.7	3	298	50	Freundlich	_	1.17	Dehghani et al. (2016)
Natural zeolite	80	1	6–7	293	300	Freundlich	_	1.83	Cheng et al. (2018)
Clay	5	20	6	398	600	Langmuir	80% at sixth cycle	1.30	Zhang et al. (2016c)
Scoria	7	4	7	298	60	Freundlich	_	0.32	Asadi et al. (2018)
Porous nanohydroxyapatite	5	2	6.5	303	30	Langmuir	_	54.40	Wimalasiri et al. (2021)
Hierarchical hydroxyapatite	20	0.4	4	298	10	Langmuir	_	29.82	Gao et al. (2019)
NaP-hydroxyapatite	5	3	4.5	298	50	Langmuir	_	11.95	Zendehdel et al. (2017)
Hydroxyapatite	15	0.7	7.5	303	60	Langmuir	_	3.12	Mourabet et al. (2015)

capacity in comparison (Raghav and Kumar 2019). SA and pectin hydrogels accomplish adsorption by exchanging hydroxyl groups in the structure with fluoride.

2.3 Carbon-Based Adsorbents

Carbon-based adsorbents have developed pore structures, large specific surface areas, stable chemical properties, easily adjustable surface properties, good regenerability, and widely available and general waste, which is of low cost with promising applications.

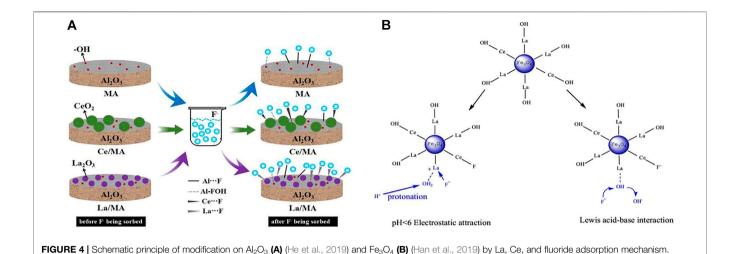
2.3.1 Biochar

Biochar (BC) is made from waste biomass from a wide range of sources such as reed (Singh and Majumder 2018), rice husks (Yadav and Jagadevan 2020), straw (Angelin et al., 2021), teak peel, and algae. BC is a carbon-rich, fine-grained, porous, and highly aromatized material and well suited as an adsorbent for the resource utilization of waste. BC contains lignocellulosic components capable of effectively adsorbing fluoride (Yadav and Jagadevan 2020). The pyrolysis temperature is a key factor in controlling the number of functional groups on the surface of BC (Wang et al., 2021). Generally, biochar prepared by hydrothermal pyrolysis below 573 K is rich in oxygencontaining functional groups (-COOH, -OH, etc.) and has stronger ion exchange capacity (Naga Babu et al., 2020). As the pyrolysis temperature increases, the abundance of hydroxyl, amino, and carboxyl groups decrease and the degree of carbonation increases (Kumar et al., 2020). Biochar prepared at 673-973 K has developed porosity (Figure 3A) and thermal

stability (Goswami and Kumar 2018). Brunson and Sabatini (2015) recorded a significant increase in specific surface area (from 0.9 m²/g to 327 m²/g) and surface zero charge point (from $pH_{PZC} = 5.8$ to $pH_{PZC} = 9.4$) when the pyrolysis temperature of charcoal was increased from 573 to 873 K. BC also contains minerals such as potassium, calcium, magnesium, and phosphorus, which can be complex with fluoride ions or precipitate. Lee et al. (2021) found that the shell biochar could contain up to 56.9% CaCO₃, and when the pyrolysis temperature was raised to 1073 K, CaCO₃ was converted to Ca(OH)₂; the structure was more conducive to the adsorption of fluoride. The adsorption mechanism was outer-sphere complexation between Ca and F. Although shell biochar has low carbon content and small specific surface area ($S_{BET} = 4.363 \text{ m}^2/\text{g}$), the maximum fluoride adsorption capacity of their prepared shell biochar MCS-800 could reach 82.93 mg/g. The biochar obtained by pyrolysis alone has an average low adsorption effect but has the advantage of being easily modified (Wang et al., 2021).

2.3.2 Activated Carbon

Activated carbon (AC) is usually made from coconut shells, hard cores, bamboo, coal, wood, and other raw materials (Collivignarelli et al., 2020), and the pyrolysis temperature is generally higher than 1173 K (Araga et al., 2019). After pyrolysis, further physical or chemical activation is required (Chen et al., 2019). Chemical activation has high activation yield but is highly corrosive to the equipment (Tomar et al., 2014). As shown in **Figure 3B**, AC has the advantage of high porosity and large



specific surface area. Araga et al. (2017) and Bhomick et al. (2019) used KOH to activate mustard seed activated carbon and commercially available activated carbon, respectively, and the modified specific surface area reached 747 m²/g and 1,005 m²/g, respectively. The -OH group on the AC surface is protonated with fluoride at pH < pH_{PZC} (acidic media). Numerous studies have demonstrated that fluoride adsorption on AC consists of the mechanism for the deprotonation of -OH functional groups on carbon surfaces (He et al., 2020).

2.3.3 Bone Char

Bone char is the charring product of animal bones and generally contains about 20% carbon and hydroxyapatite (HAp) (Medellin-Castillo et al., 2014), with the content of each component varying slightly depending on the charring temperature. When the charring temperature is below 573 K, more organic matter remains in the bones, but the specific surface area and pore structure is not well developed (Zhou J. et al., 2019). The charring temperatures above 873 K may change the structure of the hydroxyapatite and also lead to reduction in fluoride adsorption capacity. The fluoride adsorption by bone char is reported to be mainly carried out by hydroxyapatite. Medellin-Castillo et al. (2014) found that fluoride in aqueous solutions was mainly adsorbed to HAp in bone char but not to other components. HAp in bone char contains most of the OH⁻ that can be replaced by F⁻; the adsorption mechanism includes ion exchange and chemical precipitation. The detailed mechanism of fluoride adsorption by HAp is described in the following section.

2.4 Other Types of Adsorbents

Other materials such as natural mineral clays (clay (Zhang S. et al., 2016), bentonite (Mudzielwana et al., 2017), etc.), industrial solid waste (zeolite (Ghosal and Gupta 2018), etc.), and hydroxyapatite are also used for fluoride adsorption. Natural clay (**Figure 3**C) contains the main compounds SiO₂ and Al₂O₃ and has the chemical potential to adsorb fluoride (Guiza et al., 2019). Zeolite is an aqueous skeletal structure composed of aluminosilicate minerals with the lattice of many pores and

channels that have the structural potential to adsorb fluoride. However, these two types of materials usually show weak fluoride adsorption capacities (**Table 2**) and are generally modified by chemical activation or metal loading.

2.4.1 Hydroxyapatite

Hydroxyapatite [(Ca₁₀(PO₄)₆(OH)₂, HAp] is also a promising inorganic material for fluoride adsorption, with excellent biocompatibility, stability, and mechanical properties. Due to its unique crystal structure, HAp has a porous surface, large specific surface area, and high ion exchange capacity. The hydroxyl group in HAp is prone to rapid exchange with anion and has a strong binding capacity with fluoride (Raghav et al., 2018). F replaces OH, fills in the lattice of HAp forming insoluble fluorapatite (FAp), and OH- is released into solution. When high concentrations of fluoride ions are present in the solution, Ca2+ in HAp reacts with F forming CaF₂ precipitate, and phosphate is correspondingly released into the solution. Various forms of HAp have been reported for fluoride adsorption in water, such as nano-hydroxyapatite (Mourabet et al., 2015; Zendehdel et al., 2017), porous hydroxyapatite (Nijhawan et al., 2020), and layered hollow hydroxyapatite (Gao et al., 2019). The mechanism of fluoride adsorption by HAp mainly consists of the following: 1) electrostatic attraction by the surface of HAp to F-. 2) Anion exchange between OH⁻ or PO₄²⁻ and F⁻. 3) Complexation reaction of Ca²⁺ with F⁻ ligates and forms surface precipitation. 4) F can also form hydrogen bonds with OHin the HAp lattice.

3 NEW COMPOSITE ADSORBENTS OBTAINED FROM METAL MODIFICATION

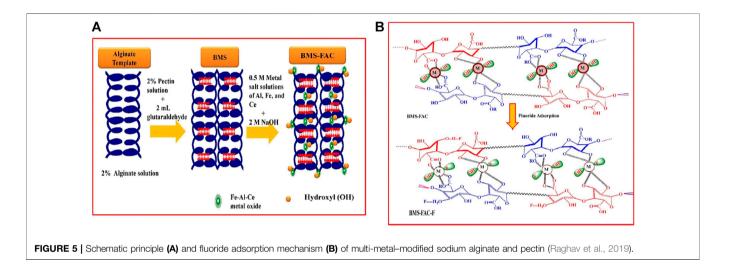
Over long periods of use and development, traditional adsorbents have gradually revealed the unique application value and drawbacks. Compared to the exploitation of novel adsorbents, research tends more to synthesize complexes of two or more adsorbents to produce synergistic fluoride adsorption. The

TABLE 3 | Adsorption conditions and performance of fluoride by muti-metal and metal-biopolymer composite adsorbents.

Adsorbents			Adsorption c	ondition		Isotherm	Regeneration	Q _{max}	Ref
	Initial C _F ⁻ (mg/L)	Adsorbent dose (g/L)	Reaction pH	Temperature (K)	Equilibrium time (min)	model	performance	(mg/g)	
Mn-Al binary metals	380	_	7	298	720	Langmuir	-	94.83	Wu et al. (2017a)
Ce-Zn binary metals	10	0.15	3–7	298	45	Langmuir	68% at sixth cycle	64.66	Dhillon et al. (2017)
Ce-Ti oxide	10	1	7	298	_	Langmuir	-	44.37	Abo Markeb et al. (2017)
Mg/Fe-LDHs	30	4	7	298	150	Langmuir	_	28.65	Wu et al. (2015)
Fe-La	10	1	6	298	60	Langmuir	_	27.42	Wang et al. (2018c)
La/MA	10	2	6	298	360	Sips	70% at fifth cycle	26.45	He et al. (2019)
Fe-Ag magnetic oxide	10	0.5	3	298	20	Langmuir	85% at sixth cycle	20.57	Azari et al. (2015)
La-modifying Fe ₃ O ₄	5	10	7.4	303	600	Langmuir	-	1.51	García-Sánchez et al (2016)
Al-modifying Fe ₃ O ₄	5	10	6.6	303	600	Langmuir	-	1.42	García-Sánchez et al (2016)
Ca-Mg-Zr oxide	100	0.5	7	298	160	Freundlich	70% at fifth cycle	370.37	Wang et al. (2022)
Ce-Ti@Fe ₃ O ₄	10	1	7	298	15	Langmuir	93% at fifth cycle	91.04	Abo Markeb et al. (2017)
Fe ₃ O ₄ @La-Ce	10	0.5	4	303	60	Freundlich	_	56.80	Han et al. (2019)
Fe ₃ O ₄ @Fe-Ti	4	1	7	298	2	Langmuir	77% at ninth cycle	41.80	Zhang et al. (2016a)
Fe-Mg-La	10	0.1	7	298	300	Langmuir	90% at third cycle	185.90	Yu et al. (2015)
Al-Zr-La	200	0.5	3	308	500	Langmuir	_	90.48	Zhou et al. (2018)
Mg/Fe/La	5	0.5	7	308	100	Langmuir	57% at fifth cycle	59.34	Wu et al. (2017b)
Fe-Mg-La	20	1	7	298	360	Langmuir		40.40	Chen et al. (2018)
Mg-Al-Fe LDH	2	1.5	6	298	600	Sips	_	20.00	Hongtao et al. (2018)
Fe-Al-Ce-Ni	10	0.4	5	303	50	Freundlich	50% at sixth cycle	250.00	Raghav and Kumar (2018)
SA-Ca@Fe/ La/Ni	10	30	5	303	30	Freundlich	55% at fifth cycle	333.00	Sapna et al. (2018)
Pectin-Fe/Al/Ni	10	0.4	7	318	90	Freundlich	86% at fifth cycle	285.00	Raghav and Kumar (2019)
Alginate-Fe/ Al/Ni	10	0.4	7	298	90	Langmuir	84% at fifth cycle	200.00	Raghav and Kumar (2019)
SA/pectin-Fe/ Al/Ce	60	0.1	7	298	35	Halsey	65% at ninth cycle	142.90	Raghav et al. (2019)
SA/CMC-Ca-Al	40	-	2	298	600	Langmuir	_	101.40	Wu et al. (2016b)
SA-Mg/Fe oxide	10	10	7	298	600	Langmuir	80% at third cycle	32.31	Wu et al. (2017c)
SA-Mg/Al/Zr	40	2.5	6	303	1800	Freundlich	_	31.72	Wang et al. (2017a)
SA-Mg/Al/Ce	40	5	6	303	3,600	Freundlich	65% at third cycle	26.12	Wang et al. (2018a)
Pectin Fe bead	10	2	5	298	600	Freundlich	_	20.00	Sharma et al. (2019)
CS-Ce	30	0.3	3	293	400	Langmuir	80% at fourth cycle	153.00	Zhu et al. (2017)
Fe ₃ O ₄ /CS/ Al(OH) ₃	10	0.1	5	298	60	Langmuir	_	76.63	Hu et al. (2018)
Fe-Al-Mn@CS	6	0.5	7	298	160	Langmuir	_	40.50	Chaudhary et al. (2021)
Rare earth CS bead	10	2	5	298	480	Freundlich 	70% at seventh cycle	22.35	Liang et al. (2018)
La ³⁺ magnetic CS	10	2	5	298	480	Langmuir	40% at seventh cycle	20.53	—
Zr-CS bead	20	1	7	303	80	Freundlich	_	17.47	Prabhu and Meenakshi (2015)
La-CS bead	20	1	7	303	80	Freundlich	_	14.49	_
Ce-CS bead	20	1	7	303	60	_	_	11.50	_
Al-CS bead	20	1	7	303	40	_	_	7.45	-
Fe ₃ O ₄ @ TiO ₂ -CS	2	0.4	5	298	30	Langmuir	75% at sixth cycle	14.62	Sadeghi et al. (2019)
Fe ₃ O ₄ -CS	5	1	7	293	60	Freundlich	88% at fifth cycle	9.26	Mohseni-Bandpi et al. (2015) led on following page)

TABLE 3 (Continued) Adsorption conditions and performance of fluoride by muti-metal and metal-biopolymer composite adsorbents.

Adsorbents			Adsorption c	ondition		Isotherm	Regeneration	Q_{max}	Ref
	Initial C_F^- (mg/L)	Adsorbent dose (g/L)	Adsorbent Reaction Temperature Equilibrium dose pH (K) time		model	odel performance			
La-CS/β cyclodextrin	10	2	7	303	30	Freundlich	56% at fifth cycle	8.14	Preethi and Meenakshi (2018)
Ce-cellulose nanobead	2.5	1	3	303	50	Langmuir	82% at fifth cycle	39.88	Sarkar and Santra (2015)
CMKGM-La-Al	40	2	2	40	120	Langmuir	-	20.37	Wu et al. (2016a)



synthesis of metal modifications to other types of adsorbents accounts for the majority.

3.1 Multi-Metal Oxide/Hydroxide Adsorbents

Different metal oxide adsorbents have their individual strengths and weaknesses for fluoride removal, so recently there have been research studies using multi-metal oxide/ hydroxide adsorbents (Chen et al., 2018). Compared to conventional metal oxides, various valence cations are often present in one multi-metal oxide, providing more chemisorption sites (Raghav and Kumar 2018). The tunability of the chemistry of each element ensures an abundance of active sites, and the components can be adjusted to each other, possessing different outstanding properties and therefore having unique quantum coupling effect and synergistic effects, resulting in more than doubling or tripling of the adsorption capacity. There are two common types of multi-metal oxide adsorbents. One is prepared by compounding each metal element in a certain ratio (Wu K. et al., 2017) such as layered double/triple hydroxides (Wu P. et al., 2017), and the other is to modify one metal oxide with others; the ones mostly reported are modified alumina (He et al., 2019) or magnetic iron oxides.

3.1.1 Layered Double/Triple Hydroxides

A series of layered double/triple hydroxides (LDHs) have a high affinity for anions with high ion exchange capacity and high adsorption volume, which are often used as anion exchangers and trapping agents. LDHs are two-dimensional layered materials structural whose formula can be expressed $[M_{1-x}^{2+}M_x^{3+}(OH)_2]^{x+}(A^{n-})_{x/n}\cdot mH_2O$, where M^{2+} is the positive divalent metal ion $(Mg^{2+}, Cu^{2+}, Ni^{2+}, Zn^{2+}, etc.)$, M^{3+} is the positive trivalent metal ion (Fe³⁺, Al³⁺, La³⁺, Ce³⁺, etc.), and A is the interlayer anion (Cl⁻, CO₃²⁻, NO₃⁻, etc.). LDH consists of positively charged main lamellae and negatively charged interlayer ions. The lamellar structure of LDH is longitudinally stable (Wu et al., 2015). This lamellar structure facilitates adequate contact between the metal sites and the fluoride ions during adsorption and accelerates the charge transfer at the interface. The surface of the main layer is rich in hydroxyl functional groups, which bind to cations in different ways such as electrostatic gravitational forces and hydrogen bonding, providing a large anion exchange capacity with fluoride ions. The synthesis of triple hydroxide by doping of layered double hydroxide with high-valent metal cations has been shown to be effective in enhancing its adsorption activity. When the highly valent cation M³⁺ replaces M²⁺, the main lamellae are positively charged and therefore require the interlayer anions to be negatively charged to balance the overall charge (Hongtao

TABLE 4 | Summary of modification methods, characteristics, and adsorption mechanisms of muti-metal and metal-biopolymer composite adsorbents.

Adsorbents	Modification method	Dimension	SBET (m2/G)	Aperture (nm)	pHPZC	Adsorption mechanism	Ref
Mn–Al binary metals	Oxidation and coprecipitation	_	43	0.33	8.7	Surface complexation	Wu et al. (2017a)
Ce-Zn binary metals	Coprecipitation, calcination at 873 K	22.4 nm	499	15	6	lon exchange	Dhillon et al. (2017)
Ce-Ti oxide	Coprecipitation	1–2 nm	_	_	_	Ion exchange	Abo Markeb et al. (2017)
Mg/Fe-LDHs	Coprecipitation, hydrothermal at 543 K	100 nm	_	-	10.42	lon exchange	Wu et al. (2015)
Ee-La	Coprecipitation, hydrothermal at 423 K	_	113	21.78	8.5	Ion exchange	Wang et al. (2018c)
_a/MA	Impregnation, calcination at 673 K	_	237	4.81	10.2	Electrostatic attraction, chemisorption	He et al. (2019)
-e-Ag magnetic oxide	Coprecipitation	5 nm	254	0.13	6.03	lon exchange	Azari et al. (2015)
_a-modifying Fe3O4	Lanthanum hydroxide soaking	_	6	-	> 10	Electrostatic attraction	García-Sánchez et a (2016)
Al-modifying =e3O4	Aluminum hydroxide soaking	_	5	_	> 10	Electrostatic attraction	García-Sánchez et a (2016)
Ca-Mg-Zr oxide	Hydrothermal, calcination at 923 K	_	119	14.03	11.5	Electrostatic attraction, ion exchange	Wang et al. (2022)
Ce-Ti@Fe3O4	Coprecipitation	15 nm	_	_	_	Ion exchange	Abo Markeb et al. (2017)
Fe3O4@La-Ce	Coprecipitation	_	40	20.3	6	Ligand exchange, electrostatic attraction	Han et al. (2019)
Fe3O4@Fe-Ti	Precipitation of Fe3O4@Fe-Ti, granulation	10 μm	99	15.3	-	Ion exchange	Zhang et al. (2016a)
=e-Mg-La Al-Zr-La	Coprecipitation Coprecipitation	40 μm —	- 36	_	6.3 8.4	Ion exchange Electrostatic attraction, ion	Yu et al. (2015) Zhou et al. (2018)
Mg/Fe/La	Hydrothermal, calcination at 873 K	_	59	22.3	_	exchange Surface complexation, ion	Wu et al. (2017b)
To Mail o	Conveninitation	65 nm	70	20	0.0	exchange	Ohan at al (0010)
Fe-Mg-La Mg-Al-Fe LDH	Coprecipitation Coprecipitation	-	78 130	30 24.47	8.8 —	Ligand exchange Interlayer ion exchange	Chen et al. (2018) Hongtao et al. (2018
Fe-Al-Ce-Ni	Coprecipitation, calcination at 873 K	_	184	51.43	6.2	lon exchange, electrostatic attraction	Raghav and Kumar (2018)
SA-Ca@Fe/La/Ni	Fe-La-Ni oxides mixing SA, CaCl2 cross-linking	1–2 mm	257	10.4	7	lon exchange, H-bonding	Sapna et al. (2018)
Pectin-Fe/Al/Ni	Aerogel formation by coprecipitation, freezing	886 nm	275	0.15	_	Isomorphic substitution	Raghav and Kumar (2019)
Alginate-Fe/Al/Ni	Aerogel formation by coprecipitation, freezing	914 nm	96	0.13	-	Isomorphic substitution	Raghav and Kumar (2019)
SA/pectin-Fe/ AI/Ce	Fe-Al-Ce coprecipitation with pectin and alginate	_	275	_	7.17	Ion exchange, H-bonding, complexation	Raghav et al. (2019)
SA/CMC-Ca-Al	SA/CMC mixing, Ca2+ cross- linking, Al3+ soaking	2–2 mm	_	_	_	Coordination reaction	Wu et al. (2016b)
SA-Mg/Fe oxide	Mg/Fe oxide mixing SA, CaCl2 cross-linking	1 mm	_	_	10.52	Ligand exchange, electrostatic attraction	Wu et al. (2017c)
SA-Mg/Al/Zr	Mg-Al-Zr oxide mixing SA, CaCl2 cross-linking	1 mm	_	_	_	Ion exchange, electrostatic attraction	Wang et al. (2017a)
SA-Mg/Al/Ce	Mg-Al-Ce oxide mixing SA, CaCl2 cross-linking	_	_	_	_	Ion exchange	Wang et al. (2018a)
Pectin Fe bead CS-Ce	Grafting, FeCl3 impregnation Coprecipitation, glutaraldehyde	43 nm 200 nm	_ 17	_	_ 5.3	Ligand exchange Electrostatic attraction, ligand	Sharma et al. (2019) Zhu et al. (2017)
Fe3O4/CS/	cross-linking AICI3 mixing, Fe3O4 NP adding	200 nm	_	-	_	exchange, and complexation Electrostatic attraction,	Hu et al. (2018)
AI(OH)3 Fe-AI-Mn@CS	Coprecipitation	-	42	_	_	complexation —	Chaudhary et al. (2021)
Rare earth CS	Rare earth mixing, Fe3O4 adding, cross-linking	-	21	7.92	5	Ligand exchange	(2021) Liang et al. (2018)
La3+ magnetic CS	La mixing, Fe3O4 adding, cross- linking	_	17	8.15	5	Ligand exchange	-

(Continued on following page)

TABLE 4 | (Continued) Summary of modification methods, characteristics, and adsorption mechanisms of muti-metal and metal-biopolymer composite adsorbents.

Adsorbents	Modification method	Dimension	SBET (m2/G)	Aperture (nm)	pHPZC	Adsorption mechanism	Ref
Hyper-branched CS beads	Glutaraldehyde cross-linking, Zr, La, Ce, Al solution immersion	1.7 mm	3	_	7	Electrostatic attraction, ligand	Prabhu and Meenakshi (2015)
Fe3O4@TiO2-CS	Fe3O4@TiO2 impregnation CS	_	_	_	6	Electrostatic attraction, H-bonding	Sadeghi et al. (2019)
Fe3O4-CS	FeCl3 impregnating CS, coprecipitation	0.15 mm	499	3.4	7	_	Mohseni-Bandpi et al. (2015)
La-CS/β cyclodextrin	Mixing, 5% glutaraldehyde cross- linking	_	_	_	4.56	Electrostatic attraction, H-bonding	Preethi and Meenakshi (2018)
Ce-cellulose nanobead	Impregnation	45 nm	_	_	_	Ion exchange	Sarkar and Santra (2015)
CMKGM-La-Al	La, Al mixed solution cross-linking	-	_	_	_	lon exchange, electrostatic attraction	Wu et al. (2016a)

et al., 2018). The addition of rare earth metals has been reported to further enhance the affinity with fluoride. Wu P. et al. (2017) introduced La into Mg/Fe LDH to form Mg/Fe/La hydrotalcite-like compounds with layered porous structure, which significantly enhanced the fluoride adsorption capacity of Mg/Fe LDH.

3.1.2 Metal-Modified Magnetic Iron Oxides

Al- and Fe-based oxides are mostly doped or load-modified by another metal. Metal-modified Al₂O₃ generally adsorbs fluoride by complexation and ion exchange (Figure 4A). Iron oxides (Fe₃O₄ or γ-Fe₂O₃), in addition to adsorption advantages, provide strong magnetic properties and large magnetic response with easy separability and controllability; thus, there have been more reported recently. Magnetic iron oxide nanoparticles can be used directly for fluoride adsorption or as a nucleus material for core-shell particles. The magnetic core particles are generally combined with metal oxide nano-shells by methods such as surface coating to ensure stronger magnetic response, more functional groups, and better properties (Zhang C. et al., 2016). Recent research has mostly used rare earth metals to modify magnetite. Rare earth ions are greater in radius than other elements in the iron oxides; doping with the appropriate amount of rare earth elements to replace some of the other elements in the iron oxides with a smaller ion radius distorts the lattice and can improve the physical activity. Most importantly, the hard Lewis acid nature of the rare earth metal ions (especially La) has a strong affinity for fluoride (Figure 4B) (Han et al., 2019). Ce can promote the dispersion of nanoparticles, giving the adsorbent a larger specific surface area, pore volume, and more active functional sites. Correspondingly, magnetic particles can attenuate the agglomeration effect of rare earth metal oxides, reducing the amount of precious metals used and improving the separation characteristics by magnetic assistance to reduce residues in water and avoid rare earth metal toxicity (Abo Markeb et al., 2017). Han et al. (2019) used VSM tests to that Fe_3O_4 and Fe₃O₄@La-Ce superparamagnetic, and it was easy to separate the particles from the solution using the external magnetic field. The adsorption amount of Fe₃O₄@La-Ce was increased up to 20 times compared to Fe₃O₄.

3.2 Metal-Biopolymer Adsorbents

Large-scale applications for fluoride removal in aqueous systems require the development of composite hydrogel materials with good mechanical properties and stability. For hydrogels with poor adsorption properties, the cross-linking of composites by cementing other high performance adsorbent materials onto biopolymers can effectively reduce the degradation of properties. The preparation of biopolymer-based composites is divided into three types: 1) doping of metals/metal oxides (Sapna et al., 2018), 2) blending with inorganic materials (Wang et al., 2020), and 3) mixing between polymeric organic substances (Preethi and Meenakshi 2018). This section summarizes the doping by metal oxide modification studies.

3.2.1 Metal-Doped Alginate/Pectin

The biocompatibility and biodegradability of natural polymeric materials make sodium alginate and pectin effective substrates for the incorporation of multivalent metal ions. Studies have reported to dope SA with metals; co-mingling and crosslinking to form a stable gel structure can improve both the stability and mechanical properties of SA (Wu T. et al., 2017), while having an anchoring effect on metal oxides, reducing the agglomeration and leaching of metal oxides and maximizing the adsorption properties (He et al., 2020). Furthermore, the doping of metals can increase the metal active sites in the porous structure and combine the properties of organic and inorganic components to improve the adsorption capacity (Zhao et al., 2021). Mono and multi-metal doping options are available. Recent research has focused on the doping of sodium alginate and pectin with multi-metals. Compared to monometals, the multi-metals provide an enhanced abundance of active sites as mentioned earlier. In addition, the multi-metals used in the studies tend to be the composite of +2 valent and higher valent cations. The addition of +3 and +4 valent metal ions, especially rare earth metals, can improve the stability, recyclability, and adsorption capacity. Raghav and Kumar (2019) obtained a high adsorption capacity (Table 3) for all the composite hydrogels prepared by SA and pectin embedding Fe-Al-Ni (285 mg/g and 200 mg/g) and SA/pectin co-embedding Fe-Al-Ce (142.9 mg/g) (Raghav et al., 2019). Figure 5 shows the

TABLE 5 | Summary of modification methods, characteristics, and adsorption mechanisms of metal-modified carbon and other adsorbents.

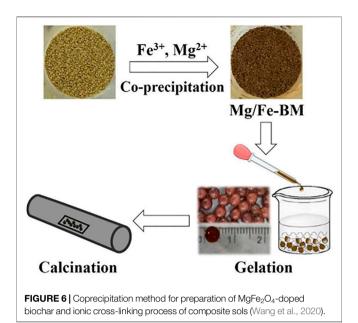
Al-modified com Pyrolysis at 823 K,	Adsorbents	Modification method	Dimension	S _{BET} (m²/G)	Aperture (nm)	pH _{PZC}	Adsorption mechanism	Ref
Discretary Control C	Wood biochar-La	Impregnation, pyrolysis	0.8 mm	165	3.91	6.6	Ion exchange	Habibi et al. (2019)
Carpine Carp	Al-modified corn biochar		_	1	410	2	lon exchange	Zhang et al. (2021a)
1073 K 270, seed shell	MgO shell biochar		0.5 μm	182	2–10	_		Wan et al. (2019)
	Pomelo peel BC-La		_	269	_	5.8	Ion exchange	Wang et al. (2018b)
Ag-Mr-Zr AC	=	1 1 0	_	_	_	4.45	lon exchange	Mei et al. (2020)
coprecipitation copresipitation copresipitatio	Magnetic biochar		100 μm	494	0.3	11		Bombuwala Dewage et a (2018)
La-functionalized AC Impregnation, rotary evaporation, neary evaporation, heat evaporation precipitation and precipitation evaporation eva	Mg-Mn-Zr AC	·	_	834	2.43	11.9		Mullick and Neogi (2019)
evaporation, heat was evaporation, perceptation ultrasound impregnation, precipitation upregnation, precipitation upregnation, precipitation unpregnation, precipitation unpregnation, precipitation unpregnation, perceptation unpregnation unpregn	Zr-impregnated AC	Ultrasonic impregnation	14 µm	1,104	2.30	5.03	Electrostatic attraction	Mullick and Neogi (2018)
Decontaining bone Impregnation, heat treatment 0.7 mm — — — — — — — — — — — — — — — — — —	_a-functionalized AC	· · · ·	0.5 mm	367	0.68	7.3		
wagnetic bone impregnated biomass, — 42 17.45 2.4 lon exchange Zhou et al. (2019a) inciderar calcination Graphene oxide Hydrothermal at 453 K, — 278 2.55 7 Electrostatic attraction, ion exchange with Ti calcination — 44 84.63 6 Electrostatic attraction, ion exchange with Ti calcination — 44 84.63 6 Electrostatic attraction, ion increase exchange exchange exchange with Ti calcination — 44 84.63 6 Electrostatic attraction, ion increase exchange excha		Ultrasound impregnation,	_	126	3.54	3	Ion exchange, physical	
calcination Graphene oxide Hydrothermal at 453 K, — 278 2.55 7 Electrostatic attraction, ion exchange Na-polyacrylic acid Impregnation — 44 84.63 6 Electrostatic attraction, ion exchange Electrostatic attraction, ion exchange Na-polyacrylic acid Impregnation — 117 µm 86 2.5–97 3.9 Electrostatic attraction, ion exchange Nagnetic γ-Fe ₂ O ₃ — Fe coprecipitation, La — — — 7.9 Ion exchange, when et al. (2019) impregnation (acidination — 632 — 7.9 Ion exchange, which is pregnation (acidination — 632 — 7.3 Ligand exchange, which is pregnation (acidination — 632 — 7.3 Ligand exchange, electrostatic attraction, ion exchange (acidination — 7.9 Ion exchange) (acidinatic attraction — 7.9 Ion exchange) (acidination — 7.0 Ion exchange, electrostatic attraction — 8.0 Ion exchange, electrostatic attraction — 8.0 Ion exchange, electrostatic — 8.0 Ion exchange, electrosta	-	Impregnation, heat treatment	0.7 mm	_	_	_		Zúñiga-Muro et al. (2017)
with Ti calcination	0		-	42	17.45	2.4	lon exchange	Zhou et al. (2019a)
Al-polyacrylic acid Impregnation — 44 84.63 6 Electrostatic attraction, ion exchange DeO ₂ @SiO ₂ Coprecipitation 117 μm 86 25-97 3.9 Electrostatic attraction, ion exchange electrostatic attraction, ion exchange objects of the prognation of th	•	,	-	278	2.55	7	,	Nehra et al. (2019)
CeO ₂ @SiO ₂ Coprecipitation 117 μm 86 25–97 3.9 Electrostatic attraction, chemisorption incresphere Pe ₂ O ₃ - Fe coprecipitation, La — — — — 7.9 Ion exchange, complexation complexatio			_	44	84.63	6	Electrostatic attraction, ion	Xu et al. (2017)
GO-La impregnation, calcination Zn-modifying slag impregnation One-step ultrasound On		Coprecipitation	117 µm	86	25–97	3.9	Electrostatic attraction,	Wang et al. (2019a)
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Aluminum/olivine Wet impregnation, calcination — — — — — — — — — — — — — — — — — — —	e-modifying pumice	Impregnation	200 μm	25	_	3	_	Dehghani et al. (2016)
Polyhydroxy-iron Impregnation — 100 — 8 — Muschin et al. (2021) BD Y-GO hydrogels GO-mixing SA, YCl ₃ cross- Inking Inking Al2O3-chitosan HBO ₃ cross-linking, calcination — — — 6 Ion exchange Jiang et al. (2018) Braphene oxide/ Braph		In-suit hydrolysis	_	203	7.1	1.8	lon exchange	Kuang et al. (2017)
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Ca-pectin- Coprecipitation - 157 3.1 7 Ion exchange, electrostatic Raghav et al. (2018) attraction			2 mm	237	3.97	8.26	-	Wei et al. (2022)
		•	_	157	3.1	7	Ion exchange, electrostatic	Raghav et al. (2018)
		Mixing, FeCl ₃ impregnation				8.6		Wang et al. (2017c)

reaction process of multi-metal-modified SA and pectin and the exchange sites for fluoride adsorption.

3.2.2 Metal-Doped Chitosan

Chitosan (CS) is an N-deacetylated derivative of the natural polysaccharide chitin and is rich in free amino acids. The

-NH₂ group in chitosan is more reactive (Zhu et al., 2017), easy to be chemically modified (Chaudhary et al., 2021), and exhibits high adsorption potential. Despite the numerous advantages such as biodegradability, biocompatibility, flexibility, hydrophilicity, and versatility, CS tends to be readily soluble in acidic solutions and has a weak chemical resistance



(Dong and Wang 2016), especially in column continuous flow adsorption. Current research into the adsorption of fluoride ions by CS is also mostly metal-doped, but unlike sodium alginate and pectin, the modification of CS is more oriented toward monometallic impregnation followed by cross-linking using glutaraldehyde (Table 4). The size of the beads formed is much smaller, typically in the micron range (Prabhu and Meenakshi 2015). One of the top research hotspots is the magnetic modification of Fe₃O₄, mainly because the hydroxyl group on the surface of Fe₃O₄ can interact with the amino and hydroxyl groups of CS through hydrogen bonding (Sadeghi et al., 2019), enabling CS to remain stable under acidic conditions. The CS composite adsorbent is also endowed with magnetic ease of separation properties (Mohseni-Bandpi et al., 2015). Hu et al. (2018) obtained nano-microsphere Fe₃O₄/CS/Al(OH)₃ beads by facile impregnation, which can rapidly accomplish high capacity adsorption of fluoride and rapid sedimentation under low magnetic fields.

3.3 Metal-Carbon Adsorbents

Carbon-based adsorbents have the advantage of large specific surface area and rich pore structure (Shang et al., 2022), but they have low adsorption capacity for fluoride removal alone and require some modification. Research on carbon composites has focused on the doping or surface loading of carbon with nanometal oxides/hydroxides (Dehghani et al., 2018). The affinity between fluoride ions and highly valent cations such as Al³⁺, Fe³⁺, Ca²⁺, and Mg²⁺ can improve the selectivity of carbon to fluoride. When the two are compounded, on the one hand, the metal nanoparticles provide a large number of active sites (Mohanta and Ahmaruzzaman 2018) to compensate for the absence of functional groups that can interact with fluoride ions after high temperature carbonization. On the other hand, the carbon-based adsorbent has large specific surface area and pores, which can act as carriers and dispersants to avoid agglomeration of the metal

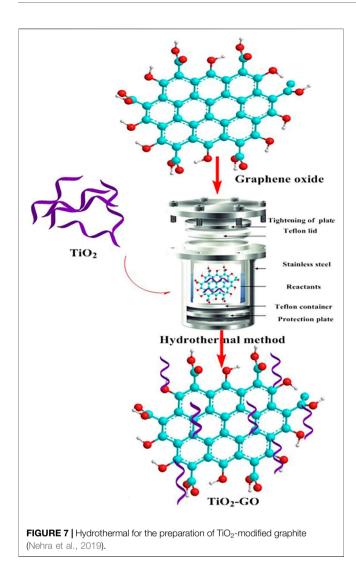
nanoparticles (Cai et al., 2022). More individual metal loadings are used, and multi-metal modifications are also available. More active sites enhance the adsorption performance, and the modified adsorbent surface is richer in specific types of adsorption sites, which may further increase the adsorption capacity.

3.3.1 Metal-Modified Biochar

The ability of biochar to remove pollutants is greatly influenced by the nature of the raw material, preparation technology, and pyrolysis conditions. Unsuitable pyrolysis conditions tend to under-carbonize or over-carbonize BC, so the adsorption performance of unmodified BC is limited. The raw biochar has a relatively poor adsorption effect on anions as the negative charge occupies the majority of the functional groups (Mei et al., 2020). Highly valent metal cations can provide sufficient positive charge to effectively alter surface physicochemical properties (Wang et al., 2019c). AlCl₃ has been reported to generally increase the anion exchange capacity in all BC. Brunson and Sabatini (2015) studied the changes in charcoal surface area and surface chemistry following aluminum nitrate impregnation and found that the aluminum modification reduced the zero charge point of the charcoal in water (from $pH_{PZC} = 9.6$ to $pH_{PZC} = 5.7$) but significantly increased the adsorption capacity. Rare earth metal ions such as Ce³⁺, Zr⁴⁺, and La³⁺ are more alkaline, have a relatively low ionic potential, and show strong tendency to dissociate hydroxyl groups into ions. The possibility of ionic exchange with F is higher and the affinity is stronger. Habibi et al. (2019) modified woody BC with LaCl₃ and showed that the maximum adsorption capacity of 164.23 mg/ g and adsorption equilibrium could be reached within 30 min. They concluded that H⁺ in functional groups such as carboxyl and sulfate groups on the surface of BC may exchange with La³⁺ ions. The presence of La³⁺ increased the adsorption mechanism with Lewis acid-base interaction and ion exchange. The F adsorption rate of the adsorbent was still 80% at fifth recycling, indicating that the rare earth metals loaded on the BC are not easily leached. The modification of iron oxides can confer magnetic properties to BC, improving the separation and recovery performance. BC has good electrical conductivity, which is conducive to electron transfer and reduction of Fe³⁺. The stronger synergistic effect can further promote the fluoride adsorption performance (Wang et al., 2019c).

3.3.2 Metal-Modified Activated Carbon

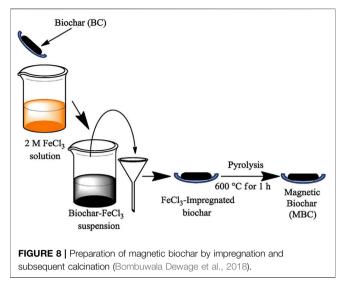
Activated carbon has large specific surface area and pores, which can act as carriers and dispersants to avoid agglomeration of the metal nanoparticles (Cai et al., 2022). More individual metal loadings are used, and multi-metal modifications are also available. More active sites enhance the adsorption performance, and the modified adsorbent surface is richer in specific types of adsorption sites, which may further increase the adsorption capacity. Li et al. (2018) precipitated Ti(OH)₄ on the surface of AC, which further increased the specific surface area of Ti-AC to 1700 m²/g, providing more adsorption sites for fluoride ions. They confirmed that the adsorption capacity of Ti-AC was



produced by $Ti(OH)_4$ loaded on AC. The saturation adsorption capacity of $Ti(OH)_4$ in Ti-AC was 62.1 mg/g, which was much higher than that of $Ti(OH)_4$. It has also been reported that the loading of different metal oxides/hydroxides can form new functional groups on the AC surface with high affinity for fluoride adsorption, significantly improving the adsorption efficiency. A et al. used ultrasonically assisted polymetallic impregnation of AC (Mohanta and Ahmaruzzaman 2018; Mullick and Neogi 2018). The specific surface area decreased after modification, but the pH_{PZC} increased to 11.9 and the adsorption capacity increased by four times compared to monometallic impregnation (Mullick and Neogi 2019).

3.3.3 Metal - Other Types of Adsorbents

Graphene oxide (GO) is a two-dimensional honeycomb carbon nanomaterial formed by the close packing of carbon atoms in a sp-hybridization pattern (Kanrar et al., 2016). GO carries various functional oxygen-containing groups (such as -OH, -COOH, C=O, and -CH(O)CH-) and provides active sites to connect to other substances (Jeyaseelan et al., 2021). GO generally adsorbs



fluoride through electrostatic attraction, π - π stacking, and hydrogen bonding. It has been reported to have a huge theoretical specific surface area (up to 2,630 m²/g) (Mohan et al., 2017) and can be an excellent host for metal nanoparticles. In turn, nanometallic particles provide structural rigidity by inhibiting the restacking of different layers of GO and provide a higher surface area and many active centers (Mohan et al., 2017). Mohan et al. (2017) hydrothermally synthesized ZrO_2/GO with $S_{RET} = 632 \text{ m}^2/\text{g}$. The fixed-bed continuous flow experiments showed that the desorption elution efficiency of the adsorption column regenerated with 10% NaOH solution was greater than 95% for F within three cycles, indicating the role of the ion exchange mechanism in the adsorption of F-. Nehra et al. (2019) hydrothermally synthesized TiO₂/GO with a maximum fluoride adsorption capacity of 342 mg/g, which is the highest reported capacity available. Ti⁴⁺ forms strong bonds with the oxygen-containing functional groups of GO by electrostatic attraction and reacts with NaOH on the GO side to form basic titanium hydroxide on the GO layer. The adsorption mechanism for fluoride consists of a complexation reaction with Ti and F and an ion exchange between OH and F.

3.4 Multiple Types of Metal-Modified Composite Adsorbents

Studies have also reported on composite adsorbents synthesized from three or more types of materials, with combinations of metal-modified biopolymers and inorganic materials making up the bulk of the adsorbents (**Table 5**). The compound of metallic, inorganic, and biomaterials effectively combine the advantages of different types and can yield further synergistic effects. He et al. (2018) achieved a maximum adsorption capacity of 288.96 mg/g for yttrium-based GO/SA hydrogels prepared by sol–gel. Wei et al. (2022) mixed reed biomass powder with SA, cross-linked with CeCl₃ solution, and then calcined to obtain cerium alginate biochar beads. The composite adsorbent RBM-Ce has greatly

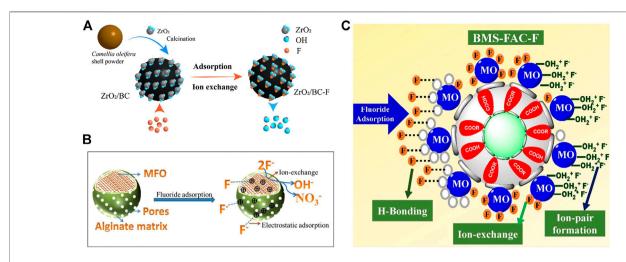


FIGURE 9 | Respective adsorption mechanisms of composite adsorbents from different metal-modified materials. (A): ion exchange (Mei et al., 2020), (B): electrostatic attraction (Wu T. et al., 2017), (C): ion pair (Raghav et al., 2019).

improved the maximum adsorption capacity, S_{BET} , pH_{PZC} , and stability compared to individual components.

3.5 Modified Synthesis Methods

In summary of the aforementioned composite adsorbent synthesis methods (**Tables 4**, 5), it can be seen that the general principle of metal-modifying adsorbents is to coat the opposing surface with metal salts. The main methods of modification are chemical coprecipitation, impregnation, and hydrothermal methods, which are described here.

3.5.1 Chemical Coprecipitation

Chemical coprecipitation is a common method for the preparation of multi-metals (Table 4) and metal-modified inorganic adsorbents (Table 5). In the preparation of multimetal nanoparticles, the chemical coprecipitation method first mixes each metal salt solution in proportion to the atoms of the target product to be prepared to form an aqueous solution of the metal ions. The metal ions are then simultaneously precipitated out of the solution by the addition of appropriate precipitants to form hydroxide precipitate (Wu et al., 2013). The precipitates are separated out and then dried or calcined to obtain powdered multi-metal hydroxide/oxide nanoparticle adsorbents (Zhou et al., 2018). When modifying inorganic adsorbents with metals, the inorganic material is first put into a metal salt solution via methods such as adjusting the pH of the solution; the metal ions in the solution are induced to produce nano-metal particles that precipitate and load onto the surface and pore paths of the inorganic material, which are then dried or calcined to form composite adsorbents (Figure 6) (Wang et al., 2019b). The coprecipitation method is simple and not time-consuming. However, due to the different precipitation rates of different elements, there is sometimes a stratification of the precipitation, which makes the precipitate not uniformly dispersed and the composition of the product somewhat biased.

3.5.2 Hydrothermal

The hydrothermal method is also commonly used for the preparation of multi-metals (Table 4), and some studies have also been used for the modification of other materials by metals. Similarly, the metal ions are first prepared in a mixed solution in a certain proportion and then placed in a hydrothermal reactor at 423–573 K for a specific time. The principle of the hydrothermal method is that in a closed reaction environment, the precursor undergoes high temperature and pressure to fully dissolve in the solvent (Nehra et al., 2019). Then hydrolysis and nucleation according to a certain crystallization mode to grow nanomicrocrystalline particles, to obtain a uniform particle size and good dispersion of composite powder (Figure 7). The nanomaterials prepared by the hydrothermal method have homogeneous morphology and the products are well dispersed. However, high pressure and temperature-resistant instrumentation are required, with long reaction times and production cycles, which are not conducive to mass production. Thus, it is often used in the laboratory to prepare nanomaterials with special morphologies for research. By controlling the crystallization time, crystallization temperature, and other factors, nanopowders with different morphologies can be prepared.

3.5.3 Impregnation

Impregnation is commonly used for metal-modified inorganic materials (carbon, clay, GO, etc. **Table 5**). The powdered inorganic material is first pre-treated by immersion in a metal salt solution (AlCl₃, CaCl₂, FeCl₃, LaCl₃, etc.). The metal ions in the solution can be loaded on an inorganic surface or internally *via* auxiliary heating and ultrasonic dispersion. The composite adsorbent is then dried or calcined (**Figure 8**). The impregnation preparation method is also facile but slightly more time-consuming, relying on the specific surface area of the inorganic material and bonding of the active sites on the surface to the metal.

TABLE 6 | Adsorption conditions and performance of fluoride by metal-modified carbon and other adsorbents.

Adsorbents	Adsorption condition					Isotherm	Regeneration	\mathbf{Q}_{\max}	Ref
	Initial C_F^- (mg/L)	Adsorbent dose (g/L)	Reaction pH	Temperature (K)	Equilibrium time (min)	model	performance	(mg/g)	
Wood biochar-La	40	5	6	298	50	Langmuir	53% at sixth cycle	164.20	Habibi et al. (2019)
Al-modified corn biochar	50	1	6.8	298	100	Langmuir	_	74.14	Zhang et al. (2021a)
MgO shell biochar	20	1	6–8	298	360	Langmuir	_	57	Wan et al. (2019)
Pomelo peel BC-La	10	2	6.5	298	1,200	Freundlich	66% at sixth cycle	19.86	Wang et al. (2018b)
ZrO ₂ -seed shell biochar	10	1.6	3–9	298	180	Langmuir	50% at third cycle	9.63	Mei et al. (2020)
Magnetic biochar	10	2	2–9	308	5	Langmuir	_	9.04	Bombuwala Dewage et al. (2018)
Mg-Mn-Zr AC	10	1	2–10	303	180	Langmuir	_	26.27	Mullick and Neogi (2019)
Zr-impregnated AC	10	2	4	303	180	Langmuir	33% at fifth cycle	5.40	Mullick and Neogi (2018)
La-functionalized AC	200	1	7	303	180	Sips	_	10.51	Merodio-Morales et al. (2019)
Activated carbon@ SnO ₂	10	0.3	6	303	180	Langmuir	80% at third cycle	4.60	Mohanta and Ahmaruzzaman
Ce-containing bone	50	2	5	303	840	Sips	_	47.16	(2018) Zúñiga-Muro et al.
char Magnetic bone biochar	20	5	8	298	1,440	Freundlich	38% at fourth cycle	5.23	(2017) Zhou et al. (2019a)
Graphene oxide with Ti	50	3.5	6	308	100	Langmuir	54% at sixth cycle	342	Nehra et al. (2019)
Al-polyacrylic acid	10	1	2	298	200	Freundlich	_	283.48	Xu et al. (2017)
CeO ₂ @SiO ₂	50	1.5	3	298	45	Langmuir	57% at fourth	257.70	Wang et al. (2019a)
microsphere							cycle		
Magnetic γ-Fe ₂ O ₃ - GO-La	10	0.2	7	298	30	Langmuir	78% at sixth cycle	77.12	Wen et al. (2015)
Zn-modifying slag	50	0.5	5	298	30	Freundlich	_	60	Sarkar et al. (2019)
ZrO ₂ -graphene oxide	25	0.5	7	303	50	Langmuir	59% at fifth cycle	45.7	Mohan et al. (2016)
Hydrous Fe/Al GO	10	3	5	308	60	Langmuir	_	22.9	Kanrar et al. (2016)
Fe-modifying pumice	3	0.7	3	298	50	Freundlich	_	21.74	Dehghani et al. (2016
FeOOH-graphene oxide	25	2.5	2–10	298	120	Langmuir	_	17.672	Kuang et al. (2017)
Aluminum/olivine	10	2	6	303	60	Langmuir	_	12.94	Ghosal and Gupta (2018)
Polyhydroxy-iron	25	1	7	298	40	Freundlich	_	11.09	Muschin et al. (2021)
3D Y-based GO hydrogels	20	0.2	4	293	1,440	Langmuir	72% at third cycle	288.96	He et al. (2018)
Al2O3-chitosan biochar	20	1	3	298	1,440	Langmuir	_	196.1	Jiang et al. (2018)
Graphene oxide/ eggshell	30	0.25	7	298	120	Langmuir	_	56.6	Nor et al. (2020)
Ce-SA/BC beads	10	1	3–9	293	20	Langmuir	_	34.86	Wei et al. (2022)
Ca-pectin- hydroxyapatite	10	1	7	298	30	Freundlich	_	28.47	Raghav et al. (2018)
Polypyrrole onto BC	10	1	6.5	298	_	Langmuir	53% at 4th cycle	18.52	Wang et al. (2017c)

Some preparations are calcined after coprecipitation, impregnation, or hydrothermal treatment (**Figures 6–8**). For example, metal-modified biochar is calcined to form metal oxide nanoparticles on the surface of BC, which further

enhances the adsorption capacity (**Table 5**). LDH is also sometimes calcined (**Table 4**). During heating, LDH can be transformed into mixed metal oxides as the interlayer anions are eliminated by thermal decomposition. After the adsorbent is

put into a fluoride solution, it will undergo a rehydration process. During rehydration, these oxides are in turn rebuilt into original layered structures by adsorbing various anions from the aqueous solution, known as the "memory effect" (Wu P. et al., 2017). The specific surface area and anion exchange capacity of LDH increases further after calcination. After coprecipitation or impregnation, the modification of biopolymers is generally achieved by the sol–gel method for the preparation of hydrogels (Wang A. et al., 2017).

3.6 Adsorption Mechanism

The adsorption mechanism can be divided into physical adsorption and chemisorption. Physical adsorption is generally considered to be caused by van der Waals forces, which are nonselective and reversible, and can be desorbed under certain conditions. Current research on the physical adsorption of fluoride ions is mainly based on electrostatic attraction and hydrogen bonding. Chemisorption is mainly the formation of chemical bonds between molecules and is described by the Langmuir model; the adsorption is selective and irreversible and desorption is more difficult. Physical adsorption depends mainly on the active pore volume and specific surface area (Wang H. et al., 2017), while chemisorption depends more on chemical or electroaffinity. The fluoride adsorption mechanism by various metal-modified adsorbents is summarized in Tables 4, 5. A total of four main adsorption mechanisms can be found: electrostatic attraction, ion exchange, hydrogen bonding, and complexation. The actual adsorption process is usually accompanied by several mechanisms (Figure 9).

When metal oxide enters the aqueous solution, the hydrogen ions are attracted to lone pair electrons of the oxygen element in metal oxide, forming a hydroxyl ligand (Zhang and Jia 2016). The fluoride removal by metal oxides and metal-modified composite adsorbents exploits the large number of hydroxyl groups on the surface (**Figure 9A**). When the solution pH is less than zero charge point (pH_{PZC}) of the composite adsorbent, hydroxyl functional groups become protonated, forming OH_2^+ and are positively charged. The positive charge surface attracts negatively charged fluoride ions by electrostatic attraction (**Figure 9B**).

Fluoride is attracted to the surface of composite adsorbents for immobilization, but ion pairs (Figure 9C) are weakly interacting with each other and easily desorbed. Several studies have confirmed the involvement of hydroxyl groups in the adsorption reaction by FTIR and XPS characterization. F- has the same charge and similar radius composition as OH and can replace OH in the structure of composite adsorbents (Figure 9A). F is bonded to a metal-occupying active site, OH is released, and the solution pH rises after adsorption. Most studies have been based on the anion exchange mechanism. As pH rises above the pH_{PZC} of the adsorbent, there is no significant decrease in adsorption, indicating that adsorption is mainly controlled by ion exchange. Generally, when the solution pH > 10, the large amount of free OH in the solution competes with F⁻, resulting in a significant decrease in adsorption

capacity. Complexation between metals and fluoride has also been suggested (Suzuki et al., 2013).

Metal-modified composite adsorbents often have polar functional groups containing hydrogen, such as -OH, -COOH, and -NH $_2$ (Yang et al., 2017). The shared electron pairs of polar functional groups are strongly biased toward oxygen or nitrogen, leaving the hydrogen atom almost naked. The lone pair electrons of electronegative fluoride will interact with the hydrogen atom forming a hydrogen bond with a bond angle of 180° and immobilize (**Figure 9C**).

4 CONCLUSION AND FUTURE DIRECTION

Comparison of **Table 2** with **Tables 3**, **6** reveals an overall increase in fluoride adsorption capacity of metal-modified composites. It indicates that most of the modifications are successful with application prospects. However, there are still many issues that need to be considered to achieve a big breakthrough in practical applications. The multi-metals enrich active sites for fluoride, but agglomeration and easy leaching are still problems, and individual preparation still requires some cost. Metal-modified biopolymers improve the stability of hydrogels, and metals can also be dispersed and immobilized in the macromolecular structure. However, it is reported that the dense surface of hydrogel makes it difficult for fluoride ions to enter the internal pores of beads, and beads sink easily so they have a limited contact area with fluoride. Metal-modified carbon, mineral clay, and other inorganic materials can also improve the dispersion and immobilization of metals to some extent, but there are still problems of dissolution, and loaded metals are easily dislodged and poorly recycled. Low-cost inorganic materials balance the price of rare earth metals and reduce the amount of metals, but at the same time, present the safety risk of waste use. The metal and inorganic materials are both in powder form, and the issue of separation and recycling has not been addressed. Studies combining metals, inorganic materials, and biopolymers appear to address the agglomeration and immobilization of metals, expanding the pore space and fluoride contact area of hydrogel beads, while improving the separation and recovery properties of inorganic materials. However, more than 90% of studies mentioned in this review avoided exploring metal dissolution concentrations and less than 10% of adsorbents were able to achieve more than 80% fluoride adsorption at the fifth cycle. Future studies will need to pay attention to the simplicity, efficiency, and cost of preparation procedure. Overall, the search for future defluoridation adsorbents is not limited to the requirement for increasing adsorption capacity. More important is the attention to cost levels, regeneration performance, separation and recovery, and safety issues for practical applications.

AUTHOR CONTRIBUTIONS

YW summarized and wrote the article under the guidance of LW. All authors contributed to conceptualizing, editing, commenting on, and reviewing the manuscript.

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Synthesis and Photocatalytic Activity of Pt-Deposited TiO₂ Nanotubes (TNT) for Rhodamine B Degradation

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Dye wastewater has attracted more and more attention because of its high environmental risk. In this study, a novel TiO₂ nanotube (TNT) catalyst was prepared and its morphology and structure were characterized. The synthetic catalyst was used to degrade Rhodamine B (RhB) under UV light and evaluated for the application performance. According to the characterization results and degradation properties, the optimum synthetic conditions were selected as 400°C calcination temperature and 10 wt% Pt deposition. As a result, the degradation efficacies were sequenced as TNT-400-Pt > TNT-500-Pt > TNT-400 > TNT-300-Pt. In addition, the effect of pH and initial concentration of RhB were explored, and their values were both increased with the decreased degradation efficacy. While the moderate volume of 11 mm of H₂O₂ addition owned better performance than that of 0, 6, 15 mm. Scavengers such as tertbutanol (t-BuOH). ethylenediaminetetraacetate (EDTA-Na₂), and nitroblue tetrazolium (NBT) were added during the catalytic process and it proved that superoxide radical anions (O_2^{\bullet}) , photogenerated hole (h+) and hydroxyl radical (OH•) were the main active species contributing for RhB removal. For the application, TNT-Pt could deal with almost 100% RhB, Orange G (OG), Methylene blue (MB), and Congo red (CR) within 70 min and still kept more than 50% RhB removal in the fifth recycling use. Therefore, TNT-Pt synthesized in this study is potential to be applied to the dye wastewater treatment.

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INTRODUCTION

With increasing technological and industrial development, a diverse set of pollutants have been discharged into water bodies, leading to the increasing concern about water contamination and environmental risks (Xu et al., 2021; Zeng et al., 2021). Colored dyes, represented by Rhodamine B (RhB), Orange G (OG), methylene blue (MB), and Congo red (CR) are widely used in the textile, printing, and plastic industries, which have high concentration levels in wastewater (Skjolding et al., 2021). Seriously, most dye pollutants cannot be easily degraded in water due to their complex composition, deep color, and chemical and physical stability (Sutar et al., 2022). Therefore, several techniques, such as adsorption, coagulation, biodegradation, and photocatalysis have been used in treating dyeing wastewater (Hao et al., 2021; Liu et al., 2021; Pu et al., 2017). Among these technologies, photocatalysis is increasingly regarded as a favorable option in recent years due to the advantages of its simple operation process, low

energy consumption, and comparatively high degradation efficacy for pollutant removal (Xu et al., 2017a; Xu et al., 2017b).In addition, compared with photolysis, photocatalysis has the synergistic benefit of a specific catalyst combined with light irradiation (Xu et al., 2018; Xu et al., 2020a). Among many candidates of photocatalysts, TiO₂ is the most widely studied material, currently the most likely photocatalyst for industrial-scale application in terms of high chemical stability, durability, high hydrophilicity, photoactivity efficiency, low toxicity, and low cost (Xu et al., 2020b; Hao et al., 2022).

While during photocatalysis by TiO₂, the high recombination rates of photogenerated electron-hole pairs result in reduced photocatalytic efficiency (Perera et al., 2012). Accordingly, a series of strategies for the preparation of TiO₂-based nanocomposites have been developed (Mi et al., 2021; Wang et al., 2021; Wu et al., 2021). TiO₂-based nanotubes (TNTs) were first synthesized by electrochemical deposition in a porous aluminum oxide mold (Hoyer, 1996). Compared with commonly used TiO₂ nanoparticles (NPs), TNTs exhibit unique photocatalytic properties including larger specific surface area (up to 478 m²/g) and larger pore volume (up to 1.25 cm³/g), comparatively strong ion-exchange capability; significant fast and long-distance electron-transport ability; and enhanced light absorption due to the high tube diameter ratio (Liu et al., 2014).

In addition, noble metals (e.g., Pt, Pd, and Ag) with TiO₂ deposited can bend the valence band (VB) and conduction band (CB) as the difference in the Fermi level between metals and semiconductors (SC) to form a Schottky barrier (Christoforidis and Fornasiero, 2017). The work function (φ) increases with the greater Schottky barrier in the metal-SC heterojunction, causing a better charge separation effect, which is a key step in most photocatalytic processes. For example, TiO₂ modified with Pt, Pd, and Ag has higher decomposition activity for the pollutants removal, with the pseudo-first-order kinetic rate constants of were 0.7267, 0.4369, and $0.1257 \, h^{-1}$, which were 12.5, 7.5, and 2.2 times higher than that of pure TiO2, respectively (Li et al., 2016). While among these noble metals, platinum (Pt) has a comparatively high work function ($\varphi = 5.93 \text{ eV}$) with good performance as a TiO₂cocatalyst (Fu et al., 2008; Chiarello et al., 2010). The reason has been explained that photogenerated electrons are used more efficiently in Pt atoms (Nguyen and Juang, 2019). In this study, TNT-Pt was prepared by hydrothermal synthesis, calcined at different temperatures (300, 400, 500°C), and different amounts of Pt loading (3, 5, 10, and 20 wt%). All catalysts were characterized for their morphology and structure and tested for the degradation performance of RhB in the photochemical reactor under UV irradiation. Meanwhile, the solution pH, initial concentration of the pollutants, and H₂O₂ addition affecting the degradation efficacy was discussed and the photocatalytic mechanism was explored by quenching experiments.

MATERIALS AND METHODS

Preparation of TNT-Pt

Briefly, $1.2\,\mathrm{g}$ commercial $\mathrm{TiO_2}$ (AeroxideP25) and 75 ml NaOH aqueous solution (10 M) were placed in a 100 ml Teflon lined

hydrothermal autoclave reactor and kept in an oven at 110°C for 12 h. Then, the sample was washed several times with deionized water and filtered. Afterward, the sample was ultrasonically treated with 0.1 M HCl aqueous solution for 15 min and filtered. After filtering, the sample was washed several times with deionized water. The obtained samples were kept in an oven at 80°C for 12 h. After being completely dried, the samples were collected and ground, which were identified as TiO2 nanotubes (TNT). All chemicals are of analytical grade. TNT was calcined at different temperatures in a tube furnace (Nabertherm P330) with the following temperature program: from 25°C to the calcination temperatures ($T_{\rm calc}$, °C) at a heating rate of 5°C/min, and keeping 3 h at $T_{\rm calc}$. The $T_{\rm calc}$ values were set at 300, 400, and 500°C, respectively. These three samples are labeled as TNT-300, TNT-400, and TNT-500.

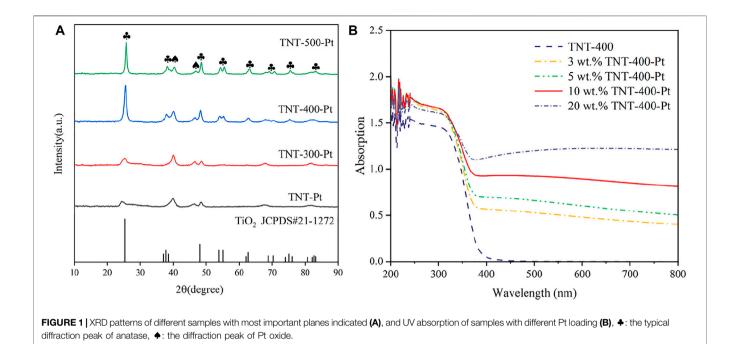
Pt was photo-deposited on all the samples (P25, TNT, TNT-300, TNT-400, TNT-500). Firstly, 50 mg photocatalyst was added into 1.05 ml $\rm H_2PtCl_6$ aqueous solution (10 g/L) to prepare 50 ml solutions and then mixed with 4 ml $\rm CH_3OH$. After irradiating under the 300 W mercury lamp for 3 h, the suspension was washed with deionized water and filtered to obtain the precipitate. After keeping in an oven at 80°C for 12 h, the sample was collected and determined to be TNT-Pt, TNT-300-Pt, TNT-400-Pt, and TNT-500-Pt, which were subsequently used in this study.

Catalyst Characterization

The crystalline structure of the samples was determined by an XRD PANalytical Empyrean diffractometer, a Cu Kα radiation of 1.54 Å, scan step-size 0.0167° and a 2θ scan range of $10-90^{\circ}$. Absorption spectra of doped and undoped Pt samples were analyzed using a UV spectrometer (Shimadzu) scanning wavelengths from 200 to 800 nm. TEM and STEM-EDS analysis were performed by using Tecnai G2 and Titan FEI transmission electron microscopes, operating at 200 and 300 kV, respectively. The sample was prepared by suspending the powder in 2-propanol, ultrasounds treated, and finally dropping 5 µL of the suspension three consecutive times on a 400-mesh Cu grid provided by Tedpella, letting the solvent evaporate at room temperature. The specific surface area and pore volume of the derived nanotubes were determined by BET (Micromeritics, ASAP 2460/2020). Determination of Pt loading on TNT-Pt by ICP-MS (Agilent 7700s). Zeta potential values were determined using a laser particle size zeta potential analysis (Malvern Zetasizer Nano As). Zeta potential was measured three times at each pH value. The preparation method referred to the previous studies by some modifications (Xiong and Xu, 2016; Scandura et al., 2019).

Photocatalytic Evaluation

The photodegradation of RhB in water was performed in a photochemical reaction instrument, which consisted of a 100 W mercury lamp with a wavelength of 365 nm, a condensation cup, and a magnetic stirrer inside a box. For degradation of RhB, the synthesized catalyst samples were added to the RhB solution with an initial concentration of 20 mg/L. Then, the suspensions were strongly stirred for 0.5 h



in the dark to reach the adsorption equilibrium state. After that, the solution was exposed to UV irradiation for 70 min. During the photocatalytic process, 2 ml solution was sampled every 10 min (8 times in total) and filtered to remove the catalyst. The supernatant was analyzed to measure the concentration of RhB with a Hitachi UV-3010 UV-vis spectrometer. All experiments were conducted in triplicate.

RESULTS AND DISCUSSION

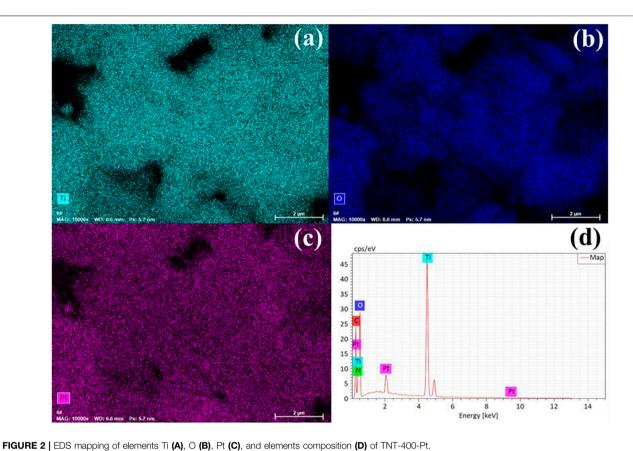
Morphologies and Structures

The evaluation of the phase and structure of the calcined TNT was observed through XRD patterns (Figure 1A). The crystallinity of these samples gets higher with the increase in calcination temperature (T_{calc}). It can be seen that TNT-300 has only a small amount of anatase diffraction peaks (Supplementary Figure S1). The spectra of TNT-400 show characteristic diffraction peaks located at 25.281°, 37.8°, and 48.049°, corresponding to the (101), (004), and (200) reflection plane (JCPDS card 21-1,272) (Lazarte et al., 2018). H₂Ti₃O₇ (202), brookite (200), and rutile (210) reflection plane appear in TNT-500 at 24.670°, 33.050°, and 44.699°. Thus, TNT-400 owns the highest amount and purest anatase type crystal phase than that TNT-300 and 500. After Pt was deposited on the surface of TNT, new diffraction peaks at 40.186° and 63.024° that derived from PtO₂ (101) and PtO (222), respectively, appeared in the catalyst samples (JCPDS card 38-1355 and 47-1171). Moreover, the addition of Pt only passivates the diffraction peaks of anatase and does not affect the overall crystal form of the sample. In order to determine the photo absorbance properties, the UV absorption of TNT and Pt-TNT under different Pt loadings were analyzed by UV-Vis at wavelengths of 200-800 nm as shown in Figure 1B. The main light absorption wavelength of TNT-400 is in the ultraviolet range. However, with increasing Pt loading, the amount of visible light absorbed by the catalyst steadily increased, with only a slight increase in the amount of light absorption in the UV range, where 10 wt% loadings showed the best absorption of UV light in the UV rangeability. This illustrates the increased photosensitivity of Pt-modified TNTs in the visible and near-visible light wavelength range relative to pure TNTs.

Furthermore, TNT-300, 400, and 500 were modified with Pt deposition, respectively. While no obvious change in the morphology of Pt-loaded samples was observed in SEM images (Supplementary Figure S2). EDS results verified the presence of Ti, O, and Pt elements (Figure 2), indicating the successful photo-deposition of Pt particles. BET results provided in Table 1, claim that the surface areas were followed the sequence as TNT-300-Pt = $286.2 \text{ m}^2/\text{g} > \text{TNT-400} = 155.8 \text{ m}^2/\text{g}$ $g > TNT-400 = 148.2 \text{ m}^2/g > TNT-500-Pt = 81.5 \text{ m}^2/g \text{ proving}$ maximum specific surface area of TNT-300 Pt. TEM was used to further analyze the morphology of the TNT-300, 400, and 500-Pt samples as shown in **Figure 3**. From the images, all the TNT tubes present a uniform distribution with an average diameter of 7-10 nm, with an opened tube orifice (Figures 3A-C), while the surface-adsorbed Pt nanoparticles exhibit a size of about 2-5 nm (Figure 3D), demonstrated again the emergence of new photocatalytic sites. A layered structure with an apparent edge was observed, illustrating the incomplete curling of part of the TNT tube. With the increase of calcination temperature from 300 to 500 °C, TNT tube curling degree increased and the loading content of Pt nanoparticles raised (Figures 3A-C).

Photocatalytic Behavior

The irradiation time versus the RhB concentration curves has been given in Figure 4. Obviously, TNT prepared under T_{calc}



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 TABLE 1 | Surface areas and particle sizes of TNT-400 and TNT-Pt photocatalysts.

Catalyst	Surface areas (m ² /g)	Pore volume (cm ³ /g)	Pore sizes (nm)
TNT-400	155.8403	1.0586	23.632
TNT-300-Pt	286.2142	1.005651	12.3963
TNT-400-Pt	148.194	0.646873	13.9094
TNT-500-Pt	81.4997	0.450061	17.1476

400°C (TNT-400) exhibited higher photocatalytic ability for RhB removal than that of TNT-300, 500, and primitive material (TNT) as shown in Figures 4A,B. This could be explained that TNT-400 owns the highest amount of anatase type crystal phase according to the characterization results mentioned above. Commonly, the anatase type crystal phase contains more defects and vacancies, resulting in more oxygen vacancies to capture electrons, so it has higher activity (Li et al., 2021). Comparatively, TNT-300 and 500 own fewer amounts of anatase type crystal phase, especially TNT-500 with part of rutile type crystal phase, which has almost no photocatalytic activity (Phuong and Yoo, 2020). Thus, TNT-300 and 500 had poor photocatalytic capacity for RhB Removal. While after the Pt loading, the degradation performance was highly promoted as RhB was completely bleached by TNT-400-Pt within 70 min (Figure 4C). The kinetics of the photodegradation of RhB fitted well to the pseudo-first-order model ($R^2 > 0.90$) based on Eq. 1 (Mansurov et al., 2022):

$$In (C_0/C_t) = kt$$
(1)

where k is the rate constant, C_0 and C_t are the concentration of RhB in solution at irradiation time 0 and t (min⁻¹), respectively. As shown in **Figure 4D**, the rate constant (k) was ranked as $k_{TNT-400-Pt} = 0.035 \text{ min}^{-1} > k_{TNT-400} = 0.015 \text{ min}^{-1}$. As Pt loading on TNT was favorable for O_2 adsorption and the superoxide radical $(O_2^{\bullet\bullet})$ formation, which plays the key role for RhB degradation. Similarly, TNT-400-Pt owned better catalytic ability than TNT-300, 400 and original TNT-Pt, with the sequence of k value as $k_{TNT-400-Pt} = 0.035 \text{ min}^{-1} > k_{TNT-500-Pt} = 0.015 \text{ min}^{-1} > k_{TNT-300} = 0.002 \text{ min}^{-1} \approx k_{TNT-Pt} = 0.002 \text{ min}^{-1}$, which further proved the high activity of TNT-400-Pt. This might be attributed to the various Pt contents deposited in TNT. Under different T_{calc} , the

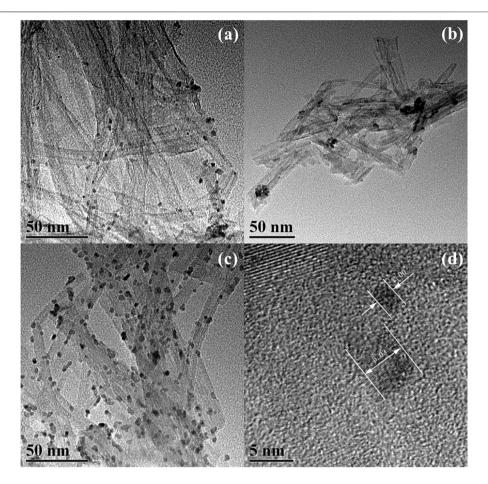


FIGURE 3 | TEM images of TNT-300-Pt (A), TNT-400-Pt (B), and TNT-500-Pt (C), scale bar: 50 nm, Pt nanoparticle size (D).

Pt contents deposited in TNT-300, 400, 500 detected by ICP-MS were 7.3 wt%, 7.5 wt%, and 6.8 wt%, thus TNT-400-Pt owned the highest amount of Pt deposited in the catalyst. Furthermore, TNT-400 owns the highest amount of anatase type crystal phase, leading to the stronger photocatalytic ability for pollutant removal.

In this case, the effects of different experimental factors were investigated on photocatalysis by TNT-400-Pt. First, the loading amount of Pt during the synthesis process is essential for the catalytic performance as shown in **Figure 5A**. As a result, only a proper amount of Pt 10 wt% loading has a positive effect on RhB removal. A higher or lower amount of Pt (20 wt% or 5 wt% and 3 wt%) loading had the reduced degradation efficacies, which were all better than that of pure TNT. This could be explained that Pt deposition could provide active species for the pollutant oxidation, while the excess loading may cover active sites on the TiO₂ surface, thereby reducing photodegradation efficiency, which was also discussed by previous literature (Shawky et al., 2020). In addition, the UV-vis results (**Figure 1B**) exhibit that 20 wt% TNT-Pt had higher absorption values than that of others, which also could be the reason for its higher degradation performance.

Moreover, the photodegradation of RhB by TNT-400-Pt (10 wt%) was evaluated at various initial solution pHs of 3, 5, 7, and 9 as shown in **Figure 5B**. The degradation efficacy is higher

under acid conditions than that under neutral and alkali conditions, which is probably due to fact that the charge of TNT-400-Pt at the pH of 6.1 is zero as shown in **Supplementary Figure S3** in the appendix. This suggests that the TNT surface was positively charged at pH < 6.1, while negatively charged at pH > 6.1. At low pH, H $^+$ adsorbed on the catalyst surface has a large proton exchange capacity, which could react with the photogenerated electrons to form hydrogen radical (H \bullet). Meanwhile, a lower pH solution has electronegative centers, leading to the promoted adsorption on the surface of TiO₂, which also increase the degradation rate under acid condition. A similar explanation has also been mentioned in the previous literature (Mohanty et al., 2020).

Figure 5C exhibits the effect of initial concentration in the range of 5–25 mg L $^{-1}$ on the catalytic performance. The results show that the degradation efficacy was highest at the RhB concentration of 5 mg L $^{-1}$. While it decreased with the concentration increasing as the rate constant (k) was ranked from highest to lowest as $k_{5~mg/L}=0.092~\text{min}^{-1}>k_{10~mg/L}=0.055~\text{min}^{-1}>k_{20~mg/L}=0.034~\text{min}^{-1}>k_{30~mg/L}=0.011~\text{min}^{-1},$ which could be explained as the active radicals generated on the catalyst surface were reduced due to the occupation of pollutant molecules in the active sites. Furthermore, H_2O_2 reported as an

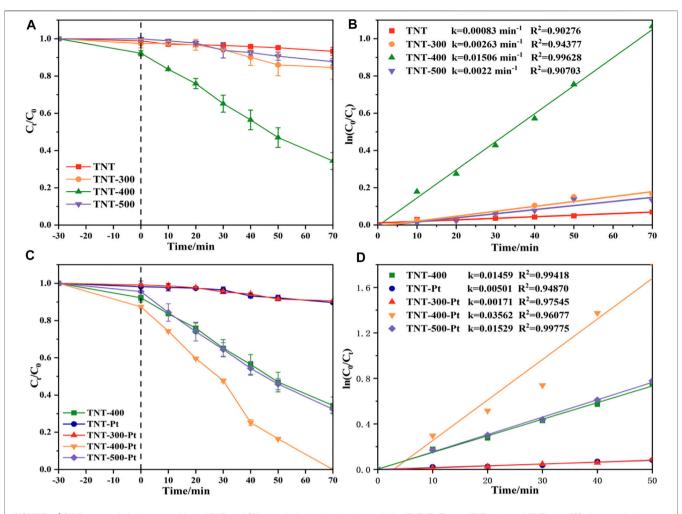


FIGURE 4 | (A) Photocatalytic decomposition of RhB and (B) pseudo-first-order kinetic model by TNT, TNT-300, TNT-400, and TNT-500, (C) photocatalytic decomposition of RhB, and (D) pseudo-first-order kinetic model by TNT-Pt, TNT-300-Pt, TNT-400-Pt and TNT-500-Pt, pH = 6.83, initial RhB concentration = 20 mg/L.

electron acceptor also plays role in the RhB removal. **Figure 5D** reveals that H_2O_2 in the RhB solution enhanced the degradation efficacy, especially 11 mm addition with the promoted rate constant of 0.057 min⁻¹, higher than that of 7 mm and no H_2O_2 addition. The reason could be attributed to the generation of hydroxyl radical (OH \bullet) reacting from the reaction of H_2O_2 with electron (e $^-$) as the **Eq. 2** (Wang J.-F. et al., 2022).

$$e^- + H_2O_2 \rightarrow OH^- + OH^{\bullet}$$
 (2)

While a limiting value for the degradation rate occurred when the $\rm H_2O_2$ addition achieved 15 mM due to the scavenging reaction as shown in Eq. 3.

$$H_2O_2 + OH \bullet \rightarrow H_2O + HO_2 \bullet$$
 (3)

Photocatalytic Mechanism

During the photocatalytic process, the main active species include photogenerated holes (h⁺) and electrons (e⁻), hydroxyl radicals

(OH•), and superoxide radical anions $(O_2^{\bullet\bullet})$ that could be produced based on the following Eq. 4-6.

$$TNT - Pt + hv \rightarrow TNT - Pt(h^{+} + e^{-})$$
 (4)

$$h^{+} + H_{2}O \rightarrow OH \bullet + H^{+} \tag{5}$$

$$e^- + O_2 \to O_2^{-\bullet} \tag{6}$$

To confirm the significance of these active species, tertbutanol (t-BuOH), disodium ethylenediaminetetraacetate (EDTA-Na₂), and nitroblue tetrazolium (NBT) as the scavengers of OH \bullet , h⁺, and $O_2^{\bullet\bullet}$, respectively were added during the photocatalytic process. As shown in **Figure 6A**, it could be easily observed that the degradation efficacy was poorest with NBT addition, followed by EDAT-Na₂ and t-BuOH addition, compared with the performance by TNT-Pt without scavengers. This proves that $O_2^{\bullet\bullet}$ plays an essential role in the RhB degradation, then was a photogenerated hole (h⁺) and OH \bullet contributed to the pollutant removal. Accordingly, the possible photocatalytic mechanism could be speculated as shown in **Figure 7**. Under UV irradiation, the RhB molecules were activated as shortlived active transient, adsorbed over Pt metal sites. Meanwhile, Pt

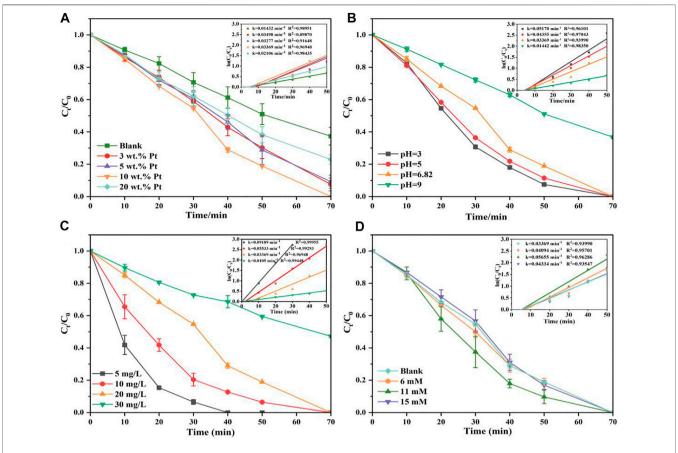


FIGURE 5 | Change Pt load on TNT-400 **(A)**, effects of pH_{Ini} **(B)** on RhB photodegradation by TNT-400-Pt (10), the effect of initial concentration of RhB on the photocatalytic degradation of TNT-400-Pt (10) **(C)**, effects of H₂O₂ **(D)** on RhB photodegradation by TNT-400-Pt.

loading induced the $O_2^{-\bullet}$ generation of pollutant oxidation, and nano-structure holes of TNT could provide unique space and electronic environments for Pt active sites, which was easier to inhibit the recombination of photogenerated electron and hole pairs, leading to the prior photocatalytic ability dealing with RhB. This was consistent with the literature (Ding et al., 2022; Wang X. et al., 2022). Therefore, the catalytic activity for RhB was significantly improved by TNT with Pt deposition.

Application to Other Dye Pollutants and Recycling

TNT-Pt-400 (10wt%) was also used for other dye pollutants such as CR, MB, and MO as shown in **Figures 6B,C**. As a result, at initial concentrations of 10 mg/L, almost all RhB, CR, MB, and OG could be removed within 70 min by TNT-Pt. While at the concentration of 20 mg/L, 100% RhB and CR, 65% MB and 90% OG could be degraded within 70 min. Thus, the obtained catalysts of TNT-Pt own a comparatively strong capacity for dye pollutants removal. In addition, the reuse capacity of the synthesized materials (TNT-Pt-400, 10 wt%) was evaluated by five cycling usages as shown in **Figure 6D**. Obviously, the performance stained well as almost 100% RhB removal in the first three cycles, 80% removal remained in the third time of cycling, and

more than 60% removal was achieved in the fifth time, indicating that the synthesized catalysts were reusable and exhibited high potential on the applications of real wastewater treatment.

CONCLUSION AND FUTURE PERSPECTIVE

In summary, TNT-Pt was synthesized successfully and exhibited well-characterized morphology and structure. During the synthetic process, 400°C calcination temperature and 10 wt% Pt deposition was determined to be the preferable condition to form a better crystal morphology based on the characterization results. In the photodegradation experiments, the rate constant (k) was ranked as $k_{TNT-400-Pt} = 0.045 \text{ min}^{-1} > k_{TNT-400} = 0.014 \text{ min}^{-1}$. In addition, acid solution (pH 3) and lower initial concentration of RhB (5 mg/ L) both increased the degradation process, while a moderate volume of 11 mm H₂O₂ addition had the promoted degradation performance. Furthermore, in the quenching experiment, NBT had the most significant inhibition effect on the photocatalytic efficacy than other scavengers, suggesting the dominant active species $O_2^{-\bullet}$. Besides, the synthesized TNT-Pt could remove almost CR, MB, and OG as well as RhB, and its catalytic capacity stained well in five recycling usages.

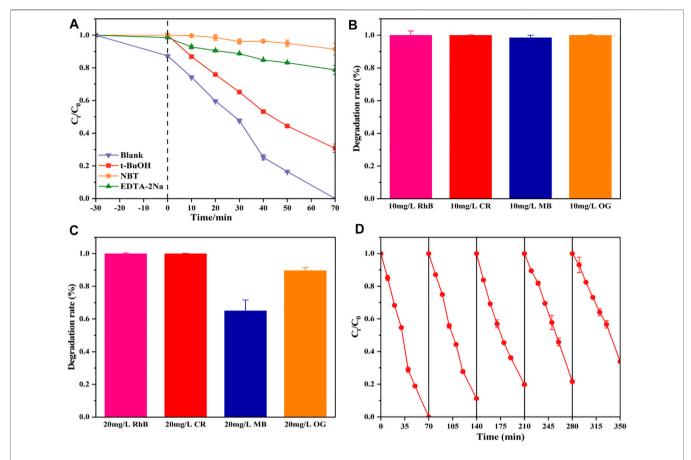
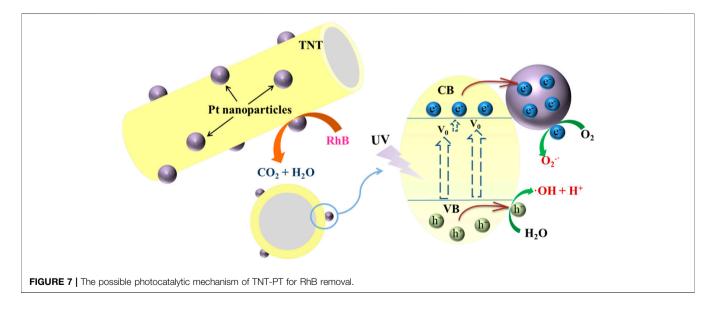


FIGURE 6 | Photocatalytic activities of the TNT-400-Pt sample for RhB degradation with disparate scavengers (A), photocatalytic degradation of different dyes within 70 min by TNT-400-Pt at an initial concentration of 10 mg/L (B), and 20 mg/L (C), five cycles of degradation of TNT-400-Pt (D).



So far, large datasets have existed on the synthesis of photocatalyst materials and their degradation ability for particular pollutant removal (Xu et al., 2020a). Nevertheless,

information on the controlling factors of the photocatalysis process and the immobilization and recycling use of catalysts are limited. Thus, future research should focus on the follows:

- ◆ Assessing dissolved oxygen (DO) and dissolved organic matters (DOM) effect on the photocatalytic performance of the as-synthesized TNT-Pt;
- ◆ Exploring the immobilization of the synthesized catalysts when dealing with real dye wastewater;
- ◆ Utilizing the electron paramagnetic resonance (EPR) to detect the active radicals directly for the further investigation of the reaction mechanism;
- ◆ Synthesizing more functionalized yet low-cost catalyst polymers decomposing the dye water with high efficacy.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

AUTHOR CONTRIBUTIONS

XQ, ZW, XX and YY designed the study and wrote the main manuscript. XQ, MP made theoretical calculations and prepared

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the figures and tables. XQ, ZW and MP performed the experiments and data collection. MP and CH obtained funding for the research. All authors reviewed the manuscript, made amendments, and contributed with their expertise.

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SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: https://www.frontiersin.org/articles/10.3389/fchem.2022.922701/full#supplementary-material

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Fabrication of Cocatalyst NiO-Modified BiVO₄ Composites for Enhanced Photoelectrochemical Performances

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In this work, NiO modified BiVO₄ (BiVO₄/NiO) nanocomposite was synthesized using hydrothermal and calcination method. The composite of BiVO₄/NiO, further employed as a low-overpotential photoanode, was consisted of BiVO₄ nanoparticles and NiO nanosheets, in which the BiVO₄ nanoelectrode served as the matrix for the attachment of NiO nanosheets. Photoelectrochemical (PEC) tests show that BiVO₄/NiO displayed improved PEC performance compared with pure BiVO₄. The BiVO₄/NiO photoanode delivers a photocurrent density of 1.2 mA/cm² at 1.23 V vs. RHE in a Na₂SO₄ electrolyte under an AM 1.5G solar simulator, which is 0.3 mA/cm² higher than pure BiVO₄ photoanode. Meanwhile, the onset potential also generates a 350 mV cathodic shift. The enhanced performance of the BiVO₄/NiO nanocomposite is attributed to NiO unique lamellar structure capable of providing a large number of active sites. Measurements of electrochemical impedance spectra (EIS) and the incident photon-to-current efficiency (IPCE) illustrate that the enhanced PEC activities are ascribed to the improved charge carrier separation/transport and the promoted water oxidation kinetics furnished by the decoration of NiO cocatalyst.

Keywords: bismuth vanadate, nickel oxide, photoelectrochemical, cocatalyst, water oxidation

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INTRODUCTION

Due to the excessive consumption of fossil energy that results in severe environmental pollution worldwide, the development of clean and sustainable energy technologies has received increasing attention. (Iwase et al., 2011; Guo et al., 2014; Zeng et al., 2021a) Clean hydrogen production is seen as a promising strategy, capable of simutaneously addressing climate change and environmental issues related to fossil fuel combustion. (Wang L. et al., 2018; Fukuzumi et al., 2018; Kim et al., 2018) Photoelectrochemical (PEC) water splitting, capable of directly converting solar energy into chemical energy, is considered a promising technology for converting solar energy into stable chemical energy, thus becoming attractive for reducing pollution associated with energy production. (Zhang J. et al., 2016; Wang and Wang, 2018; Weng et al., 2018; Zeng et al., 2019) In the PEC system, the photoanode acts the role of reaction sites for effective oxygen evolution. (Liu et al., 2014; Roger et al., 2017) In conclusion, the development of efficient photoanode materials is of great significance for constructing a practical PEC water splitting system. Various semiconductors including TiO₂ (Crake et al., 2017; Zeng et al., 2020), ZnO (Han et al., 2015; Hong et al., 2015), α-Fe₂O₃ (Dotan et al., 2011; Huang et al., 2016), WO₃ (Huang et al., 2017; Li et al., 2018), BiVO₄ (Wang

et al., 2017a; Wang Q. et al., 2018) and BiOBr (Wang Z.-Q. et al., 2020) etc. have been developed as photocatalytic materials. Among them, scheelite-monoclinic bismuth vanadate (BiVO₄) has been widely studied for PEC water splitting owing to its relatively narrow band gap of 2.4 eV for visible-light absorption, as well as an appropriate band position for effective water oxidation and high stablility. (Malathi et al., 2018) However, the application of BiVO₄ is still restricted by its inherent defects such as low charge transport (Zhou et al., 2018), high charge recombination (Zhang Y. et al., 2016) and slow poor water oxidation kinetics (Zhai et al., 2017). The photocurrent density of the pure BiVO₄ is obviously lower than its theoretical value of 7.5 mA/cm² (Xu et al., 2014; Chen, 2015) To overcome these issues, transition metal-based catalysts used as cocatalysts are one of the effective ways to improve the PEC water splitting performance.

Transition metal-based materials, especially (Co., Ni, Fe)based materials, comparable to precious metals because of their low cost and advanced catalytic performance, are considered to be the most promising OER catalysts. (Zhang Q. et al., 2016; Kuang et al., 2016; Wang Z. et al., 2020)The combination of the OER catalyst and the semiconductor light absorber can not only improve the PEC activity by providing an interface reaction active site that reduces overpotential, but also improve the PEC stability by rapidly consuming photo-generated carriers of semiconductor materials against electrolytes (Zhou et al., 2015). (Trotochaud et al., 2014; Zeng et al., 2021b) Recently, Dai (Kenney et al., 2013; Li et al., 2017) and colleagues deposited an ultra-thin nickel film on the n-type silicon substrate as a physical protective layer. It was found that a 2 nm nickel film played a crucial role in the sustainability of n-type silicon photoanodes in the solar-driven water oxidation process. The ultra-thin nickel was used as a protective layer and a passivation layer, and the natural NiO_x formed during the test was employed as an OER promoter. The NiOx/Ni/n-Si photoanode can work under constant photocurrent of 10 mA/cm², and still have excellent stability after water oxidation of 80 h. In addition, Lewis (Zhou et al., 2019) and his colleagues introduced an ultra-thin CoOx film as an intermediate layer between NiOx layer and n-Si to enhance the interaction between co-catalysts/ semiconductors. It was found that further passivation of the CoO_x layer on the n-Si surface can change the initiation. The potential was more negative than NiO_x/SiO_x/n-Si photoanode. NiOx/ CoO_x/SiO_x/n-Si showed the most negative flat band position, which was related to the barrier height in the semiconductor, and therefore highly improved the separation and collection of charge carriers. The above results indicate that the combination of NiO and other favorable semiconductors can remarkably reduce the overpotential of the photoelectrode.

In this study, a BiVO₄ photoanode, acting the role of photoelectrocatalysis substrate, is synthesised by a electrodeposition-calcination method. On the other hand, a nanosheet structured NiO, playing the performance of the water oxidation cocatalyst to combine with the BiVO₄ photoanode and thus improve the PEC performance, is preprared via a hydrothermal-calcination. Under AM 1.5G sunlight, the BiVO₄/NiO film produced a relatively high

photocurrent density of $1.2~\text{mA/cm}^2$ at 1.23~V vs. RHE, much higher than that of the pure BiVO₄ film. More importantly, the onset potential is negatively shifted by 350 mV relative to pure BiVO₄. The special structure of NiO is believed to be beneficial to absorb more incident photons through the light-harvesting effect, thereby enhancing the separation and transport of photo-induced charge carriers. Furthermore, the deposition of NiO cocatalyst on the surface of the BiVO₄ photoanode significantly promotes the water oxidation kinetics.

EXPERIMENTAL

Chemicals

Bi(NO₃)₃·5H₂O (Sinopharm Chemical Reagent Co., Ltd., 99.0%), potassium iodide, ethylene glycol are purchased from chemical reagent co, Ltd. P-benzoquinone (Tianjin Institute of Fine Chemicals, 99.0%). Ni(NO₃)₂·6H₂O (Sinopharm Chemical Reagent Co., Ltd., 99.0%), hexamethylenetetramine (HMTA, Chengdu Cologne Chemicals Co., Ltd., 99.0%), Anhydrous ethanol was purchased from Sinopharm Chemical Reagent Co., Ltd. All aqueous solutions were prepared with deionized water.

Preparation of BiVO₄

The preparation of BiVO₄ was synthesized with reference to previous reported work. Systematically, 50 ml of 0.4 M KI solution was first adjusted to pH 1.7 with 1 M HNO3, and then 5 mmol Bi(NO₃)₃·5H₂O was added with rapid stirring until dissolved, resulting in an orange-red mixed solution. Then 20 ml of ethanol containing 4.6 mmol of 1,4benzoquinone was slowly added dropwise to the above solution and stirred for several tens of minutes. Next, BiOI nanosheets were synthesized in a three-electrode system by electrodeposition. Among them, the platinum electrode was used as the counter electrode, the clean FTO glass was used as the working electrode, and the Ag/AgCl (3.5 M KCl) electrode was used as the reference electrode. Cyclic voltammetry (CV) was used for electrodeposition, and the resulting membrane was rinsed with distilled water to obtain a clean BiOI membrane. Immediately after, 150 µl of 0.2 M vanadyl acetylacetonate (VO(acac)₂) DMSO solution was dropped onto the above BiOI nanosheets. Calcined at 450°C for 2 h at a ramp rate of 2°C/min. The cooled membrane was washed with 1 M NaOH solution to remove excess V_2O_5 from the BiVO4 electrode.

Preparation of BiVO₄/NiO Photoanode

The BiVO₄/NiO photoanode was prepared by a hydrothermal method. The configuration takes 60 ml of solution in which the volume ratio of deionized water and ethanol solution is 2:1. After ultrasonically mixed uniformly, 1.5 mmol Ni(NO₃)₂·6H₂O and 6 mmol HMTA were added thereto, and stirred until dissolved. Then 20 ml of the above mixture was added to a PTFE-lined stainless steel autoclave (100 ml). And the as-prepared BiVO₄ photoanode was placed obliquely with the conductive side facing upwards, heated at 90°C for 4 h. The photoanode was washed three times with water and ethanol and dried at 60°C for 12 h.

Finally, the BiVO₄/NiO photoanode was obtained after calcination in air with a heating rate of 2°C/min at 300°C for 2 h.

Characterizations

The microscopic morphology of the samples was characterized by scanning electron microscopy (SEM, JSM-6701E). The crystal structure of the as-prepared photoanode was measured by X-ray diffraction (XRD) tests on the X-ray diffractometer (D/MAX-2200/PC). UV-Vis diffuse reflectance spectroscopy was used to investigate the response of the prepared photoelectrode to visible light on a UV-3100 spectrometer.

PEC Characterizations

The photoelectrochemical tests of the as-prepared photoanodes were carried out on a CHI 660D electrochemical workstation. A three-electrode system was used, in which a platinum sheet, Ag/ AgCl (3.5 M KCl), and the samples were the counter electrode, the reference electrode and the working electrode, respectively. The electrolyte is $0.5 \text{ M Na}_2\text{SO}_4$ solution (pH = 6.86). All tests were performed with FTO backside irradiation at room temperature. The scan rate for linear sweep voltammetry (LSV) was 10 mV s⁻¹. The light intensity was calibrated to 100 mW/cm² with an optical power meter. And the incident photon current efficiency (IPCE) was measured using a 300 W xenon lamp with a monochromator in 0.5 M Na₂SO₄ electrolyte at 1.23 V vs. RHE. The photogenerated photocurrent (J_{abs}) undergo two major losses of charge carriers recombination in bulk and at interface. Hence the measured photocurrent during water oxidation (J_{H_2O}) is expressed as follows:

$$J_{\rm H_2O} = J_{abs} \times \eta_{\rm inj} \times \eta_{\rm sep}$$

where J_{abs} is obtained by integrating the distribution of solar power density $P(\lambda)$ with light absorption $\alpha(\lambda)$ of the photoanode as equation:

$$J_{abs} = e \int_{0}^{\lambda_{abs}} \alpha(\lambda) \frac{P(\lambda)}{h\nu} d\lambda$$

where $\alpha(\lambda) = 1 - 10^{-A}$, A is the absorbance according to the UV-vis spectrum, $P(\lambda) =$ the distribution of solar power density.

The photocurrent during sodium sulfite oxidation was measured $(J_{SO_3^{2-}})$ in order to calculate charge separation efficiencies. Since the interface charge separation efficiency of sodium sulfite oxidation is almost 100% $(\eta_{\text{sep}}, \text{SO}_3^{2-} = 1)$, the charge separation efficiencies can be calculated as follows:

$$\eta_{inj} = J_{SO_3^{2-}} / J_{abs}$$

$$\eta_{sep} = J_{H_2O} / J_{SO_3^{2-}}$$

RESULTS AND DISCUSSION

Characterization of the BiVO₄/NiO Composite Photoanode

The morphology and elemental compositions of the synthesized BiVO₄, BiVO₄/NiO composite photoanode were studied with

SEM and energy dispersive spectroscopy (EDS) in Figures 1A-H. Figure 1A exhibits the SEM image of nanoporous BiVO₄ film. Figure 1B shows the SEM image of BiVO₄/NiO. NiO nanosheets with size distribution about 5-10 nm are fairly continuous and uniformly loaded on the surface of BiVO₄ in large area. The elemental composition and content of BiVO₄/NiO anodes were further investigated by EDS. Figure 1C shows the EDS pattern of BiVO₄/NiO photoanode, the weight percentage of elements present in the BiVO₄/NiO photoanode composites are 39.4%, 31.1%, 18.6% and 10.09% for Bi, O, V and Ni, respectively. No other elements or impurities are found. The elemental composition and distribution in the BiVO₄/NiO photoanode were further observed by EDS elemental mapping (Figures 1D-H). The results clarify that the elements of Bi, O, V and Ni are present and uniformly distributed in the BiVO₄/NiO photoanode.

The optical absorption properties of pure BiVO₄ and BiVO₄/NiO films were investigated by UV-Vis diffuse reflectance spectroscopy. It can be seen that BiVO₄ and BiVO₄/NiO show good light absorption properties around 500 nm (**Figure 2A**), corresponding to a band gap of 2.4 eV. Notably, the BiVO₄/NiO sample shows almost the same absorption edge as bare BiVO₄ due to the blocking by the thicker BiVO₄ layer, indicating that coating of NiO almost rarely affects light absorption of BiVO₄/NiO. But the BiVO₄ photocathode loaded with NiO co-catalyst shows the relatively low light absorption capacity. The reason is primarily ascribed to the poor optical transparency of the nickel based co-catalyst. (Zhou et al., 2020)

The XRD pattern characterization reveals that the product is composed of three kinds of materials with distinct crystal structures. **Figure 2B** displays the XRD patterns of BiVO₄ and BiVO₄/NiO nanocomposites. The XRD diffraction peaks of BiVO₄ and BiVO₄/NiO nanocomposites are completely consistent with monoclinic BiVO₄ (JCPDS No. 14-0688) and tetragonal SnO₂ (JCPDS No. 46-1088) derived from FTO substrates. No other impurity phases were detected. The appearance of characteristic diffraction peaks at $2\theta = 43.3^{\circ}$ is corresponding to the (200) crystal plane of the cubic phase NiO, which can be concluded that the composite sample has been successfully prepared.

Performance of the BiVO₄/NiO Composite Photoanode

In order to explore the effect of supported NiO on the PEC performance, the photoelectrochemical water splitting performance of BiVO₄ photoanode modified by NiO cocatalyst was studied by electrochemical workstation. Linear sweep voltammetry (LSV) curves reflect the water oxidation properties of BiVO₄/NiO and pure BiVO₄. As shown in **Figure 3A**, the photocurrent density of unmodified BiVO₄ at 1.23 V vs. RHE is 0.9 mA/cm² and the onset potential is about 0.58 V vs. RHE, which is due to its unique structure and specific crystal orientation, leading to rapid transfer and separation of photogenerated carriers. After loading the NiO cocatalyst on BiVO₄, the photoelectrode showed significant enhancement at all potentials, obtaining a photocurrent of 1.2 mA/cm² at 1.23 V

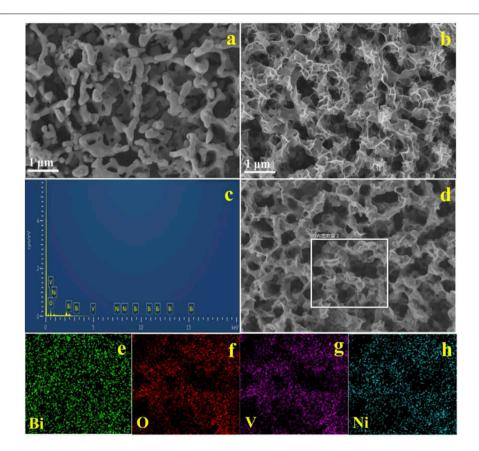
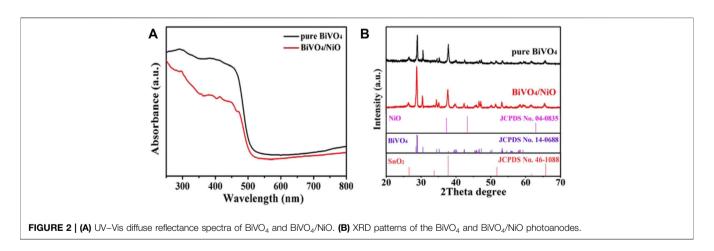


FIGURE 1 | SEM images of the typical samples: (A) BiVO₄/NiO, EDS pattern (C) and the EDS elemental mapping (D-H) of as prepared BiVO₄/NiO photoanode.



vs. RHE, which was higher than that of pristine $BiVO_4$. In particular, $BiVO_4/NiO$ obtained a more negative onset potential compared to pure $BiVO_4$, with a negative shift of about 0.35 V (**Figure 3B**). The increased photocurrent density and negatively shifted onset potential clearly indicate that the addition of NiO cocatalyst is a feasible way to enhance the water oxidation capacity of $BiVO_4$ photoanode. **Figure 3C** shows the chopped photocurrent density–voltage (J–V) curves of $BiVO_4/$

NiO and pure BiVO₄. All the photoanodes show an obvious "photo-switching" effect with fast response. Clearly, the BiVO₄/NiO photoanode exhibits a much better PEC performance than BiVO₄ film.

The electron-hole pair recombination and charge generation kinetics of photoanode in PEC water oxidation process can be analyzed by EIS. The photoanode was measured at $1.23~\rm V$ vs. RHE at AM $1.5\rm G$ ($100~\rm mW/cm^2$), and the frequency range of the

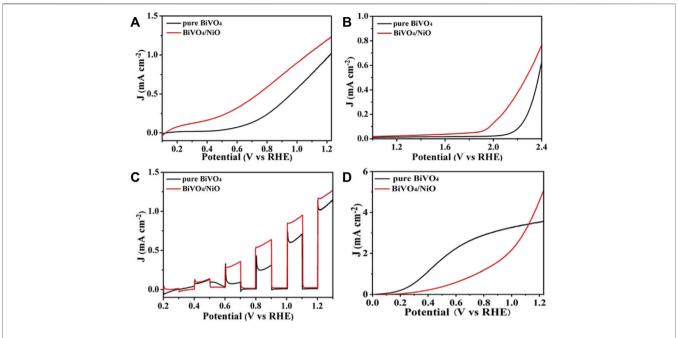


FIGURE 3 | (A) Photocurrent density-voltage curve of BiVO₄ and BiVO₄/NiO photoanodes. (B) Photocurrent density-voltage curve of BiVO₄ and BiVO₄/NiO photoanodes in the absence of light. (C) Chopped linear sweep photocurrent-potential curve of BiVO₄ and BiVO₄/NiO. (D) Sulfite oxidation current curves.

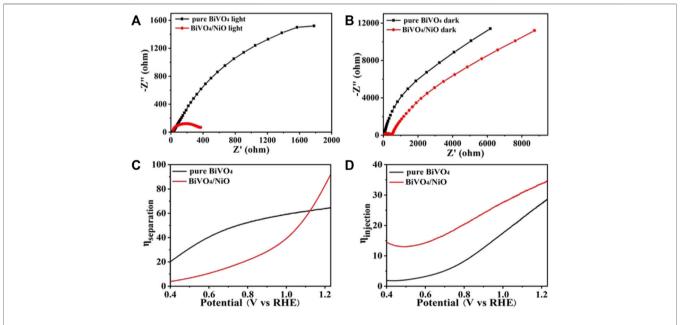


FIGURE 4 | (A) EIS curves of pure $BiVO_4$ and $BiVO_4/NiO$ under the light, (B) and in the dark. The EIS was measured at 1.23 V vs. RHE under an AM 1.5G solar simulator. (C) Charge separation efficiency versus potential curves and (D) charge injection efficiency versus potential curves of $BiVO_4/NiO$.

Nyquist plot was from 100 kHz to 0.1 Hz. The results of impedance spectra are useful for analyzing electrochemical surface reactions. The charge transfer resistance of the photoanode surface is estimated from the small semicircle in the Nyquist diagram, and the smaller the radius, the more effective the separation of charges. In addition, the EIS test

result of dark reaction condition (**Figure 4B**) is consistent with that under light conditions in **Figure 4A**. The $BiVO_4/NiO$ photoanode exhibits the highest charge transportation, suggesting good charge separation ability.

To further explore the charge recombination at the BiVO₄ and BiVO₄/NiO photoanode interfaces, the charge separation and

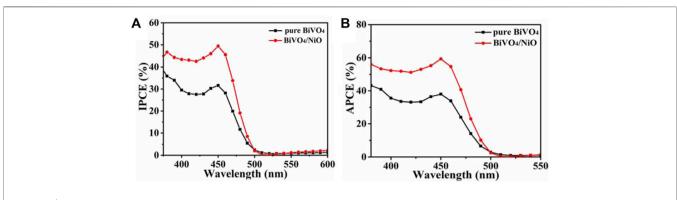
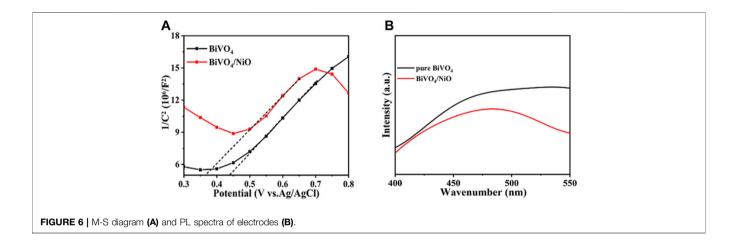
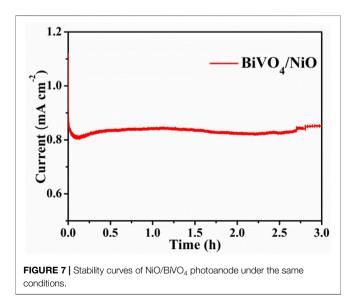


FIGURE 5 | (A) IPCE of BiVO₄, BiVO₄/NiO measured at 1.23 V vs. RHE in the incident wavelength range from 380 to 600 nm. (B) APCE spectra for BiVO₄, BiVO₄/NiO photocathodes along with the AM 1.5 irradiance spectrum.





injection efficiencies were tested in **Figures 4B,C**. Charge separation efficiency is an important parameter to evaluate the proportion of carriers reaching the electrode surface/electrolyte interface to participate in water oxidation (Wang et al., 2017b).

Therefore, the constant charge separation efficiency is shown in **Figure 3D**, ascribed to the photocurrent density of the BiVO₄/NiO photoanode at an applied potential of 0.6 V vs. RHE when Na₂SO₃ was added to the electrolyte. The separation efficiency of the pure BiVO₄ photoanode increases with the applied potential, especially it can reach about 60% at 1.23 V vs. RHE. However, the BiVO₄/NiO nanostructured array photoanode exhibits a charge separation efficiency of 90% at 1.23 V vs. RHE. From this point of view, the cocatalyst NiO supported on BiVO₄ can significantly improve the charge separation efficiency and facilitate the flow of charge carriers to the electrode surface/electrolyte interface to participate in water oxidation.

The photogenerated holes generated on the surface of the photoanode participate in the water oxidation reaction or recombine with electrons. The charge injection efficiency, defined as the fraction of those holes at the photoanode and electrolyte interface that is used for water oxidation reactions, can be improved by reducing surface recombination or accelerating hole transfer kinetics. (Zhou et al., 2020) As shown in **Figure 4D**, the charge injection efficiency of the pure BiVO₄ photoanode reaches 28% 1.23 V vs. RHE. While the charge injection efficiency of the BiVO₄/NiO photoanode increases to 35% in the potential range of 1.23 V vs. RHE.

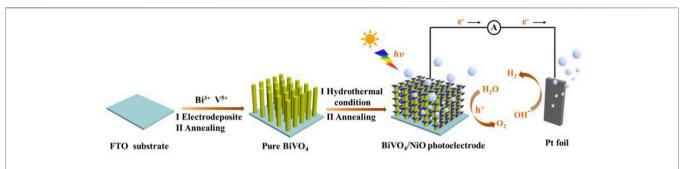


FIGURE 8 | Schematic illustration of the fabrication process of BiVO₄/NiO and the light harvesting and carrier separation mechanism in the BiVO₄/NiO composite photoanode system

The quantum efficiencies of BiVO₄, BiVO₄/NiO photoanodes were determined by measuring incident photon current efficiency (IPCE) and absorbed photon current efficiency (APCE). (Wang et al., 2017b) The calculation of IPCE can refer to the following equation:

IPCE =
$$(J \times 1240)/(P \times \lambda)$$

where J is the current density (mA/cm²) measured at each specific wavelength, λ is the wavelength of the incident light (nm), and P is the power density of the incident light (mW/cm²). As shown in Figure 5A, BiVO₄/NiO nanocomposites exhibit slightly higher IPCE values in the 450–500 nm range compared to bare BiVO₄. The PEC performance mainly depends on the light-harvesting efficiency, charge separation efficiency, and collection yield. Since the light-harvesting efficiency is almost unchanged after the modification of the NiO cocatalyst, the enhancement of IPCE may be due to the fast separation of charge carriers and the accelerated water oxidation kinetics of the reaction, resulting in the enhanced photocurrent. The IPCE results are consistent with the above J-V measurements.

To obtain the absorbed photon-current efficiency, the APCE value of the photoanode was measured at 0.6 V vs. RHE, as shown in **Figure 5B**. The APCE value of BiVO₄/NiO photoanode is significantly higher than that of BiVO₄ from 380 to 500 nm, which is consistent with the overall PEC performance.

Figure 6A shows the Mott Schottky barrier of BiVO₄ and BiVO₄/NiO. The capacitance-voltage curve is usually used to analyze the reasons for the enhancement of semiconductor performance. In order to better study the reasons for the increase of photocurrent after supporting the cocatalyst. Therefore, the capacitance-voltage curves of BiVO4 and BiVO4/NiO electrodes were measured under dark reaction conditions, and the x-axis tangent was made on the curves of BiVO4 and BiVO4/NiO. The tangent was positive, indicating that BiVO₄ and BiVO₄/NiO are both n-type semiconductors. The smaller slope of the composite electrode, the greater the carrier density. Thus, the BiVO₄/NiO electrode has the largest carrier density. The increased carrier density causes the conductivity of BiVO4 to increase and ultimately increases its photocurrent density. Fluorescence spectroscopy (PL) can be used to effectively analyze the separation and recombination effects of photogenerated carriers. As shown in Figure 6B, it can be observed that the peak intensity of the BiVO₄/NiO electrode is weaker than that of the pure BiVO₄ electrode, which indicates that after NiO is loaded on the ${\rm BiVO_4}$ surface, the recombination rate of photo-generated electrons and holes becomes slower and the charge separation efficiency is improved.

Stability test is an important index parameter to evaluate the effect of photoelectric catalyst and whether it has application value. The stability test of the ${\rm BiVO_4/NiO}$ photoanode was analyzed under continuous irradiation under AM 1.5G. As shown in **Figure 7**, it can be observed that under the continuous irradiation of 3 h, the photocurrent density of the ${\rm NiO/BiVO_4}$ electrode is not significantly attenuated, indicating that the stability of the ${\rm BiVO_4}$ photoanode can be improved after loading NiO.

DISCUSSION ON MECHANISM

Based on above results, the possible mechanisms for the enhancement in photoelectrocatalytic activity of BiVO₄/NiO composite photoanode and the specific photogenerated charge carriers transfer are shown in **Figure 8**. In BiVO₄ with monoclinic scheelite structure, the Bi 6s and O 2p orbits hybridize to form the valence band. When the BiVO₄/NiO composite is irradiated with visible light, electron-hole pairs are generated in BiVO₄, in which electrons in the valence band are excited to the conduction band and holes stay in the conduction band. With the NiO coated on the surface of BiVO₄, NiO as a cocatalyst regulates the built-in electric field of BiVO₄ photocatalyst, accelerates the charge separation rate of BiVO₄, and thus the PEC performance of BiVO₄ is improved.

CONCLUSION

In conclusion, we successfully fabricated an efficient nanostructured BiVO $_4$ /NiO photoanode by a two-step method of hydrothermal calcination synthesis. The PEC performance of the NiO-modified BiVO $_4$ photoanode was improved in 0.5 M Na $_2$ SO $_4$ (pH = 6.86) electrolyte, reaching 1.2 mA/cm 2 at 1.23 V vs. RHE, higher than that of the pure BiVO $_4$ sample. In particular, the onset potential of the composite photoanode has a significant negative shift. The excellent PEC performance could be attributed to NiO abundant nano flake structure, the improved charge separation/transport efficiency and accelerated water oxidation kinetics thanks to the deposited NiO

cocatalyst. Our work shed a light for design and fabrication of nanostructured photoelectrode with efficient PEC performances.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

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AUTHOR CONTRIBUTIONS

Z-QW: Writing—review and editing. HJW: Methodology.

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Electrocatalytic Reduction of Nitrate via Co₃O₄/Ti Cathode Prepared by Electrodeposition Paired With IrO₂-RuO₂ Anode

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Nitrate pollution is already a global problem, and the electrocatalytic reduction of nitrate is a promising technology for the remediation of wastewater and polluted water bodies. In this work, Co₃O₄/Ti electrodes were prepared by electrodeposition for the electrocatalytic reduction of nitrate. The morphology, chemical, and crystal structures of Co₃O₄/Ti and its catalytic activity were investigated. Then, the electrocatalytic nitrate reduction performance of Co₃O₄/Ti as the cathode was evaluated by monitoring the removal efficiencies of nitrate (NO₃⁻-N) and total nitrogen (TN), generation of reduction products, current efficiency (CE), and energy consumption (EC) at different operating conditions. Under the catalysis of Co_3O_4/Ti , NO_3^- was reduced to N_2 and NH_4^+ , while no NO_2^- was produced. After the introduction of chloride ions and IrO₂-RuO₂/Ti as the anode, NH₄⁺ was selectively oxidized to N₂. The removal efficiencies of NO₃⁻-N (at 100 mg/L) and TN after 2 h were 91.12% and 60.25%, respectively (pH 7.0; Cl⁻ concentration, 2000 mg/L; current density, 15 mA/cm²). After 4 h of operation, NO₃⁻-N and TN were completely removed. However, considering the EC and CE, a 2-h reaction was the most appropriate. The EC and CE were 0.10 kWh/g NO₃⁻N and 40.3%, respectively, and electrocatalytic performance was maintained after 10 consecutive reduction cycles (2 h each). The cathode Co₃O₄/Ti, which is prepared by electrodeposition, can effectively remove NO₃-N, with low EC and high CE.

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1 INTRODUCTION

Nitrate (NO_3^-) contamination of surface water and groundwater is a global environmental problem associated with increasing populations, and its hazards have attracted much attention (Jasper et al., 2014; Khalil et al., 2016; Serio et al., 2018). The accumulation of plant nutrients such as NO_3^- and phosphate in water can accelerate eutrophication, a process that increases the biomass of a water body as its biological diversity decreases, for example, due to increases in invertebrates and fish. In the extreme, a state of hypoxia can exist, resulting in the loss of the aquatic ecosystems (Kubicz et al., 2018; Zhang et al., 2021). Although NO_3^- is chemically stable, it can be microbially reduced to reactive nitrite in the oral cavity and stomach, which has been linked to liver damage, methemoglobinemia, and cancer in animals (Spalding and Exner, 1993; Elmidaoui et al., 2001; Barakat et al., 2020).

Currently, microbial denitrification is widely used for the large-scale remediation of NO₃⁻ pollution (Clauwaert et al., 2007; Della Rocca and Belgiorno V Meriç, 2007). Many other methods of NO₃⁻ removal have been explored such as reverse osmosis, ion exchange, ammonia stripping, electrodialysis, catalytic reduction, and electrocatalytic reduction (Kapoor and Viraraghavan, 1997; Yang and Lee, 2005; Della Rocca and Belgiorno V Meriç, 2007). Among these techniques, the electrocatalytic reduction of NO₃⁻ is a promising and clean technology because the electron reductants neither introduce pollutants nor adversely affect the environment (Garcia-Segura et al., 2018; Gayen et al., 2018).

The mechanism of the electrochemical NO_3^- reduction reaction (NO_3^- -RR) involves anodic oxidation and cathodic reduction in which NO_3^- is reduced to NO_2^- , NH_4^+ , and N_2 on the active sites of the cathode according to **Eqs 1–3** (Zhang et al., 2021):

$$NO_3^- + 2e^- + H_2O \rightarrow NO_2^- + 2OH^-,$$
 (1)

$$NO_2^- + 6e^- + 6H_2O \rightarrow NH_4^+ + 8OH^-,$$
 (2)

$$2NO_3^- + 10e^- + 6H_2O \rightarrow N_2 + 12OH^-.$$
 (3)

The choice of the cathode material is important in this process. To date, most studies have used high-cost noble metal cathodes, such as Pt, Rh, and Pd, which may limit their commercial application (Taguchi and Feliu, 2007; Yang et al., 2014; Soto-Hernández et al., 2019). Co₃O₄ is a cost-effective catalyst, and the preparation of a CuO-Co₃O₄/Ti electrode by the sol-gel method for electrochemical reduction of NO₃⁻ was recently reported (Yang et al., 2020). The system demonstrated the complete removal of NO₃⁻ after 3 h at a current density of 20 mA/cm².

 NO_2^- and NH_4^+ generated at the cathode (**Eqs. (1)** and **(2)**) diffuse to the anode where they are adsorbed onto the surface and subsequently oxidized to NO_3^- and N_2 (**Eqs. (4)** and **(5)**) (Zhang et al., 2021):

$$NO_2^- + H_2O \rightarrow NO_3^- + 2e^- + 2H^+,$$
 (4)

$$2NH_4^+ \rightarrow N_2 + 6e^- + 6H^+.$$
 (5)

When Cl^- is present in the electrolyte, the following reactions also occur at the anode (**Eqs. 6–9**) (Zhang et al., 2021):

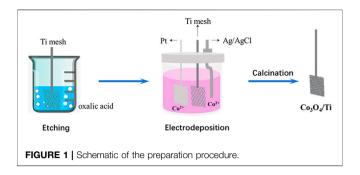
$$2Cl^{-} \rightarrow Cl_2 + 2e^{-}, \tag{6}$$

$$Cl_2 + H_2O \rightarrow HOCl + Cl^- + H^+,$$
 (7)

$$HOCl \rightarrow ClO^- + H^+,$$
 (8)

$$2NH_4^+ + 3ClO^- \rightarrow N_2 + 3H_2O + 2H^+ + 3Cl^-.$$
 (9)

The electrochemical NO₃⁻-RR involves NO₃⁻ reduction at the cathode and ammonium nitrogen (NH₄⁺-N) oxidation at the anode. Cl₂ generated at the anode (**Eq. (6)**) immediately forms hypochlorite (**Eq. (7)**), which selectively oxidizes NH₄⁺ to N₂ (Su et al., 2017). Hence, the efficient anodic oxidation of chloride ions is a key requirement for this process, and the anode materials used in the chlor-alkali industry, which obtain Cl₂ by electrolysis of sodium chloride, provide a useful reference (Yi et al., 2007). Among these materials, IrO₂-RuO₂ is a good choice due to its low overpotential, high chlorine selectivity, and long-term stability (Chen et al., 2007). In addition, the electrocatalytic reduction of



NO₃⁻-N is also affected by reaction potential, current, solution pH, battery structure, and anode material.

Here, a catalytic cathode was prepared by the *in situ* electrodeposition of $\text{Co}_3\text{O}_4/\text{Ti}$) to obtain improved electrocatalytic performance. $\text{IrO}_2\text{-RuO}_2/\text{Ti}$ was employed as the anode for the effective removal of $\text{NH}_4^+\text{-N}$ and TN. The aim of this study was to obtain simultaneous electrochemical NO_3^- reduction and oxidation of the *in situ*-generated NO_2^- and NH_4^+ into N_2 gas. The morphology and structure of $\text{Co}_3\text{O}_4/\text{Ti}$ were characterized using conventional methods, and its performance in NO_3^- removal was evaluated under different operating conditions. The current efficiency (CE) and energy consumption (EC) of the system were also measured to assess its commercial application.

2 EXPERIMENTAL SECTION

2.1 Chemicals and Materials

The Ti mesh and Ti plate (99.5% purity, 0.6 mm, 10 mesh) were purchased from Lanruiyinde Electrochemical Materials Co., Ltd. (China). The Pt plate was obtained from Aidahengsheng Co., Ltd., (Tianjin, China). All chemicals were of analytical grade. Potassium nitrate and sodium hydroxide were purchased from Aladdin Biochemical Technology Co., Ltd. (Shanghai, China). Cobalt nitrate hexahydrate, sodium eicosyl, hexachloroiridic acid, and ruthenium (III) chloride were obtained from Macklin Biochemical Technology Co., Ltd. (Shanghai, China). Solutions were prepared using deionized water (>15 $\mathrm{M}\Omega$ cm) obtained from an Elix $^{\circ}$ 3 purification system (Millipore, United States). Simulated wastewater was prepared by adding potassium nitrate to deionized water.

2.2 Preparation of Co₃O₄/Ti Cathode and IrO₂-RuO₂/Ti Anode

Samples of the Ti mesh and Ti plate $(3 \times 4 \text{ cm}, 12 \text{ cm}^2)$ were degreased with NaOH solution (40 wt%) at 95°C for 2 h before etching by boiling in oxalic acid solution (10 wt%) for 2 h. The treated samples were then rinsed with deionized water and stored in ethanol until further use.

As shown in **Figure 1**, the $\text{Co}_3\text{O}_4/\text{Ti}$ electrode was prepared using an electrodeposition method. A three-electrode system was employed in a single compartment cell using the pretreated Ti mesh as the cathode, the Pt plate as the anode, and an Ag/AgCl

reference electrode. The electrodeposition solution comprised boric acid (0.5 M), cobalt nitrate hexahydrate (0.1 M), and sodium eicosyl sulfonate (2.0 g/L). Following electrodeposition at a current of 0.25 A for 5 min, the electrode was cleaned with deionized water and oven-dried (60°C) before heating at 5°C/min to 500°C (hold 2 h) in a muffle furnace to effect calcination. The treated samples were allowed to cool naturally to room temperature.

The IrO₂-RuO₂/Ti anode was prepared by using a thermal decomposition method. A mixed solution of hexachloroiridic acid and ruthenium (III) chloride in n-butanol (molar ratio, 2:1) was evenly coated onto the surfaces of the pretreated titanium plate, dried at 105°C for 10 min, and then calcined at 500°C for 15 min. The process was repeated until the weight of the titanium plate increased by about 10 g/cm². Finally, the electrode was washed with deionized water before use.

2.3 Characterization of the Co₃O₄/Ti Cathode

Surface morphology and elemental composition were studied by field-emission scanning electron microscopy (SEM) and energy-dispersive X-ray spectroscopy (EDS) on a Phenom ProX system (Thermo Fisher Scientific, United States) at an accelerating voltage of 15 kV. The crystal structure of Co_3O_4 was examined by X-ray diffraction (XRD) with an X'pert Powder system (Malvern Panalytical, Malvern, UK) using Cu K α (λ = 1.5406 Å) irradiation.

2.4 Electrochemical Measurements

 NO_3^- -RR tests were performed in a single chamber electrolytic cell (200 ml) using a three-electrode system, with Co_3O_4/Ti (or Ti as required), Pt plate, and Ag/AgCl as the working, counter, and reference electrodes, respectively. The electrolyte was prepared using Na_2SO_4 (0.1 M) and different concentrations of NO_3^- -N (KNO₃) as required. Linear sweep voltammetry (LSV), and electrolysis tests were performed in an electrochemical workstation (Metrohm Autolab M204, Switzerland). Prior to the electrochemical test, oxygen was removed by bubbling high-purity N_2 through the electrolyte for \geq 20 min, and continuously fed during the experiments.

Electrolysis measurements were performed at an optimum current density of 15 mA/cm^2 , and aliquots of the reaction solutions (2 ml) were removed at predetermined time intervals to measure the concentrations of NO_3^- -N, NO_2^- -N, and NH_4^+ -N. The effects of chlorine on NO_3^- -RR and the stability of the Co_3O_4/Ti cathode electrode were assessed at a current density of 15 mA/cm^2 for 2 h and an initial NO_3^- -N concentration of 100 mg/L.

2.5 Analytical Methods

During the NO_3^- -RR, the formation of NO, N_2O , and NH_3 are negligible, and hence, the generated gaseous products can be considered as N_2 (Teng et al., 2018). UV-Vis spectroscopy was used to measure the concentrations of NO_3^- -N, NO_2^- -N, NH_4^+ -N, and total nitrogen (TN) (Evolution 201, Thermofisher Scientific Co., Ltd.), and

their removal efficiencies were calculated according to Eqs (10)-(12):

$$NO_{3}^{-} - N \ removal = \frac{C_{0} \left(NO_{3}^{-} - N\right) - C_{t} \left(NO_{3}^{-} - N\right)}{C_{0} \left(NO_{3}^{-} - N\right)} \times 100\%,$$
(10)

$$NH_4^+ - N \ generation = \frac{C_t \left(NH_4^+ - N \right)}{C_0 \left(NO_3^- - N \right)} \times 100\%,$$
 (11)

$$TN \ removal = \frac{C_0 (TN) - C_t (TN)}{C_0 (TN)} \times 100\%,$$
 (12)

where $C_0(NO_3^--N)$ (mg/L) is the initial concentration of NO_3^--N , $C_t(NO_3^--N)$ (mg/L) is the concentration of NO_3^--N at time t, $C_t(NH_4^+-N)$ (mg/L) is the concentration of NH_4^+-N at time t, $C_0(TN)$ (mg/L) is the initial concentration of TN, and $C_t(TN)$ (mg/L) is the concentration of TN at time t.

EC was calculated using Eq. 13 (Zhang et al., 2016):

$$EC = \frac{UIt}{V(C_0 - C_t)},$$
(13)

where *U* is the cell potential (V), I is the current (A), t is the reaction time (h), and V is the volume of reaction solution (L). The CE for TN removal rates was obtained using **Eq. 14**:

CE(%) =
$$\frac{(C_0 - C_t) \times V}{M \times Q} \times n \times 96485 \times 100\%,$$
 (14)

where M is the molar mass of N (14 g/mol), Q is the amount of electricity passing through the electrode, and n is the number of electrons obtained from the complete reduction of NO_3^- -N (calculated according to the conversion of NO_3^- to N, n = 5).

3 RESULTS AND DISCUSSION

3.1 Electrode Characterizations and Chemical Tests

SEM was used to depict the electrode surface morphology of $\text{Co}_3\text{O}_4/\text{Ti}$. **Figure 2** shows that spherical particles (3–5 µm) of Co_3O_4 were observed on the surface of $\text{Co}_3\text{O}_4/\text{Ti}$ at different magnifications, confirming its deposition on the Ti mesh. SEM-EDS elemental mapping of a surface region of the $\text{Co}_3\text{O}_4/\text{Ti}$ cathode (**Figure 3**) gave a value of 26.26 atom% for Co, indicating that the element was successfully deposited on the titanium mesh.

Figure 4 shows the XRD patterns of the calcined Co_3O_4/Ti electrode and their comparison with the reference powder patterns of cubic phase Co_3O_4 (PDF#42–1467) and Ti (PDF#44–1294). The characteristic peaks observed at 2θ of 35.1° , 38.4° , 40.2° , 53.0° , 62.9° , 70.7° , 76.2° , and 77.4° correspond to (100), (002), (101), (102), (110), (103), (112), and (201) planes of Ti (PDF#44–1294), respectively (**Figure 4A**). Inspection of the enlarged pattern obtained from the Co_3O_4/Ti cathode (**Figure 4B**) showed that the main peaks of Co_3O_4 at 2θ =31.3°, 36.9° , 44.8° , 59.4° , 65.2° , and 74.1° , correspond to the (220), (311), (400), (511), (440), and (620) planes of Co_3O_4 , respectively. These results were in good agreement with the standard cubic phase (PDF#42–1467).

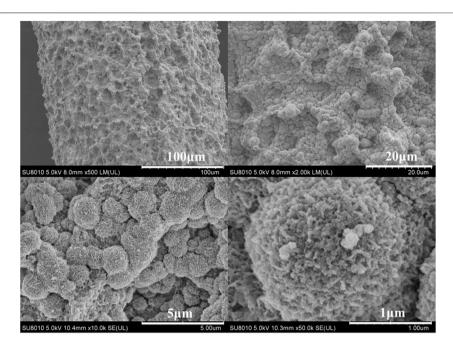
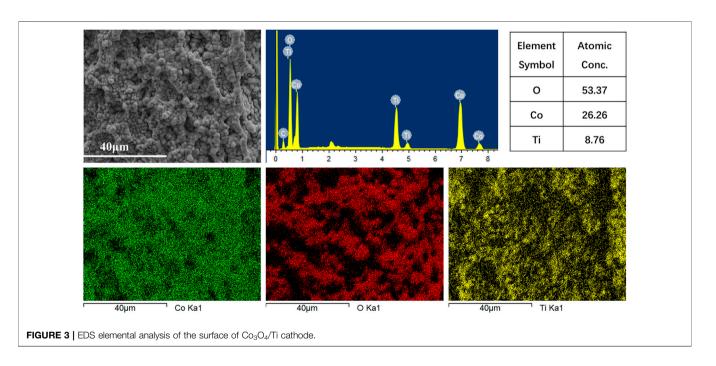
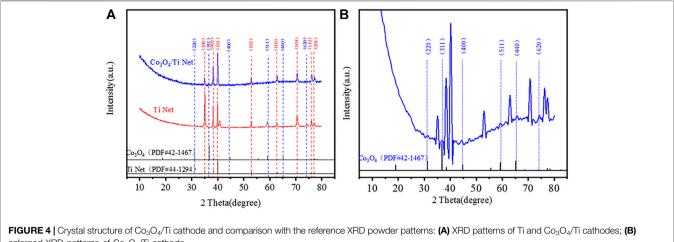


FIGURE 2 | SEM image of Co₃O₄/Ti at different resolutions.



LSV was used to evaluate the electrocatalytic performance of the catalysts toward NO_3^- -RR. **Figure 5A** shows the LSV curves obtained with Co_3O_4/Ti and Ti in the presence of NO_3^- -N. The onset potential for NO_3^- -RR using the Co_3O_4/Ti cathode (-0.7 V) was more positive than that using the Ti mesh (-1.0 V), indicating the improved performance with the composite catalyst. From -0.7 to -1.6 V, Co_3O_4/Ti gave a larger current response at all potentials due

to its higher activity toward the NO_3^- -RR compared with the Ti mesh. **Figure 5B** shows the effects of increasing NO_3^- -N (0–500 mg/L) using Co_3O_4/Ti as the cathode. In the absence of NO_3^- -N, the onset potential (i.e., for the electrolysis of water to produce H_2) was -0.9 V. The addition of NO_3^- produced a positive shift in the onset potential, and the corresponding current increased with increasing initial NO_3^- -N due to the enhanced reduction reaction activity.



enlarged XRD patterns of Co₃O₄/Ti cathode.

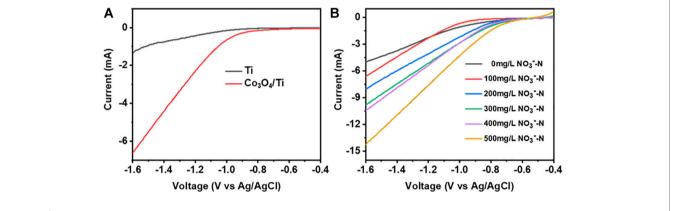


FIGURE 5 | LSV curves illustrating the NO₃-N removal performance of the catalysts (0.1 M Na₂SO₄, 10 mV/s). (A) Effects of different catalysts at constant initial NO₃-N concentration (100 mg/L). (B) Effects of increasing initial NO₃-N concentrations using the Co₃O₄/Ti cathode.

3.2 Effects of Electrochemical Reaction Parameters on NO₃⁻-RR Using the Co₃O₄/Ti Cathode

3.2.1 Catalytic Activity of the Co₃O₄/Ti Cathode

To determine the effect of Co₃O₄ on NO₃⁻RR activity, the NO₃⁻-N (100 mg/L) removal efficiencies of the Co₃O₄/Ti and Ti mesh cathodes were compared at a current density of 15 mA/cm² with a Pt plate as the anode (Figure 6). The results showed that the Co₃O₄/Ti cathode could achieve a NO₃⁻-N removal efficiency of ~98% in 2 h, compared with 6.4% using the Ti mesh, demonstrating the important role of Co₃O₄ in improving the performance of NO₃⁻-RR.

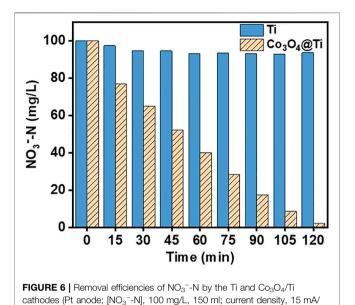
3.2.2 Effects of Current Density

Figure 7A,B show the rate of NO₃-N removal using the Co₃O₄/Ti cathode and the corresponding fit of the experimental data to first-order kinetics. The increased removal efficiency with increasing current density over 5-15 mA/cm² could be attributed to enhanced electron transfer on the electrode surface of Co₃O₄/Ti, which

increased the rate of NO₃-RR. However, when the current density was increased from 15 to 20 mA/cm², the removal efficiency of NO₃-N did not improve significantly. At higher current densities, the competing hydrogen evolution reaction consumes the extra charge, and the NO₃-N removal efficiency decreases. Figure 7C shows that there was good correspondence between the reduction of NO₃⁻-N and the generation of NH₄⁺-N. The reduction products were NH₄⁺-N and N₂, while NO₂⁻-N was not detected (Figure 7D).

3.2.3 Effect of Initial NO₃⁻-N Concentration

The effects of initial NO₃⁻N concentration on its removal efficiency using the Co₃O₄/Ti cathode and the generation of reduction products are shown in Figure 8. At initial NO₃-N concentrations of <100 mg/L, the removal efficiency of the system was close to 100% at 2 h; and the corresponding reduction products were NH₄⁺-N (60%) and N₂. At an initial NO₃-N concentration of 200 mg/L, the removal efficiency decreased to ~58%, while the NH₄⁺-N generation efficiency increased to ~79%. Under this condition, the higher



initial NO₃⁻-N concentration suppressed the competing hydrogen evolution reaction, thus reducing its charge consumption at the electrode.

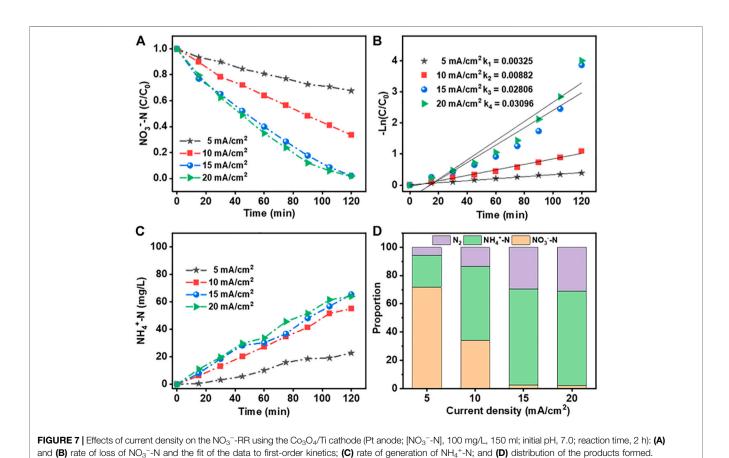
cm²; pH, 7.0; reaction time, 2 h).

3.3 Effects of CI

The main product of electrocatalytic NO₃⁻ reduction is NH₄⁺, which is also a contaminant requiring removal. However, in the presence of Cl⁻, which is widely present in drinking water and industrial water, the active species participating in the oxidative transformation of NH₄⁺-N to N₂ at the anode (Eqs 6-9) will increase TN removal. The IrO2-RuO2/Ti electrode is widely employed in the chlor-alkali industry because of its high chlorine evolution performance. To investigate the effects of Cl on NH₄+-N generation and NO₃--N removal, various concentrations of Cl were presented to a Co₃O₄/Ti/IrO₂-RuO₂/Ti NO₃-N removal system (**Table 1**). As the concentration of Cl increased from 0 to 2000 mg/L, the removal efficiencies of NO₃-N were all >90%. At 4,000 mg/L Cl⁻, the removal efficiency decreased to 83.99% due to the oxidation of NH₄⁺ to NO₃⁻ by HClO/ClO⁻. The increase in Cl⁻ concentration increased the amount of HClO/ClO⁻ generated by anodic oxidation to reduce NH₄⁺-N to N₂. Hence, NH₄⁺-N generation decreased and TN removal efficiency increased with increasing Cl⁻ concentration. The TN removal efficiency reached 78.1% with negligible NH₄⁺-N generation (0.34%) and without NO₂⁻-N accumulation.

3.4 Long-Term Stability

In addition to the initial activity, the long-term performance of a catalyst is an essential requirement for its commercial application.



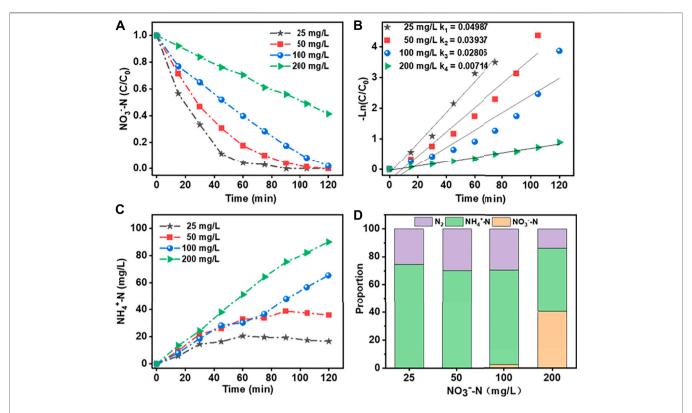


FIGURE 8 | Effects of different initial NO $_3^-$ -N concentrations on NO $_3^-$ -RR using the Co $_3$ O $_4$ /Ti cathode (Pt anode; reaction solution, 150 ml; current density, 15 mA/ cm 2 ; initial pH, 7.0; reaction time, 2 h): **(A)** and **(B)** Rate of loss of NO $_3^-$ -N and the fit of the data to first-order kinetics; **(C)** generation of NH $_4^+$ -N; and **(D)** product distributions.

 $\textbf{TABLE 1} \ | \ \text{Effects of Cl}^- \ \text{on the Co}_3 \text{O}_4 \text{/Ti/IrO}_2 \text{-RuO}_2 \text{/Ti NO}_3 \text{-N removal system}.$

Cl ⁻ Concentration (mg/L)	NO ₃ ⁻ -N removal (%)	NO ₂ ⁻ -N generation (%)	NH ₄ ⁺ -N generation (%)	TN removal (%)
0	92.2	_	54.5	24.8
1000	90.7	_	37.2	38.3
2000	91.1	_	19.9	60.3
4,000	84.0	_	0.340	78.1

Figure 9 shows the changes in NO_3^- -N removal and distribution of generated products over 4 h, and 10 consecutive cycles of 2 h each, using the system. At an initial concentration of 100 mg/L, almost all NO_3^- -N is converted into N_2 after 4 h (**Figure 9A**). After 10 cycles (**Figure 9B**), the removal efficiencies of NO_3^- -N (~90%) and TN remained unchanged.

3.5 EC and CE

EC and CE are key evaluation factors for the commercial electrochemical treatment process (Zeng et al., 2020). The EC and CE under different process conditions using the system were calculated. It can be seen from **Figure 10A,B** that within 1 h after the start of the reaction, EC is lower and CE is higher than those of the follow-up experiments, but the $\mathrm{NO_3}^-$ -N removal rate is only 58.52%. After 2 h, the $\mathrm{NO_3}^-$ -N removal efficiency reaches 93.39% with an EC of 0.10 kW h/g $\mathrm{NO_3}^-$ -N and a CE of 40.3%. There was

no significant improvement in the follow-up, but the EC continued to rise, and the CE continued to decline.

The effect of the initial NO_3^- -N concentration is demonstrated in **Figures 10C,D**. As the NO_3^- -N concentration increased, the EC decreased and CE increased. This can be explained by the increase in the contact area between NO_3^- -N and the electrode surface with increasing concentrations, which promotes the reduction reaction. From an economic viewpoint, the results indicate that the $Co_3O_4/Ti/IrO_2$ -RuO $_2/Ti$ electrocatalytic process is more suitable for wastewater with high concentrations of NO_3^- . The small amount of NO_3^- remaining in the electrochemically treated wastewater can be removed by other processes, such as the electrocatalytic removal of NO_3^- -N, which can be combined with constructed wetlands for wastewater control/remediation.

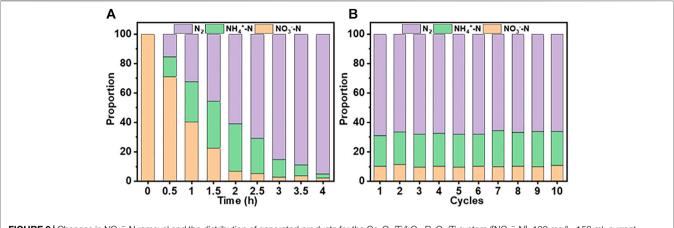


FIGURE 9 | Changes in NO₃⁻-N removal and the distribution of generated products for the Co₃O₄/Ti/lrO₂-RuO₂/Ti system ([NO₃⁻-N], 100 mg/L, 150 ml; current density, 15 mA/cm²; pH, 7.0; cycle time, 2 h). (A) Changes over 4 h. (B) Changes over 10 cycles.

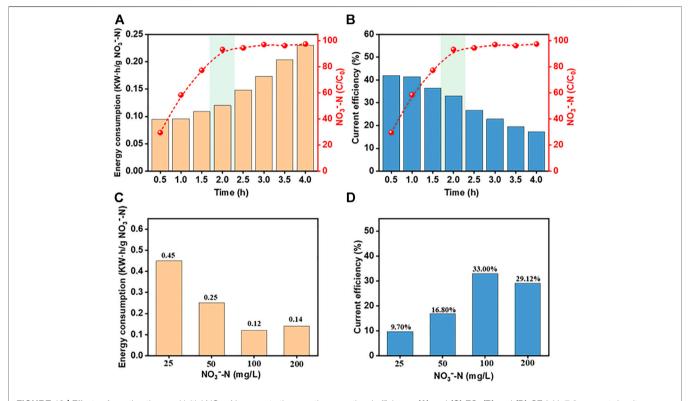


FIGURE 10 | Effects of reaction time and initial NO_3^- -N concentrations on the operational efficiency. (A) and (C) EC; (B) and (D) CE (pH, 7.0; current density, 15 mA/cm²; [Cl⁻], 2000 mg/L; reaction time, 2 h).

4 CONCLUSION

A Co_3O_4/Ti electrode was successfully prepared by electrodeposition, and the material showed good electrocatalytic performance toward NO_3^--RR . At an initial concentration of 100 mg/L NO_3^--N , the removal rate was ~98% in 2 h (Pt anode; pH, 7.0; current density, 15 mA/cm^2). The corresponding generation of

 ${
m NH_4}^+{
m -N}$ was ~60%, while ${
m NO_2}^-{
m -N}$ was not detected. When ${
m IrO_2-RuO_2/Ti}$ was employed as the anode in the presence of ${
m Cl}^-$ (2000 mg/L), the removal efficiencies for ${
m NO_3}^-{
m -N}$ and ${
m TN}$ under the same operating conditions were ~91% and ~60%, respectively, with an EC of 0.10 kW h/g ${
m NO_3}^-{
m -N}$ and a CE of 40.3%. After 4 h of continuous operation, 100% of ${
m NO_3}^-{
m -N}$ was converted into ${
m N_2}$. In addition, the system could maintain the removal

efficiencies of ~90% and ~60% for NO_3^- -N and TN, respectively, after 10 consecutive cycles (2 h each). This work provides a simple preparation method of electrodeposited Co_3O_4/Ti with good catalytic performance and stability, which provides a new preparation strategy for the Co_3O_4 catalytic electrode.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

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AUTHOR CONTRIBUTIONS

CW: conceptualization, methodology, data analysis, and writing—original draft. ZC: data curation. HH: validation. HL: resources and funding acquisition. SW: conceptualization, investigation, and writing—review and editing.

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